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PEL 8

OTWAY BASIN

069A LAND SEISMIC SURVEY

FINAL REPORT

Submitted by

Esso Exploration and Production (Aust) Inc.

1969

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AND RESOURCES SA**

CONTENTS ENVELOPE 990TENEMENT: O.E.L. No. 22TENEMENT HOLDER: Esso Standard Oil (Aust.) Ltd.REPORT:

Final Subsidy Report 069A Land Seismic Survey (pgs. 3-15)

PLANS:

Structure contours on Economic Basement	(990-1)
Structure Map on Top Pretty Hills	(990-2)
Structure Map on Base of Tertiary	(990-3)
Shot Point Map	(990-4)
Land Seismic Survey Program	(990-5)
" " " "	(990-6)
Proposed Land " "	(990-7)
Seismic Production REport	(990-8)
" " "	(990-9)
" " "	(990-10)

REPORT:

Otway 069A Land Seismic Survey (pgs. 16-38)

PLANS:

Seismic Production REport Chart	(990(2)-1)
" " " "	(990(2)-2)
Shot Point & Seismometer Array Patterns	(990(2)-3)
Noise Analysis Patterns Chart	(990(2)-4)
" " " "	(990(2)-5)
Seismic Recording Chart SP 25	(990(2)-6)
" " " SP 61	(990(2)-7)
" " " SP 100	(990(2)-8)
" " " SP 121	(990(2)-9)
" " " SP 156	(990(2)-10)
" " " SP 187	(990(2)-11)
" " " SP 265	(990(2)-12)
" " " SP 432	(990(2)-13)
" " " SP 466	(990(2)-14)
" " " SP 503	(990(2)-15)
" " " SP 326	(990(2)-16)
" " " SP 1023	(990(2)-17)
" " " SP 695	(990(2)-18)

Seismic Recording Chart	SP 726	(990(2)-19)
"	SP 756	(990(2)-20)
"	SP 806	(990(2)-21)
"	SP 665	(990(2)-22)
"	SP 1041	(990(2)-23)
"	SP 1116	(990(2)-24)
"	SP 1152	(990(2)-25)
"	SP 1643	(990(2)-26)
"	SP 1684	(990(2)-27)
"	SP 1528	(990(2)-28)
"	SP 1342	(990(2)-29)
"	SP 1709	(990(2)-30)
"	SP 1692	(990(2)-31)
"	SP 2034	(990(2)-32)

ENV 990.

0003

FINAL SUBSIDY REPORT



069A LAND SEISMIC SURVEY

SOUTH AUSTRALIAN PETROLEUM EXPLORATION LICENCE 8

by

ESSO EXPLORATION & PRODUCTION AUSTRALIA INC.

R. W. WIGGIN
R. L. GRAHAM

August 1969

TABLE OF CONTENTS

	<u>Page</u>
LIST OF ENCLOSURES	i
ABSTRACT	1
INTRODUCTION	2
INTERPRETATION	2
(a) Objectives	
(b) Regional Geology	
(c) Existing Geophysical Information	
(d) Horizons Mapped	
1. Structure on Economic Basement	
2. Structure on Pretty Hill sand-	
stone member	
3. Structure on Base of Tertiary	
4. Shot Point Map	
(e) Results	
PLAYBACK	6
BIBLIOGRAPHY	6
FIELD OPERATIONS & STATISTICAL REPORT . . .	7
"see Appendix 1 (in pocket)"	
069A EXPERIMENTAL SHOOTING	Appendix 2 (in pocket)

ENCLOSURES

0005

Figures with Text:

Figure 1	Locality Map
Figure 2	Time Depth Curve
Figure 3	Composite Seismic Section from Portions of Lines 5, 4 & 3 Across the Beachport Structure

Plates in Pocket:

Plate 1	Structure on Economic Basement
Plate 2	Structure on Pretty Hill Sandstone Member
Plate 3	Structure on Base of Tertiary
Plate 4	Shot Point Map

Appendices in Pocket:

Appendix 1	Field Operations & Statistical Report
Appendix 2	069A Experimental Shooting
	Test 1
	Test 2 & 3
	Test 4

ABSTRACT069A Seismic Survey Report

The 069A land seismic survey was designed primarily to map several prominent high basement features known from previous gravity and magnetic surveys and from sparse seismic coverage. The five features that were investigated are within the boundaries of South Australia P.E.L. 8 and are named Beachport, Lake Eliza, Lucindale, Camelback and Mount Hope.

The seismic traverses showed that the areas of interest are horst blocks in the basement formed by Lower Cretaceous faulting and are similar to, and contemporaneous with, the previously recognized Beachport High. The traverses also helped define the top and bottom of the prospective reservoir unit in the area of the seismic survey, and indicated that this unit tends to drape these highs.

INTRODUCTION

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The 069A Land Seismic Survey began on January 22nd, 1969 and was completed on May 12th, 1969. The survey was conducted within P.E.L. 8 in South Australia, where Esso has a farm-in agreement with Alliance Petroleum Australia NL, General Exploration of Australia and Beach Petroleum NL. (See Index Map fig. 1). One hundred and eighty two miles of data were recorded of which one hundred and fifty five miles were 6 fold C.D.P., twenty four miles were 3 fold C.D.P. and three miles were single fold.

INTERPRETATION

(A) OBJECTIVES

The objective of the 069A Land Seismic Survey was to detail certain gravity and magnetic anomalies which were not controlled or were poorly controlled by previous seismic work. These anomalies which were interpreted to be caused by basement highs seemed to offer good potential for hydrocarbon traps.

Existing maps showed major gravity anomalies near Beachport, Lake Eliza and Lucindale (bibliography 1). The Beachport anomaly was interpreted from seismic evidence produced by the EU 68 Marine Seismic Survey (bibliography 2) to be a basement high with the prospective sand pinching out on its flanks. It was hoped that the other gravity highs would also prove to be favourable locations.

A land gravity survey on P.E.L. 8, the Otway EV-68 survey (biblio. 3) confirmed the Beachport, Lake Eliza and Lucindale features and found residual anomalies in the Mount Hope and Camelback areas. The 069A seismic survey was shot over the five gravity features.

(B) REGIONAL GEOLOGY

The survey area is within South Australia P.E.L. 8 in the north-western part of the Otway Basin and is north of the hinge line which marks the boundary of thick Upper Cretaceous deposition. This part of the basin is an onshore extension of the "Crayfish Platform" which is bounded by the Lucindale Lineament to the north and the Cretaceous hinge line to the south (see fig. 1). It is a platform only in the sense that Upper Cretaceous and Tertiary rocks are found in relatively thin sequences thickening towards the sea. In Lower Cretaceous times an extensive depositional trough existed in the area.

The northern edge of the Otway Basin is formed by up-faulted basement on a line approximately west-northwest from Melbourne to Cape Jaffa. The basement rocks appear to be mainly metamorphosed Paleozoic sediments related to the formation of the Tasman Geosyncline which involved essentially the filling and deformation of a series of north-south trending troughs. The Otway Basin, which formed in Mesozoic times, however, trends east-west and contains sediments ranging from Mesozoic to Tertiary.

The lowermost unit, the Otway Group, comprises a thick section of non-marine Lower Cretaceous. The bottom member of this Group, the Pretty Hill Sandstone member, is a fresh water fluvial deltaic quartzose sandstone up to 10,000 feet thick. The Pretty Hill sandstone member is unconformably overlain by the finer grained greywacke-shale-mudstone sequence of the Otway Group, and the Lower Cretaceous is overlain discordantly by Upper Cretaceous sediments.

Upper Cretaceous rocks although exceeding 10,000 feet in thickness south of the Upper Cretaceous depositional hinge line are less than a thousand feet thick over most of the survey area. The top of the Upper Cretaceous is usually marked by a gentle angular unconformity.

The Eocene Paleocene sequence is a sandstone deposited in paralic to neritic conditions on a southward dipping surface. These rocks thin by onlap in the shelfward direction, thicken basinward, then thin over a gross regional clinoform to a southern zero edge. The younger Tertiary sequences consist of shales, marls and limestones.

Tertiary intrusive and extrusive rocks are common on the northern and eastern margins of the basin.

(C) EXISTING GEOPHYSICAL INFORMATION

1. South Australia Mines Department Air Magnetic Survey, contracted by BMR, in 1955 and re-interpreted by CGG, in 1965.
2. Esso's EV-68 Gravity Survey consisting of 1044 miles of coverage at $\frac{1}{2}$ mile intervals recorded in 1968-69.
3. South Australia Mines Department single-fold wiggle trace shooting covering approximately 300 miles recorded between 1960 and 1965.
4. Single-fold, analog recording seismic surveys by Alliance Oil Development including the following:
Kalangadoo - Lucindale, and Penola.
5. The Cape Grimm to Cape Jaffa Marine Single-Fold and Three-Fold Analog Seismic Survey by Hematite Exploration Pty. Ltd. 1965.
6. Offshore Otway Basin Marine Seismic Surveys, Esso Exploration and Production Australia, 1967 and 1968 (EO, EP and ER Surveys).
7. Offshore Otway EU-68 Marine Seismic Survey by Esso on SA/P8 (Aquapulse 12-fold digital recording).

D. HORIZONS MAPPED

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The enclosed structure contour depth maps are at a scale of 1:100,000. Datum is sea level. Figure 2 is a reflection time vs depth plot based on the velocity scans that were produced from the 069A Survey data. This time vs depth curve was used to convert the reflection times to depth for all mapped horizons. Considerable scatter was observed between plots of individual velocity scans. No significant regional trend was observed. The curve shown in figure 2 is an average of all scans.

The following maps are presented:

1. Plate 1 Structure on Economic Basement
2. Plate 2 Structure on Pretty Hill sandstone member
3. Plate 3 Structure on Base of Tertiary
4. Plate 4 Shot point map

This discussion gives details of reflection characteristics, data quality and pertinent geologic information relating to the mapped horizons.

1. Structure on Economic Basement, Plate 1

Economic Basement in the survey area may consist of either crystalline rocks or paleozoic metamorphics. Basement at Kalangadoo No. 1 was found to be slightly metamorphosed sandstone sequence of presumed Paleozoic age. Granite outcrops are found a few miles north of the survey area. The seismic event that is mapped as economic basement is usually a high amplitude signal that sometimes has weak unconformable events beneath it and other times is simply the deepest reflection event. The reflection quality is poor to fair.

Plate 1 is a structure map of Economic Basement. The structural style is that of block faulting with the major faults oriented NW-SE. Five significant horst blocks were located and are identified on the map as Lucindale, Camelback, Lake Eliza, Beachport and Mt. Hope. Figure 3 is a composite seismic section of portions of lines 5, 4 and 3 across the Beachport structure. This section is typical of these fault block structures. The three horizons that are mapped in this report are marked on figure 3: Economic Basement, Top Pretty Hill Sand and Base Tertiary.

2. Structure on Pretty Hill Sandstone Member, Plate 2

This horizon is characterized by a high amplitude reflection at an unconformity. Truncation of underlying beds and onlap by younger strata are often observed. The reflection marks the boundary between the mudstones of the Lower Cretaceous Otway Group and the underlying Pretty Hill sandstone member. Reflection identification has been established by correlating the land data with the marine work and tying the Esso Crayfish-1 well. Reflection ties between the isolated portions of the 069A survey were verified by reference to earlier seismic work in the area by the South Australia Mines Department and Alliance Petroleum.

Plate 2 shows the structure on the top of the Pretty Hill sand. Closure is mapped over all the anomalies that were shown on the basement map. Two additional closures, Sugar Loaf and Konetta were mapped from the earlier seismic control, however, there is only one seismic line across each anomaly.

The Pretty Hill sand thins abruptly over the basement highs and in the case of Beachport and Mt. Hope it is difficult to distinguish both a Pretty Hill reflection and a basement event. A sand pinch out has been interpreted on the crest of the Beachport structure, however the area wherein the sand is absent could be larger than presently mapped.

The data quality is fair to good and the presented map is considered reliable within the limits of control.

3. Structure on Base of Tertiary Plate 3

The Base of Tertiary is a slight unconformity in the area covered by the 069A survey and is difficult to correlate on the seismic sections. The Upper Cretaceous sedimentary wedge pinches out by onlap on the Lower Cretaceous surface as well as through truncation by Tertiary beds. Further complications are caused by the bedding patterns of the early Tertiary rocks which prograde over both the Lower Cretaceous and Upper Cretaceous subcrop. Well control at Beachport-1 and Robe-1 was an aid in horizon identification. The reflection quality was poor to fair.

The Base of Tertiary horizon does not reflect the buried basement and Lower Cretaceous structures. The principal features of the map are regional thinning to the north-east and a wide trough extending NW-SE through the centre of the area.

4. Shot Point Map Plate 4

This map is a compilation of all Esso and other company shooting including South Australian Mines Department. The location of all permanent markers that were established during the 069A survey is shown on this map as well as the location of the velocity scans.

(E) RESULTS

The 069A seismic survey has shown that the gravity anomalies at Beachport, Lake Eliza, Lucindale, Camelback and Mt. Hope are basement controlled structural features. The basement anomalies are essentially flat-topped horst blocks. Closure on the Pretty Hill sand has been mapped in all five areas. The Base of Tertiary horizon was mapped and found to bear no resemblance to the buried Lower Cretaceous structures.

PLAYBACK

0011

Twenty-three lines totalling 182.39 miles of the 069A survey were processed at the Geophysical Service International's digital processing center in St. Leonards, N.S.W. Final sections were processed using the optimum parameters determined through processing experimentation and data analysis.

Field data recorded on S.I.E. analogue tapes were transcribed to two millisecond sample rate in T.I.A.C. digital format, then processed at four millisecond sample with corrections for near surface statics, amplitude equilization, six fold stack, and time varying deconvolution after stack.

Final sections were plotted as variable density film with time varying filter.

Near surface static corrections were adjusted for surface elevations and shot elevations from uphole times. Reflection times were corrected to sealevel datum using a sub-weathering velocity of 6000 feet/second. Part of line 069A-3 was recorded and processed single fold due to irregular surface terrain.

Computer automated velocity gathers were extracted from the six fold data at intervals of approximately five miles. Velocity functions input for normal moveout corrections were derived from the gathers and distributed over the line on the basis of single fold section. The velocity functions are identified on the section.

Quality of the final sections graded from fair to good.

BIBLIOGRAPHY

1. Geological Interpretation of Seismic Time Sections in the Gambier Embayment.
K. Rochow, Department of Mines, South Australia.
2. Final Subsidy Report, EU-68 Marine Seismic Survey,
Esso Exploration & Production, Australia, Inc.
3. Final Subsidy Report, EV-68 Land Gravity Survey,
Esso Exploration & Production, Australia, Inc.

FIELD OPERATIONS AND STATISTICAL REPORT

0012

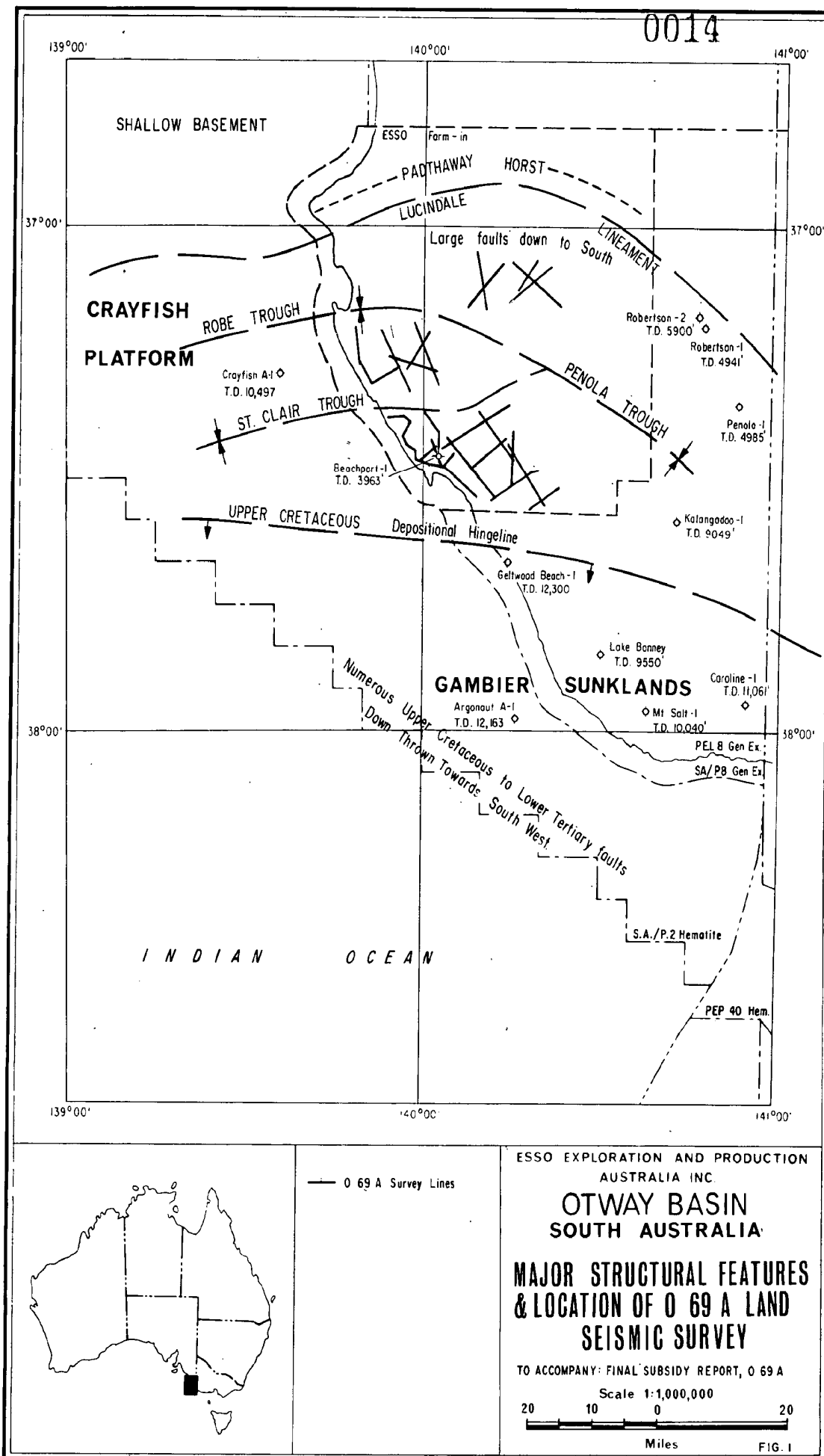
Geophysical Associates Pty. Ltd. has prepared a statistical summary of the field operations which is attached as appendix 1 to this report. An experimental shooting programme was conducted at the start of the survey. The results of these field tests are included in the attached appendix 2.

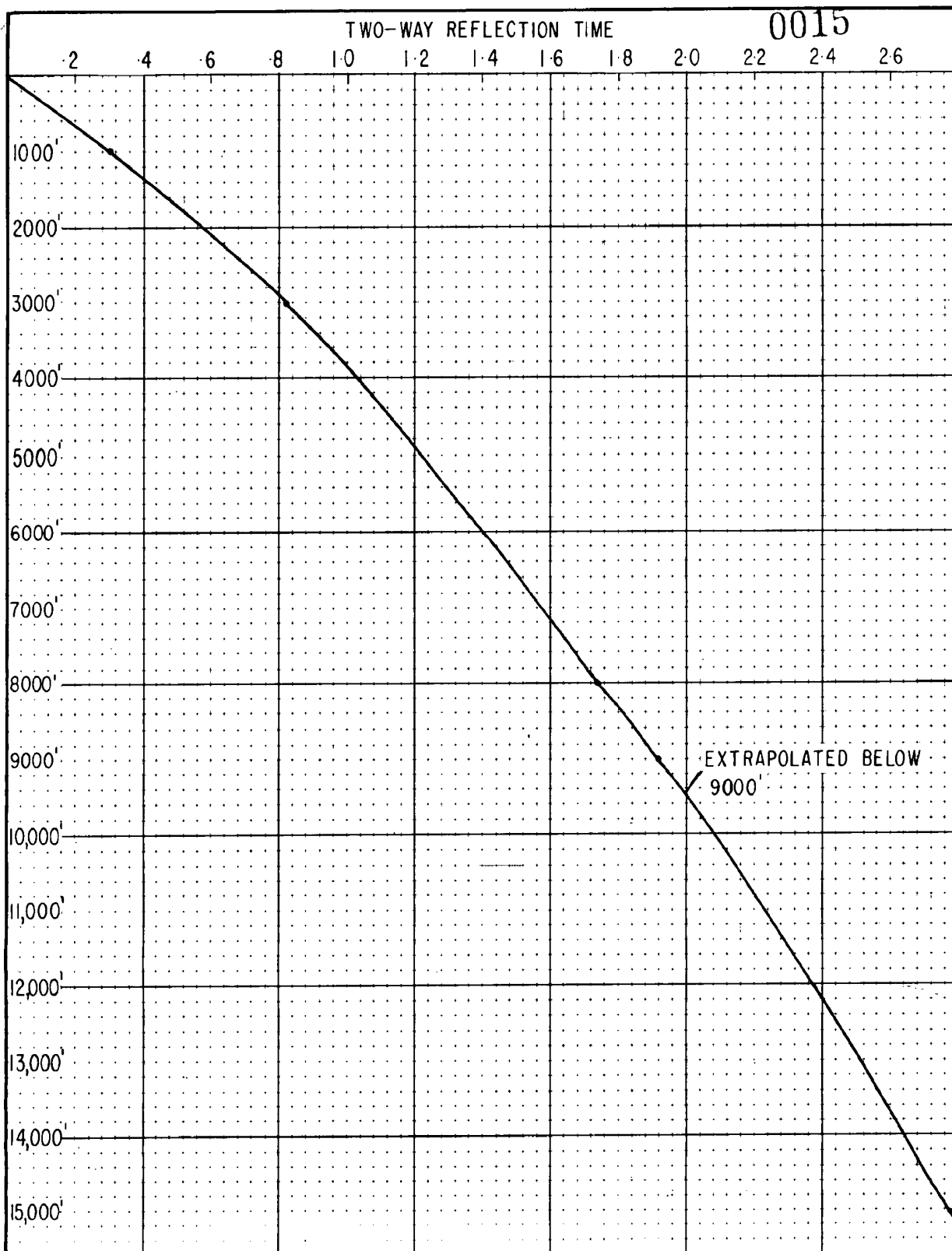
The following is a list of Line numbers and shot points included in the 069A survey:

<u>Line</u>	<u>From</u>	<u>To</u>
1	1	168
2	169	289
	393	438
3	439	521
	573	601
	385	388
4	290	316
	332	359, 470
5	317	322 332
	522	572
6	392, 602	634
7	950	978
	979	1024
8	681	773
9	845	899
10	775	844
11	635	679
12	900	949
13	not shot	
14	1189	1239
15	1025	1106
16	1107	1188
17	1534	1635
18	1449	1518
19	1636	1702
20	1395	1448
	1519	1533
21	1240	1308
21A	1309	1394
22	390, 504, 362	384, 550, 389
23	1703	1770
24	1953	2037

By R. W. Wiggin
R. L. Graham

R. W. Wiggin
R. L. Graham





ESSO EXPLORATION AND PRODUCTION AUSTRALIA INC.

OTWAY BASIN

TIME DEPTH CURVE

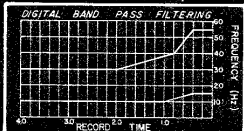
BASED ON VELOCITY SCANS FROM THE
069A LAND SEISMIC SURVEY
IN P.E.L.8 & S.A./8 SOUTH AUSTRALIA

TO ACCOMPANY: FINAL SUBSIDY REPORT

069A LAND SEISMIC SURVEY

FIG. 2

DWG.1178/G/2



GSI DIGITAL PROCESSING CENTRE

SYDNEY, N.S.W., AUSTRALIA

1. SAMPLE PERIOD 4 ms. 2. TAR. B₂ db, α₂ db/sec.

3a. AUTOMATED RESIDUAL STATICS Gate to ms.

3. NMO Equalization gate 1000 to 3000 ms.

4. DECON 30 pfs, 4 ms. dec. Design Gate 400 1950 1950 3500 ms.

No. of gates/trace 3

5. DIGITAL FILTER 35 pfs, 4 ms. dec. Hz.

6. DPS ☒ OWBS ☐ TVD ☐ DCN ☐ ARD ☐ AR2 ☐ DGF ☐ TVF ☐ M-4 ☐

7. TIAC Reg 1121 B Hold Tape 4032 S. P/B Gain 8 db.

GSI Input Crew 851 Date APR '69

ESSO STANDARD OIL (AUST) PTY. LTD.

SYDNEY, N.S.W., AUSTRALIA

AREA OTWAY LAND

LINE 069A-5

RECORDING PARAMETERS

S P off GPJ

Source DYNAMITE Charge Size 5 lbs./Hole

5 Holes Inline Int. Hole Depth 40 ft

Cable Length 4600 ft. Group Interval 200 ft

S P Interval 400 ft

24 Series 10 ft Interval

Recording Filters 16 78

GAI Field Crew 6 Gate MAR'69



NEG
DESIGN DATE FOR
AUTO RES. STATICS
1200 - 1500ms
331 - 530
531 - 580
581 - 572
900 - 1300

Dwg 1178/G/3

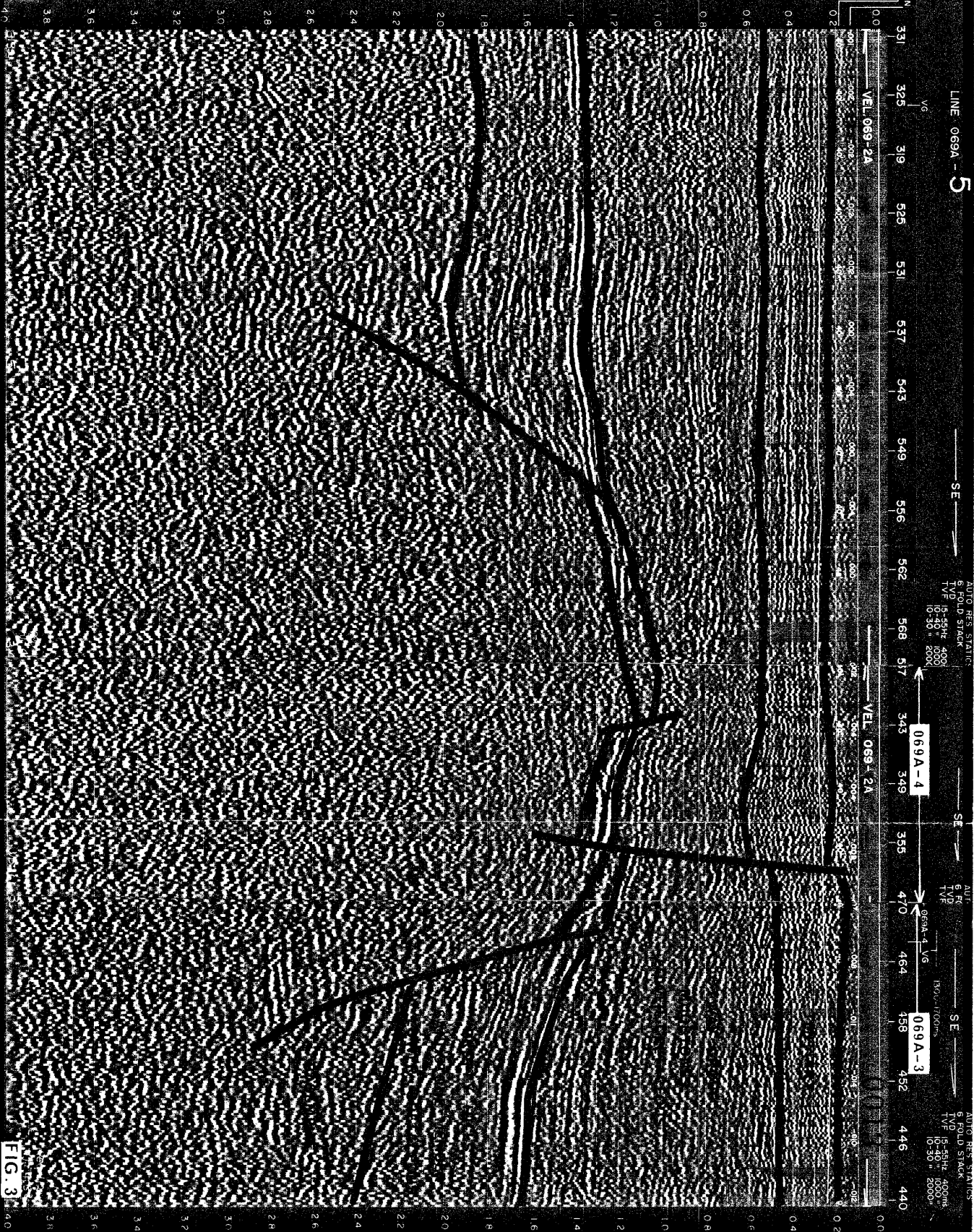


FIG. 3

ENV 990.

Appendix 1



0016

OTWAY 069A LAND SEISMIC SURVEY

OEL 22 SOUTH AUSTRALIA

ESSO STANDARD OIL (AUSTRALIA) LTD

BOX 4047 G.P.O. SYDNEY, N.S.W.

GEOPHYSICAL ASSOCIATES PTY. LTD.

399 HONOUR AVENUE, GRACEVILLE, QUEENSLAND.

July, 1969

0017

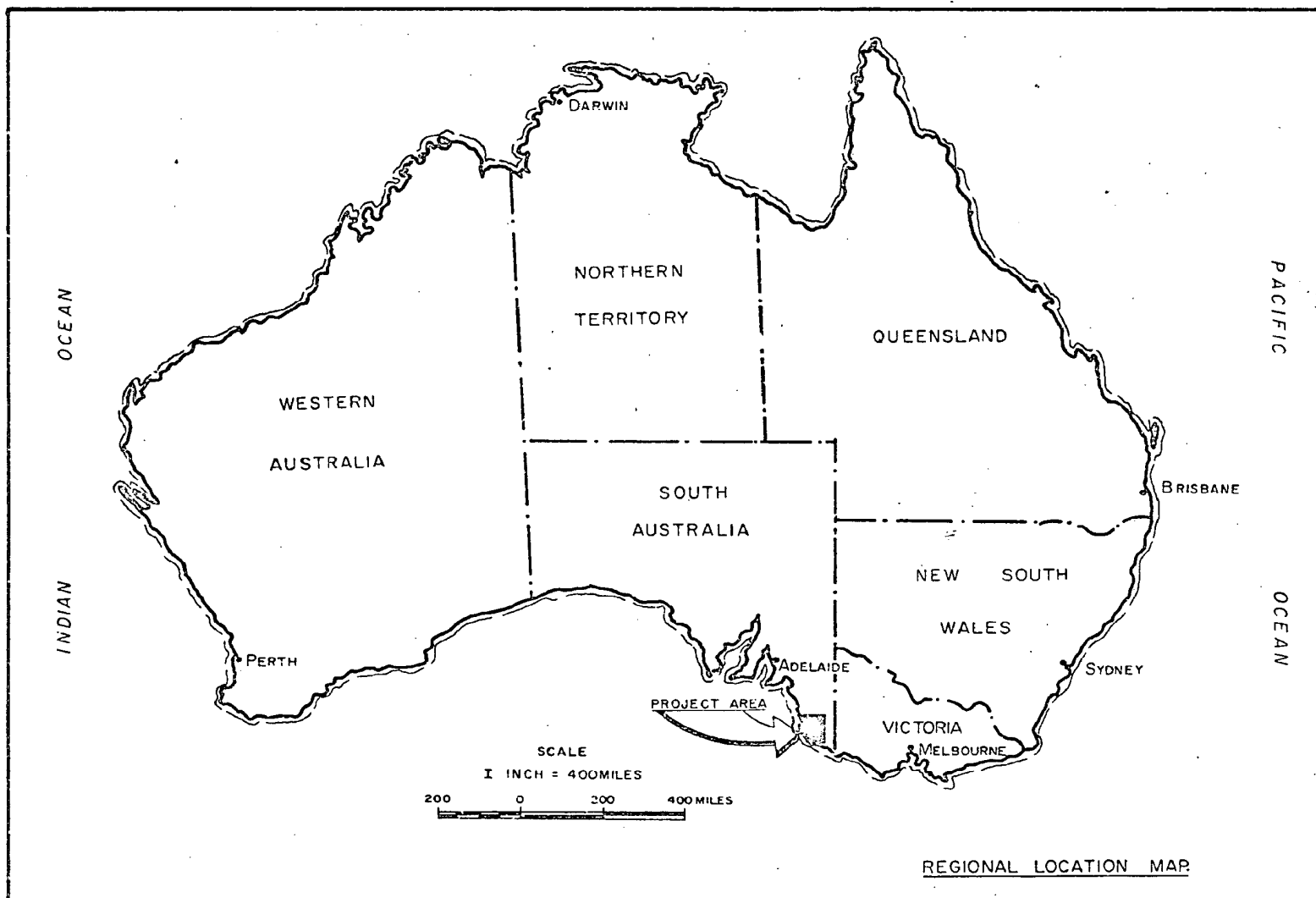


Figure 1

INDEX

	<u>Page</u>
I OPERATIONAL REPORT	
(a) Location and Date	1
(b) Access and Clearing	1
(c) Surveying	2
(d) Drilling	2
(e) Shooting	5
(f) Recording and Record Quality	6
(g) Computation	9
II EQUIPMENT	11
III PERSONNEL	14
IV STATISTICS	15

ILLUSTRATIONS

Figure 1	Location Map - Frontispiece	
Figure 2	Line Location Map	opp. 1
Figure 3	Shot Point and Geophone Spread Diagram	opp. 6

I OPERATIONAL REPORT

0020

(a) Location and Date

Esso Exploration (Australia) Ltd., Box 4047 G.P.O. Sydney, N.S.W. selected Geophysical Associates Pty. Ltd., 399 Honour Avenue, Graceville, to conduct land seismic survey 069A in Oil Exploration Lease 22, South Australia.

The GAPL crew departed Brisbane January 16, 1969 field operations commenced January 22. The programme was completed May 12, 1969, the crew returning to Brisbane May 17. Recording totalled 1113 hours during which time 1855 locations were shot yielding a subsurface coverage of 182.39 miles. (Figure 2)

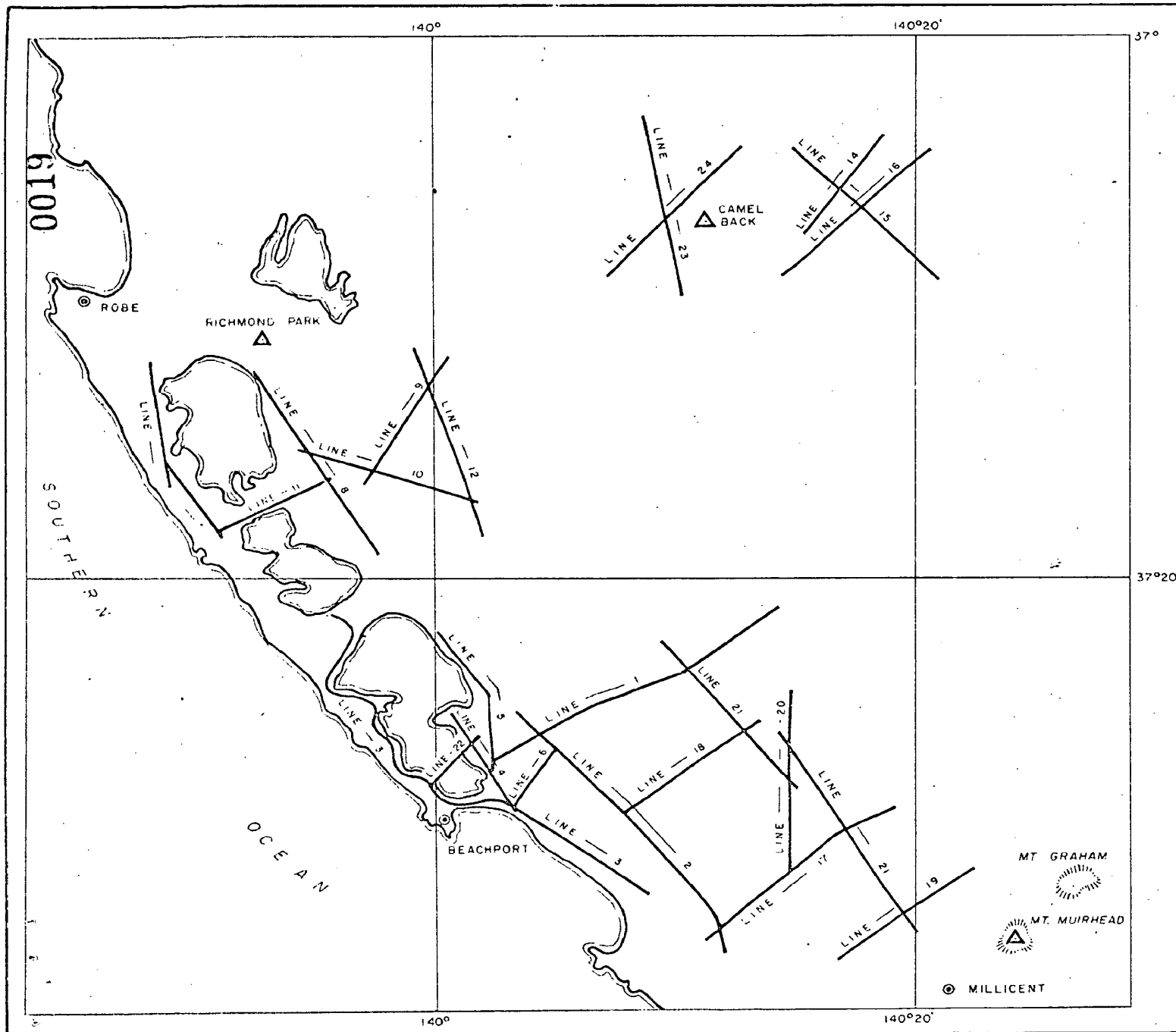
Area 069A is located between 139°45' to 140°30' east longitude, 37°00' to 37°35' south latitude. A completely self contained camp was positioned on the "Woakwine" property of Mr. A. McCourt some four miles north of Beachport. The camp and the entire operation were supplied from Millicent (22 miles) and Mt. Gambier (55 miles) on good paved roads.

(b) Access and Clearing

The area is cut diagonally by the Prince's Highway, this, together with a grid of good sealed or gravel roads provided easy access to all parts of the project. The camp was not shifted during the survey thus drives of almost 40 miles were necessary to the distant portions of the project.

A Caterpillar D7 tractor supplied by Mr. A. McCourt was utilized for line clearing. This machine worked a total of 233 hours and was held in standby for 129 hours. In addition, a grader was used for 12½ hours in March for levelling on lines 2 and 5. Dozing was necessary on lines 3, 7, 8, 10, 15, 16 and 24.

LINE LOCATION MAP



(c) Surveying

All lines were surveyed with a Topcon AG-2 theodolite. Surveying was greatly facilitated by bench marks established during the EV68 Land Gravity Survey (Esso April, 1969) which had been tied vertically to the South Australia Land Department third order survey and horizontally to trigonometrical stations at Mt. Muirhead, Camelback, Richmond Park, Mt. Benson, Elgin, Furner and Bradleys Hill. Accuracy was held to better than ± 1 ft vertically and 300 ft horizontally. All intersections, line-ends and at five mile intervals along traverses were permanently marked with a five foot steel picket and aluminium tag.

A final shot point map, 1:100,000 scale showing shot point and permanent mark locations was submitted to Esso on completion of the survey.

(d) Drilling

Soon after the start of the seismic survey it became obvious that the three drills contracted for in the original agreement would be totally inadequate. Five hole patterns were found necessary. Drilling was slow and difficult with hard limestone stringers, shell beds, layers of sand and strong flows of underground water that dictated the use of large amounts of drilling mud, bran and other additives. Early in February four extra drills (three from GAPL in Brisbane and one from Thompson Drilling, Millicent) were added to the drilling complement. In addition, two water trucks were hired locally.

No trouble was experienced moving the drills in the area with the possible exception in the sand hills along the beach front and on line 2 where a deep bog caused the abandonment of the line.

A line by line description of the drilling encountered follows:

Line 1 - Mainly hard limestone stringers accompanied by unconsolidated sands. Occasional

0022

layers of hard sandstone were also encountered. Holes were drilled to a depth of 50 ft. Solid surface conditions at the beginning of the line deteriorated westerly.

Line 2. Hard limestone, unconsolidated sand and clay were encountered. The presence of loose rocks near the surface aggravated drilling conditions in the central section of the line. The average drilling depth was 50 ft. A reasonably level hard surface presented no difficulties.

Line 3. Beach sand, shell beds and limestone stringers prevailed. Sand hills around Lake George hampered severely the mobility of the rigs. Drilling depth was increased in the sand hills to place charges on a level plane.

Line 4. Strata consisted of limestone, shell beds and sand, with occasional cavities being encountered. The holes were drilled to a depth of 50 ft. No mobility difficulties arose.

Line 5. Limestone, clay and sand strata with occasional cavities were the main features. Drilling depth remained at 50 ft, and a hard level surface was favourable.

Line 6. Poor drilling conditions persisted with the presence of numerous cavities in hard limestone stringers, shell beds, sand and clay. Hole depths were mainly 50 ft but a few were left shallower as a result of the adverse conditions. Surface conditions were good.

Line 7. Limestone, sand and clay with occasional shell beds. The hilly terrain made drilling difficult although mobility was unaffected. The hole depths were increased with elevation increases in hilly areas.

Line 8. Drilling conditions slightly better, but reasonable quantities of bran and mud still required, in sand and limestone encountered.

Line 9. Some hard drilling was experienced. Bran and mud was consistently used, holes drilled to 50 ft. Fairly level terrain and reasonable surface was encountered.

0023

Line 10. Fair drilling conditions, mainly limestone, sand and clay. No surface difficulties were experienced, with holes at 50 ft depth.

Line 11. Hilly terrain with some very soft areas in the west hampered operations. Drilling through shell beds, limestone and numerous cavities coupled with the presence of underground water further contributed to the poor drilling conditions. Holes were drilled to 50 ft, with a few shallower exceptions.

Line 12. Drilling conditions similar to line 9. Hole depths were 50 ft. Some surface undulations but no difficulty in moving was experienced.

Line 14. Fair drilling on this line. On the sand hills five hole patterns to 50ft depth were drilled with single holes on the level portions to depths of 100-120 ft.

Line 15. Sand dunes still encountered, mainly in central and south eastern sections. Drilling conditions varied from poor to fair. Five hole patterns at 50 ft depth in sand dune areas and single holes of 80-100 ft in level areas were utilized.

Line 16. Similar conditions to line 14. Fair drilling conditions experienced. Sand dunes in north eastern sections necessitated 5 hole patterns at 50 ft. The remainder of the line being shot using single holes of 80-100 ft.

Line 17. Consisted mainly of limestone, sandstone and sand strata. Hole depths remained at 50 ft.

Line 18. Limestone, clay and shell beds persisted. Holes remained at 50 ft depths. The surface was mainly level with some rolling hills in the central and western areas.

Line 19. Limestone, clay and some sand continued to be present. Hole depths were 50 ft.

Line 20. Drilling conditions were fair on this line. Still chiefly limestone and sand, with hole depths of 50 ft. Surface conditions were hard and level presenting no difficulties.

Line 21. Fair drilling encountered, stratigraphically similar to line 20 with the presence of occasional shell beds. Hole depths still 50ft and the surface hard and fairly level.

Line 22. Poor drilling was experienced here. Cemented shell beds and sand coupled with the soft surface of Lake George were contributing factors. Patterns were 5 holes at 50 ft depth. Mobility was restricted and a bulldozer was required to pull drills from bogs.

Line 23. Poor drilling conditions existed. Hard limestone lenses and numerous cavities necessitated the use of large quantities of mud and bran to maintain circulation. The five hole patterns were drilled to a depth of 50 ft. Hilly but hard surfaced terrain was experienced.

Line 24. Poor drilling conditions continued. Five holes at 50 ft depth, except for S.P.'s 2000-2020 where 20 hole patterns at 20 ft depths were used.

(e) Shooting

Holes were extremely difficult to load throughout the area. The use of a preloader was mandatory as holes left for only a few minutes after drilling tended to block off. Two additional shooters were employed in this capacity from February 1 to the end of the contract.

Early in February, following several misfires in deeper holes where the powder burnt rather than detonated, the crew was visited by explosives experts from I.C.I. Melbourne. Their advice, which became the general practise was that all charges be doubly primed with RDX boosters. This reduced the misfire rate but added appreciably to the loading time and the explosives cost.

The average charge was five pounds per hole to the total drilled depth. After shooting,

SHOT POINT AND SPREAD DIAGRAMS

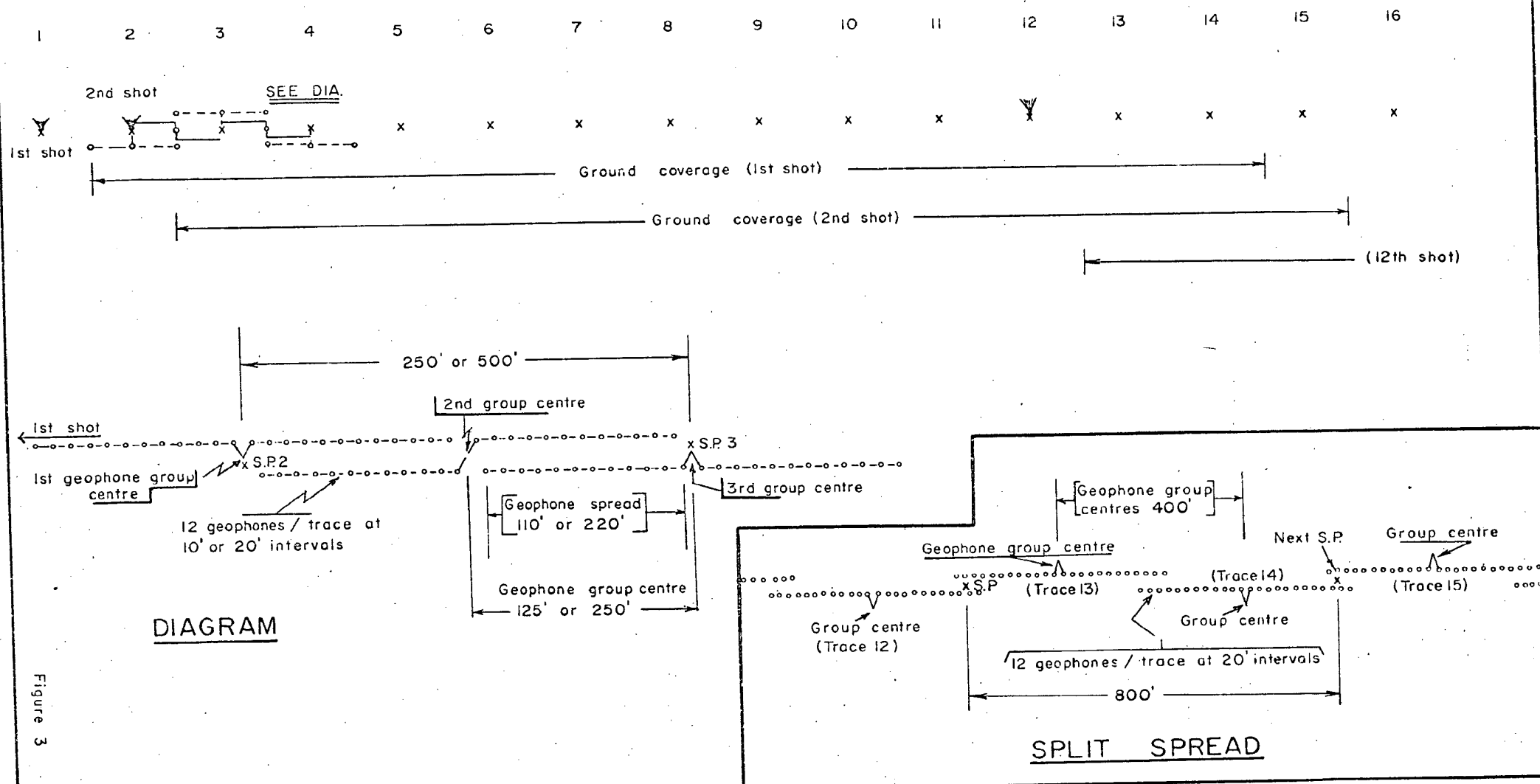


Figure 3

all holes were sealed at the surface with Dresser 8" aluminium hole plugs. Subsequent to the completion of the survey, an investigation by Esso personnel disclosed that many of the hole plugs had failed in the soft near surface sand; others had been removed by local scavengers in an attempt to recover detonator wires. GAPL personnel required almost two weeks to remedy the situation.

(f) Recording and Record Quality

A test programme was initiated on January 23 and concluded on January 24. This programme commenced with a standard noise spread, and continued on through various shot hole patterns, shot depths, charge sizes, geophone arrays and spread lengths.

A shot point configuration of five 40 ft holes with 50 ft separation and 5 pounds of powder per hole was selected as the optimum shooting method.

Spread configuration (Figure 3), was standardised at 200 ft intervals between geophone centres with 24 series-parallel geophones per trace at 10 ft intervals. End on shooting techniques were utilized with 400 ft spacing between shot points, each shot point coinciding with alternate geophone centres, the shot point 400 ft offend.

The instruments used during the survey were manufactured by Dresser Industries, Houston, Texas. They comprised one 24 channel SIE PT-100 portable transistorized seismic amplifier system, a SIE model VRO-6 camera and a SIE PMR 20 magnetic recording system. The monitor seismogram and FM tape were recorded simultaneously at each shot point with filter settings of out-out and later 16-78. A quality control playback record was made with filter settings of 16-78.

Record quality ranged from poor to good and was dependant largely on the sub-surface conditions. It was generally found that where sand hills were encountered quality deteriorated.

Line by line recording techniques and record quality were;

Line 1. Record quality was fair to good using an out-out filter setting and 400 ft spacing between shot points and 200 ft between group centres.

Line 2. Quality remained fair to good using the same spread configuration. The northern end of the line was deleted due to boggy surface conditions.

Line 3. Here, record quality and production were good. The line was shot using 500 ft spacing between shot points and 250 ft between geophone centres until shot point 394. Shot point 395 to 601 was recorded using a split spread configuration of 800 ft between shot points and 400 ft between geophone centres. A lay down filter setting of 16-78 was used to reduce noise level. Record quality was poor to fair over sand hills. Three profiles of 4600 ft - 4800 ft in length were recorded at the north end of the line. Shots were taken from each end of the cable for two way coverage.

Line 4. Record quality was fair to good. Shot point spacing of 500 ft was used.

Line 5. Record quality was good using a 400 ft spacing between shot points with a filter setting of 16-78 cps.

Line 6. Record quality was fair to good using a 500 ft shot point spacing and filter settings of 16-78 cps.

Line 7. Parts of line 7 produced records of very poor quality. The poor character of these records was presumably due to the large depth of sand encountered, limestone caverns and the possibility of the presence of faulting in this area. Four holes were drilled at S.P. 950 to test record quality. These holes were fired at 40/42 ft and 150/158 ft and yielded poor results in both cases. The line was shot using a shot point spacing of 500 ft.

Line 8. The record quality varied from very poor to fair. The reason for the very poor quality could be explained by the fact that for most of its length the line runs at the base of a long low range of hills where there is a possibility of faulting. This line was shot using 500 ft spacing between shot points.

Line 9. The quality of seismograms for the entire line were of very poor quality. Like line 8 this could possibly be contributed to limestone caverns and poor near surface conditions.

Line 10. Record quality was fair to poor, the line being shot at shot point spacing of 500 ft.

Line 11. Seismogram quality ranged from poor to fair. Unconsolidated near surface conditions contributing to weak signal return. This line was shot using 500 ft shot point spacing.

Line 12. The line which intersects line 9 at the north end produced records of the same poor quality. Again it is presumed that poor returns were due to the presence of limestone caverns and poor near surface conditions. This line was recorded using 500 ft shot point spacing.

Line 14. Part of the line was shot using the 500 ft spacing between shot points and the remainder was shot using a spacing of 250 ft between shot points. This was used in an attempt to enhance shallower recorded data. Data was greatly affected by topography and near surface conditions. Seismograms recorded over consolidated sand dunes were of very poor quality due to poor energy returns. In the level areas single holes with 20 pound charges were used with fair results.

Line 15. Record quality ranged from fair to very poor. The reasons being the same mentioned for line 14. 500 ft spacing between shot points was used with five hole patterns on the sand dunes and single holes on level areas.

Line 16. Again the record quality was affected by topography and near surface conditions. The quality was fair to the south west but

gradually deteriorating as the recording progressed north east. The same spread configuration was used as on lines 14 and 15.

Line 17. Record quality was fair to poor. The line was shot using a three hole pattern at 100 ft spacing and 10 ft geophone spacing and 500 ft between shot points.

Line 18. Record quality was fair to poor. Spread configuration was the same as line 17.

Line 19. Record quality varied from fair to poor. Spread configuration remained at 3 hole patterns at 100 ft spacing and 10 ft geophone spacing, shot points located 500 ft apart.

Line 20. Record quality was fair to poor. The line being shot using a 3 hole pattern at 100 ft spacing with shot points located 500 ft apart.

Line 21. Record quality varied from poor to fair, part of the line was shot using 5 hole patterns at 50 ft separation. The remainder was shot using 3 hole patterns at 100 ft separation. Shot points were located at 500 ft intervals.

Line 22. Record quality varied from fair to good. Shot points located at 500 ft intervals.

Line 23. Record quality was fair to good with horizons continuous throughout. This line was recorded using 125 ft group separation and shot points located at 500 ft intervals.

Line 24. Record quality was fair to poor and recorded events semi-continuous. The south west portion of the line was recorded using 125 ft group spacing and shot points located every 500 ft. The remainder of the line being shot using 125 ft group separation with 20 hole patterns 20 ft deep located every 500 ft.

(g) Computation

The observed reflection times were corrected to a reference datum plane of sea level by

the standard uphole method employing the formula:-

$$T_c = \frac{2(E_s - D_s - E_d)}{V_d} + T_{uh} \text{ where,}$$

T_c = Total correction to datum
 E_s = Shot point elevation
 D_s = Depth to top of charge
 E_d = Datum plane elevation
 V_d = Datum correction velocity (6000'/sec)
 T_{uh} = Uphole time

Shallower shots when taken were corrected to the deepest recording in each hole by a factor equal to the difference in uphole times.

First breaks were plotted for all shot points and where necessary corrections for weathering were applied. Total corrections obtained from the above formula were used to correct traces and correction for alternate traces averaged. Data was then forwarded to Esso for further reduction.

Weekly statistical reports were phoned to Esso, Sydney each Thursday morning. Monthly progress reports with a completed statistical sheet and shot point location map were forwarded to the Bureau of Mineral Resources, Canberra and to Esso Sydney.

GEOPHYSICAL ASSOCIATES PTY.LTD.

.....*F. L. Hickey*.....

0031

II EQUIPMENT

Recording

- 1 Toyota Land Cruiser truck with stainless steel recording cabin
- 1 set 24 channel Southwestern Industrial Electronics PT-100 transistorized seismic instruments
- 1 SIE model VRO-6 oscillograph
- 1 SIE PMR-20 FM magnetic recording system
- 2 SIE SCD-2000 BA multicap blasters
- 14 Portable CDP reflection cables, 1260 ft long 3 take-outs per cable, 420 ft between take-outs
- 996 HSJ 14 cps reflection geophone series mounted 12 per string with end take-out and 20 ft geophone intervals
- 3 Communication radios
- 1 CDP rollalong switch
- 1 Shooting truck Toyota Land Cruiser FJ-45, four wheel drive, with 350 pound dynamite storage and 100 ft hole loading poles
- 6 1200 ft shooting cables
- 2 Cable and geophone trucks, Toyota Land Cruiser equipped with cable and geophone storage
- 1 Portable powder magazine, 4000 pound capacity
- 1 Detonator storage box

Preloading

- 1 Preloading vehicle Ford F-750 4 X 4, with 800 gallon water tank, 2000 pound dynamite storage and 100 ft hole loading poles
- 1 Preloading vehicle - Toyota FJ-45 short wheel base four wheel drive with dynamite and cap storage and 100 ft hole loading poles

0032

Surveying

- 1 Toyota Land Cruiser FJ-45, four wheel drive equipped with auxiliary fuel tanks, and instrument storage
- 1 K&E transit and tripod
- 1 Topcon AG-2 transit and tripod
- 2 Survey rods
- 1 Survey chain
- Auxiliary survey equipment

Drilling

- 4 Ford T-750, 6 wheel drive trucks each mounted with Mayhew 1000 heavy duty drill, WCQ air compressor, 5" x 6" Gardner Denver mud pump, 300 ft Mayhew regular drill stem, water injection piping
- 2 Ford F-800 4 wheel drive trucks, each mounted with Mayhew 1000 heavy duty drill, WCQ air compressor, 5" x 6" Gardner Denver mud pump, 300 ft Mayhew regular drill stem, water injection piping
- 1 Chevrolet Army Blitz, 6 wheel drive, mounted with Mayhew 1000 heavy duty drill, WCQ air compressor, 5" x 6" Gardner Denver mud pump, 300 ft Mayhew regular drill stem, water injection piping
- 1 Water truck - Bedford with 1000 gallon tank
- 6 Water trucks, F-750 4 wheel drive with 1000 gallon flatbed tanks and auxiliary 2" centrifugal water pumps
- 1 spare water truck - Bedford with 1000 gallon tank
- 1 spare water truck - Bedford with 1200 gallon tank
- 1 Tool Push vehicle FJ-45 Toyota, 4 wheel drive with auxiliary maintenance equipment

Supply

- 1 Toyota Hi-Ace supply truck

Office

0033

- 1 Toyota Crown station sedan, party chief vehicle
- 1 Toyota Hi-Ace party manager - permit vehicle

Camp

- 1 Kitchen-utility caravan with dining and storage annexes, completely equipped
- 1 Office caravan, fully equipped with Rotolite printer, light table, all drafting and computing gear
- 1 Executive trailer for supervisory and client use
- 1 workshop trailer fully equipped with spare parts, tools, welding gear
- 1 set of sleeping tents (8) fully equipped
- 1 600 gallon water storage tank
- 1 500 gallon trailer-mounted water tank
- 1 Lister HA-3 18 KVA trailer-mounted lighting plant
- 1 Lister 8 KVA standby power plant.

III PERSONNEL

0034

Party Chief	T.A. Magub
Party Manager	B.M. Warr
Chief Computer	A. Gell
Computers	P. Baxter
	A. Koger
Instrument Supervisor	H. Holm
Observer	L. Kruk
Junior Observer	P. Wade
Shooters	A. Norris
	M. Edginton
	A. Bencsevich
Surveyor	J. Baxter
Drill Supervisor	N. Griffin
Drillers	B. Handley
	T. Brady
	R. Desjardines
	F. Ward
	D. McKenna
	C. Cunningham
	D. Herbert
	B. Harvey
	R. Thompson
Mechanic	C. Ogden
	G. Bashford
Cook	E. Hoare

In addition to the key personnel listed above the following helpers were employed -

Rodmen	2
Recording helpers	6
Cable truck drivers	2
Supply truck driver	1
Drill helpers	7
Cook's helper	1
Camp Attendant	1

Administrative and field supervision GAPL -

J.H.B. Campbell

Geophysical supervisor Esso - W.R. Stone

0035

IV STATISTICS

Profiles recorded	1,759
Number of shot points	1,855
Test shots	15
Number of shots	1,810
Field recording hours	878.5
Field travel time	130
Other hours -	
Weather time	10
Equipment time	20
Camp moves	0
Holidays	0
Standby	71.5
Total recording hours	1,113
Number of days worked	97
Holes per day (average)	19.12
Holes per recording hour	2.11
Miles traversed (subsurface) -	

Line #1 = 13.00 mi	Line #9 = 5.65 mi	Line #17 = 10.10 mi
2 = 12.93 mi	10 = 7.17 mi	18 = 7.07 mi
3 = 15.57 mi	11 = 4.61 mi	19 = 6.79 mi
4 = 5.84 mi	12 = 5.18 mi	20 = 6.98 mi
5 = 5.43 mi	14 = 5.05 mi	21 = 15.48 mi
6 = 3.76 mi	15 = 8.21 mi	22 = 3.00 mi
7 = 7.99 mi	16 = 8.21 mi	23 = 6.66 mi
8 = 9.44 mi		24 = 8.27 mi

Total = 182.39 mi

Miles per day (average)	1.88
Explosives - pounds (Anzite and Geopex)	45,150
Pounds per shot (average)	25.02
Detonators	15,340
RDX Boosters	9,256

0036

Cordtex (feet)	3,000
Magnetic tapes	1,923
Bulldozing-work hours	233
standby hours	129
Grader work hours	12.5

Drill # 1

Holes	1,255
Footage	61,527
Drilling hours	1,002.5
Travelling hours	154.75
Standby	25.0
Penetration ft/hr average	61.37

Drill # 2

Holes	1,589
Footage	75,490
Drilling hours	1,043
Travelling hours	156
Standby	32.5
Penetration ft/hr average	72.38

Drill # 3

Holes	1,270
Footage	66,225
Drilling hours	997
Travelling hours	128.75
Standby	41.5
Penetration ft/hr average	66.42

0037

Drill # 4

Holes	1,003
Footage	52,158
Drilling hours	923
Travelling hours	138.75
Standby	0
Penetration ft/hr average	56.51

Drill # 5

Holes	999
Footage	51,175
Drilling hours	813.25
Travelling hours	117.05
Standby	20
Breakdown	8.75
Penetration ft/hr average	62.93

Drill # 6

Holes	875
Footage	46,820
Drilling hours	694.25
Travelling hours	125.25
Standby	10
Penetration ft/hr average	67.44

Drill # 7

Thompson Drilling

Holes	1,228
Footage	65,810
Drilling hours	911.75
Travelling hours	144.25
Standby	0
Penetration ft/hr average	72.18

0038

Drilling Supplies

Bran (bags)	1,853
Mud (bags)	3,349
Starter bits $5\frac{5}{8}$ "	12
Blades $4\frac{1}{2}$ "	343
Blades $4\frac{3}{4}$ "	429
Blades $5\frac{1}{8}$ "	186
Blades $5\frac{5}{8}$ "	42
Insert bit $5\frac{1}{8}$ "	5
Rock bits $4\frac{1}{2}$ "	34

069A EXPERIMENTAL SHOOTING

On January 22 and 23, 1969, an experimental program was conducted in O.E.L. 22 South Australia in the 069A land seismic survey. This program consisted of four individual tests, and the following outline presents the information desired, tests carried out, and the results obtained.

Test #1 This test consisted of a noise analysis to determine the different types of noises present in the area, and also the optimum shooting depth.

To accomplish this, an L spread was laid out with 18 geophones in line and 6 broadside to the shot holes, and a geophone spacing of 40 feet. The shot holes were drilled at such spacings to give continuous sub-surface coverage with a depth point every 20 feet until a maximum surface offset of 5040 feet was attained.

The shot holes were drilled to a depth of 90 feet, and shot at depths of 90 feet, 70 feet, 50 feet and 30 feet.

The results of this noise analysis showed that the noises present were all in line, and consisted of a ground roll with a velocity of approximately 3400 Fps and a wavelength of 310 feet, plus a range of noises with wavelengths varying from 85 feet to 390 feet.

The results of the optimum shooting depth tests indicated that the 50 foot to 30 foot shot depths gave much cleaner signals.

Test #2 The purpose of these tests were to determine the amount of noise
and #3 attenuation obtained with three different in line geophone arrays.



ENV 990.

This was done by laying out four parallel 12 channel spreads with a configuration of 400 foot group intervals and an in line offset of 400' - 4800'. The four individual cables had the geophone laid out as follows:-

Cable #1 -- 24 phones clustered

Cable #2 -- 24 phones inline, 115' array, 5' interval

Cable #3 -- 24 phones inline, 230' array, 10' interval

Cable #4 -- 24 phones inline, 460' array, 20' interval.

The 230' array gave the best results in noise attenuation, indicating that the noise wavelength spectrum was composed predominantly of wavelengths between 50 and 230 feet.

Test #4 The purpose of this test was to determine the optimum shot hole pattern that would give the greatest noise cancellation.

This was done by laying out two parallel 12 channel cables with the same spread configuration as was used in Tests #2 and 3. The geophone configuration consisted of a 24 phone cluster on one cable and a 24 phone - 230 foot inline array on the second cable.

The shot hole patterns attempted were as follows:-

1 3 inline holes, 50' apart, 40' deep, 5# per hole

2 5 inline holes, 50' apart, 40' deep, 5# per hole

3 3 inline holes, 100' apart, 40' deep, 5# per hole

The results of this test indicated that the 5 hole pattern gave the best noise cancellation, particularly with respect to the ground roll noise.

This experimental program consumed a total of two days, and the following configurations were decided upon to give the best quality results:-

1. Geophone Configuration

24 - 14 cycle 70% damped geophones laid out inline with a 10 foot phone interval and covering 230 feet on the ground.

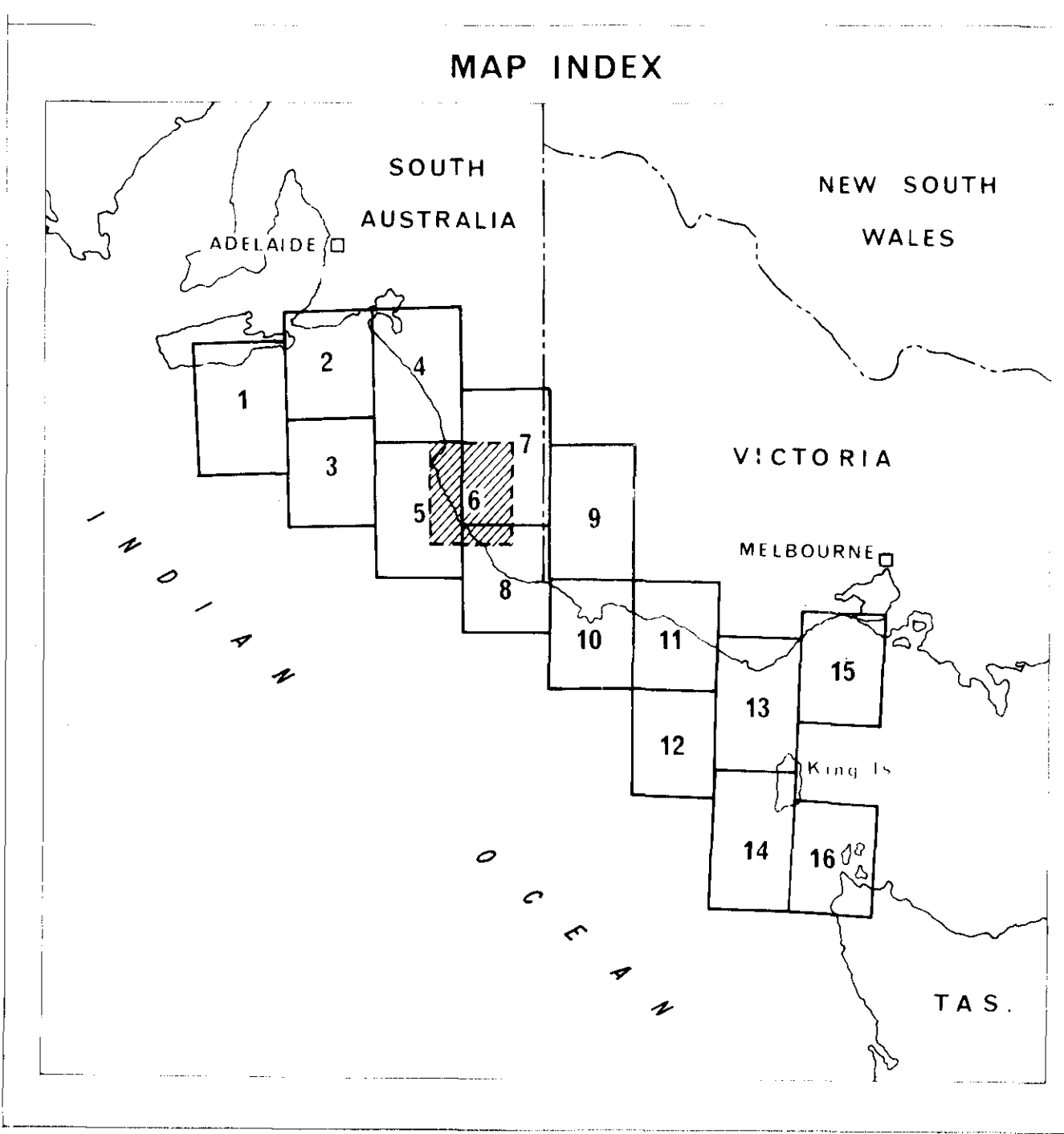
2. Spread Configuration

An inline offset of 400' - 4800'. This is a geophone station spacing of 200 feet.

3. Shot Point Configuration

A 5 hole inline shot pattern with 50 foot hole interval, 40 feet deep, and loaded with 5# per hole.

It should be pointed out that these recording parameters were adjusted from area to area depending upon the local noise and sub-surface conditions that were present, but that the greatest percentage of the program was recorded with the parameters determined from this experimental program.

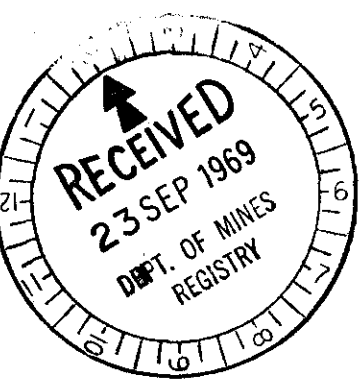


LEGEND

- | | |
|-----------|--------------------------------------|
| EU - 6 | ESSO EU SURVEY |
| EP - 6 | ESSO EP SURVEY |
| 069 A - 6 | ESSO 069 A SURVEY |
| M - SB | S.A. MINES DEPT. SB LINE |
| B | ALLIANCE B LINE |
| ○ | Drilling Location |
| ✱ | Dry and abandoned with a show of gas |
| ◇ | Dry and abandoned well |
| ○ | Seismic shot point |
| U | Fault - "U" - Downthrown side |
| D | Fault - "D" - Upthrown side |
| --- | Petroleum Tenement boundary |

ESSO EXPLORATION AND PRODUCTION AUSTRALIA INC.
THE OTWAY BASIN
SOUTH AUSTRALIA

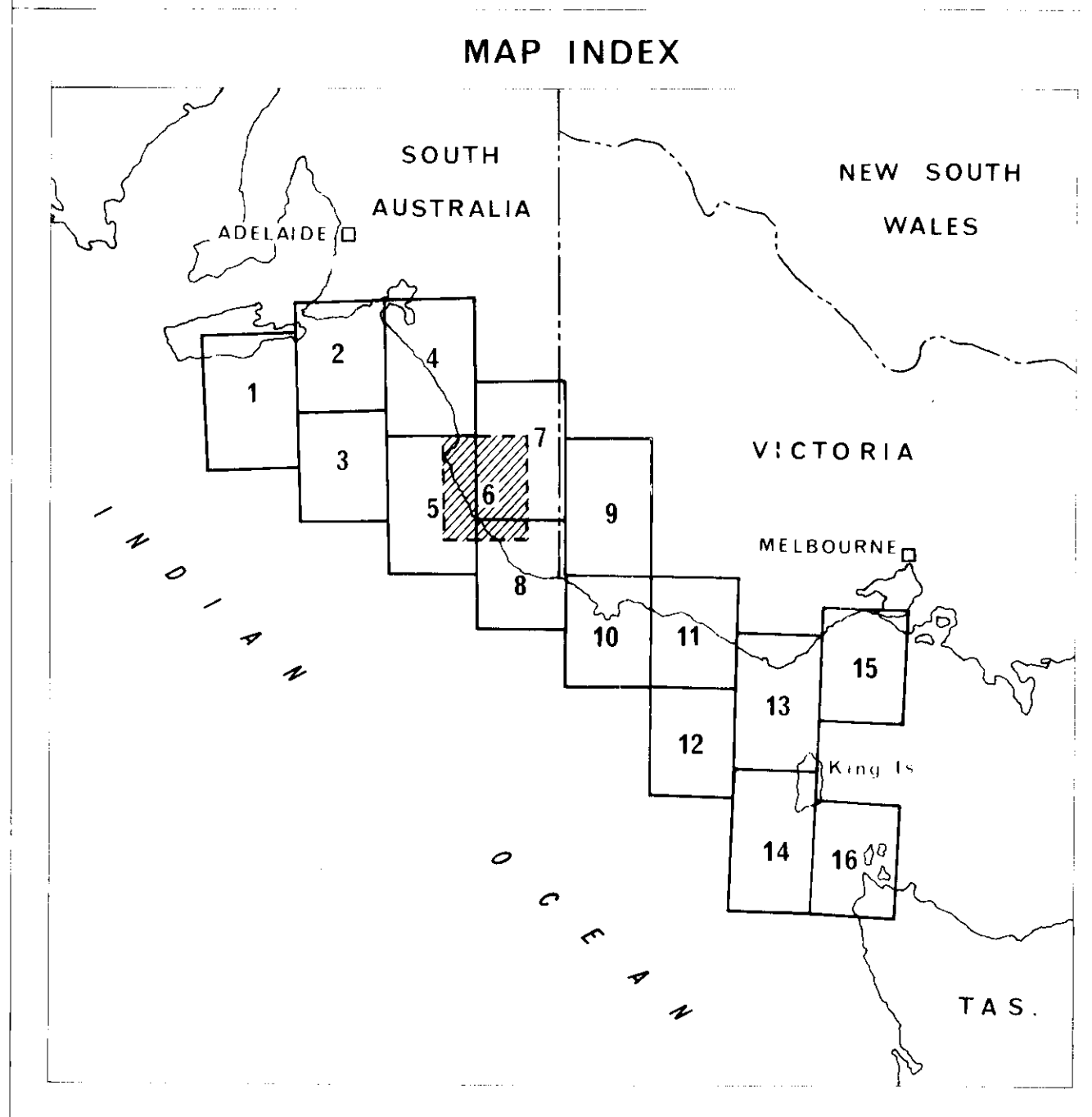
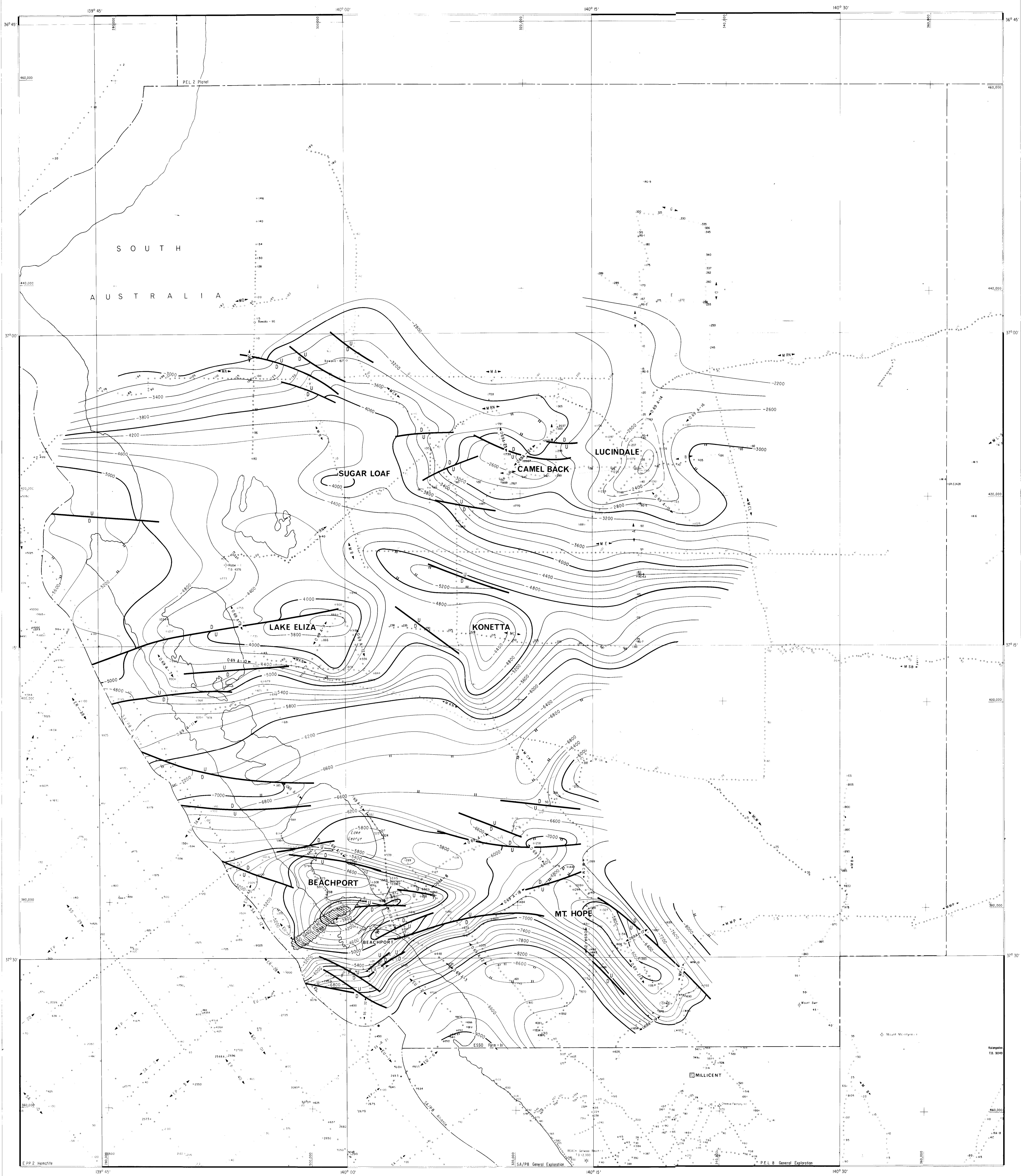
STRUCTURE CONTOURS ON
ECONOMIC BASEMENT
(Pre-Cretaceous Surface)



CONTOUR INTERVAL: 600 FEET
Scale 1:100,000
MILES
2 1 0 1 2
DRAUGHTED BY: M.R. CHATENAY
DATE: SEPTEMBER 1989
SHEET 8
PLATE 1

ENV 990-1

Dwg 1178 G 4

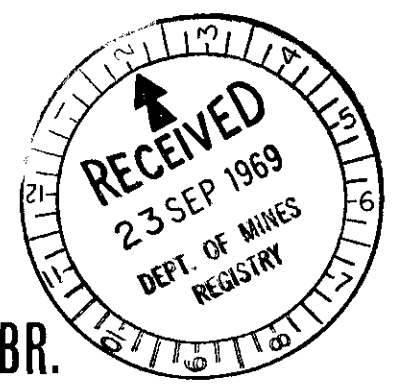


LEGEND

- | | |
|-----------|--------------------------------------|
| EU - 6 | ESSO EU SURVEY |
| EP - 6 | ESSO EP SURVEY |
| 069 A - 6 | ESSO 069 A SURVEY |
| M - SB | S.A. MINES DEPT SB LINE |
| B | ALLIANCE B LINE |
| ○ | Drilling Location |
| ☆ | Dry and abandoned with a show of gas |
| ◇ | Dry and abandoned well |
| • | Seismic shot point |
| U | Fault - "U" - Downthrown side |
| --- | Petroleum Tenement boundary |

ESSO EXPLORATION AND PRODUCTION AUSTRALIA INC.
THE OTWAY BASIN
SOUTH AUSTRALIA

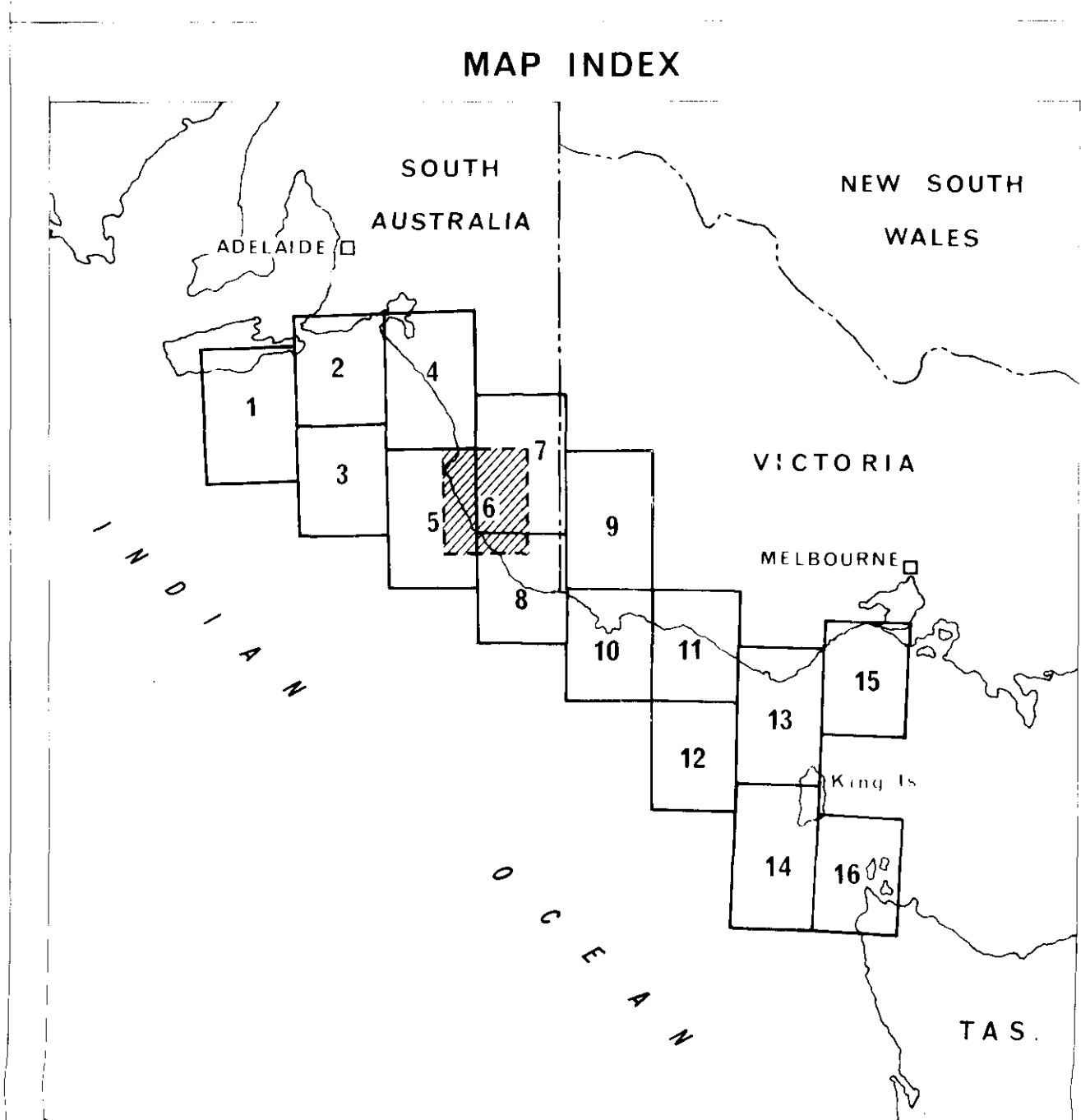
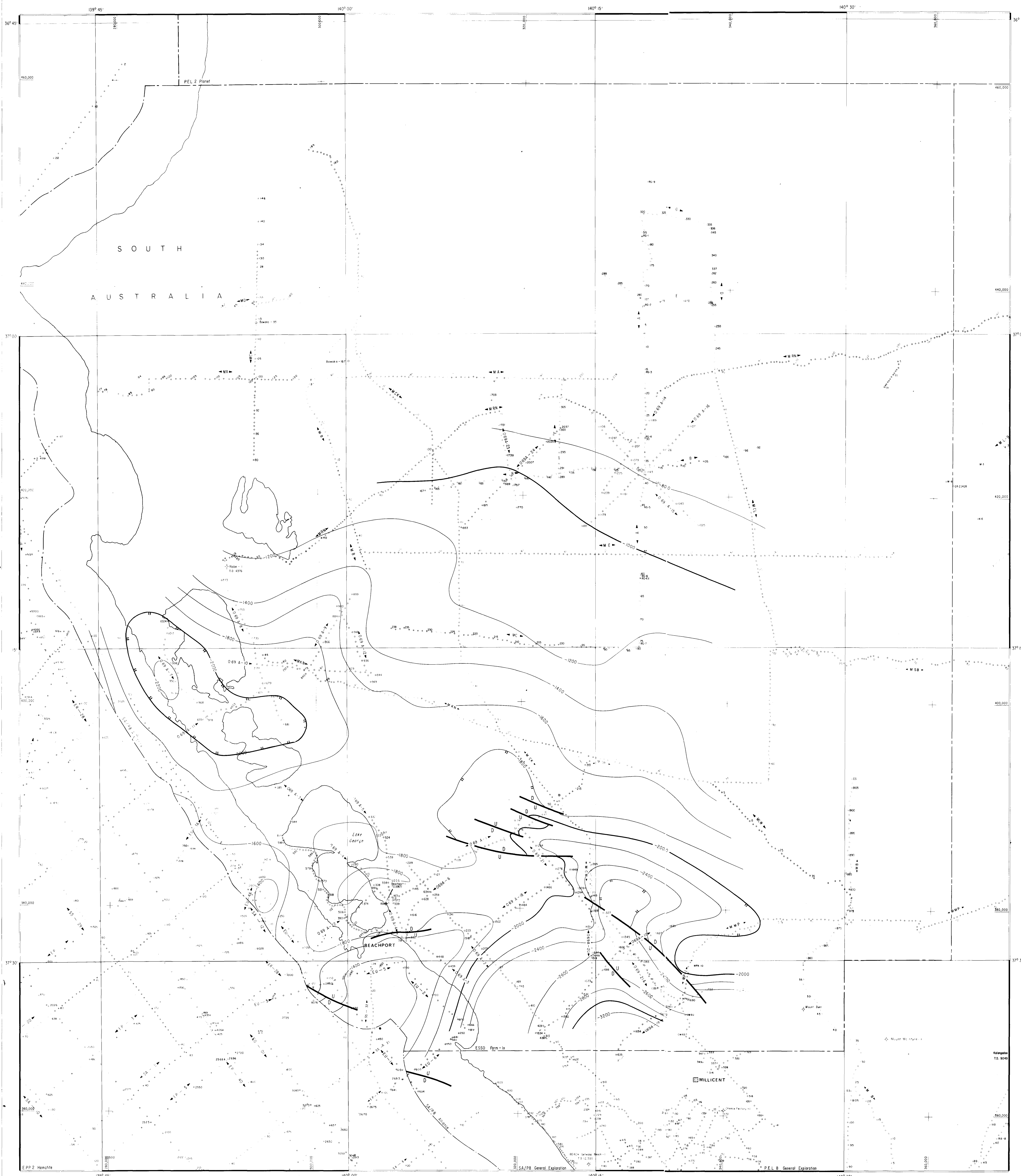
STRUCTURE MAP ON
TOP OF PRETTY HILLS SS. MBR.
(Crayfish Sand)



CONTOUR INTERVAL: 200 FEET
Scale 1:100,000
MILES
DATUM: SEA LEVEL

AUTHOR: R.W. WIGGIN
TO ACCOMPANY: FINAL SUBSIDY REPORT
SHEET 8
DRAFTED BY: M.R. CHATELAIN
DATE: SEPTEMBER 1989
PLATE II

ENV 990-2



LEGEND

- | | |
|-----------|--------------------------------------|
| EU - 6 | ESSO EU SURVEY |
| EP - 6 | ESSO EP SURVEY |
| 069 A - 6 | ESSO 069 A SURVEY |
| M - SB | S.A. MINES DEPT. SB LINE |
| B | ALLIANCE B LINE |
| ○ | Drilling Location |
| ✱ | Dry and abandoned with a show of gas |
| ✱ | Dry and abandoned well |
| ○ | Seismic shot point |
| U | Fault - "U" - Downthrown side |
| --- | Petroleum Tenement boundary |

ESSO EXPLORATION AND PRODUCTION AUSTRALIA INC. **THE OTWAY BASIN** SOUTH AUSTRALIA

STRUCTURE MAP ON
BASE OF TERTIARY

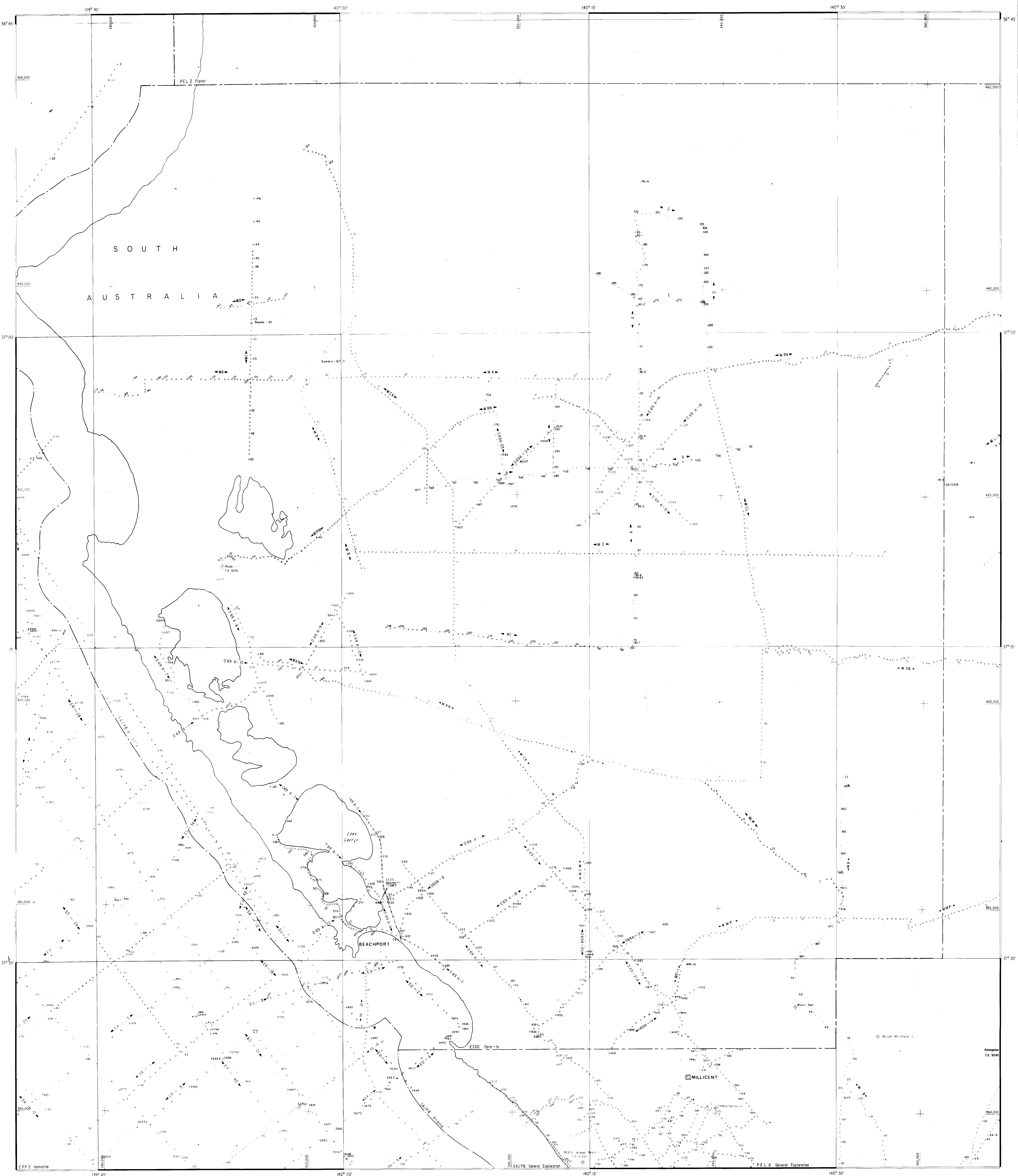


CONTOUR INTERVAL: 200 FEET DATUM: SEA LEVEL

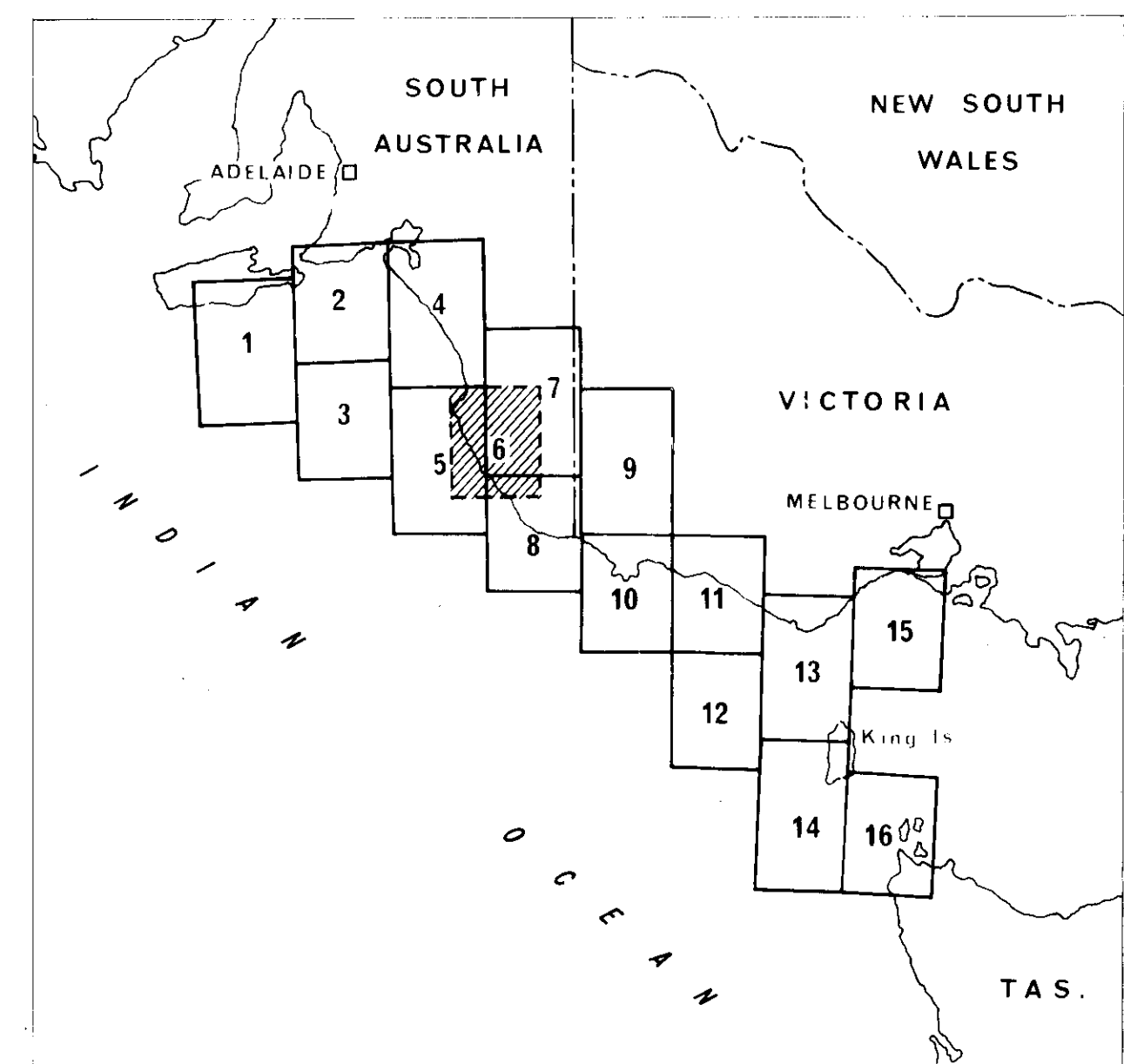
Scale 1:100,000
MILES

AUTHOR: R.W. WIGGIN
TO ACCOMPANY: FINAL SUBSIDY REPORT
SHEET 6

DRAFTED BY: M.R. CHATENAY
DATE: SEPTEMBER 1988
PLATE III



MAP INDEX



LEGEND

- | | |
|-----------|--------------------------------------|
| EU - 6 | ESSO EU SURVEY |
| EP - 6 | ESSO EP SURVEY |
| 069 A - 6 | ESSO 069 A SURVEY |
| M - SB | S.A. MINES DEPT. SB LINE |
| B | ALLIANCE B LINE |
| ○ | Drilling Location |
| ☆ | Dry and abandoned with a show of gas |
| ✱ | Dry and abandoned well |
| ● | Seismic shot point |
| —○— | Fault - "O" - Downthrown side |
| --- | Petroleum Tenement boundary |

VELOCITY SCANS	
069 A LINE NO.	SHOT POINT NO.
1	26, 61, 100, 121, 156
2	187, 265, 432
3	466, 503
5	326
7	1023
8	695, 726, 756
10	806, 838
11	665
15	1061
16	1116, 1152
19	1663, 1684
20	1528
21A	1362
23	1709
26	1692, 2036

PERMANENT MARKERS	
069 A LINE NO.	SHOT POINT NO.
1	1
2	56
2	262
2	209
2	438
3	439
3	469
3	385
3	388
5	522
5	572
7	952
7	978
7	979
7	1004
8	681
8	712
8	773
9	886
10	905
10	839
14	1189
14	1239
15	1025
15	1070
15	1106
16	1107
16	1188
17	1534
17	1579
19	1636
19	1702
20	1395
21	1308
21	1309
21	1394
23	1703
23	1752
23	1770
24	1953
24	2037

ESSO EXPLORATION AND PRODUCTION AUSTRALIA INC.
THE OTWAY BASIN
VICTORIA-SOUTH AUSTRALIA

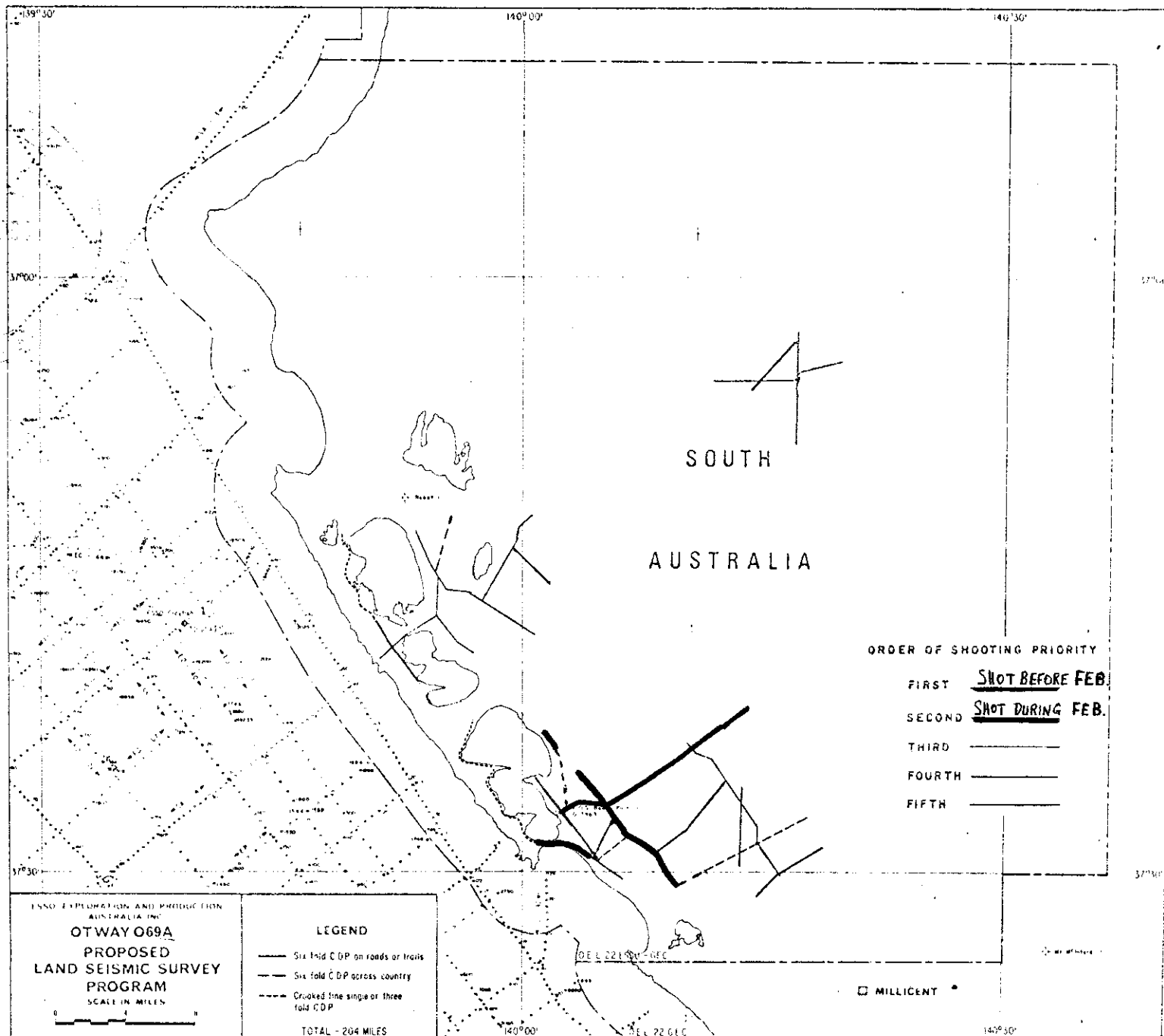
SHOT POINT MAP

CONTOUR INTERVAL : 200 FEET
Scale 1:100,000
MILES
2 1 0 2 4
DRAFTED BY: MR. CHATENAY
DATE: SEPTEMBER 1969
SHEET 6
6 69 A SEISMIC SURVEY
PLATE IV
Dwg 1178/G/



ENV 990-4

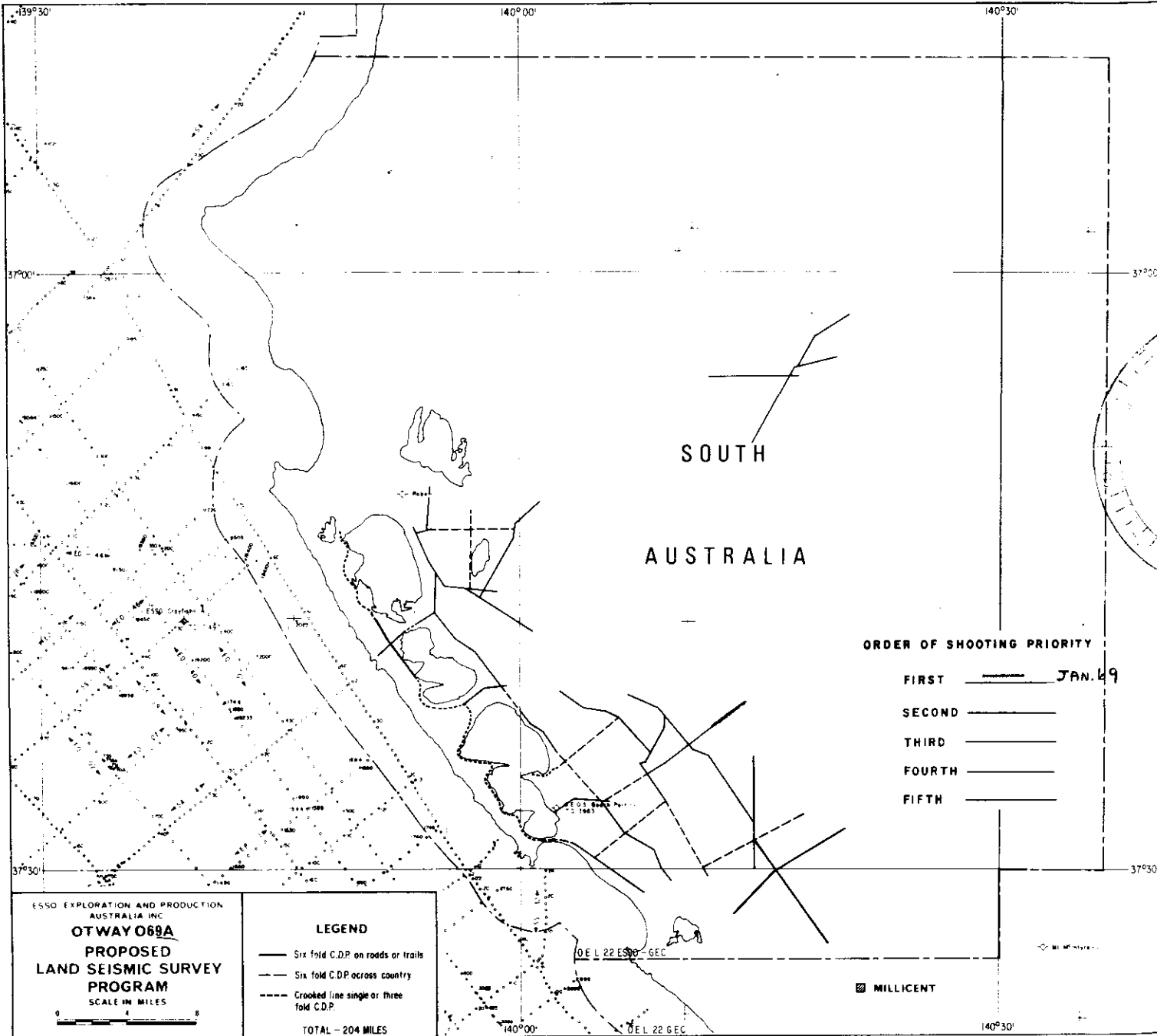
ENV 990



JAN. 1969

DWG 656/OP/14

ENV 990 - 5



JAN. 1969

DWG 856/OP/14

ENV 990-6

SEISMIC PRODUCTION REPORT

[illegible]

SEISMIC PRODUCTION REPORT

NOTES		BASIC CREW TIME	
* Denotes check totals which should appear on print in RED INK		Carry Over	NIL
Denotes refraction statistics.		Current	103
		Total Hours	103
		Contract	900
		Carry Over	103
	REFLECTION	REFRACTION	TOTALS
No. of shot points	65		65
Profiles recorded *	50		50
To date	50		50
Miles surface coverage	2.095		2.095
Total depth shots	51		51
Wx and other	-		-
Miles to field	-		-
Hours travel	6		6
Hours field	75 1/2		75 1/2
Hours lost - Weather	-		-
Hours lost - Equipment	-		-
Hours moving camp STAND BY	2 1/2		2 1/2
Hours holidays	10		10
Total hours/day *	103		103
To date	103		103
Holes drilled	111		111
Holes washed out	4		4
Footage drilled *	5890		5890
To date	5890		5890
Miles to field	-		-
Hours travel	9 1/2		9 1/2
Hours drilling	86 1/2		86 1/2
Total hours/day *	100		100
To date	100		100
Footage/drilling hour	58.90		58.90
(under total only) STAND BY	4		4
Holes drilled	107		107
Holes washed out	2		2
Footage drilled *	5580		5580
To date	5580		5580
Miles to field	-		-
Hours travel	9 1/2		9 1/2
Hours drilling	91 1/2		91 1/2
Total hours/day *	101		101
To date	101		101
Footage/drilling hour	55.24		55.24
(under total only) STAND BY	0		0
Holes drilled	114		114
Holes washed out	4		4
Footage drilled *	5960		5960
To date	5960		5960
Miles to field	-		-
Hours travel	9 1/2		9 1/2
Hours drilling	94 1/2		94 1/2
Total hours/day *	104		104
To date	104		104
Footage/drilling hour	57.30		57.30
(under total only) STAND BY	0		0
Time lost-equipment			
Drill No. (see remarks)			
Miles line cut			
Hours (work & travel) *			
To date			
Miles line cut			
Hours (work & travel) *			
To date			
Received Type 5 1/2			
Used GEOPHON	1645		
On hand	7855		
Received Type 125'			
Used CAPS	15		
On hand	65		
Received Type 100'			
Used CAPS	79		
On hand	41		
Received Type 80'			
Used CAPS	198		
On hand	2		
Received Type BOOSTER			
Used CAPS	248		
On hand	970		
Received Type CORDTEX			
Used	200		
On hand	800		
Received Type			
Used			
On hand			
Received Type			
Used			
On hand			
Received Type BRAN	70		70
Used	43 1/2		43 1/2
On hand	26 1/2		26 1/2
Received Type MUD	96		96
Used	86 1/2		86 1/2
On hand	9 1/2		9 1/2
Received Type			
Used			
On hand			
Received WM Type ROCK 4 1/2	12		12
Used	0		0
On hand	12		12
Received WM Type STARTERS	12		12
Used	12		12
On hand	0		0
Received WM Type BLADES	192		192
Used	54		54
On hand	138		138
Received WM Type BLADES	26		26
Used	3		3
On hand	23		23
Received SK Type BLADES	36		36

ENV 990-1

<

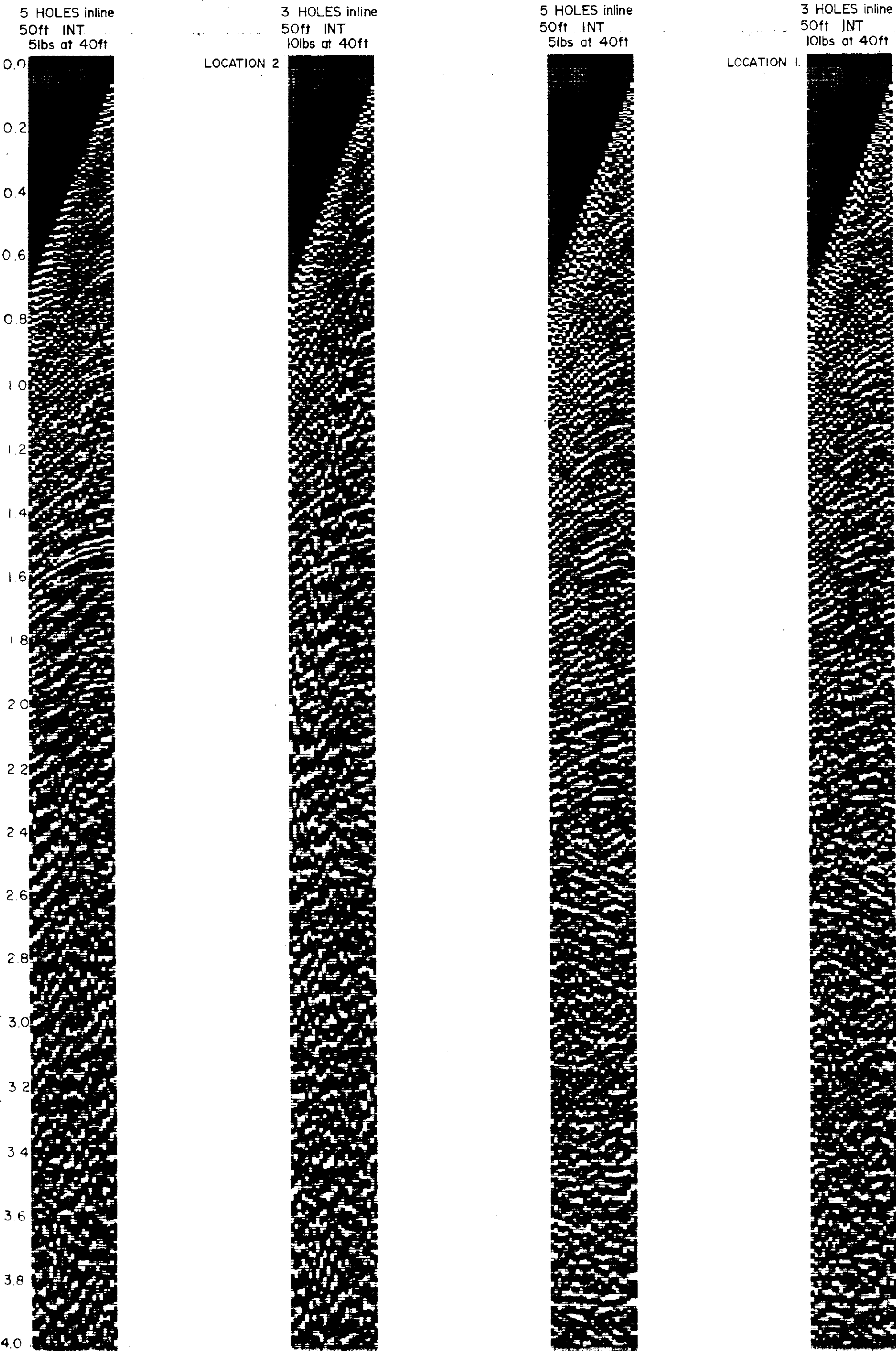
ENV 990 TT - 1

SEISMIC PRODUCTION REPORT

[illegible]

NEG.
SHOT POINT ARRAY COMPARISONS

S.P. OFFSET=400ft inline GROUP INT.=200ft
24 SEISES inline/GP 10ft INT. 230ft ARRAY FILTER=OUT/OUT



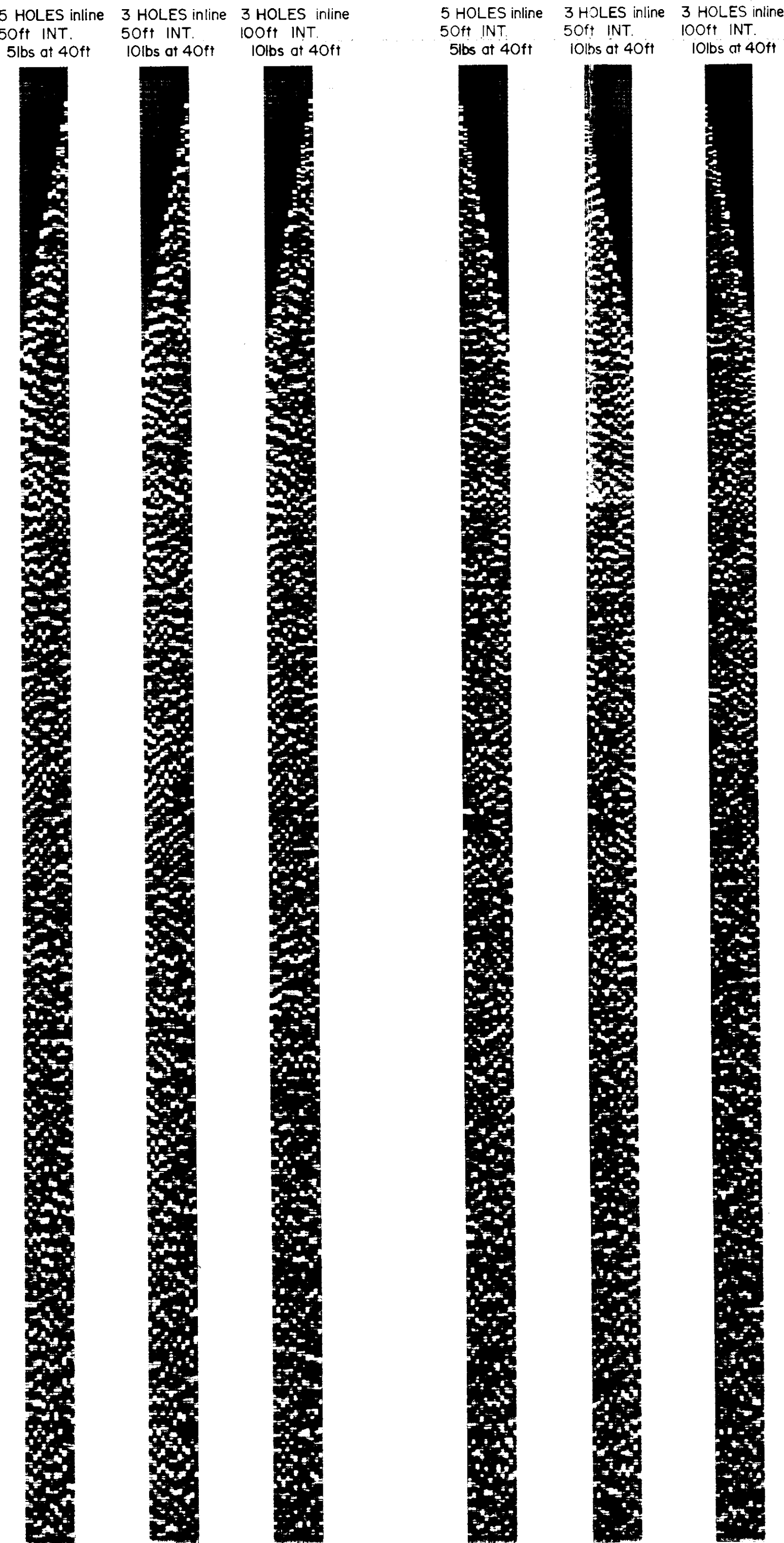
OTWAY LAND
SOUTH AUSTRALIA
FOR
ESSO STANDARD OIL
(AUSTRALIA) PTY LTD

SEISMOMETER ARRAY & SHOT POINT ARRAY
COMPARISONS

S.P. OFFSET=400ft inline GROUP INT.=200ft
FILTER=OUT/OUT
24 SEISES inline/GP 10ft INT. 230ft ARRAY 24 SEISES clustered

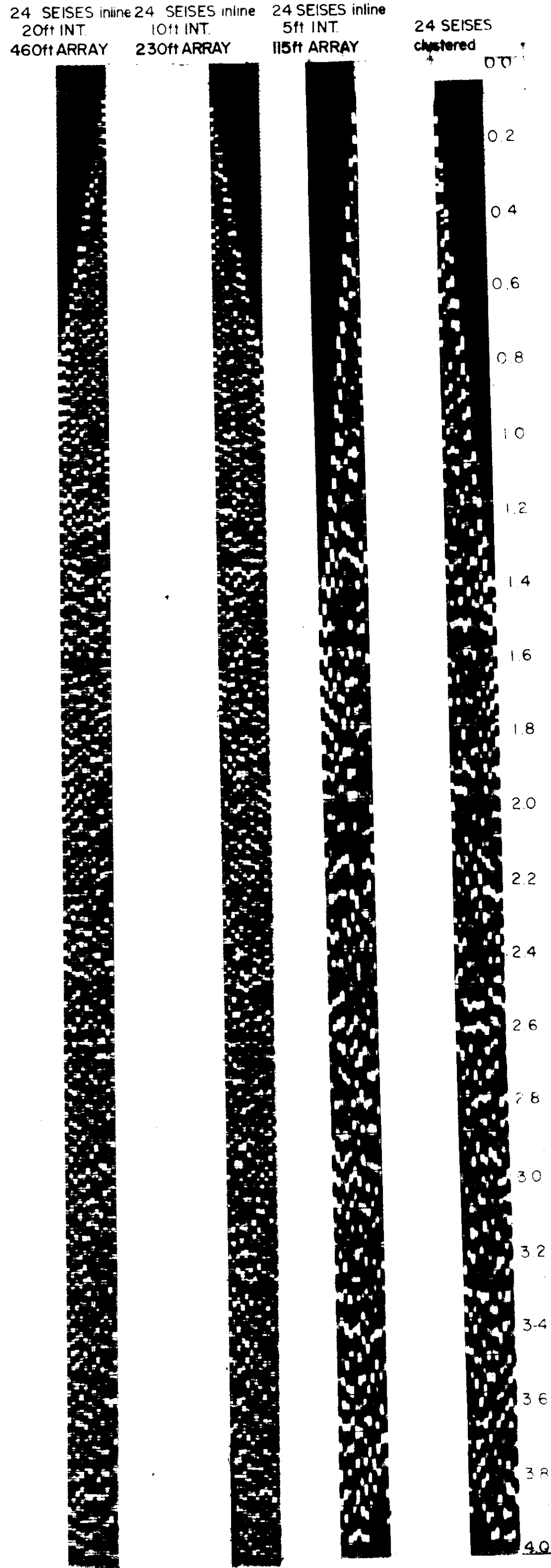


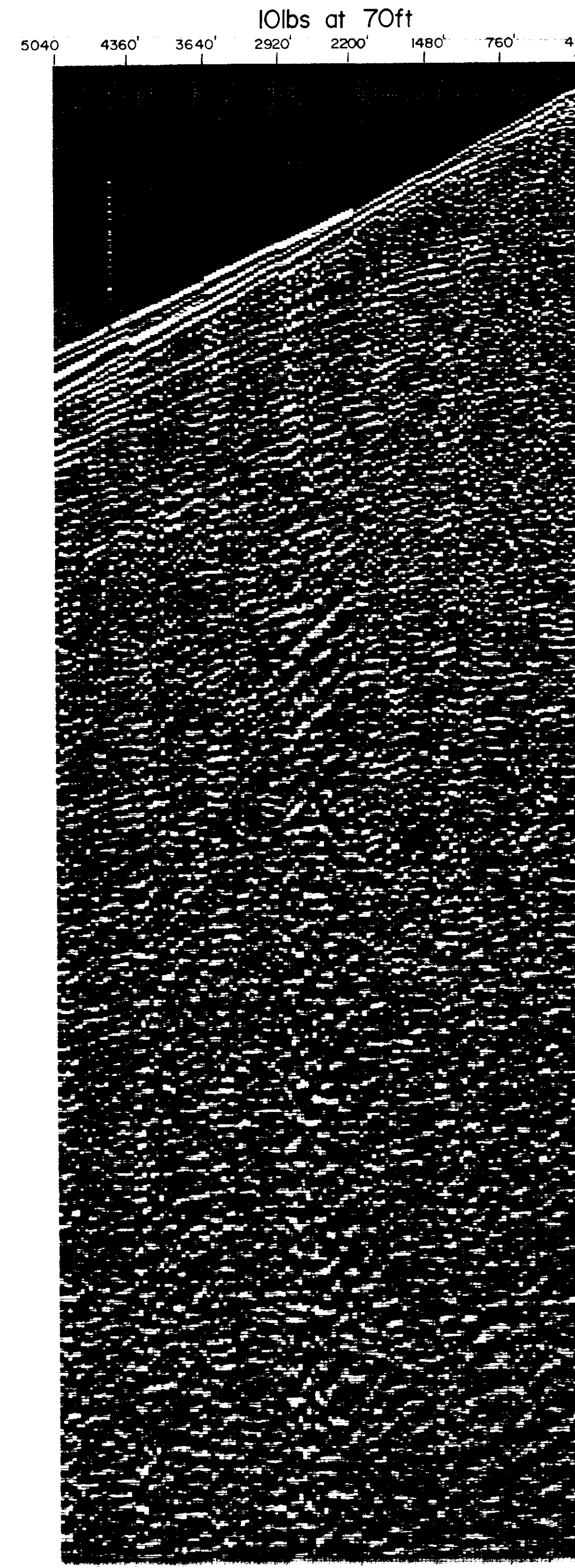
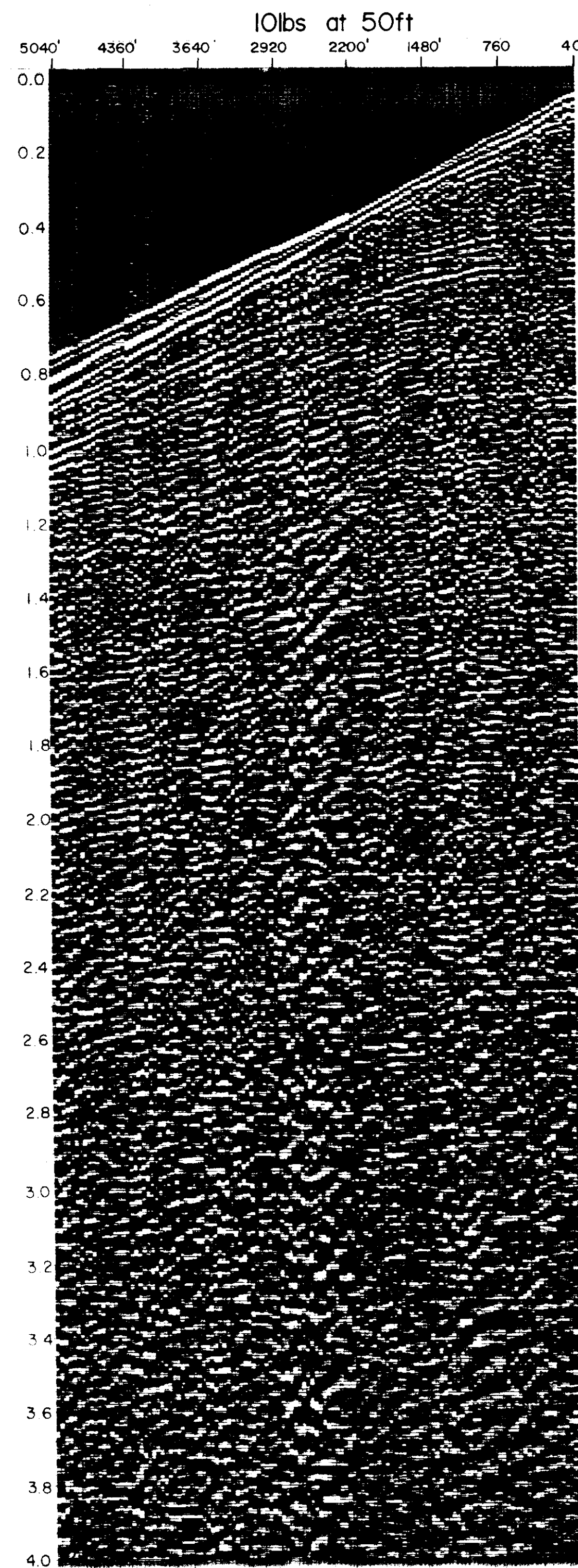
To accompany: O 69 A SEISMIC SURVEY
FINAL SUBSIDY REPORT
APPENDIX 2
LINE O 69 A - 1 Shot point 45
TEST 4



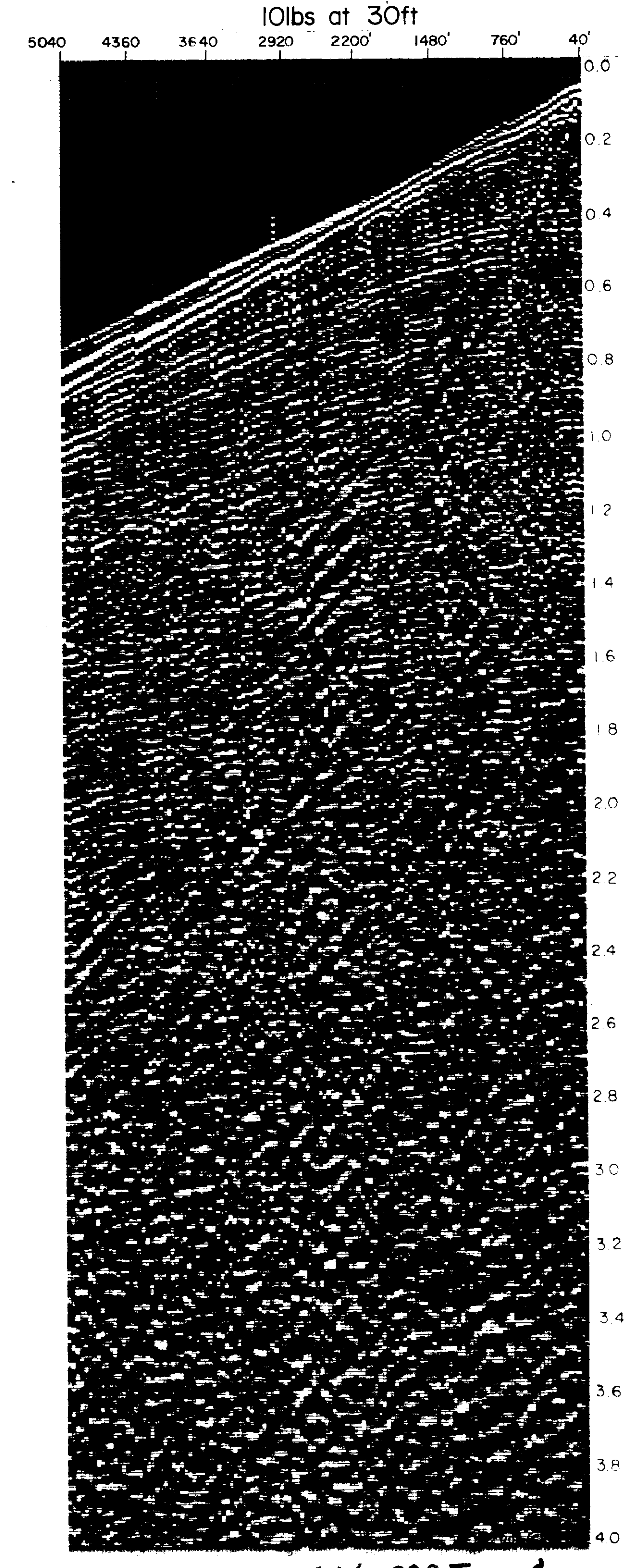
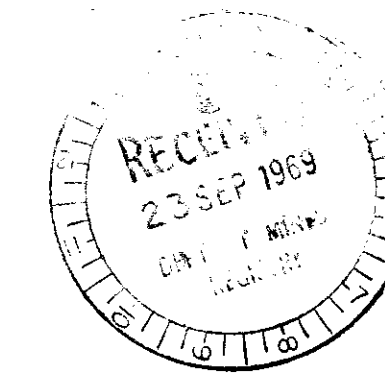
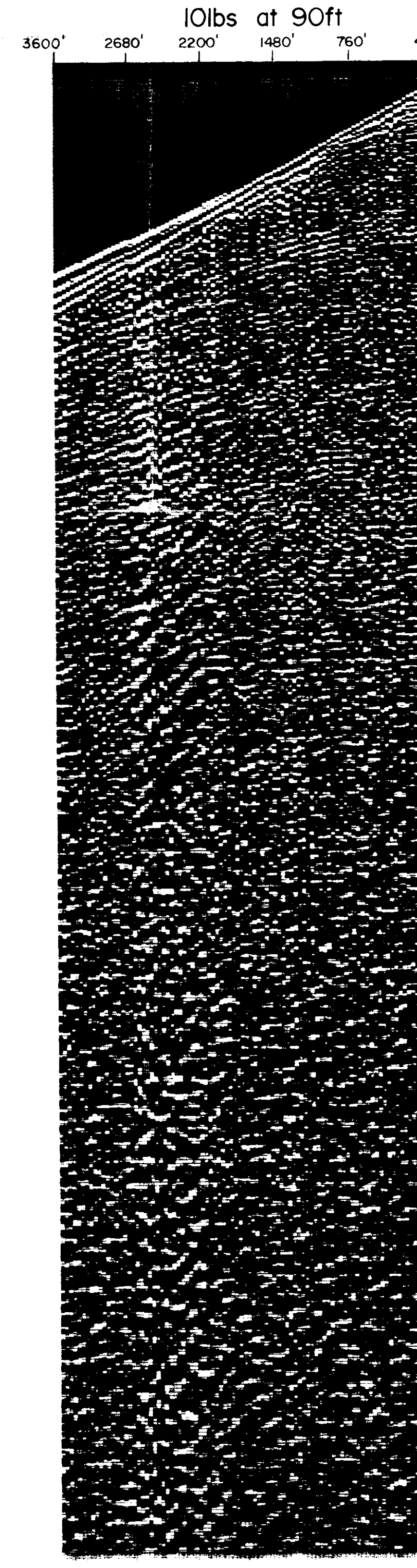
SEISMOMETER ARRAY
COMPARISONS

SINGLE HOLE 15lbs at 40ft
S.P. OFFSET=400ft inline GROUP INT.=200ft
FILTER=OUT/OUT





— SHOT TO TRACE DISTANCE —

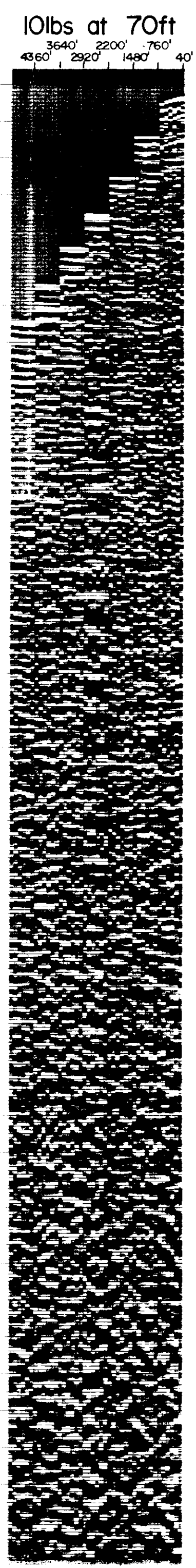
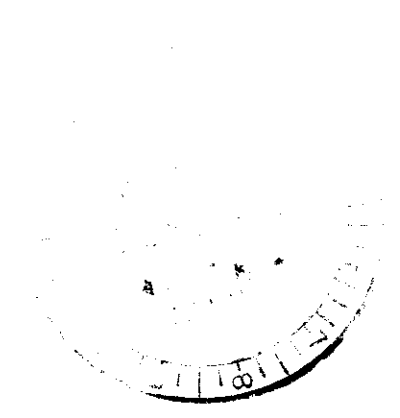
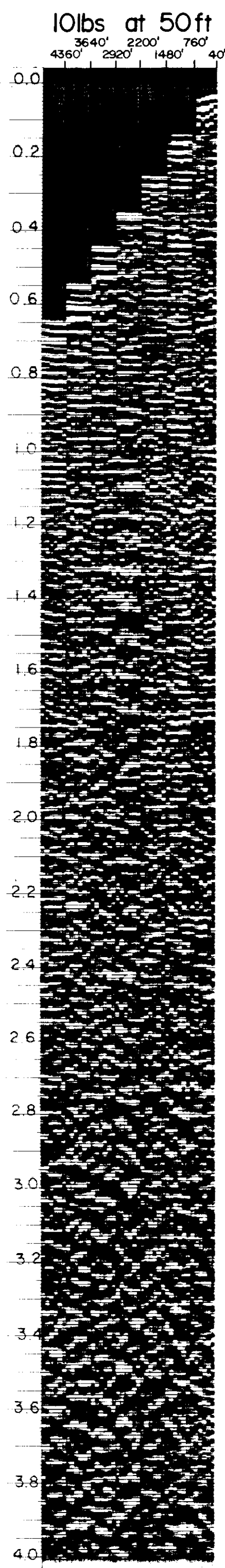


ENV 990 - 15

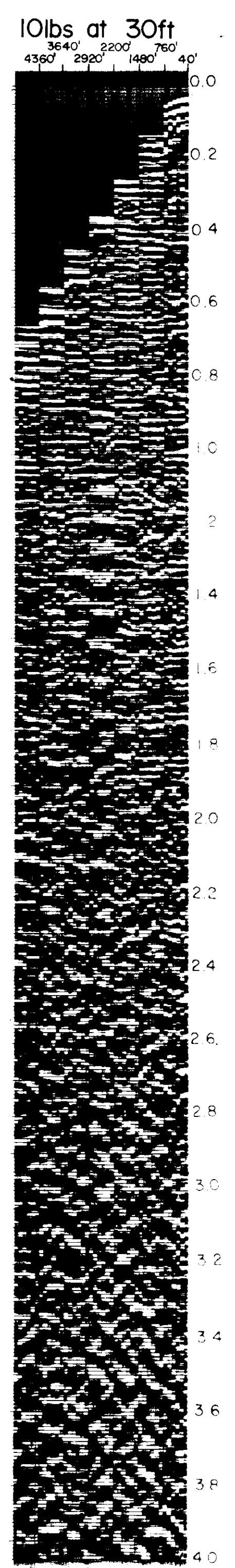
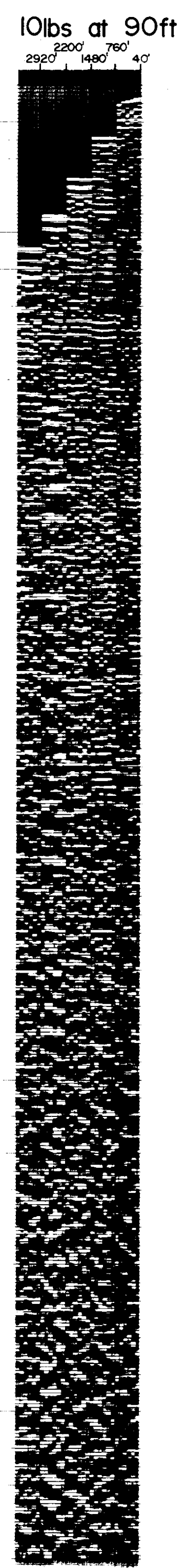
NEG.
OTWAY LAND
SOUTH AUSTRALIA
FOR
ESSO STANDARD OIL (AUSTRALIA) PTY LTD

NOISE ANALYSIS - BROADSIDE
SINGLE HOLE
FILTER: OUT/OUT

To accompany : 0 69 A SEISMIC SURVEY
FINAL SUBSIDY REPORT
APPENDIX 2
TEST 1
LINE 0 69 A - 1 Shot point 1-5



— SHOT TO TRACE DISTANCE —



ENV 990 II - 5

24 Tr GATHER 4 CDP (6 FOLD)
TVD (2-64) Ft Up/Tr
TVF 20-60Hz 500ms
15-55 " 600
10-50 " 700
10-40 " 1000
10-30 " 400

LINE 069A-1

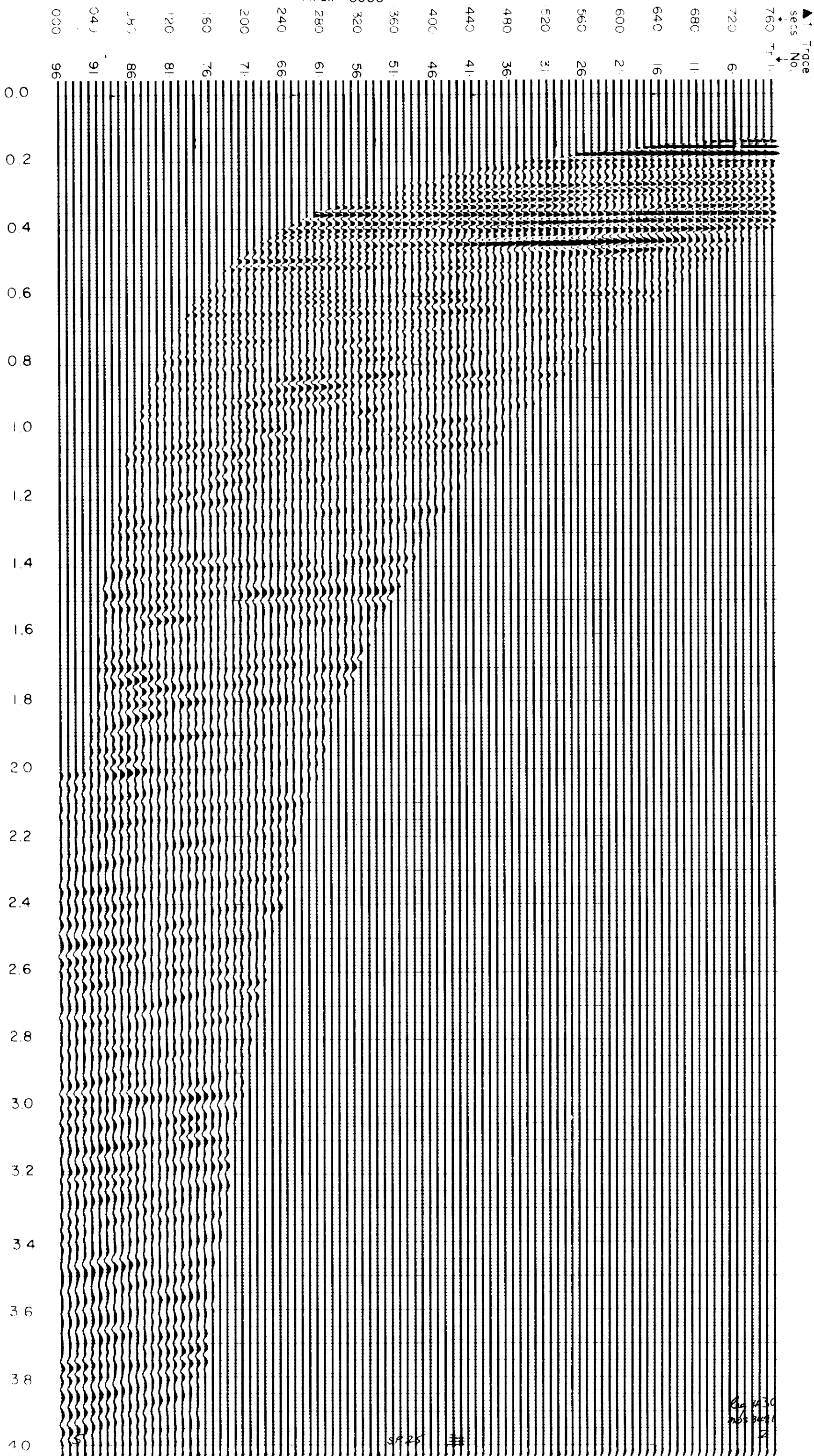
STWAY BASIN
PROCESSED BY G S I PTY 851

S.F. 25
X max = 5000'

400 Tr

24

MOVEOUT SCAN



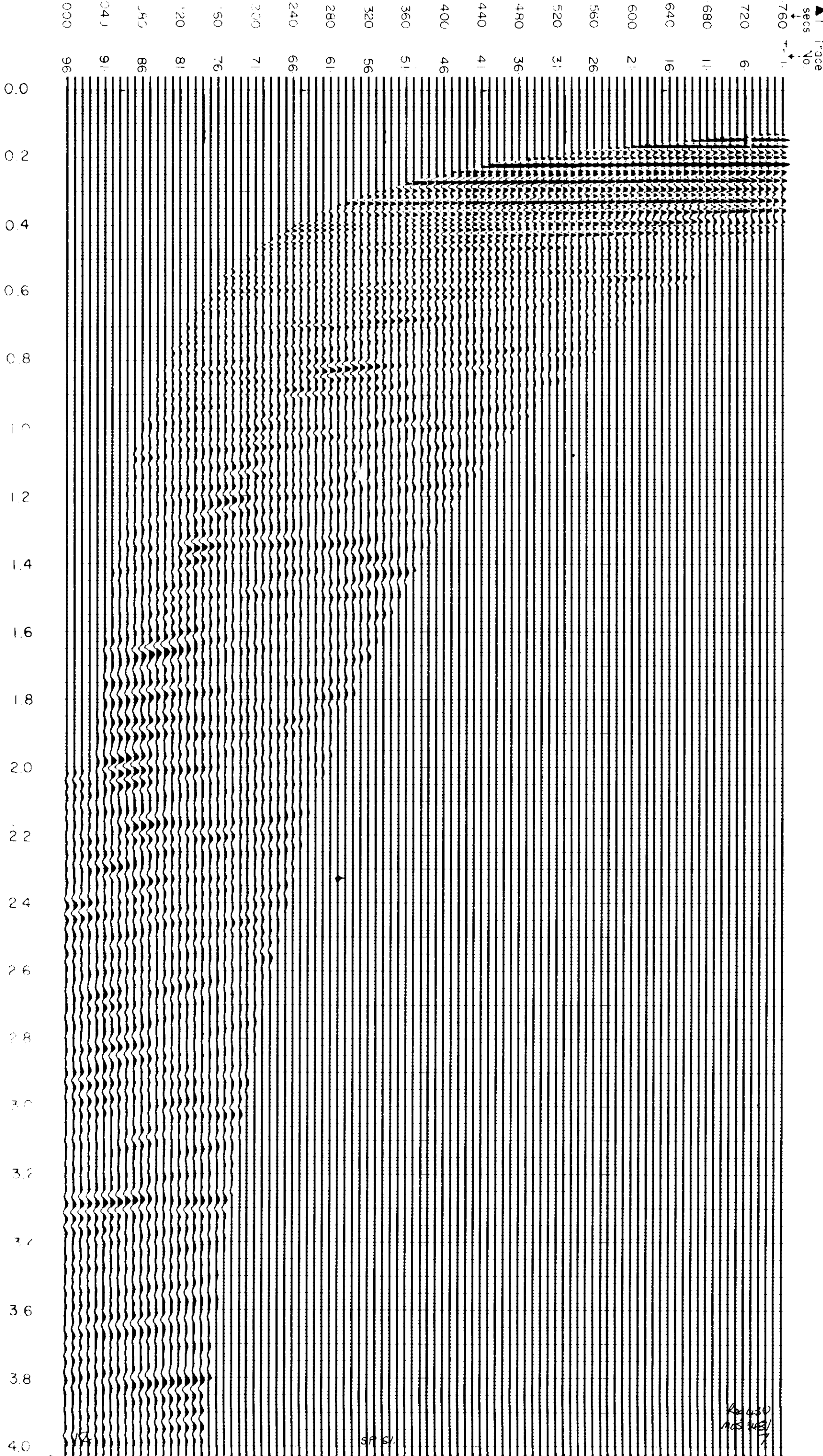
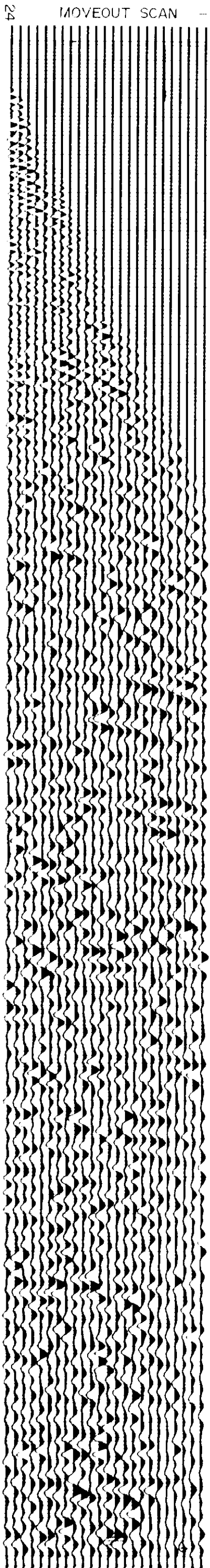
24 Tr GATHER 4 CDP (6 FOLD)
FVD 12-64) Pr Op/Tr
12F 20-60Hz 500ms
15-55 600
10-50 700
0-40 800
10-30 400

LINE 069A-1

ORWAY BASIN
PROCESSED BY G S PTY 851

S.F. 61

X max = 5000

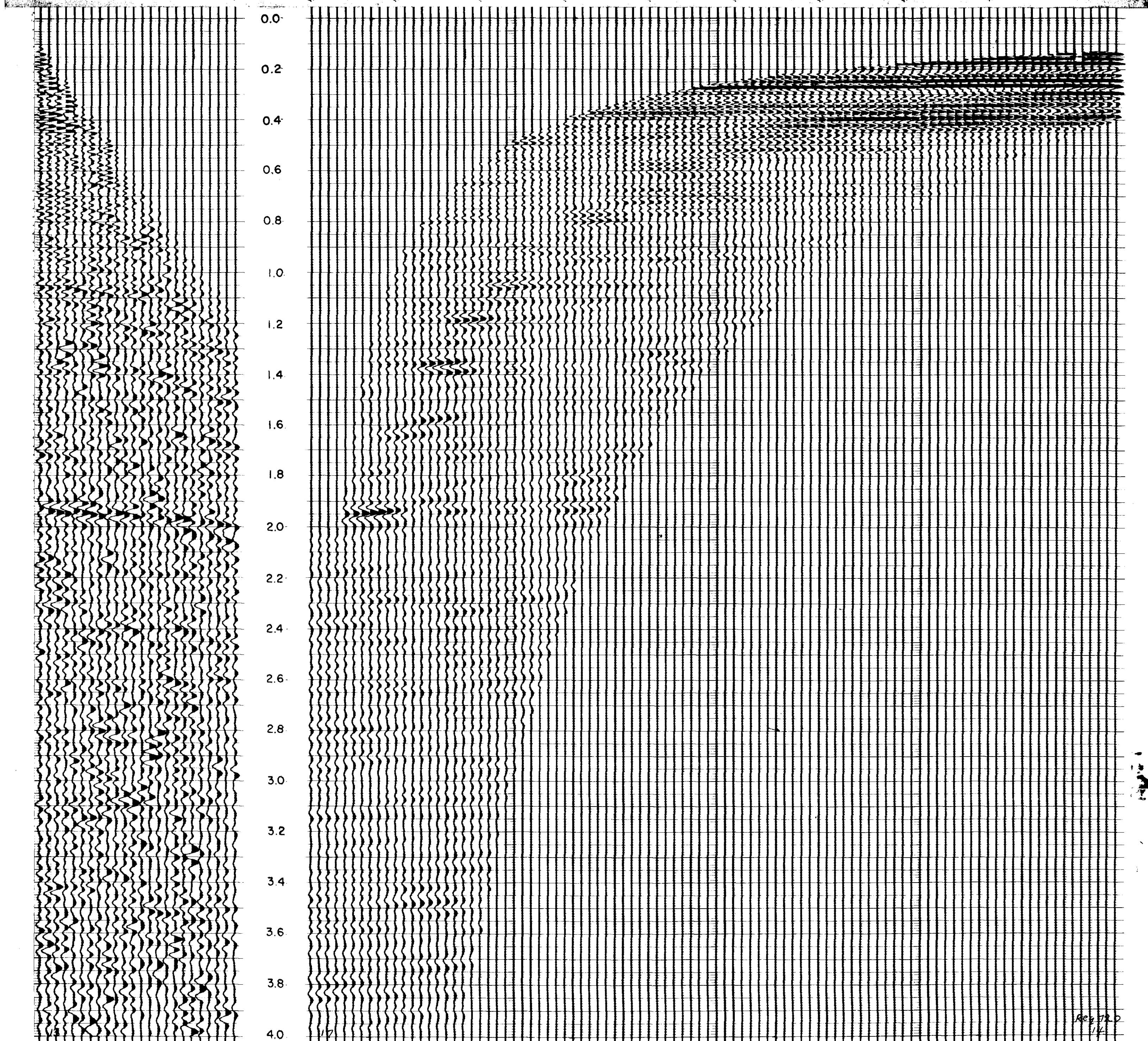


ΔT
secs
↑
.760

400 Tr

AT secs ↓	Track No.	Time
.760	11	1.1
.720	6	1.1
.680	11	1.1
.640	16	1.1
.600	21	1.1
.560	26	1.1
.520	31	1.1
.480	36	1.1
.440	41	1.1
.400	46	1.1
.360	51	1.1
.320	56	1.1
.280	61	1.1
.240	66	1.1
.200	71	1.1
.160	76	1.1
.120	81	1.1
.080	86	1.1
.040	91	1.1
.000	96	1.1

MOVEOUT SCAN



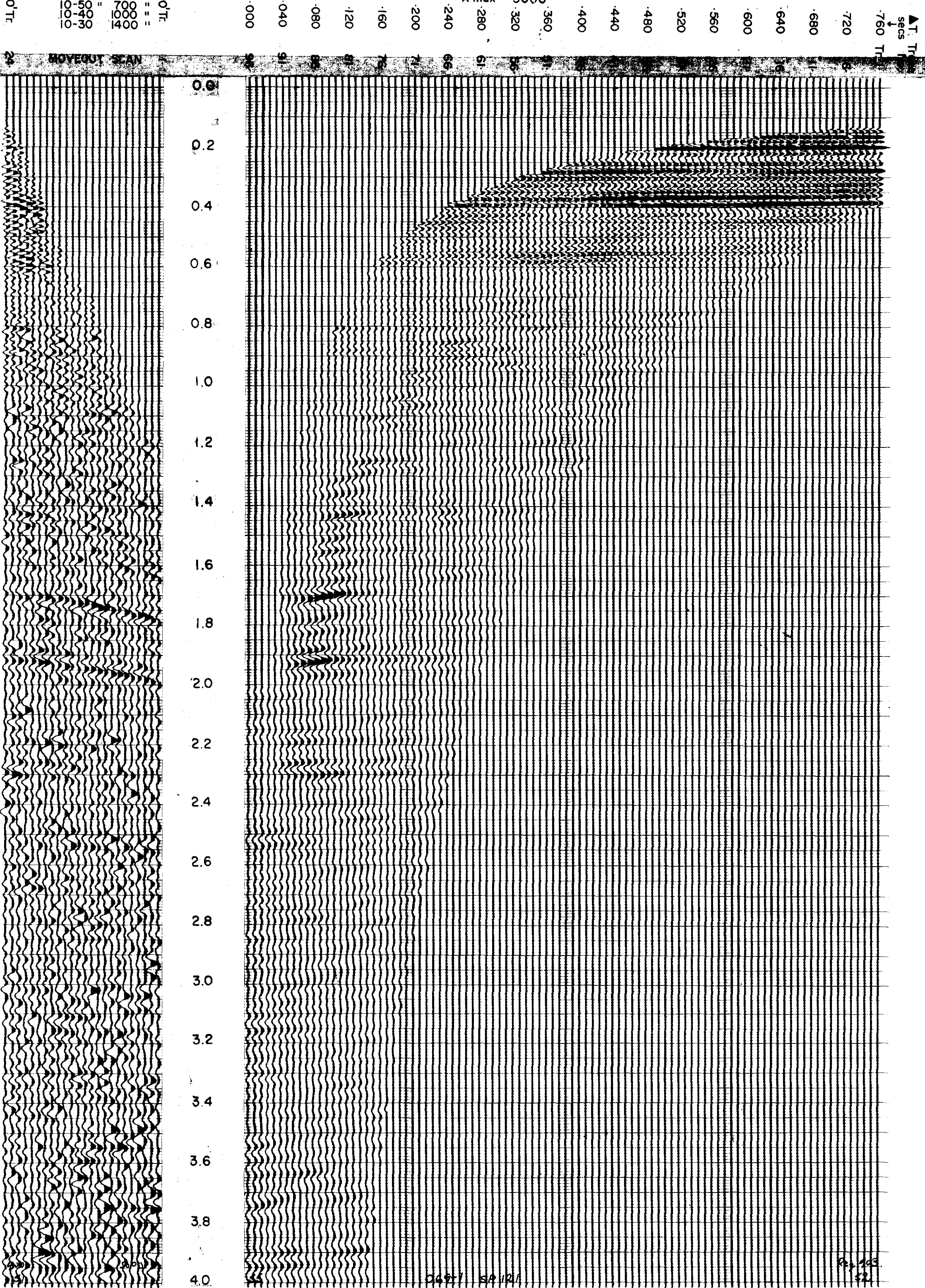
Ref 720
14

ENV 990 II -78

24 Tr. GATHER 4 CDP (6 FOLD)
TVD (2-64) Pt. Op/Tr
TVF 20-60Hz. 500ms.
15-55 " 600
10-50 " 700
10-40 " 800
10-30 " 900
5000 Tr.
400 Tr.

LINE 069A-1
S.P. 121
X max = 5000

OTWAY BASIN
PROCESSED BY G.S.I. PTY. 851



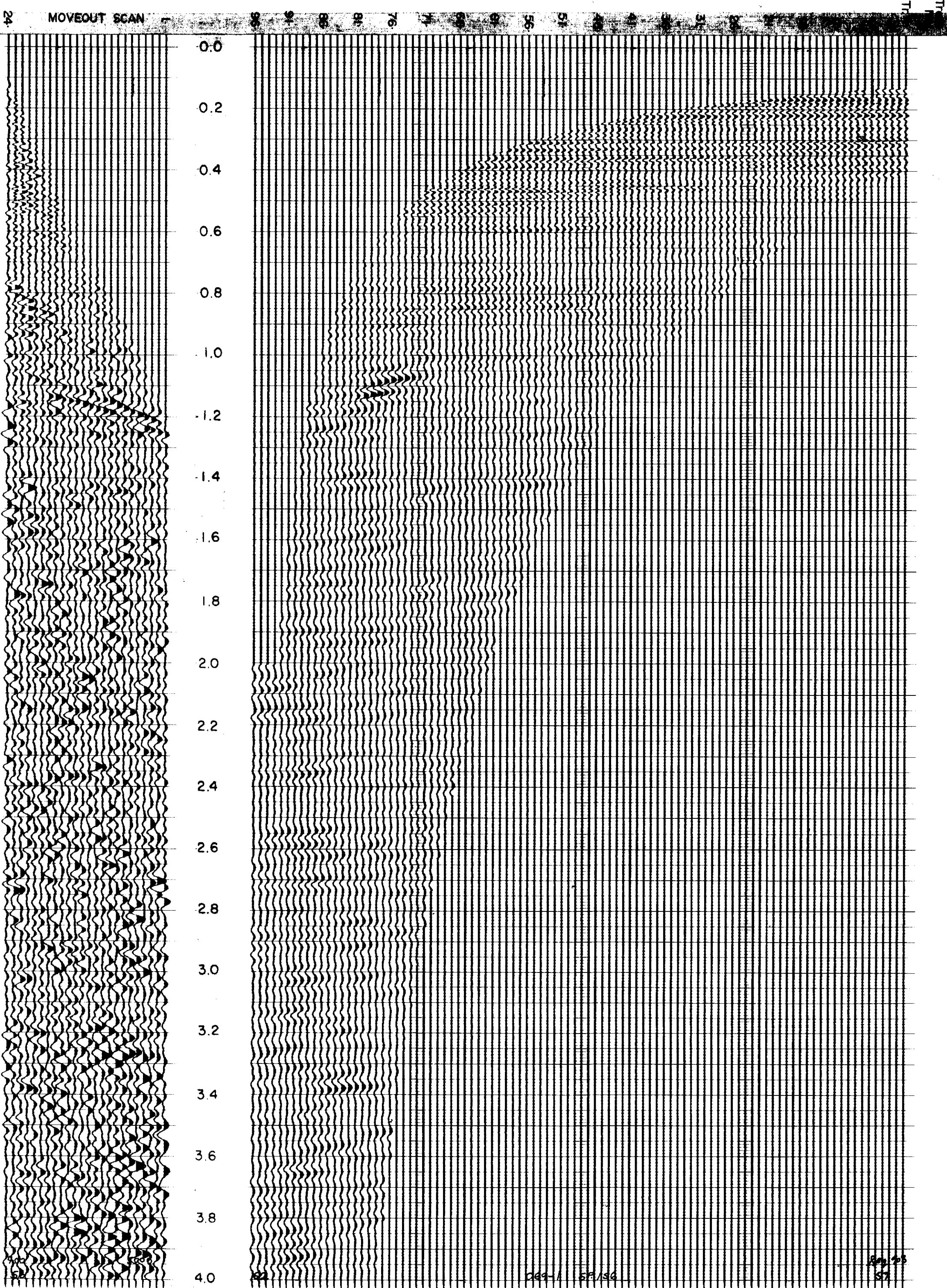
24 Tr. GATHER 4 CDP (6 FOLD)
TVD (2-64) Pt. Op/Tr
TVF 20-60Hz. 500ms.
15-55 " 600
10-50 " 700
0-40 " 1000
0-30 " 4000

LINE 069A-1
S.P. 156
X max = 5000'

OTWAY BASIN
PROCESSED BY G.S.I. PTY. 851

400 Tr.

0.00 0.04 0.08 0.12 0.16 0.20 0.24 0.28 0.32 0.36 0.40 0.44 0.48 0.52 0.56 0.60 0.64 0.68 0.72 0.76 0.80



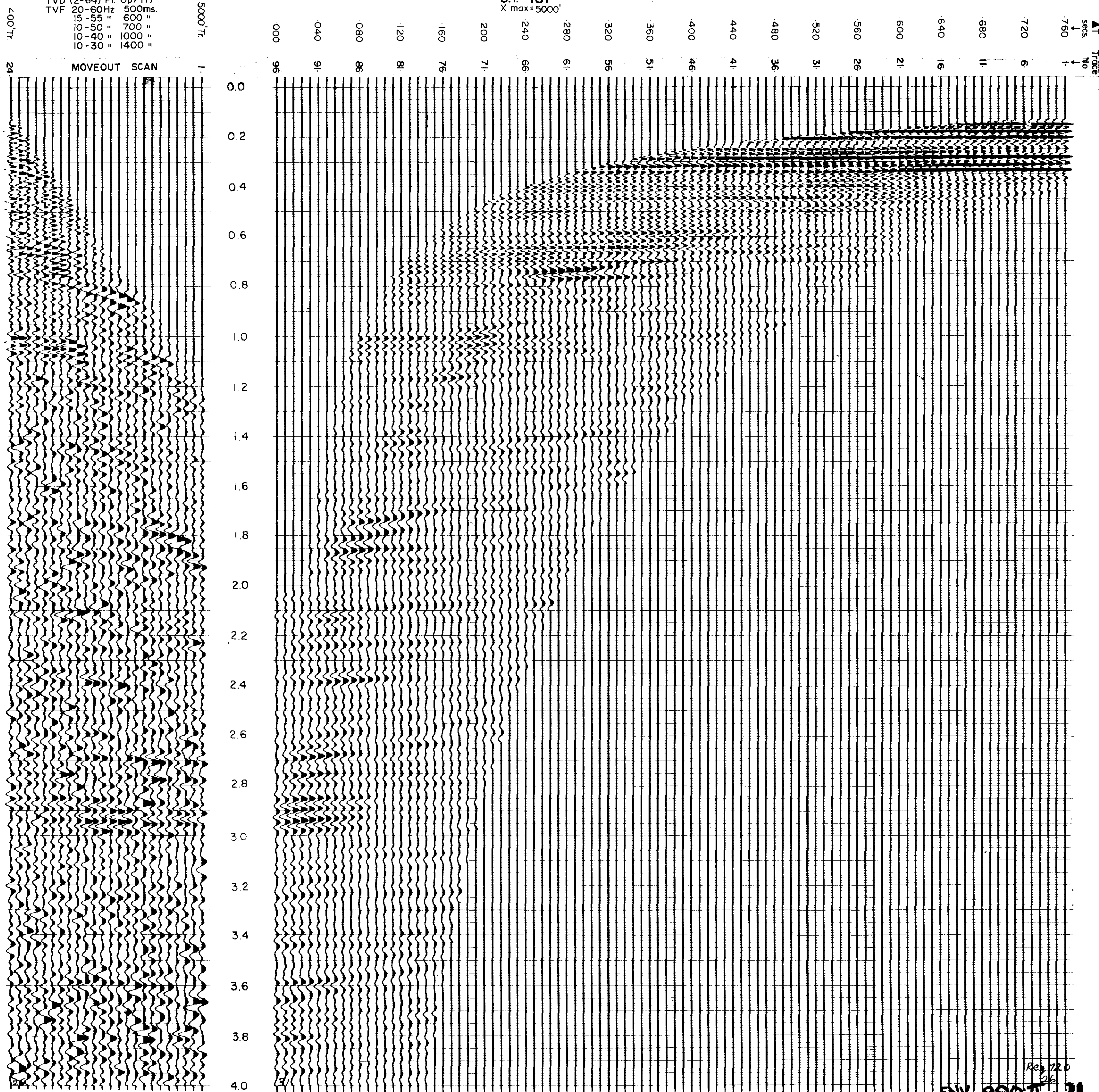
069-1 SP/196

Reg 23
57

ENV 990 II -20

24 Tr. GATHER 4 CDP(6 FOLD)
TVD (2-64) Pt. Op/Tr)
TVF 20-60Hz. 500ms.
15-55 " 600 "
10-50 " 700 "
10-40 " 1000 "
10-30 " 1400 "

LINE 069A-2
S.P. 187
X max = 5000'



Re 720
26

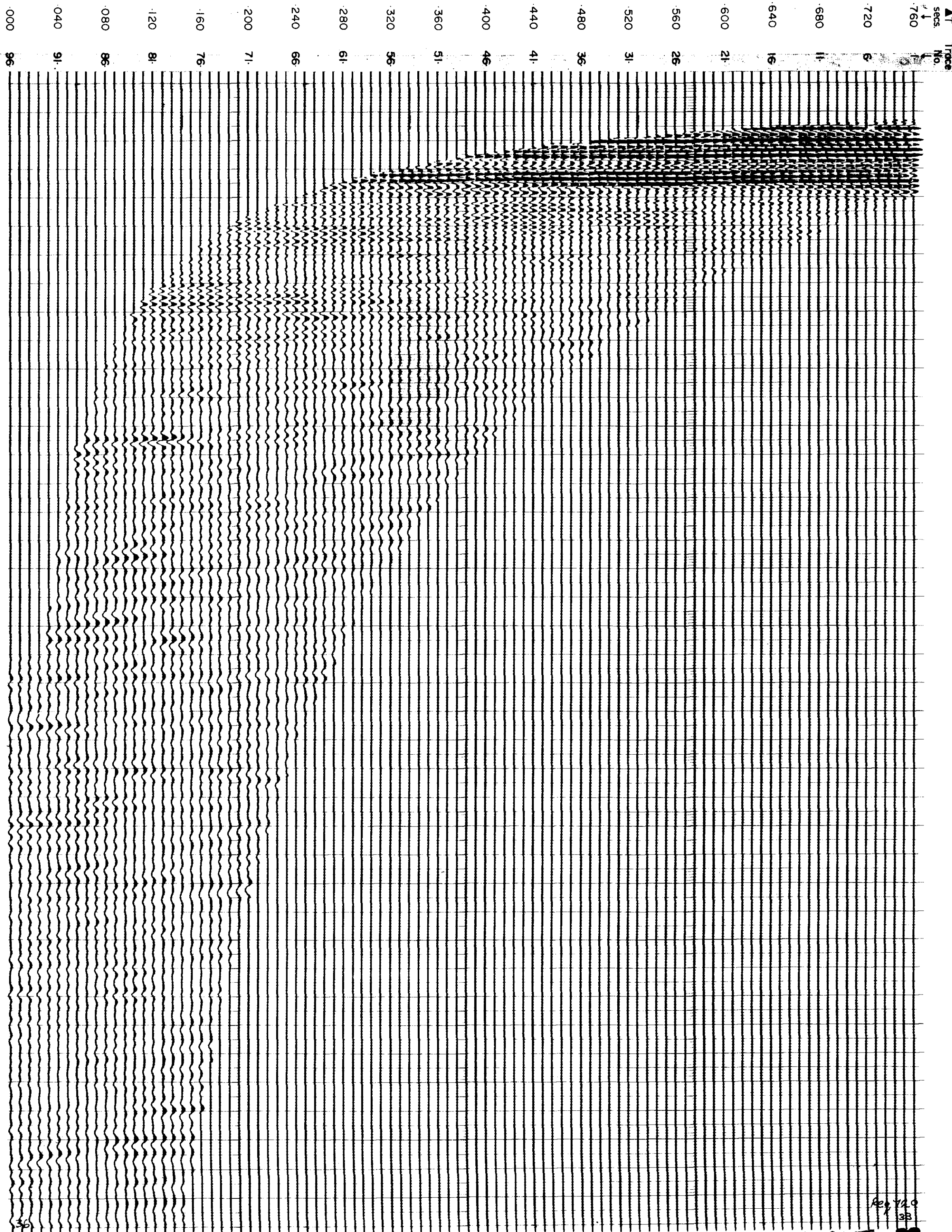
ENV 990 II-20

LINE 069A-2
S.P. 265
X max=5000'

24 Tr. GATHER 4 CDP(6 FOLD)
TVD (2-64) Pr. Op/Tr)
TVF 20-60Hz. 500ms.
15-55 " 600 "
10-50 " 700 "
10-40 " 1000 "
10-30 " 1400 "

5000' Tr.

400' Tr.



MOVEOUT SCAN

24 Tr. GATHER 4 CDP (6FOLD)
TVD (2-64) Pt. Op./Tr)
TVF 20-60Hz. 500ms.
15-55 = 600
10-50 = 700
10-40 = 1000
10-30 = 1400

400' Tr.

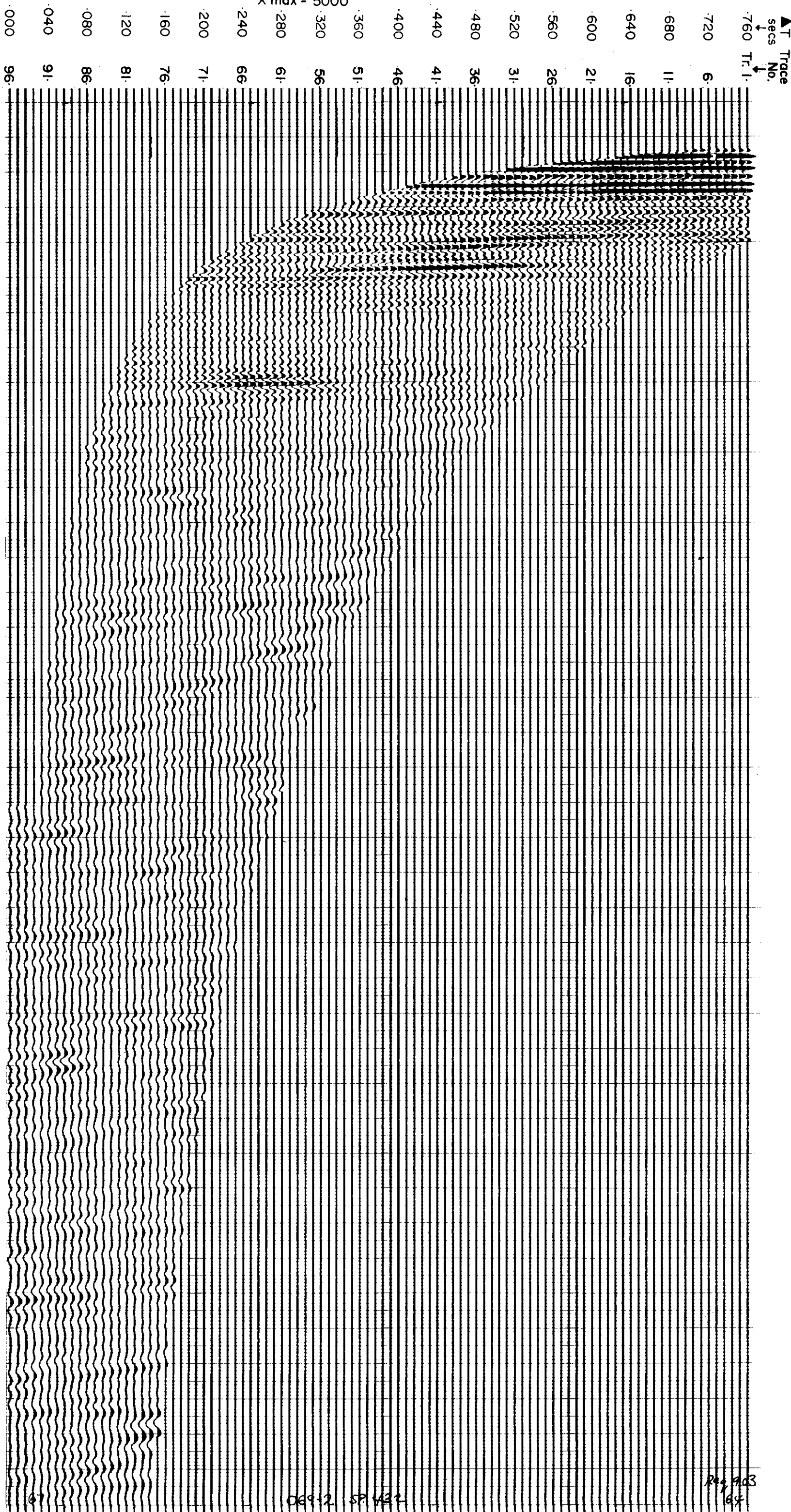
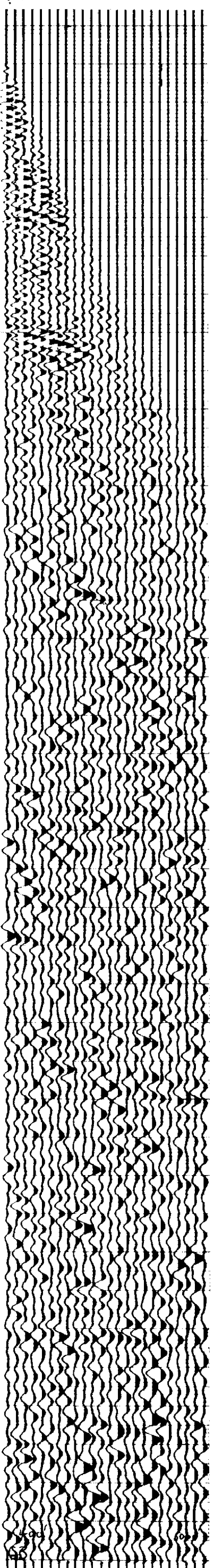
LINE 069A-2

S.P. 432

X max = 5000'

OTWAY BASIN
PROCESSED BY G.S.I. PTY. 851

MOVEOUT SCAN 1



Reg 903
165

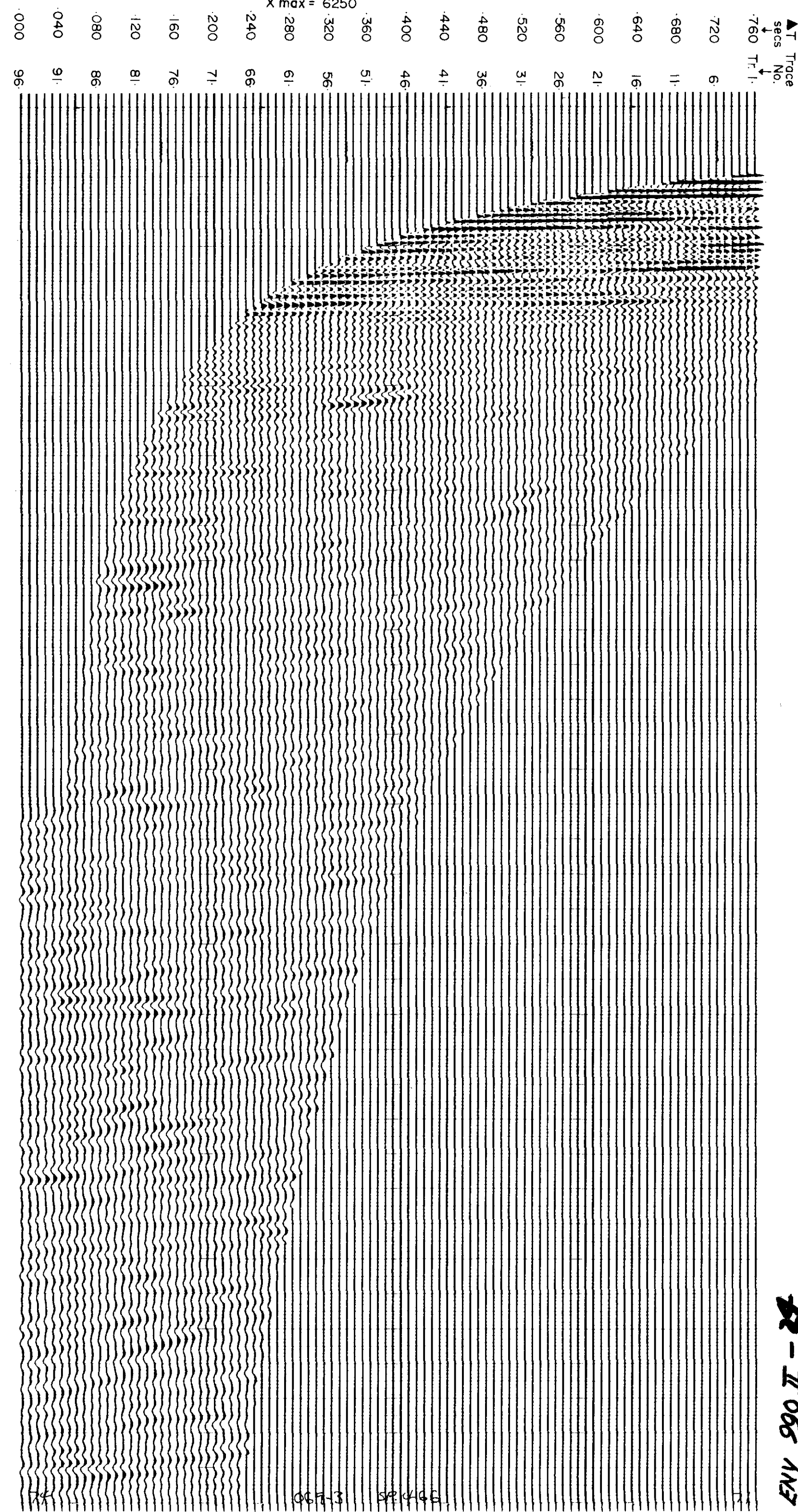
ENV 990 I - 23

24 Tr. GATHER 4 CDP (6 FOLD)
TVD (2-64) Ft. Op/Tr
TVF 20-60Hz. 500ms.
15-55 " 600
10-50 " 700
10-40 " 1000
10-30 " 400

LINE 069A-3
S.P. 466
X max = 6250'

OTWAY BASIN
PROCESSED BY G.S.I. PTY. 851

500' Tr. 24
MOVEOUT SCAN



LINE 069A-3
S.P. 503
X max= 4200'

24 Tr. GATHER 2 CDP(12 FOLD)
TVD (2-64) Pt Op/Tr
TVF 20-60Hz 500ms.
15-55 " 600 "
10-50 " 700 "
10-40 " 1000 "
10-30 " 1400 "

4200' Tr.

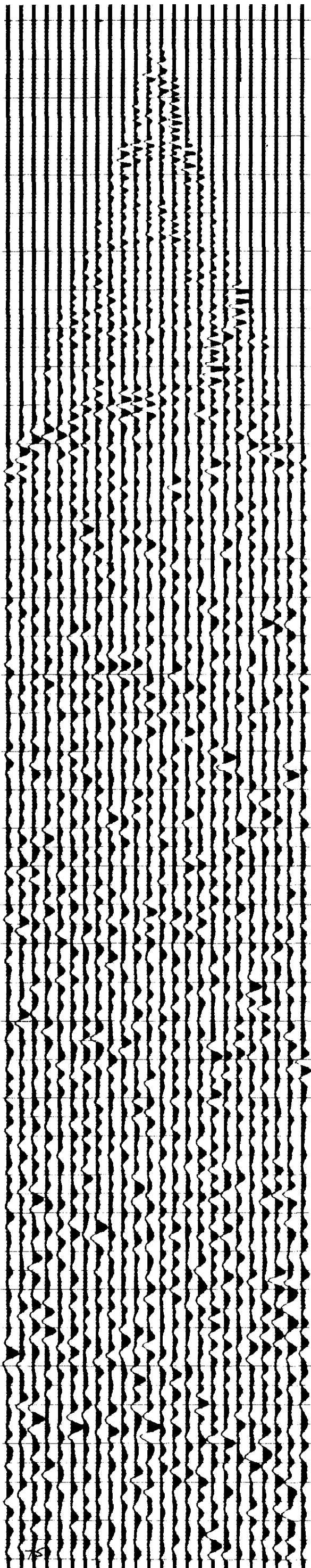
4200' Tr.

▲ Trace
secs. No. ↓
760 1
720 6
680 11
640 16
600 21
560 26
520 31
480 36
440 41
400 46
360 51
320 56
280 61
240 66
200 71
160 76
120 81
80 86
40 91
000 96

MOVEOUT SCAN

1-

0.0
0.2
0.4
0.6
0.8
1.0
1.2
1.4
1.6
1.8
2.0
2.2
2.4
2.6
2.8
3.0
3.2
3.4
3.6
3.8
4.0



Reg 903
76

ENV 990II - 25

LINE 069A-5
S.P. 326
X max=5000'

24 Tr. GATHER 4 CDP(6 FOLD)
TVD (2-64) Pt. Op/Tr)
TVF 20-60Hz. 500ms.
15-55 " 600 "
10-50 " 700 "
10-40 " 1000 "
10-30 " 1400 "

400' Tr.

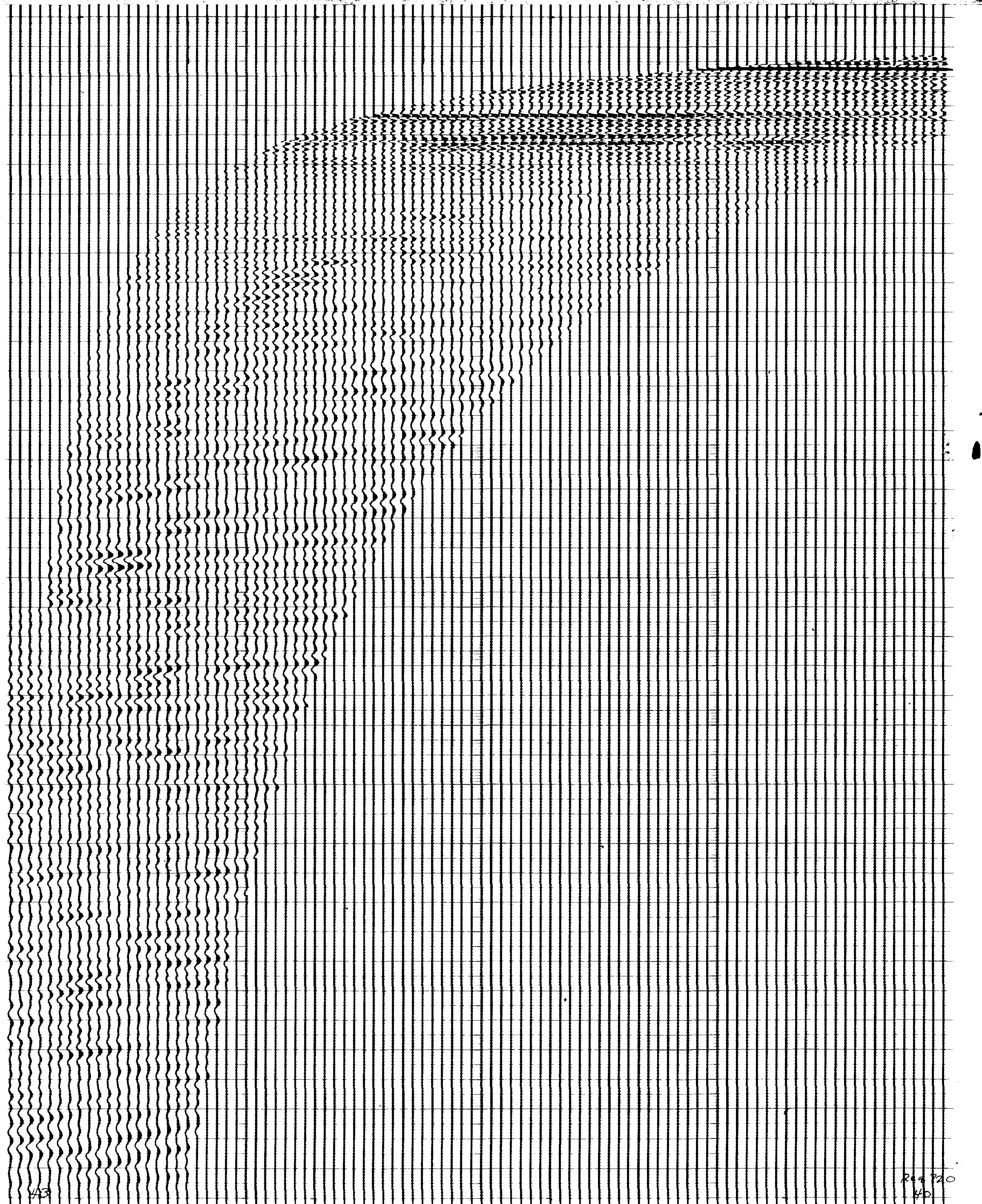
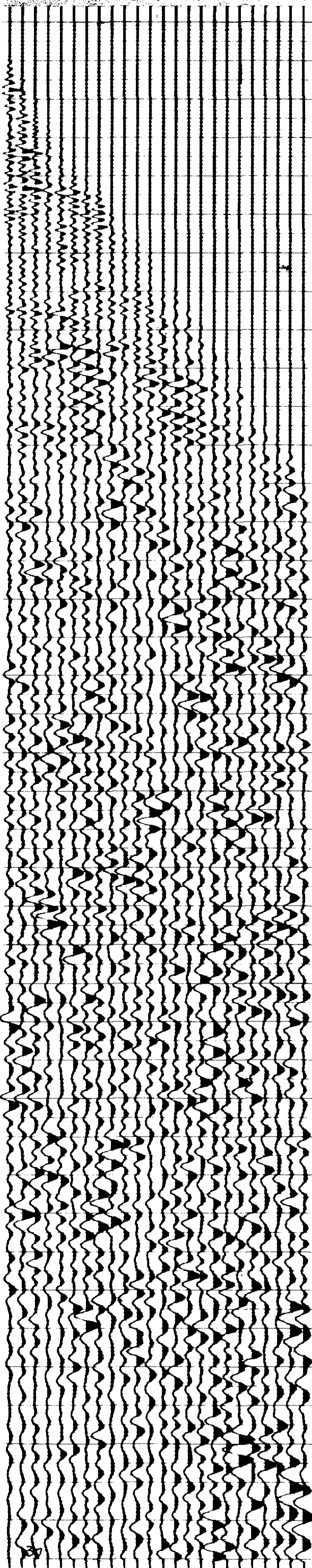
5000' Tr.

0.00 0.40 0.80 1.20 1.60 2.00 2.40 2.80 3.20 3.60 4.00 4.40 4.80 5.20 5.60 6.00 6.40 6.80 7.20 7.60

96 91 86 81 76 71 66 61 56 51 46 41 36 31 26 21 16 11 6

MOVEOUT SCAN

0.0
0.2
0.4
0.6
0.8
1.0
1.2
1.4
1.6
1.8
2.0
2.2
2.4
2.6
2.8
3.0
3.2
3.4
3.6
3.8
4.0



24 920
40

ENV 990 II-26

LINE 069A-7
S.P. 1023
X max= 6250'

24 Tr. GATHER 4 CDP (6 FOLD)
TVD (2-64' Pt. Op/Tr)
TVF 20-60Hz. 500ms.
15-55 " 600 "
10-50 " 700 "
10-40 " 1000 "
10-30 " 1400 "

500' Tr.

24

MOVEOUT SCAN

6250' Tr.

1



12- II 066 1113

Aug 1936
1103 3047
140

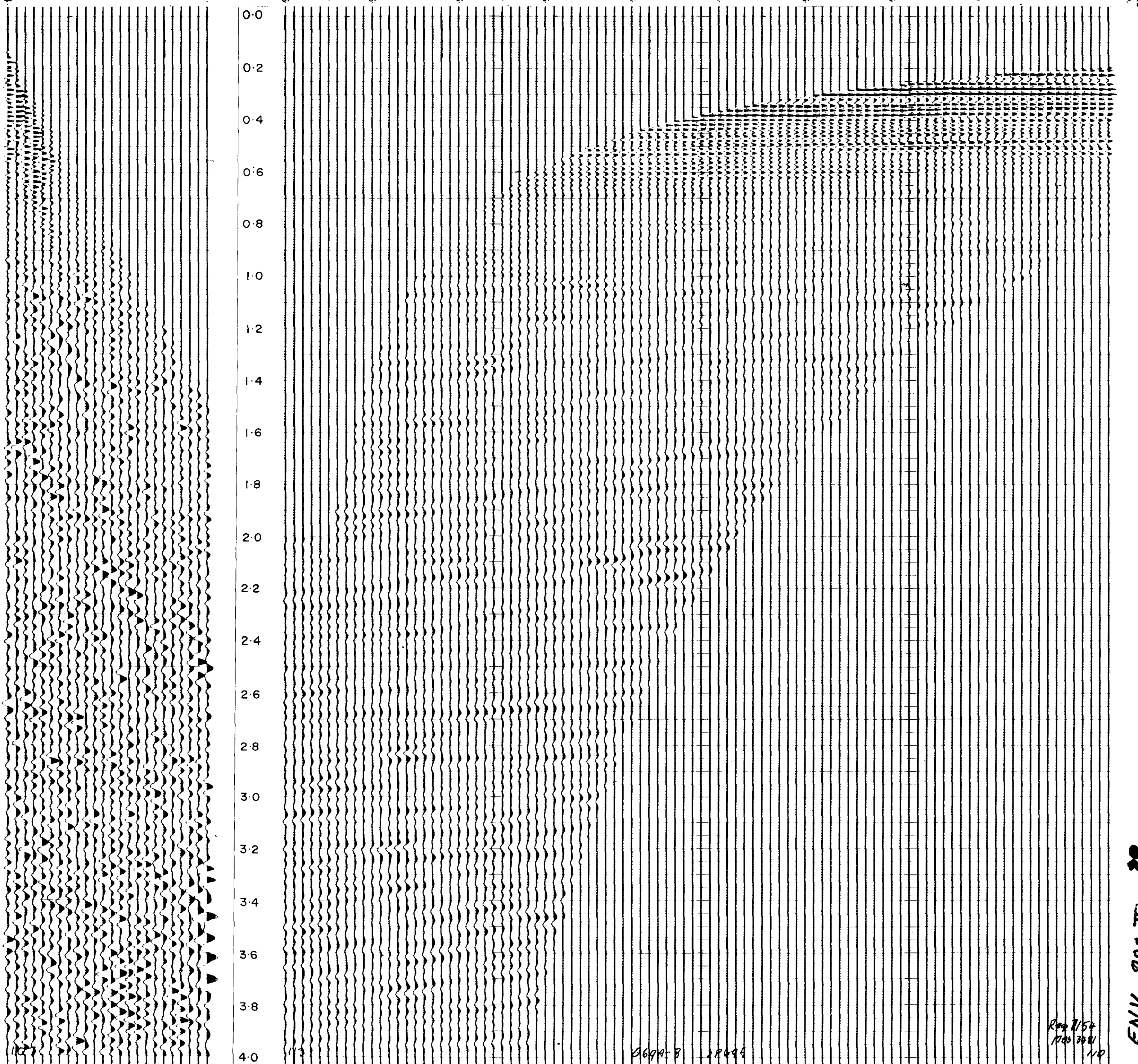
LINE 069A-8
S.P. 695
X max= 6250'

24 Tr. GATHER 4 CDP(6 FOLD)
TVD (2-64 Pt. Op/Tr)
TVF 20-60Hz. 500ms.
15-55 " 600 "
10-50 " 700 "
10-40 " 1000 "
10-30 " 1400 "

6250Tr.

500Tr.

MOVEOUT SCAN



82-11066 NNS

Reg 7/54
Pos 3081

1/0

LINE 069A-8
S.P. 726
X max= 6250'

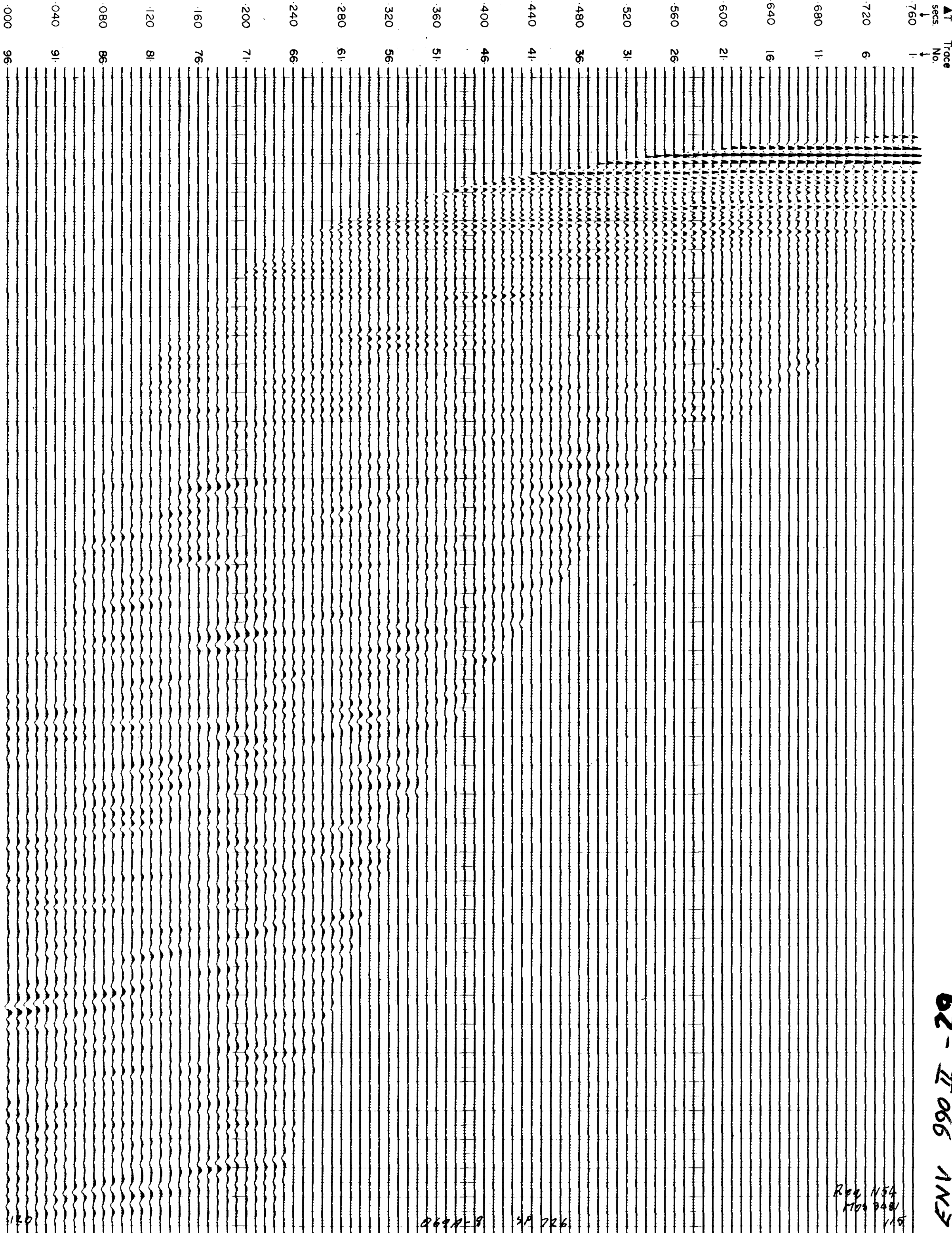
24 Tr. GATHER 4 CDP (6 FOLD)
TVD (2-64 Pt. Op/Tr)
TVF 20-60Hz. 500ms.
15-55 " 600 "
10-50 " 700 "
10-40 " 1000 "
10-30 " 1400 "

500' Tr.

24

MOVEOUT SCAN

6250' Tr.



62 - II 066 1N3

Reg. N54
1700 3481
1/15

069A-8

S.P. 726

LINE 069A-8
S.P 756
X max = 6250'

500' Tr.

24

MOVEOUT SCAN

6250' Tr.

AT Trace
secs. No. ↓

760 1
720 6
680 11
640 16
600 21
560 26
520 31
480 36
440 41
400 46
360 51
320 56
280 61
240 66
200 71
160 76
120 81
80 86
40 91
000 96

069A-8 SP-56

Rag 1/54
1103 1481
122

ENV 990 II - 30

P 69 1454
1103 9481
122

LINE 069A-10
S.P. 806
X max= 6250

24 Tr. GATHER 4 CDP(6 FOLD)
TVD (2-64 Pt Op/Tr)
TVF 20-60Hz. 500ms.
15-55 " 600 "
10-50 " 700 "
10-40 " 1000 "
10-30 " 1400 "

Trace
No.

secs.

760

720

680

640

600

560

520

480

440

400

360

320

280

240

200

160

120

80

40

000

6250 Tr.

1.

SCAN

MOVEOUT

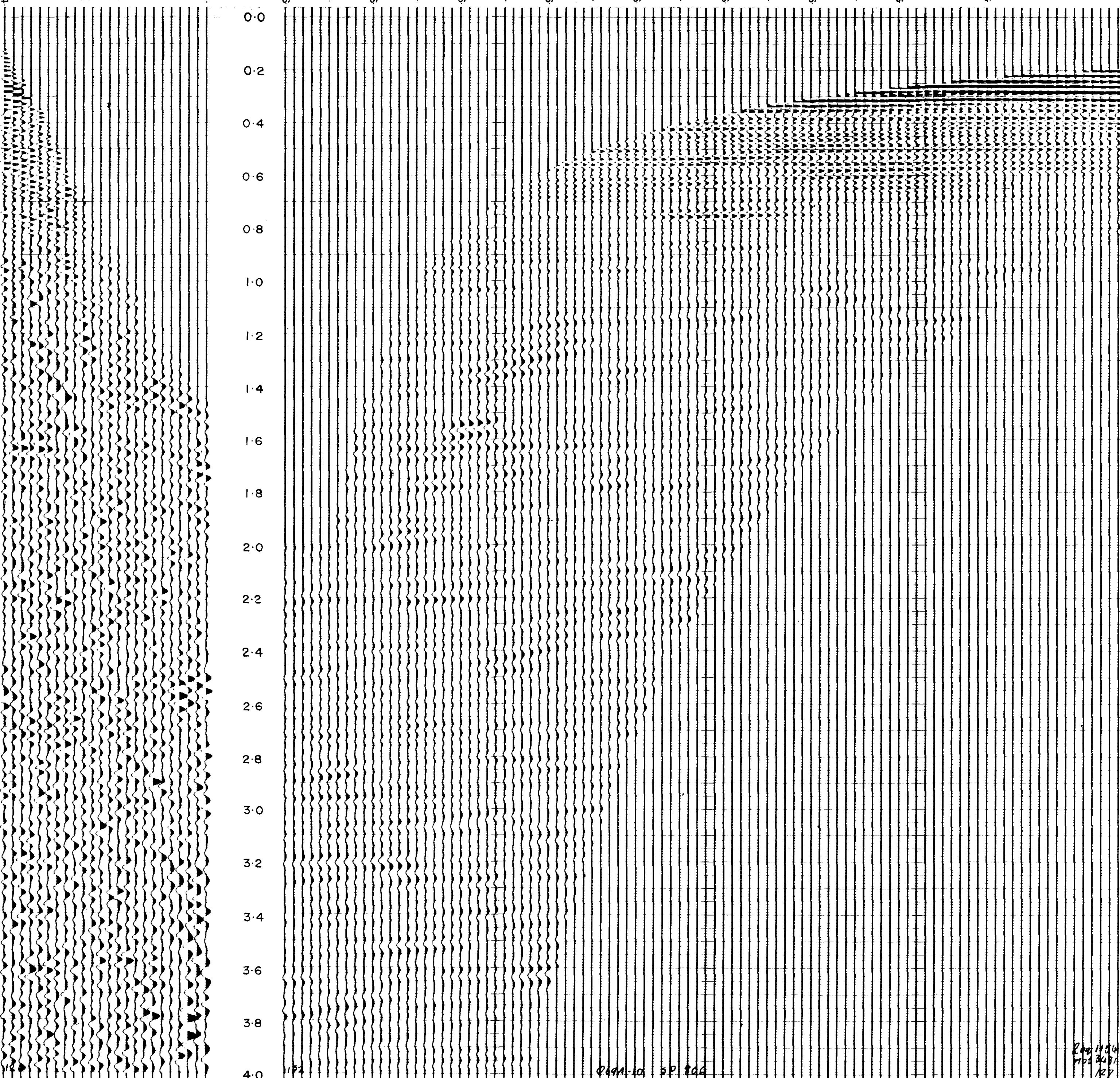
24

18-II 066 NW3

200 1454
1701 3487
127

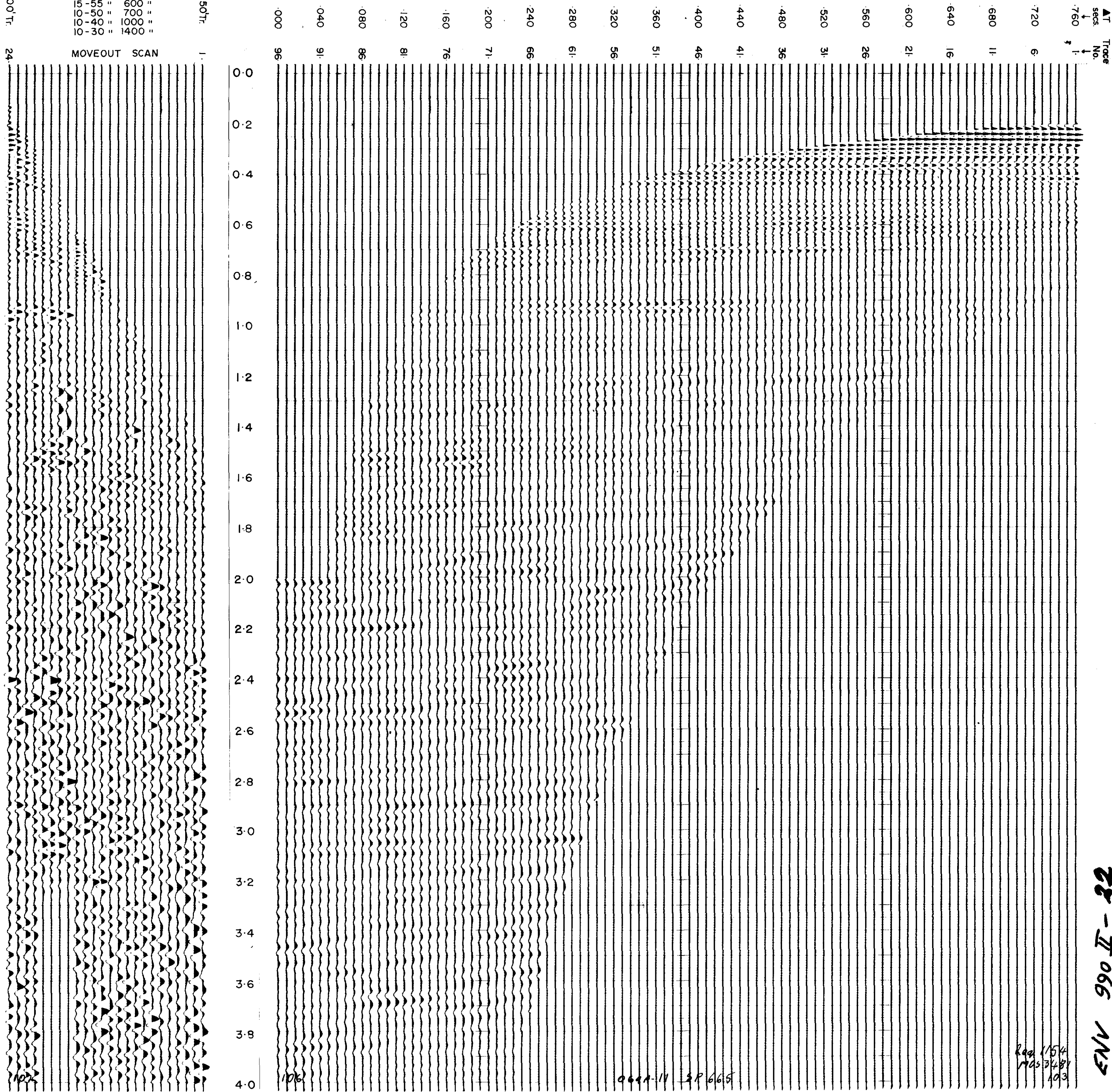
069A-10 SP 806

171



7.

500' Tr.	24 Tr.	GATHER	4 CDP (6 FOLD)	
	TVD	(2-64 Pt.	Op/Tr)	
	TVF	20-60Hz.	500ms.	
		15-55 "	600 "	6250 Tr.
		10-50 "	700 "	
		10-40 "	1000 "	
		10-30 "	1400 "	



LINE 069A-15
S.P 1041
X max= 6250'

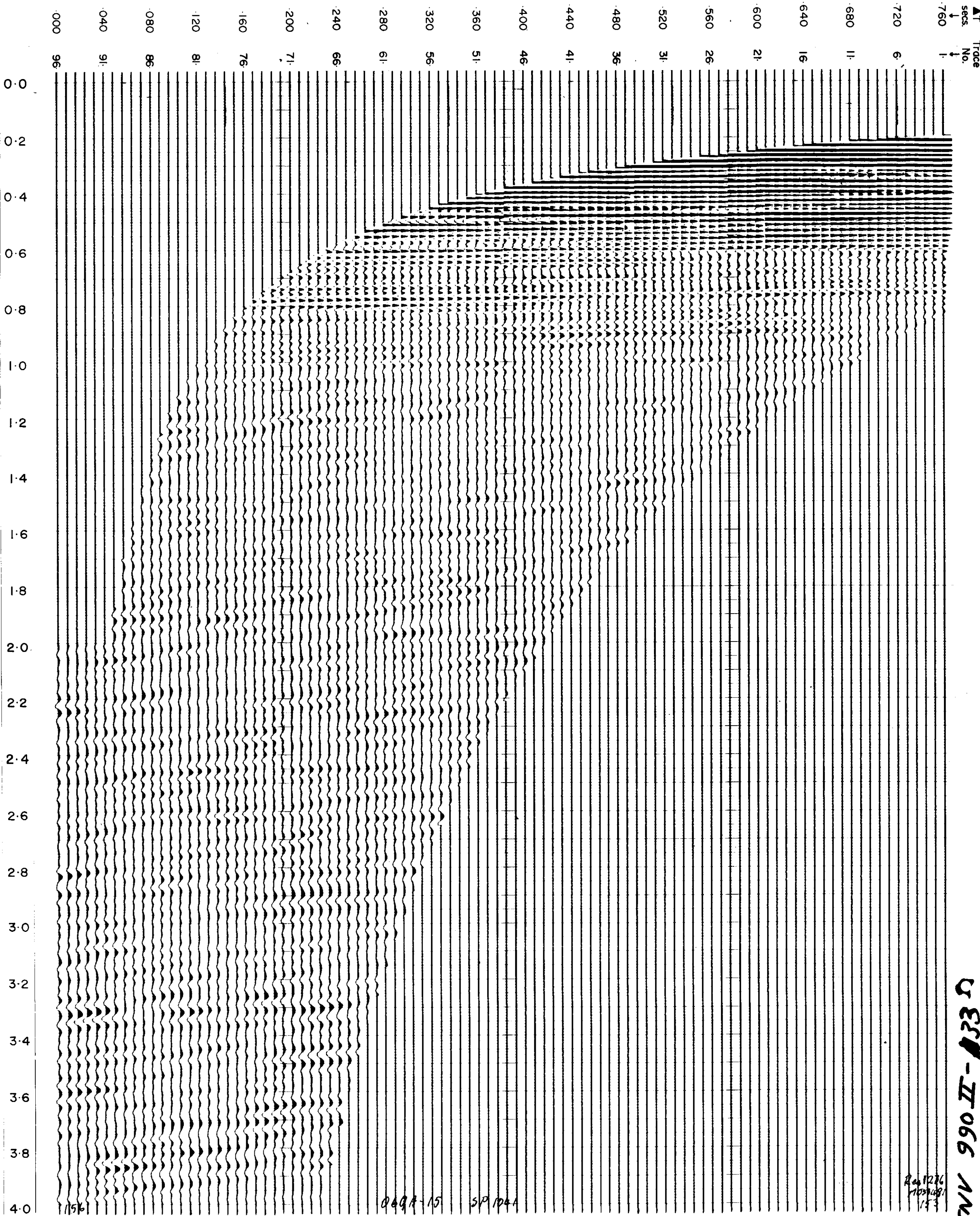
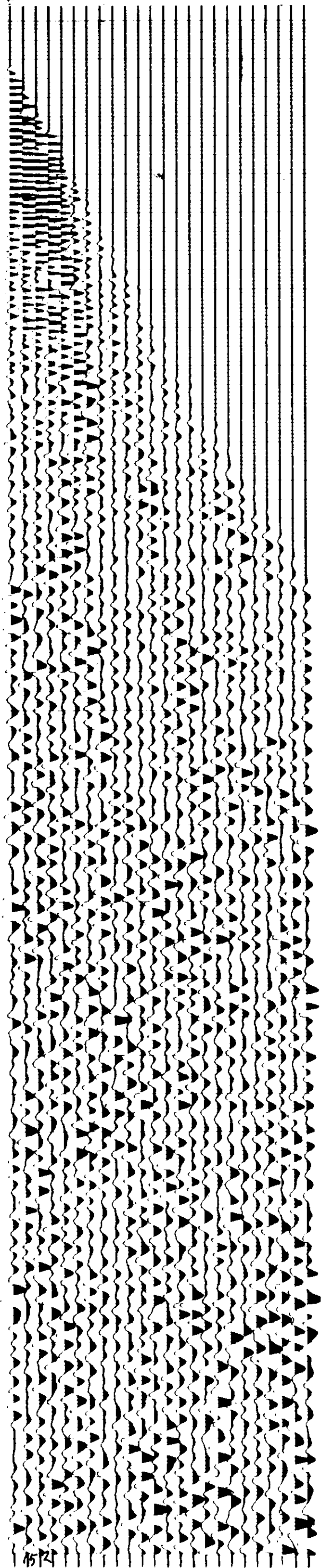
24 Tr. GATHER 4 CDP(6 FOLD)
TVD (2-64 Pt Op/Tr)
TVF 20-60Hz. 500ms.
15-55 " 600 "
10-50 " 700 "
10-40 " 1000 "
10-30 " 1400 "

6250' Tr.

500' Tr.

24

MOVEOUT SCAN



U 830-11066 AN3

Rev 12/86
10/24/87
153

24 Tr. GATHER 4 CDP (6 FOLD)
TVD (2-64 Pt Op/Tr)
TVF 20-60Hz 500ms.
15-55 " 600 "
10-50 " 700 "
10-40 " 1000 "
10-30 " 1400 "

LINE 069A-16
S.P. III 6
X max= 6250'

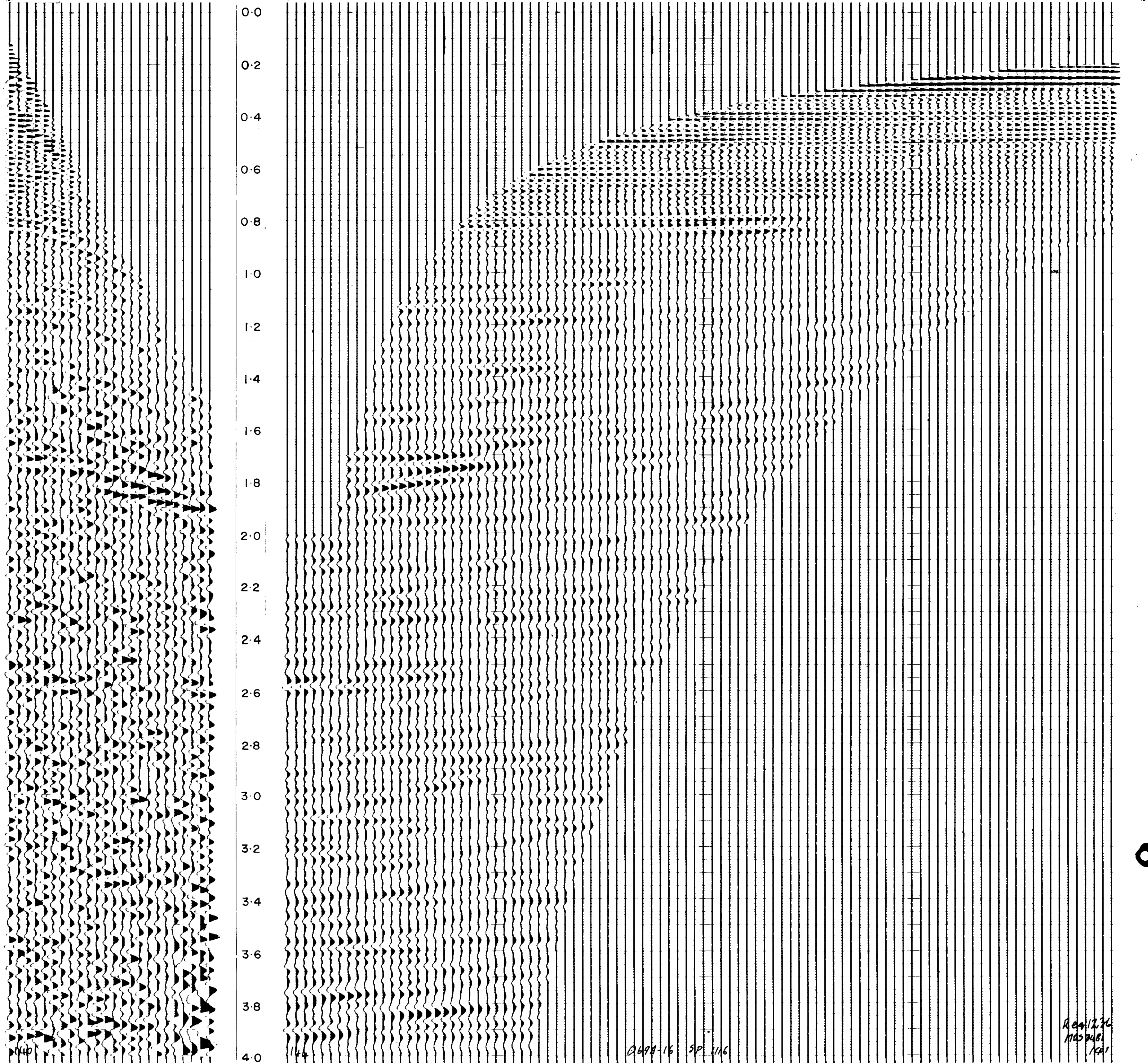
OTWAY BASIN
PROCESSED BY G.S.I. PTY. 851

500' Tr.

6250' Tr.

24

MOVEOUT SCAN



Req 12.26
105348
KAI

ENV 990 II-34

24

24

24



24

LINE 069A-19
S.P. 1643
X max= 6250

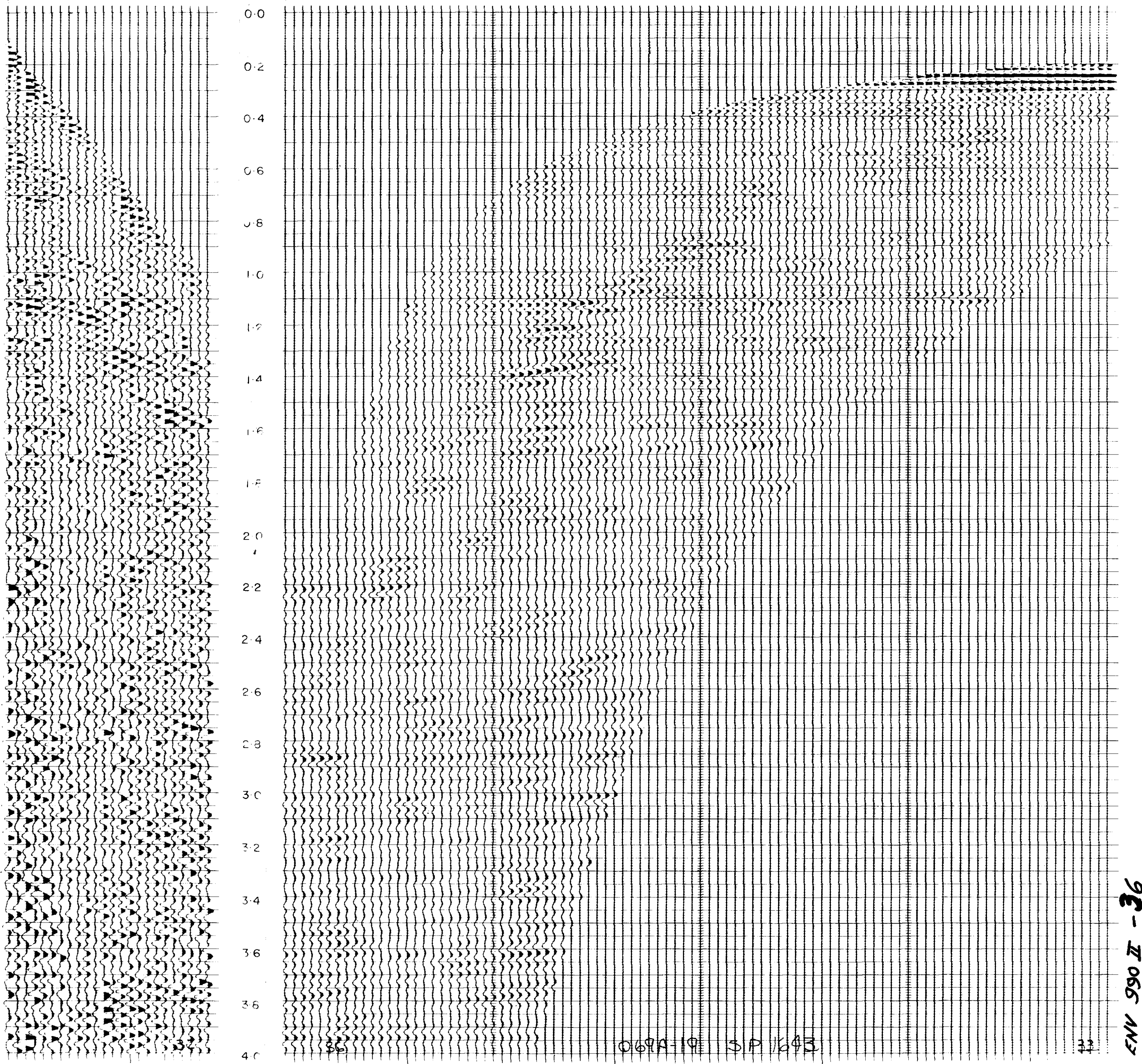
24 Tr. GATHER 4 CDP (6 FOLD)
TVD (2 64 Pt Op/Tr)
TVF 20 60Hz 500ms
15 55 " 600 "
10 50 " 700 "
10 40 " 1000 "
10 30 " 1400 "

500 Tr

24

MOVEMENT PLAN

6250 Tr



069A-19 S.P. 1643

96-11066 AN3

24 Tr. GATHER 4 CDP(6 FOLD)
TVD (2-64 Pt. Op/Tr)
TVF 20-60Hz 500ms.
15-55 " 600 "
10-50 " 700 "
10-40 " 1000 "
10-30 " 1400 "

500 Tr.

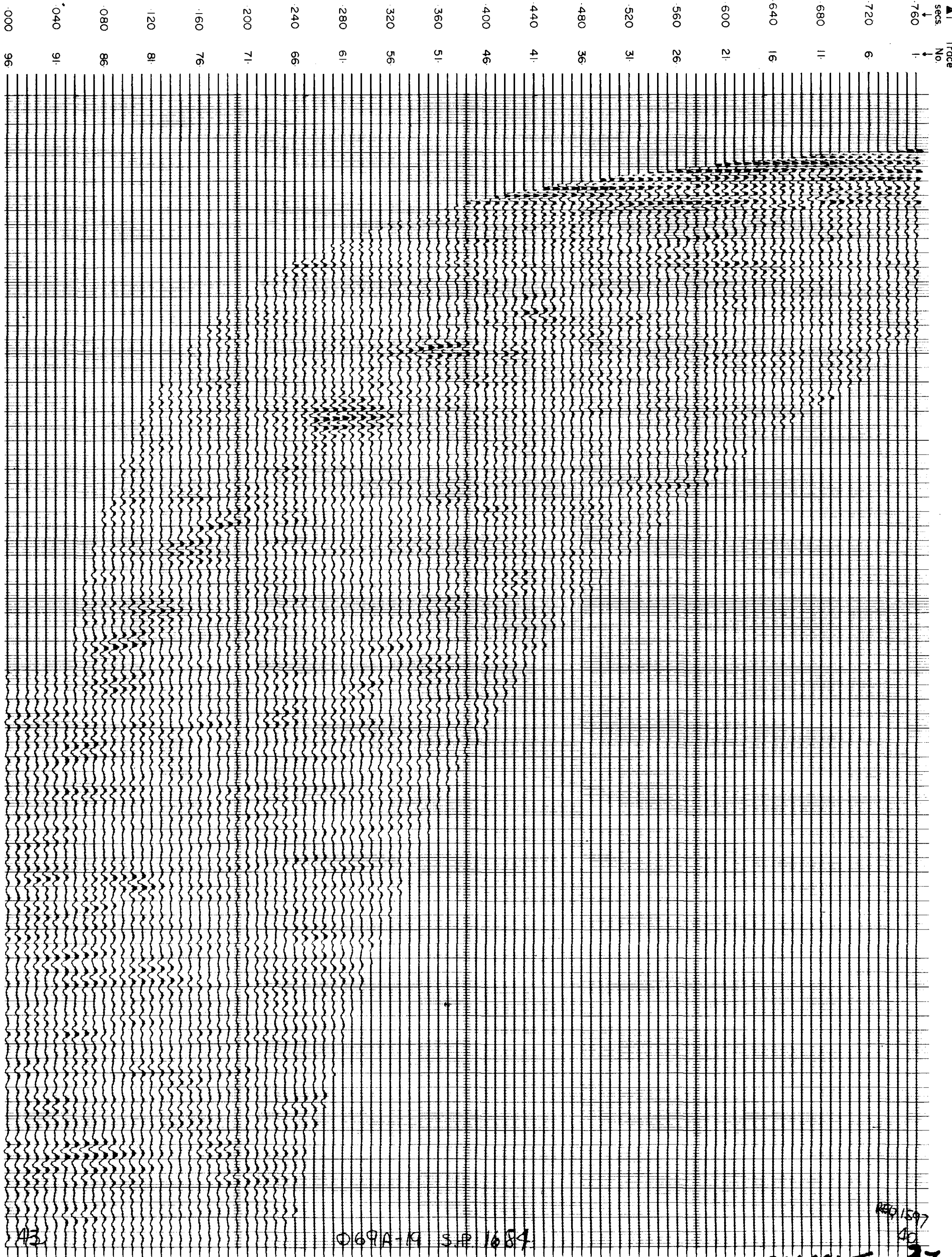
24

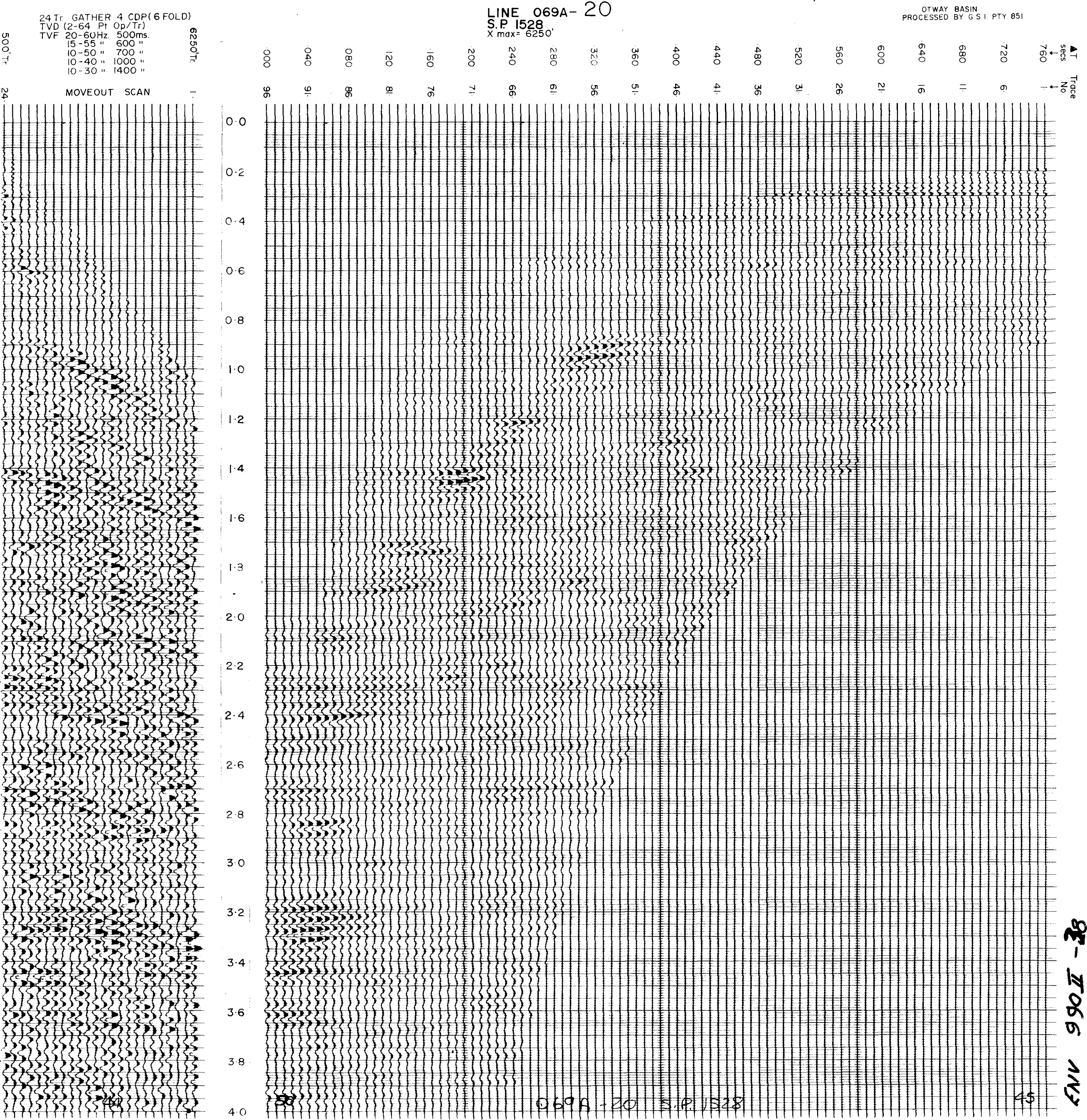
MOVEOUT SCAN

6250 Tr.

LINE 069A-19
S.P. 1684
X max= 6250

OTWAY BASIN
PROCESSED BY G.S.I. PTY. 851





24 Tr. GATHER 4 CDP (6 FOLD)
TVD (2-64 Pt Op/Tr)
TVF 20-60Hz 500ms.
15-55 " 600 "
10-50 " 700 "
10-40 " 1000 "
10-30 " 1400 "

6250 Tr.

MOVEOUT SCAN

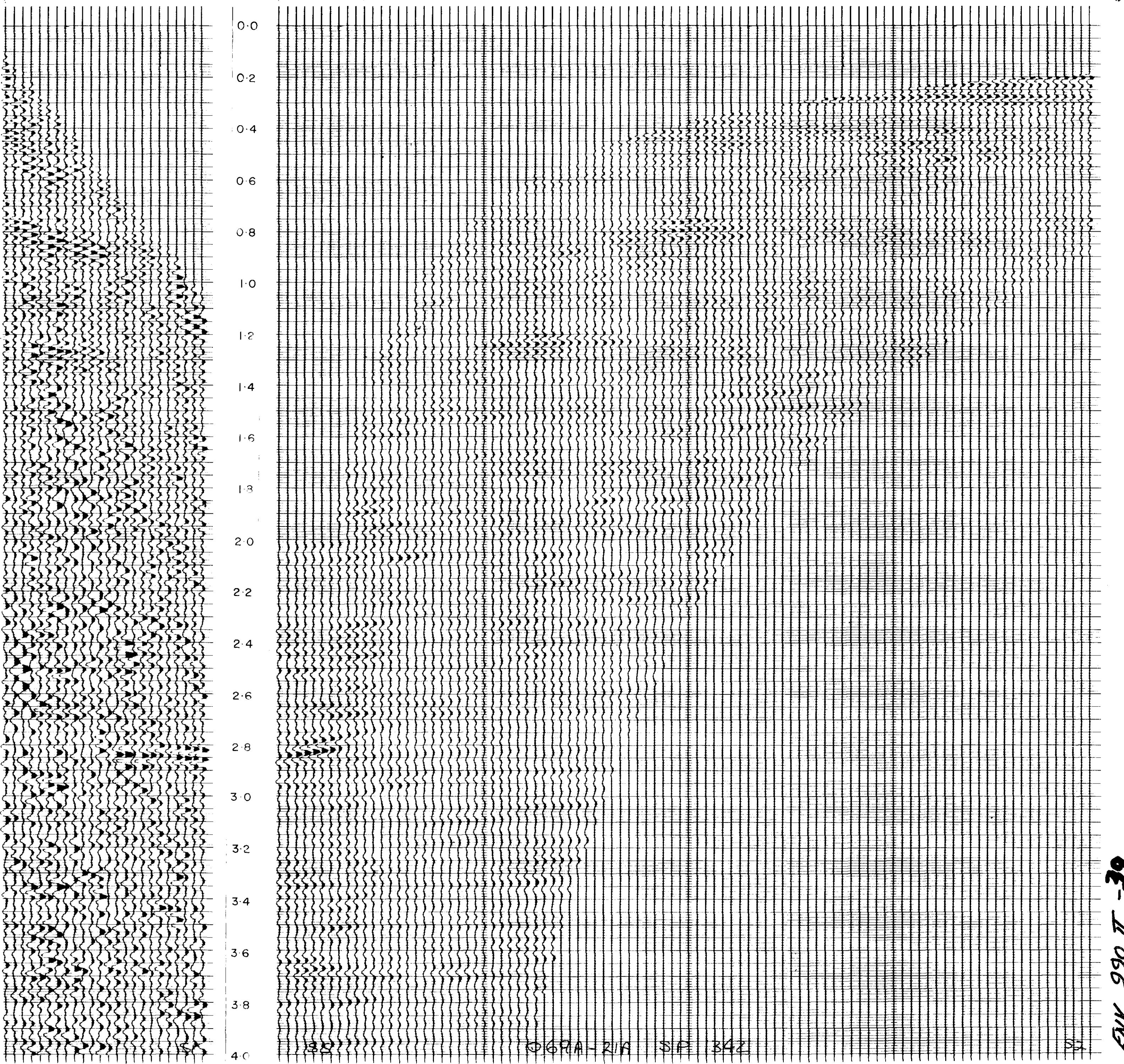
LINE 069A-21A
S.P 1342
X max= 6250'

OTWAY BASIN
PROCESSED BY G.S.I. PTY. 851

500 Tr.
24

Trace
No.
760
↓

000 040 080 120 160 200 240 280 320 360 400 440 480 520 560 600 640 680 720 760
96 91 86 81 76 71 66 61 56 51 46 41 36 31 26 21 16 11 6



66-11066 ANZ

LINE 069A -23

S.P. 1709

X max = 3375'

OTWAY BASIN, S.A. 33T
PROCESSED BY PETRO-85

Tr 1
TVD (1 - 111 p/Tr)
TVE 20 - 10 Hz 500 ms
15 - 55 Hz 600 ms
10 - 50 Hz 700 ms
10 - 40 Hz 1000 ms
10 - 30 Hz 1400 ms

50 - 24

MOVEOUT SCAN

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

Tr 1

0.0

0.2

0.4

0.6

0.8

1.0

1.2

1.4

1.6

1.8

2.0

2.2

2.4

2.6

2.8

3.0

3.2

3.4

3.6

3.8

4.0

069A-2B S.P. 1709

57

07-17066 ANJ

24 Tr. Gather 8 CDP (3 Fold),
TVD (2-64 Pt. Op./Tr.)
TVF 20 - 60 Hz 500 ms.
15 - 55 Hz 600 ms.
10 - 50 Hz 700 ms.
10 - 40 Hz 1000 ms.
0 - 30 Hz 1400 ms.

LINE 069A - 24

S.P. 1692

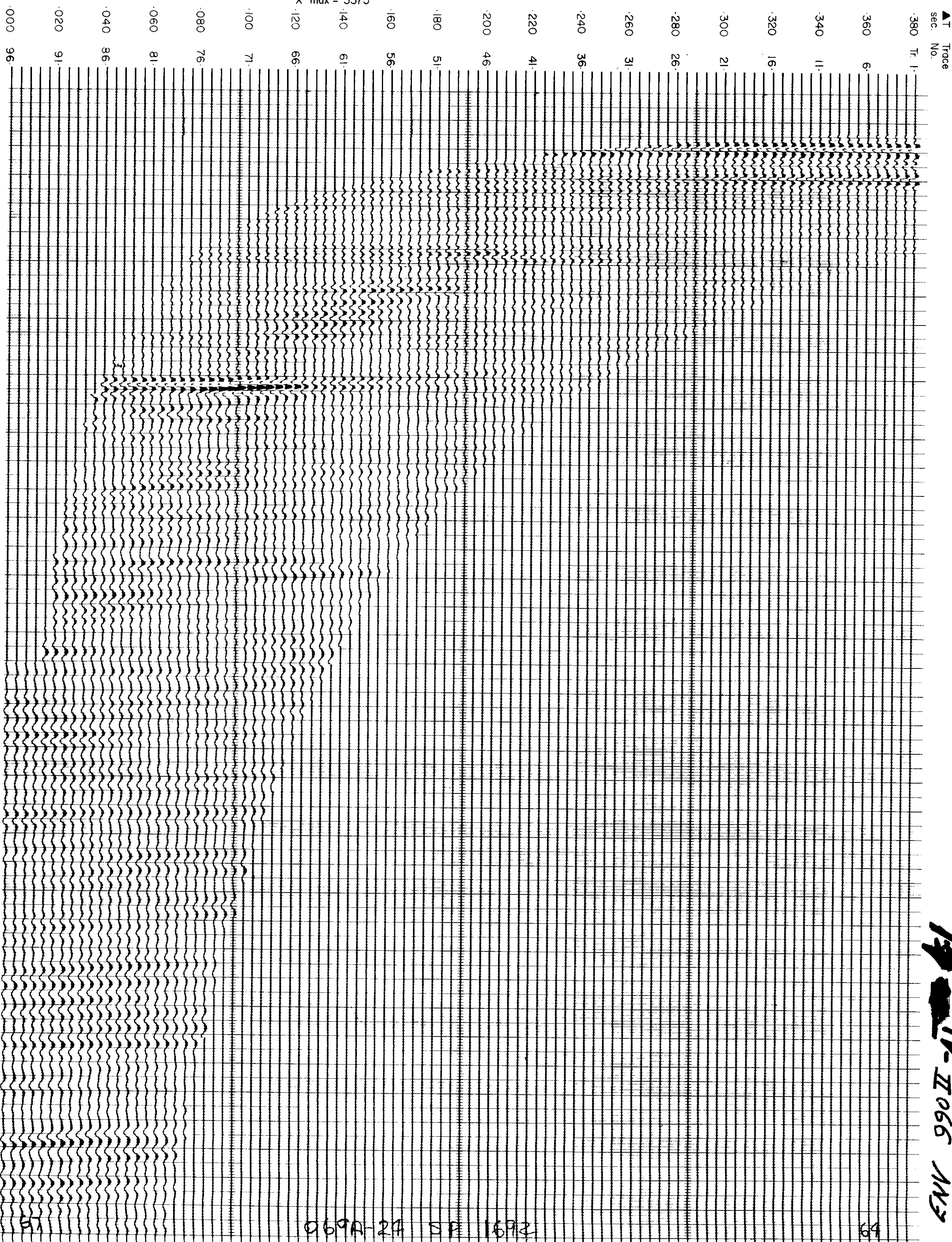
X max = 3375'

OTWAY BASIN, S. AUST.
PROCESSED BY GSI Pty 851

500' Tr. 24

MOVEOUT SCAN

3375' Tr. 1



Trace No.

14-11-066 ANJ

24 Tr. Gather 8 CDP (3 Fold),
TVD (2-64 Pt. Op./Tr.)

TVD 20 - 60 Hz 500 ms.
50 - 55 Hz 600 ms.
50 - 55 Hz 700 ms.
50 - 55 Hz 1000 ms.
50 - 55 Hz 1400 ms.

500' Tr. 24

LINE 069A - 24

S.P.2034

X max = 3375'

OTWAY BASIN, S. AUST.
PROCESSED BY GSI Pty 851

Trace
No.

3375' Tr. 1

MOVEOUT SCAN

0.0
0.2
0.4
0.6
0.8
1.0
1.2
1.4
1.6
1.8
2.0
2.2
2.4
2.6
2.8
3.0
3.2
3.4
3.6
3.8
4.0

0.00 96

0.020 91

0.040 86

0.060 81

0.080 76

0.100 71

0.120 66

0.140 61

0.160 56

0.180 51

0.200 46

0.220 41

0.240 36

0.260 31

0.280 26

0.300 21

0.320 16

0.340 11

0.360 6

0.380 Tr. 1

069A-24 SP 2034

ENV 990II-42