CONTENTS ENVELOPE 6679

TENEMENT:

TENEMENT HOLDER: Mt. Gunson Mines Pty. Ltd.

REPORTS: Report On A combined Induced Polarization Seismic And	Pgs. 3-42
Electromagnetic Survey In The Mt. Gunson Area.	
PLANS: Cattle Grid Prospect - Induced Polarization And Resistivity Survey.	6679–1
Cattle Grid Area - Induced Polarization And Resistivity	
Survey - Line 18600N	6679–2
Line 18600N	6679-3
Line 18600N	6679-4
Line 3770E	6679-5
Line 0	6679–6
Line 0	6679–7
Line 115W	6679–8
Line 30S	6679–9
Electromagnetic Survey:-	
Mt. Gunson - Cattlegrid Area	
Rx Line No. 18600N	6679–10
Rx Line No. 00 (DHMG 14D)	6679–11
Airstrip Area	
Rx Line No. 30S.	6679–12
Seismic Survey - Mt. Gunson Area	
3570E/18600N	6679–13
3570E/18680N	6679–14
3570E/18800N (1) 6679–15
(2) 6679–16
3570E/18900N (1) 6679–17
3570E/18900N (2) 6679–18
3570E/19000N	6679–19
300/400D.H. (1	
(2	
50'N OF CG 78 (1	
(2	
60'N Of D.H. 100/400 (1	
(2) 101N OF 02 74	
40'N Of CG 74	6679–26

PLANS:	North Pernatty Grid - Gravity And Magnetic Survey (1981)	Pgs. 43-76
	6530000N To 6540000N.	
REPORTS	: Magnetic Survey - Gunyot Dyke System.	Pgs. 77-95
PLANS:	Magnetic Surveys.	6679–27
	E.L. 81 - Mt. Gunson Area - I.P. & E.M. Survey Location Plan	
	- Main Open Cut Sheet.	6679–28

REPORT ON A COMBINED INDUCED POLARISATION SEISMIC AND ELECTROMAGNETIC SURVEY IN THE MOUNT GUNSON AREA, SOUTH AUSTRALIA FOR PACMINEX PTY. LTD.

McPHAR GEOPHYSICS PTY. LTD.

REPORT ON A

COMBINED INDUCED POLARISATION, SEISMIC AND ELECTROMAGNETIC SURVEY

IN THE

MOUNT GUNSON AREA, SOUTH AUSTRALIA

FOR

PACMINEX PTY. LTD.

, <u>SUMMARY</u>

An orientation geophysical survey has been completed in the Mt. Gunson area for Pacminex Pty. Ltd.

The purpose of the survey was firstly to test the applicability of Induced Polarisation and Electromagnetic techniques in the detection of the known copper ore body; and secondly to test the applicability of the shallow seismic refraction method to determine the depth to the top of the Pandurra formation which is the host rock for the ore zone.

The Induced Polarisation method was successful in detecting the known ore body and several areas of interest for future exploration were also detected.

The electromagnetic method was found to be principally

affected by surface conductive zones, and could not be recommended as a viable reconnaissance tool.

- 2 -

The shallow seismic refraction method is shown to be useful in determining the depth to the Pandurra formation although it seems likely that the interface detected is actually the base of the weathered layer within this unit.

The Bison Signal Enhancement seismograph employed in the survey would require a more energetic source than the standard hammer if it is to be used to obtain penetration below 40 metres. The viability of using a more powerful 12 channel system should be investigated.

TABLE OF CONTENTS

- 1. Introduction.
- 2. Results of Induced Polarisation and Resistivity Survey.
- 3. Results of Electromagnetic Survey.
- 4. Results of Seismic Refraction Survey.
- 5. Conclusions and Recommendations.

LIST OF ILLUSTRATIONS

Dwg. No. 4295A

Plan of the Cattle Grid Prospect

1. <u>I.P. Pseudo Sections</u> :		
(a)	Cattle Grid Area:	
Dwg. No.	Line No.	Electrode Interval
IP 5031A-1	18600N	30 metres
IP 5031A-2	18600N	60 metres
IP 5031A-3	18600N	60 metres
IP 5031A-4	3770N	60 metres

- 4 -

(b) DH MG14D Area:

Dwg. No.	Line No.	Electrode Interval
IP 5031A-5	00	30 metres
IP 5031A-6	00	60 metres
IP 5031A-7	115W	30 metres
(c)	Airstrip Area:	
IP 5031A-8	305	60 metres

2.Electromagnetic Profiles:Dwg. No.Line No.EM 5033A-118600N (Cattle Grid Area)EM 5033A-2North-south baseline (DH MG14D)EM 5033A-330S (Airstrip Area)

3. Seismic Refraction Profiles:

Dwg. No.	Setup Point	Hammer Spread To
S 5032A-1	3570E / 18600N	North
S 5032A-2	3570E/ 18670N	North
S 5032A-3	3570E / 18800N	North
S 5032A-4	3570E / 18800N	North
S 5032A-5	3570E / 18900N	South

Dwg. No.	Setup Point	Hammer Spread To
S 5032A-6	3570E / 18900N	North
S 5032A-7	3570E / 19000N	North
S 5032A-8	DH 300 / 400	South
S 5032A-9	DH 300 / 400	South
S 5032A-10	50' N of DH CG78	North
S 5032A-11	50' N of DH CG78	South
S 5032A-12	60' N of DH 100/400	North
S 5032A-13	60' N of DH 100/400	South
S 5032A-14	40' S of DH CG74	South

- 5 -

1. INTRODUCTION

At the request of Mr. W. Langron, Chief Geophysicist for Pacminex Pty. Ltd., we have conducted an orientation geophysical survey in the Mt. Gunson area, about 90 miles north from Port Augusta, South Australia.

The main area of interest was the Cattle Grid prospect where a known deposit of copper sulphides has been proven by percussion drilling. The ore body occurs within a fossil weathered surface layer of the Pandurra Quartzite, and is overlain generally by the Whyalla Sandstone.

The sulphide body varies in thickness from zero to a few metres and its depth varies from 25 metres to 40 metres. From overburden - ore ratios observed within the main ore body it seems unlikely that ore of the same type detected at depths greater than 40 metres would be economically viable.

It was therefore envisaged that the seismic method could be used to delineate areas where the depth to the Pandurra formation was much greater than 40 metres, and eliminate such areas from further immediate exploration.

A Bison 1750B signal enhancement seismograph was employed for the survey using a 14 lb sledgehammer as an energy source. Initially a 6 inch square steel plate was used as a hammer strike, however because of the very soft surface, a larger 15 inch diameter plate was found

- 6 -

necessary to provide adequate energy transfer.

7 -

The Induced Polarisation and Resistivity survey was conducted using McPhar variable frequency IP equipment operating at frequencies of 2.5 and 0.3 Hz, and using the dipole-dipole array with electrode separations of 30 and 60 metres.

The electromagnetic survey employed McPhar VHEM equipment operating at frequencies of 600 and 2400 Hz. Tests were conducted using both the horizontal loop (in phase-out of phase) system and the vertical loop (broadside) system.

Previous geophysical test surveys have been conducted on this prospect and include Induced Polarisation reconnaissance lines by Geoscience Inc. in 1964, by Austral Exploration in 1971 and by C.G.G. in 1973. C.G.G. also conducted mise-a-la-masse tests in 1973.

In 1972 Austral Exploration carried out refraction seismic tests over the ore body and environs.

A grid pattern was flown over the area in 1973 with the Geoterrex INPUT system.

Pacminex Pty. Ltd. have surveyed all pegged traverses with both ground magnetometer and self potential methods.

None of the results of these previous surveys have been made available for comparison with results of the current survey.

2. RESULTS OF INDUCED POLARISATION & RESISTIVITY SURVEY

The IP results are plotted in the manner described in the notes appended to this report and are shown on the enclosed sections.

The definite, probable and possible Induced Polarisation anomalies are indicated by bars, in the manner shown on the legend, on the plan map as well as on the data plots. These bars represent the surface projection of the anomalous zones as interpreted from the location of the transmitter and receiver electrodes when the anomalous values were measured.

Since the Induced Polarisation measurement is essentially an averaging process, as are all potential methods, it is frequently difficult to exactly pinpoint the source of an anomaly. Certainly, no anomaly can be located with more accuracy than the electrode interval length; i.e., when using 60 metre electrode intervals the position of a narrow sulphide body can only be determined to lie between two stations 60 metres apart. In order to definitely locate, and fully evaluate, a narrow, shallow source it is necessary to use shorter electrode intervals. In order to locate sources at some depth, larger electrode intervals must be used, with a corresponding increase in the uncertainties of location. Therefore, while the centre of the indicated anomaly probably corresponds fairly well with the source, the length of the indicated anomaly along the line should not be taken to represent the exact edges of the anomalous material.

- 8 -

- 9 -

(a) Cattle Grid Prospect:

Two traverses were surveyed across the known ore zone on the Cattle Grid Prospect.

Line 18600N:

The grid pegs for this traverse were marked 18500N, but it has been referred to its actual grid position to simplify future relocation.

The traverse was initially surveyed from 2400E to 4110E using electrode intervals of 30 metres. The results are anomalous to some extent from 2760E to 3870E. The definite anomaly marked at 3630E to 3750E shows strong metal factors on the 3rd and 4th separations accompanied by a significant increase above background in frequency effect. This anomaly coincides with the known richest portion of the ore body. Because the anomaly showed maximum response on the larger separations the area was resurveyed using electrode intervals of 60 metres.

The probable anomaly at 3270E to 3300E reflects a shallow source (say about 20 to 30 metres) and seems likely to represent a local increase in sulphide concentration.

The probable anomaly at 3060E to 3120E reflects a slightly deeper source, as does the anomaly at 2880E to 2940E.

Both these anomalies have been covered by a survey using 60 metre electrode intervals. The former anomaly is confirmed as a source

- 10 -

shallower than 60 metres, while the latter source is probably at a similar depth but of greater areal extent.

These areas certainly warrant testing by drilling and vertical drill holes are suggested at 3080E and 2900E.

The single high metal factor at 2805E on the 30 metre data is considered to be due to a spurious resistivity measurement and has not been given significance in the interpretation.

Line 3770E:

This traverse was surveyed using 60 metre electrode intervals, across the centre of the known ore zone.

An anomalous response was detected at 18480N to 18840N with a definite anomaly defined from 18660N to 18780N. The apparent source of the anomaly agrees closely with the observed limits of the ore zone.

A possible anomaly at 19080N to 19200N on this line is due to a shallow source and may warrant further attention. Before testing by drilling this anomaly should be confirmed by surveying with 30 metre electrode intervals.

(b) Area Near DH MG14D:

This grid was designed to test the source of an anomaly detected by the airborne INPUT survey. The grid is approximately northsouth, east-west and the position of drillhole MG14D is 30 metres north

- 11 -

and 115 metres west of the origin of the grid.

In this drillhole some minor intersections of copper sulphides have been reported.

The north-south baseline was initially surveyed using electrode intervals of 60 metres. The probable anomaly detected at 60N to 240N was confirmed using electrode intervals of 30 metres. The frequency effect response within the anomaly is only weak but it is considerably above background.

The source certainly warrants testing by drilling and a suitable site for a vertical drillhole would be at 100N on this line.

To test the possibility that the existing drillhole had already tested the source of the anomaly, Line 115W was surveyed using 30 metre electrode intervals. The defined anomaly (possible from 30N to 120N and probable north of 120N) indicates that the drillhole was sited on the very edge of a possible sulphide zone. In view of the encouraging copper horizon encountered in this hole, the area should receive high priority in any future exploration.

(c) <u>Airstrip Area:</u>

This traverse was designed to test the source of an anomaly detected by the airborne INPUT survey.

Line 30S was surveyed using electrode intervals of 60 metres. The possible anomaly at 180E to 240E reflects a near surface

000015

- 12 -

low resistivity zone which is probably the source of the airborne INPUT anomaly. Weakly anomalous frequency effects at depth are not associated with significantly lower resistivities and although the metal factors in this zone are marginally anomalous, the area is not considered to be of particular significance.

3. RESULTS OF THE ELECTROMAGNETIC SURVEY

Three traverses were surveyed using the VHEM electromagnetic system.

Line 18600N on the Cattle Grid Prospect was surveyed using the horizontal loop in-line system, measuring in-phase and out-of-phase response. Because of the low surface resistivities, signal strength was low, and some powerline interference was apparent.

There is no significant response over the area of the ore body and anomalous effects observed seem likely to be due to variations in the near surface resistivity.

The north-south baseline in the area near drillhole MG14D was surveyed using the VHEM in the vertical loop broadside technique. The transmitter was located on Line 90W.

Again signal strengths were low and the data is noisy. Two poorly defined cross-overs are observed at 60N and 195N and these probably correspond to local conductive zones within the conductive surface layer. This conductive surface layer probably represents the source of the INPUT anomaly.

Line 30S at the airstrip was also surveyed using the broadside method with the transmitter on Line 120S. The data is noisy due to low signal strengths. One strong cross-over located at 180E is apparently due to a shallow moderate conductor. The source seems likely to be due to multiple near surface conductors and is probably related to the near surface low apparent resistivity detected at 180E to 240E on the IP survey, and probably reflects the source of the INPUT anomaly in this area.

4. **RESULTS OF THE REFRACTION SEISMIC SURVEY**

The purpose of the refraction seismic work was to determine the depth to the top of the Pandurra formation. From a survey carried out nearby by Bluff Minerals the following seismic velocities were known:

1.	Unconsolidated overburden	300-1500 metres/sec
2.	Whyalla sandstone	1500-2100 metres/sec
3.	Woocalla dolomite	2600-3700 metres/sec
4.	Pandurra quartzite	3800-5000 metres/sec.

With these velocity contrasts it may be shown that to reliably detect the Pandurra quartzite at depths up to 40 metres, hammer

- 13 -

- 14 -

offsets in excess of 200 metres will be required. With the field techniques finally evolved during the test survey, such offsets are possible using the 141b sledgehammer source. However, the hammer operator tires rapidly and overall production would be expected to be low on a routine basis.

The results of the test survey indicate a predominantly 4 layer situation consisting of a surface layer with a velocity of 300 to 500 metres per second, an intermediate layer with a velocity of 800 to 2200 metres per second, a third layer with a velocity of 2500 to 3500 metres per second and a basement layer with a velocity in excess of 4200 metres per second.

This structure and the observed velocities agrees well with the values reported by Bluff Minerals.

The results of the refraction survey are shown on the accompanying data plots.

Setup 3570E/18600N:

A detailed spread was surveyed at this site with hammer offsets at 2 metre intervals out to 20 metres.

The data shows a clearcut layer of 2.2 metres of 390 metres per second underlain by 800 metres per second. The data points at 18 and 20 metre offsets are considered to have delays due to local ground conditions and have been tentatively discarded in the interpretation.

Although this is an observed four layer case, the first two layers are apparent only because of the small station interval. The 390 metres per second and 800 metres per second layers are therefore considered to represent the overburden. The layer with a velocity of 4460 metres per second is considered to represent the Pandurra formation because no further interface was detected at hammer offsets up to 170 metres.

With the observed depth to the Pandurra of 31.7 metres the depth determined from the seismic survey is too shallow by 15%. No reverse profile was surveyed so the effect of dip of the interface has not been determined. However, the dip of the interfaces in this area is known to be relatively small and only a minor effect on the depth calculation is anticipated.

Setup 3570E/18670N:

The survey at this site detected a similar structure to that observed at 18600N.

The interpreted layers are 2.38 metres of 320 metres per second overlying 4.42 metres of 540 metres per second and 12.18 metres of 1750 metres per second which is underlain by material with a velocity of 4050 metres per second.

The observed depth to the Pandurra quartzite at this site is

- 15 -

- 16 -

33.9 metres, and if the lower layer detected is correlated with the Pandurra then the interpreted depth is much too shallow. Because hammer offsets were only measured to 100 metres, a deeper higher velocity layer could be present. It should also be noted that the area was a particularly noisy one and the data should not be regarded as entirely reliable, at least for the larger hammer offsets.

Setup 3570E/18800N:

This profile is regarded as typical of the expected structure in the area.

The surface layer consists of 5.25 metres of 360 metres per second, underlain by 13 metres of 1490 metres per second, and then 18 metres of 2730 metres per second. The basement has an apparent velocity of 5000 metres per second. Dwg. Nos. S 5032A-3 and 4 show two slightly different interpretations of the same data.

The first gives a depth to the Pandurra of 36 metres and the second a depth of 33.4 metres. With the observed depth at this site of 38 metres, both interpretations give a depth which is too shallow by 5 and 12% respectively.

Setup 3570E/18900N:

This setup was attempted twice and the results are shown in Dwg. Nos. S 5032A-5 and 6. The first profile with the hammer to the south was extremely noisy and the data is regarded as unreliable beyond

- 17 -

the 30 metre hammer offset. The second set of data is more reliable and has been interpreted as a surface layer of 4 metres of 320 metres per second underlain by 10.5 metres of 1430 metres per second.

The underlying layer has a velocity of 3040 metres per second but the base of the layer has not been reliable detected. It seems likely that the last two data points could represent a new interface. If a 5000 metres per second layer is inferred at this point its depth would be about 37 metres which compares with the observed depth of 38 metres. Hammer offsets to at least 180 metres would be required to confirm this interpretation. Comparison of the spreads to the north and south suggests a slight southerly dip at this site.

Setup 3570E/19000N:

The data for this setup was again very noisy and the interpretation shown on Dwg. No. S 5032A-7 implies considerable smoothing. The high velocity of 6250 metres per second for the Pandurra is inferred from only two data points and is very likely subject to error. However, the presence of a higher velocity interface is apparent and the calculated depth of 37.7 metres is consistent with the observed depth of 39.6 metres.

Setup DH 300/400:

This setup was surveyed twice and the two profiles are shown on Dwg. Nos. S 5032A-8 and 9. The interpretation is similar on both

- 18 -

profiles except that the lower high velocity layer was not detected on the first profile. Also a change in the timing method resulted in slightly lower elapsed time records and results in a higher velocity for the first layer.

The distances for the hammer offsets were nominally 10 metres. However, the station interval was paced and when measured afterwards was found to be 27 feet (8.2 m). Thus although the data is plotted for and calculated with 10 metre intervals, both the observed velocities and depths must be multiplied by .82.

The observed depth to the Pandurra at this site is 25.5 metres. This comparies with the depth calculated from the seismic survey, of 28.9 metres. It seems likely that the Pandurra may be more deeply oxidised at this point, resulting in a lower velocity in the unit immediately below the ore zone.

Setup 50 feet North of CG78: (Station Interval 27 feet (8.2 m)).

This site was surveyed with hammer spreads to the north and south and the profiles are shown on Dwg. Nos. S5032A-10 and 11.

Comparison of the two profiles suggests a slight northerly dip at this site. The interpretations differ slightly and the true answer probably lies between the two.

However, since the Pandurra interface was not detected

and becuase this was an orientation survey only, the additional computations to resolve the differences were not performed.

If we assume that the Pandurra interface at 5000 metres per second is present just beyond the end of the spread, then the minimum depth to the interface will be about 30 metres. This compares with an observed depth of 24.8 metres and is a similar situation to that observed at DH 300/400.

Setup 60 feet North of DH 100/400: (Station Interval 27 feet (8.2 m))

This setup was surveyed with hammer spreads to the north and south and the profiles are shown on Dwg. Nos. S 5032A-12 and 13.

On Dwg. No. 12 the interface interpreted at a depth of 21 metres and presumed to be the Pandurra quartzite, is based on only two data points and may not be valid. The observed depth to the Pandurra at this site is 32 metres, so the above conclusion seems realistic. The spread to the south from this setup contained obvious offsets due to local conditions and no interpretation was attempted.

Setup 40 feet South of DH CG74: (Station Interval 27 feet (8.2 m)).

This setup was surveyed with offsets out to 100 metres but the Pandurra interface was not detected.

- 20 -

CONCLUSIONS AND RECOMMENDATIONS

(a) Induced Polarisation Survey:

5.

The IP survey has shown that the known ore zone at the Cattle Grid Prospect is a well defined IP source and that the method is applicable for routine reconnaissance surveying of the surrounding area.

For such reconnaissance work an electrode interval of 60 metres is suitable. This allows rapid coverage of the ground and sufficient sensitivity to detect a relatively small source. Additional followup using electrode intervals of 30 metres should be planned to detail any anomalies detected.

The survey completed on the Cattle Grid Prospect detected the main ore zone and in addition detected several other areas of interest. Two drill holes have been suggested on Line 18600N at 3080E and 2900E to test two of these sources.

On Line 3770E additional work using 30 metre electrode intervals is suggested to detail an anomaly at 19080N to 19200N.

In the area around drillhole MG14D an IP source was detected north and east of the drillhole. It seems likely that the copper mineralisation detected in this hole represents the edge of this zone. An additional drillhole at 100N on the north-south baseline has been recommended to test the source.

- 21 -

No significant IP anomaly was detected in the Airstrip Area.

(b) Electromagnetic Survey:

Electromagnetic surveys were conducted on three lines in the area using both the vertical loop and horizontal loop methods.

Signal strengths were low because of surface low resistivities and the data was very noisy. All anomalies detected are attributed to surface conductors and the method is not considered suitable for reconnaissance in this area.

(c) <u>Seismic Survey</u>:

The seismic survey has shown that the method is ideally suited to detect the known layered structure within the sediments.

With the average depth to the Pandurra quartzite of 40 metres, the hammer seismic system is operating at or beyond its reliable limit using the normal energy source.

Two alternatives are available. Either a more powerful source could be used, for example, a portable pile driver, or a normal 12 channel seismic system could be used.

From the small quantity of work so far performed it is obvious that the surface layer varies considerably in velocity and thickness and these variations can affect individual observations. Therefore a

- 22 -

higher data density should be employed for any future work.

The 12 channel system would certainly be desirable if accurate depth information is required, because more sophisticated interpretation techniques could be applied to the high data density. If the smaller hammer system is used the survey technique should include a hammer station interval of 5 metres or less, with hammer offsets out to 200 metres, coupled with routine reciprocal shooting to take account of the dip of the beds.

McPHAR GEOPHYSICS PTY. LTD.

J.E. HAIGH GEOPHYSICIST.

Dated; 27th September 1973.

McPHAR GEOPHYSICS

NOTES ON THE THEORY, METHOD OF FIELD OPERATION, AND PRESENTATION OF DATA FOR THE INDUCED POLARIZATION METHOD

Induced Polarization as a geophysical measurement refers to the blocking action or polarization of metallic or electronic conductors in a medium of ionic solution conduction.

This electro-chemical phenomenon occurs wherever electrical current is passed through an area which contains metallic minerals such as base metal sulphides. Normally, when current is passed through the ground, as in resistivity measurements, all of the conduction takes place through ions present in the water content of the rock, or soil, i.e. by ionic conduction. This is because almost all minerals have a much higher specific resistivity than ground water. The group of minerals commonly described as "metallic", however, have specific resistivities much lower than ground waters. The induced polarization effect takes place at those interfaces where the mode of conduction changes from ionic in the solutions filling the interstices of the rock to electronic in the metallic minerals present in the rock.

The blocking action or induced polarization mentioned above, which depends upon the chemical energies necessary to allow the ions to give up or receive electrons from the metallic surface, increases with the time that a d. c. current is allowed to flow through the rock; i. e. as ions pile up against the metallic interface the resistance to current flow increases. Eventually, there is enough polarization in the form of excess ions at the interfaces, to appreciably reduce the amount of current flow through the metallic particle. This polarization takes place at each of the infinite number of solution-metal interfaces in a mineralized rock.

When the d.c. voltage used to create this d.c. current flow is cut off, the Coulomb forces between the charged ions forming the polarization cause them to return to their normal position. This movement of charge creates a small current flow which can be measured on the surface of the ground as a decaying potential difference.

From an alternate viewpoint it can be seen that if the direction of the current through the system is reversed repeatedly before the polarization occurs, the effective resistivity of the system as a whole will change as the frequency of the switching is changed. This is a consequence of the fact that the amount of current flowing through each metallic interface depends upon the length of time that current has been passing through it in one direction.

- 2 -

- 3 -

The values of the per cent frequency effect or F.E. are a measurement of the polarization in the rock mass. However, since the measurement of the degree of polarization is related to the apparent resistivity of the rock mass it is found that the metal factor values or M.F. are the most useful values in determining the amount of polarization present in the rock mass. The MF values are obtained by normalizing the F.E. values for varying resistivities.

The induced polarization measurement is perhaps the most powerful geophysical method for the direct detection of metallic sulphide mineralization, even when this mineralization is of very low concentration. The lower limit of volume per cent sulphide necessary to produce a recognizable IP anomaly will vary with the geometry and geologic environment of the source, and the method of executing the survey. However, sulphide mineralization of less than one per cent by volume has been detected by the IP method under proper geological conditions.

The greatest application of the IP method has been in the search for disseminated metallic sulphides of less than 20% by volume. However, it has also been used successfully in the search for massive sulphides in situations where, due to source geometry, depth of source, or low resistivity of surface layer, the EM method can not be successfully applied. The ability to differentiate ionic conductors, such as water filled shear zones, makes the IP method a useful tool in checking EM

- 4 -

anomalies which are suspected of being due to these causes.

In normal field applications the IP method does not differentiate between the economically important metallic minerals such as chalcopyrite, chalcocite, molybdenite, galena, etc., and the other metallic minerals such as pyrite. The induced polarization effect is due to the total of all electronic conducting minerals in the rock mass. Other electronic conducting materials which can produce an IP response are magnetite, pyrolusite, graphite, and some forms of hematite.

In the field procedure, measurements on the surface are made in a way that allows the effects of lateral changes in the properties of the ground to be separated from the effects of vertical changes in the properties. Current is applied to the ground at two points in distance (X) apart. The potentials are measured at two other points (X) feet apart, in line with the current electrodes is an integer number (n) times the basic distance (X).

The measurements are made along a surveyed line, with a constant distance (nX) between the nearest current and potential electrodes. In most surveys, several traverses are made with various values of (n); i.e. (n) = 1, 2, 3, 4, etc. The kind of survey required (detailed or reconnaissance) decides the number of values of (n) used.

In plotting the results, the values of the apparent resistivity, apparent per cent frequency effect, and the apparent metal factor

- 5 -

measured for each set of electrode positions are plotted at the intersection of grid lines, one from the center point of the current electrodes and the other from the center point of the potential electrodes. (See Figure A.) The resistivity values are plotted above the line as a mirror image of the metal factor values below. On a second line, below the metal factor values, are plotted the values of the per cent frequency effect. In some cases the values of per cent frequency effect are plotted as superscripts of the metal factor value. In this second case the frequency effect values are not contoured. The lateral displacement of a given value is determined by the location along the survey line of the center point between the current and potential electrodes. The distance of the value from the line is determined by the distance (nX) between the current and potential electrodes when the measurement was made.

The separation between sender and receiver electrodes is only one factor which determines the depth to which the ground is being sampled in any particular measurement. The plots then, when contoured, are not section maps of the electrical properties of the ground under the survey line. The interpretation of the results from any given survey must be carried out using the combined experience gained from field results, model study results and theoretical investigations. The position of the electrodes when anomalous values are measured is important in the interpretation. In the field procedure, the interval over which the potential differences are measured is the same as the interval over which the electrodes are moved after a series of potential readings has been made. One of the advantages of the induced polarization method is that the same equipment can be used for both detailed and reconnaissance surveys merely by changing the distance (X) over which the electrodes are moved each time. In the past, intervals have been used ranging from 25 feet to 2000 feet for (X). In each case, the decision as to the distance (X) and the values of (n) to be used is largely determined by the expected size of the mineral deposit being sought, the size of the expected anomaly and the speed with which it is desired to progress.

The diagram in Figure A demonstrates the method used in plotting the results. Each value of the apparent resistivity, apparent metal factor, and apparent per cent frequency effect is plotted and identified by the position of the four electrodes when the measurement was made. It can be seen that the values measured for the larger values of (n) are plotted farther from the line indicating that the thickness of the layer of the earth that is being tested is greater than for the smaller values of (n); i. e. the depth of the measurement is increased. When the F. E. values are plotted as superscripts to the MF values the third section of data values is not presented and the F. E. values are not contoured.

- 6 -

- 7 -

The actual data plots included with the report are prepared utilizing an IBM 360/75 Computer and a Calcomp 770/763 Incremental Plotting System. The data values are calculated, plotted, and contoured according to a programme developed by McPhar Geophysics. Certain symbols have been incorporated into the programme to explain various situations in recording the data in the field.

The IP measurement is basically obtained by measuring the difference in potential or voltage ($\Delta \vee$) obtained at two operating frequencies. The voltage is the product of the current through the ground and the apparent resistivity of the ground. Therefore in field situations where the current is very low due to poor electrode contact, or the apparent resistivity is very low, or a combination of the two effects; the value of ($\Delta \vee$) the change in potential will be too small to be measurable. The symbol "TL" on the data plots indicates this situation.

In some situations spurious noise, either man made or natural, will render it impossible to obtain a reading. The symbol "N" on the data plots indicates a station at which it is too noisey to record a reading. If a reading can be obtained, but for reasons of noise there is some doubt as to its accuracy, the reading is bracketed in the data plot ().

In certain situations negative values of Apparent Frequency Effect are recorded. This may be due to the geologic environment or spurious electrical effects. The actual negative frequency effect value recorded is indicated on the data plot, however the symbol "NEG" is

- 8 -

indicated for the corresponding value of Apparent Metal Factor. In contouring negative values the contour lines are indicated to the nearest positive value in the immediate vicinity of the negative value.

The symbol "NR" indicates that for some reason the operator did not attempt to record a reading although normal survey procedures would suggest that one was required. This may be due to inaccessible topography or other similar reasons. Any symbol other than those discussed above is unique to a particular situation and is described within the body of the report.

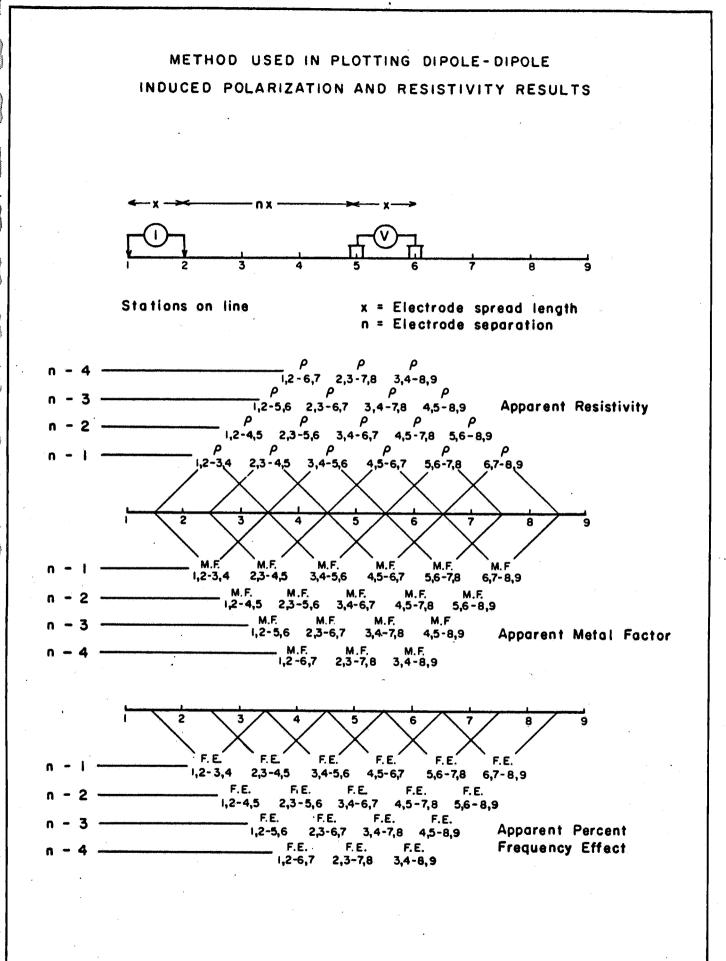


Fig. A

McPHAR GEOPHYSICS

APPENDIX

THE INTERPRETATION OF INDUCED POLARIZATION ANOMALIES FROM RELATIVELY SMALL SOURCES

The induced polarization method was originally developed to detect disseminated sulphides and has proven to be very successful in the search for "porphyry copper" deposits. In recent years we have found that the IP method can also be very useful in exploring for more concentrated deposits of limited size. This type of source gives sharp IP anomalies that are often difficult to interpret.

The anomalous patterns that develop on the contoured data plots will depend on the size, depth and position of the source and the relative size of the electrode interval. The data plots <u>are not</u> sections showing the electrical parameters of the ground. When the electrode interval (X) is appreciably greater than the width of the source, a large volume of unmineralized rock is averaged into each measurement. This is particularly true for the large values of the electrode separation (n).

The theoretical scale model results shown in Figure 1 and Figure 2 indicate the effect of depth. If the depth to the top of the source is small compared to the electrode interval (i.e. d X) the measurement for n = 1 will be anomalous. In Figure 1 the depth is 0.5 units (X = 1.0 units) and the n = 1 value is definitely anomalous; the pattern on the contoured data plot is typical for a relatively shallow, narrow, near-vertical tabular source. The results in Figure 2 are for the same source with the depth increased to 1.5 units. Here the n = 1 value is not anomalous; the larger values of (n) are anomalous but the magnitudes are much lower than for the source at less depth.

When the electrode interval is greater than the width of the source, it is not possible to determine its width or exact position between the electrodes. The true IP effect within the source is also indeterminate; the anomaly from a very narrow source with a very large true IP effect will be much the same as that from a zone with twice the width and 1/2 the true IP effect. The theoretical scale model data shown in Figure 3 and Figure 4 demonstrate this problem. The depth and position of the source are unchanged but the width and true IP effect are varied. The anomalous patterns and magnitudes are essentially the same, hence the data are insufficient to evaluate the source completely.

The normal practise is to indicate the IP anomalies by solid, broken, or dashed bars, depending upon their degree of distinctiveness. These bars represent the surface projection of the anomalous zones as interpreted from the location of the transmitter and receiver electrodes when the anomalous values were measured. As illustrated in Figure 1, Figure 2, Figure 3 and Figure 4, no anomaly can be located with more accuracy than the spread length. While the centre of the solid bar indicating the anomaly corresponds fairly well with the source, the length of the bar should not be taken to represent the exact edges of the anomalous material.

If the source is shallow, the anomaly can be better evaluated using a shorter electrode interval. When the electrode interval used approaches the width of the source, the apparent effects measured will be nearly equal to the true effects within the source. When there is some depth to the top of the source, it is not possible to use electrode intervals that are much less than the depth to the source. In this situation, one must realize that a definite ambiguity exists regarding the width of the source and the IP effect within the source.

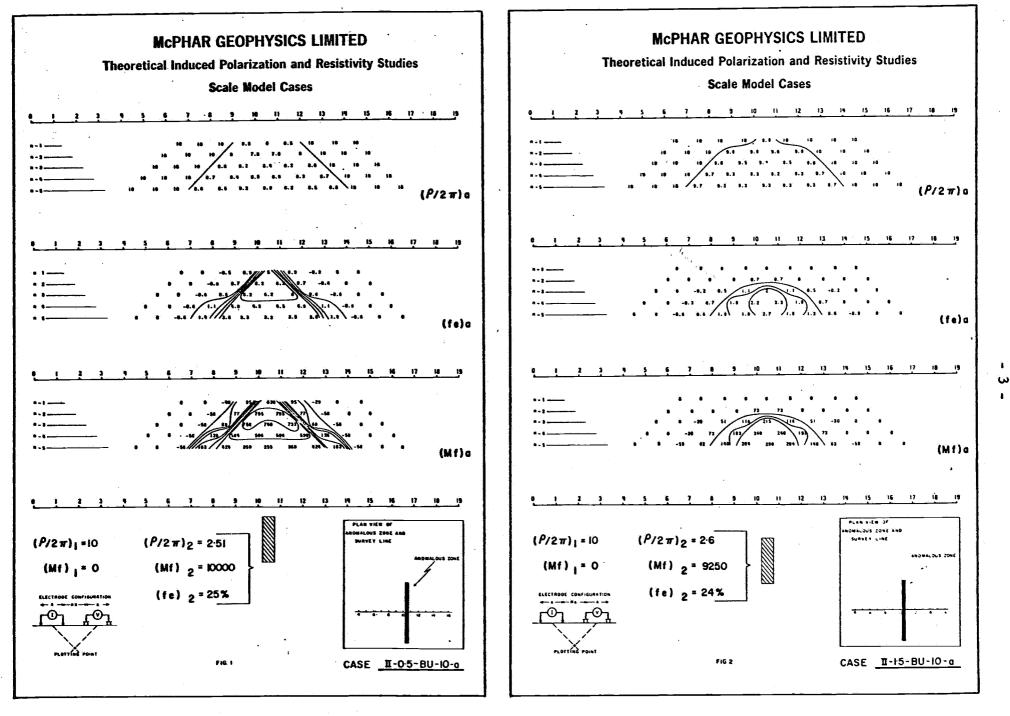
Our experience has confirmed the desirability of doing detail. When a reconnaissance IP survey using a relatively large electrode interval indicates the presence of a narrow, shallow source, detail with shorter electrode intervals is necessary in order to better locate, and evaluate, the source. The data of most usefulness is obtained when the maximum apparent IP effect is measured for n = 2 or n = 3. For instance, an anomaly originally located using X = 300' may be checked with X = 200' and then X = 100'. The data with X = 100' will be quite different from the original reconnaissance results with X = 300'.

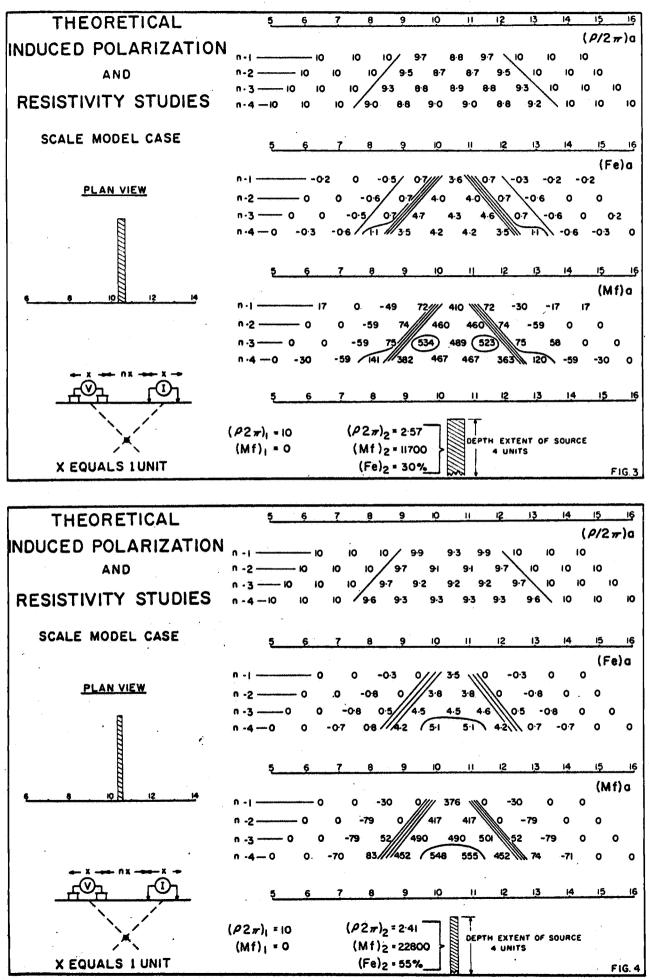
The data shown in Figure 5 and Figure 6 are field results from a greenstone area in Quebec. The expected sources were narrow (less than 30' in width) zones of massive, high-grade, zinc-silver ore. An electrode interval of 200' was used for the reconnaissance survey in order to keep the rate of progress at an acceptable level. The anomalies located were low in magnitude.

The very weak, shallow anomaly shown in Figure 5 is typical of those located by the X = 200' reconnaissance survey. Several anomalies of this type were detailed using shorter electrode intervals. In most cases the detail measurements suggested broad zones of very weak mineralization. However, in the case of the source at 20N to 22N, the measurements with shorter electrode intervals confirmed the presence of a strong, narrow source. The X = 50' results are shown in Figure 6. Subsequent drilling has shown the source to be 12.5' of massive sulphide mineralization containing significant zinc and silver values.

The change in the anomaly that results when the electrode interval is reduced is not unusual. The X = 50' data more accurately locates the narrow source, and permits the geophysicist to make a better evaluation of its importance. The completion of this type of detail is very important, in order to get the maximum usefulness from a reconnaissance IP survey.

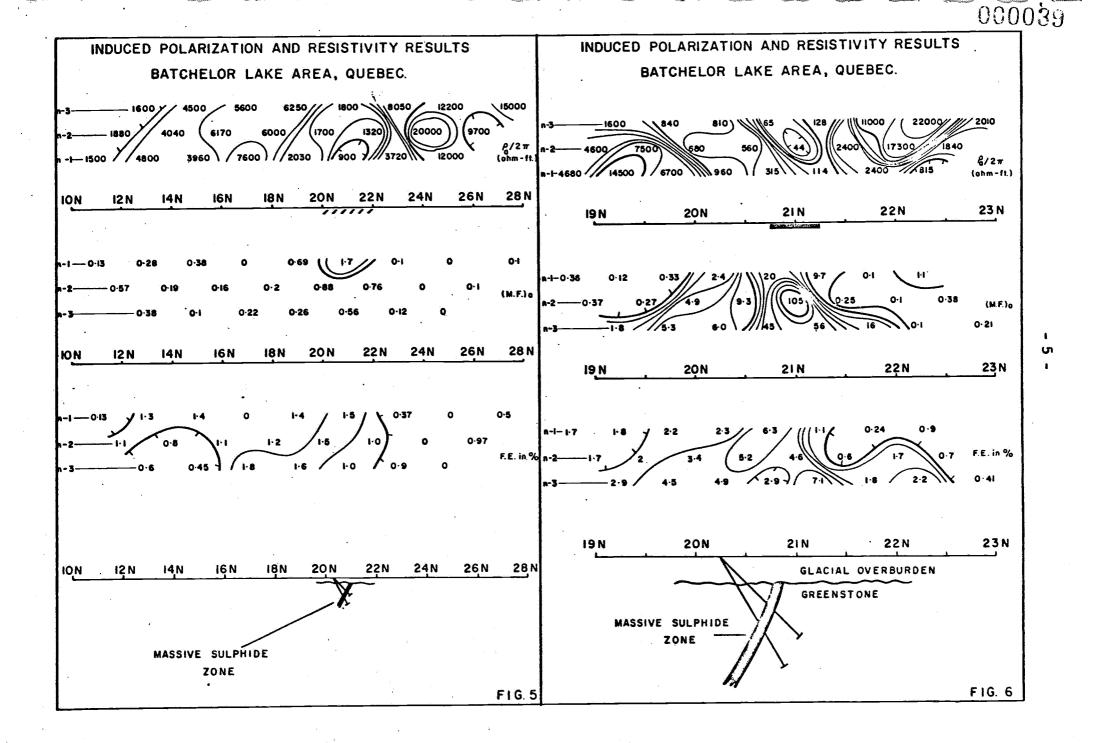
- -000037





- 4 -

.



McPHAR GEOPHYSICS

APPENDIX

EXPECTED IP ANOMALIES FROM "PORPHYRY COPPER" TYPE ZONES OF DISSEMINATED SULPHIDE MINERALIZATION

Our experience in other areas has shown that the induced polarization method can be successfully used to locate, and outline, zones of disseminated sulphide mineralization of the "porphyry copper" type. In most cases the interpretation of the IP results is simple and straightforward. The results shown in Figure 1 and Figure 2 are typical.

INDUCED POLARIZATION 37<u>N</u> 4QN 43 N 46N 49 N 6IN 64 N 52 N 55N 50 N 67 N 70 (P/2 m)a AND 480/ 570 590 130 304 60 2600 \901 / 1600 DRILLING RESULTS -2-48 510 530 355 1511 2151 FROM 40 39 73 /214 920//255 5 COPPER MOUNTAIN AREA 37N 40N 43 N 46 N 49N 52 N 55 N 58 N 61 N 64 N 67 N 70N GASPE, QUEBEC (Fe)a 2.5 50 37 34 6.0 5-0 5-7 3-8 70 7.0 7.2 7.9 4.0 5.0 48 35 63 -32 3-1 4.0 / (N) 7.1 74 5-0 4.0 5-6 LINE-3IN 37N 40N 43N 46N 52N 49N 64 N 55 N 58N 6IN 67 N 70 (Mf)a 176 184 f 4.9 FREQUENCIES - 0-31 & 2-5 CPS. 215 69 45. 192 40N 46N 37N 43N 49 N 52N 55 N 56 N 6I N 70N 64 N 67N SURFACE OXIDE MINERALIZATIC SULPHIDE MINERALIZATION DISSEMINATED COPPER ORE X EQUALS 300 FEET 4% TOTAL SULPHIDES) FIG.I

The source of the moderate magnitude IP anomaly shown in Figure 1 contains approximately 4% metallic mineralization. The zone is of limited lateral extent and enough copper is present to make the mineralization "ore grade". The presence of the surface oxidation can be seen in the fact that the apparent IP effects increase for n = 2.

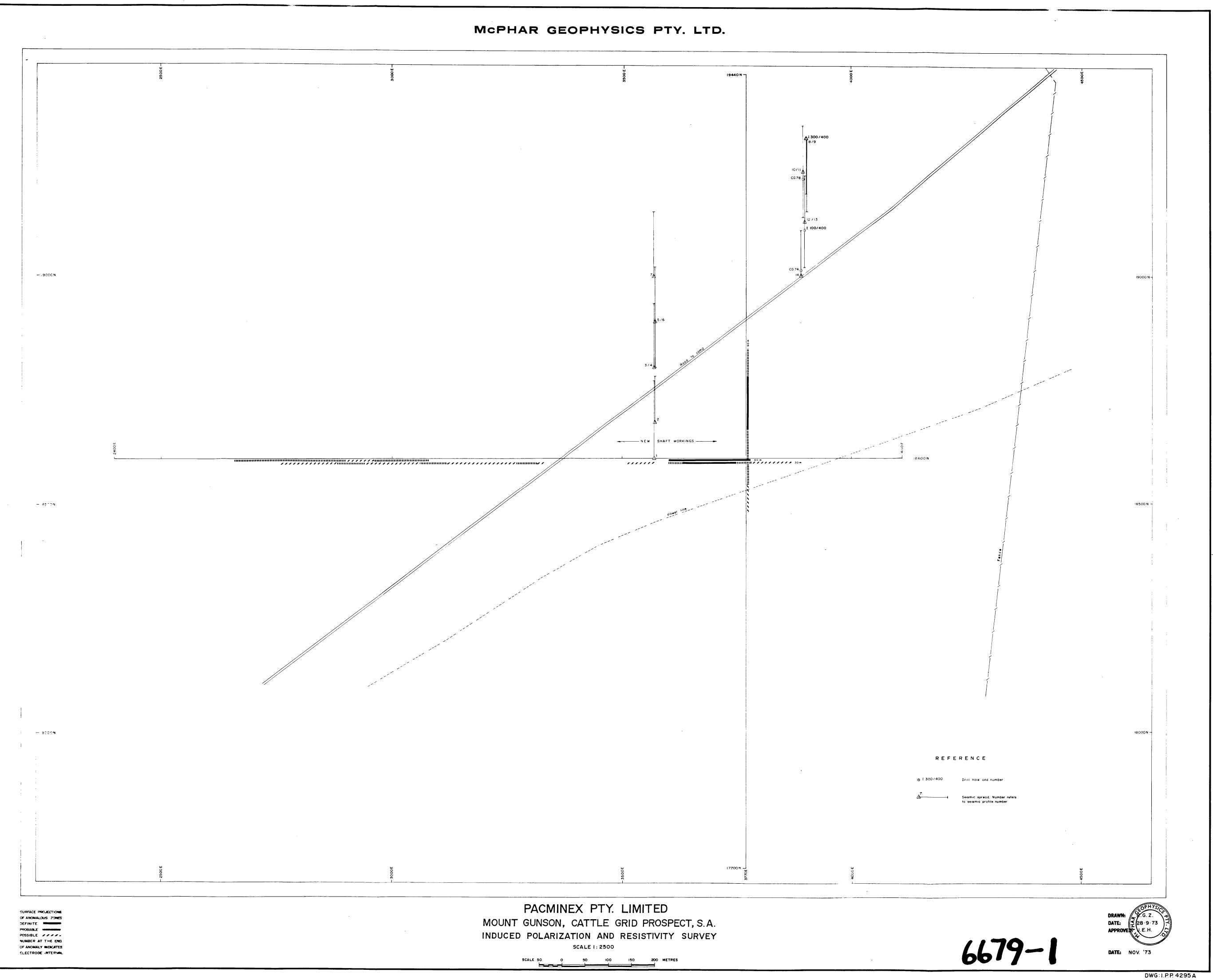
INDUCED POLARIZATION	195	175	155	135	IIS	95	76					
			<u></u>	133		80	75	55	35	IS		<u>3</u> N
AND	n - 9	\ 54	5	10/ 22	6 / 4;	2 🔺	3/ 5	0 8	50×3		(<i>P</i> /27	1
DRILLING RESULTS	n-291	90	65	(47	47	45 /	6A °	50		8/6	5 × 4 66	69
FROM	n-3-77	7 93	5	-	4	· / 6:	2 6	B (51 / 8 1	1	0 8	
FROM	n-4-75	77	82	82	62	61	71	58 .	82	67	89	65
WESTERN NEW MEXICO	19 S	17S	155	135	IIS	95	7 5		••			
						33	15	55	35	<u> IS</u>	<u>IN</u>	<u>3N</u>
U. S. A.	n-1	5 / 2.5	2	5//5	0 1 4	5 / 6	0 ~ 4	·5 3	0 2	0 3	(Fe	
	n-2-20	35	3.5	55	60	7.0	8.4	7.5	5.5	5.0	40	4-6
	n-3-4	0 47	6	0 7.	0 8:	5 8.	4 8-	9 (7	·0 7·	0 5	15 54	
	a-4-50	4.5 /	7.0	70	7.6	9.0	9.0	9.0/	7.0	6.0	65 /	4.4
		•										
LINE-40W	19 <u>5</u>	175	15 S	13.S	IIS	95	75	5 <u>S</u>	35	15	IN	<u>3</u> N
	6 al	1140		- 7 4 1	- 1			z			(Mf)	
	n-2-22	39	54 //		2/10	\sim	-		-			- I
FREQUENCIES - 0-31 8, 2-5 CPS	n-3-52		7/10			3 / 134	13 <u>3</u> 6 13:	150 2 13	125) 7 86	63	61	67
	n-4-67	58 /	86	86 /	123	48	126 /	155	86	i 7 90	9) 62 /73	67
					1							
	19S	175	155	135	IIS	95	75	55	<u>3</u> 5	IS	_1 <u>N</u>	<u>3N</u>
					45	3% 10 6% SUL	PHIOFE	130	OVERBUI	ROEN		
					230			· { 51	6 to 10%	SULPH	IDES	
X EQUALS 200 FEET					. 11	7% to 1	2%			DES		-
			D	RILLED	,0 810, 🝴	SULPHI	JE 5	3001.1			FI	G. 2

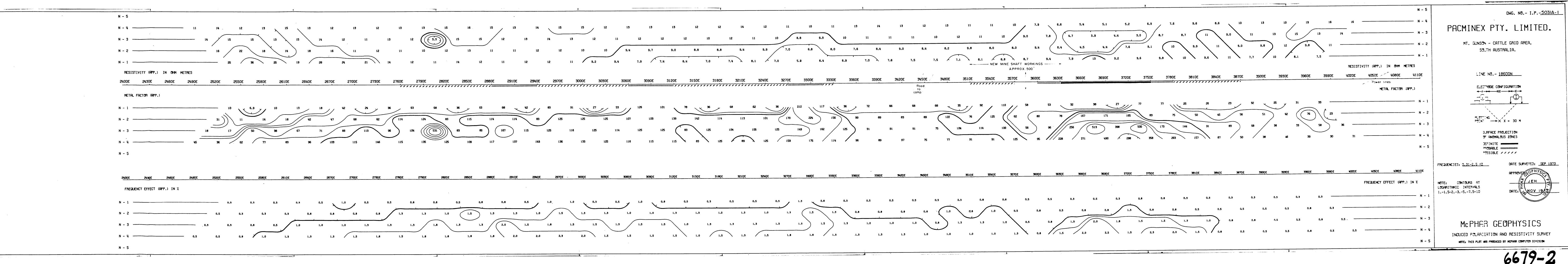
The IP anomaly shown in Figure 2 has about the same magnitude as that described above. It should be noted that appreciably greater concentrations of metallic mineralization are present; further, there is little or no copper present. These results illustrate the fact that IP results can not be used to determine the exact amount of metallic mineralization present or to determine the economic importance of a mineralized zone. In some geologic situations zoning is present; the zones of mineralization of greatest economic value may contain less total metallic mineralization than other zones in the same general area.

- 2 -

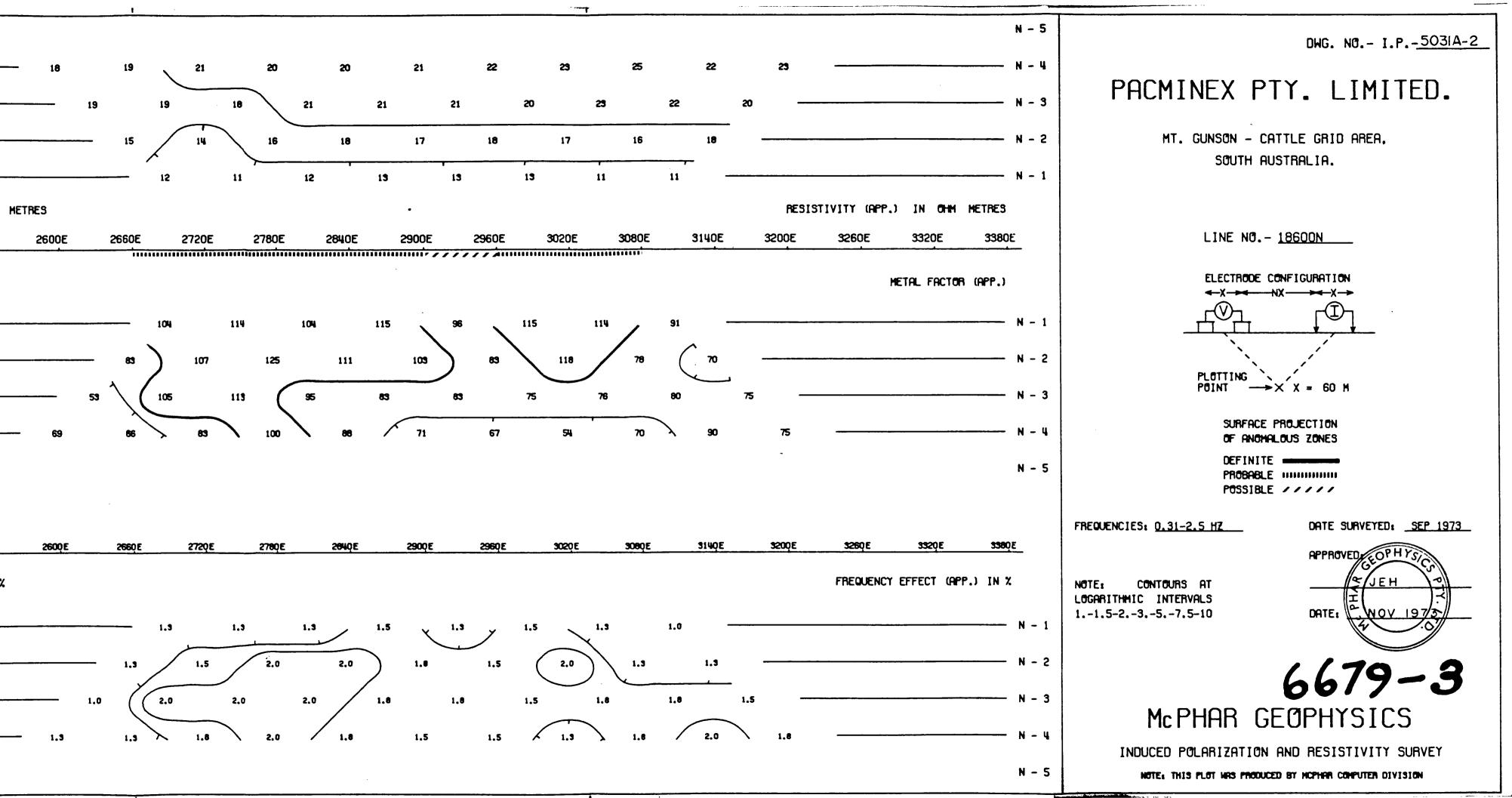
In the proper geologic environment, the method will detect even very low concentrations of metallic mineralization. The IP results shown in Figure 3 located the ore zone at the Brenda Property near Peachland, B. C. The zone contains 1.0 to 1.5 per cent metallic mineralization; however, the mineralization is "ore grade" because only molybdenite and chalcopyrite are present.

INDUCED POLARIZATION 20E 4E 12 E 16E 24 W 20W 16W 12W 8W 4W 0 8E $(P/2\pi)a$ AND 222 242 287 245 396 850/ 238 ... 267 346 387 334) (192 DRILLING RESULTS n-2-- 420 200 228 272/ 310 320) (100 242 (302 356 (290 236 . 247 n-3-FROM 322 297 192 270 322 368 245 196 222 BRENDA AREA 24 W 20 W 16 W 12W 8W 4 W 4 E 8Ė 12 E IĢE 20E PEACHLAND, B.C. (Fe)a 0.9 1.5 40 3.5 30 2.6 n -2 -0.5 0.6 3-5 3.0 2.0 0.6 5.0 3.0 n.3 3-01 / 2.5 3.2 50 10 03/ 30 (N) ŀ5 2.4 LINE-8S 20W 16W 12W 8W 4E 8E 12E 16E 20E 4W 0 (Mf)a 7.5/ 2.9/ 58 17 6.7, 13 63 3.0 (98 4.0 (10 10 8 FREQUENCIES - 0-31 8. 5-0 CPS. 127 (N) н 15 8E 12 E 16E 20E 20W 16W 12W 8W 4E 24W DISSEMINATED SULPHIDE ZONE HIDES **X EQUALS 400 FEET** FIG.3

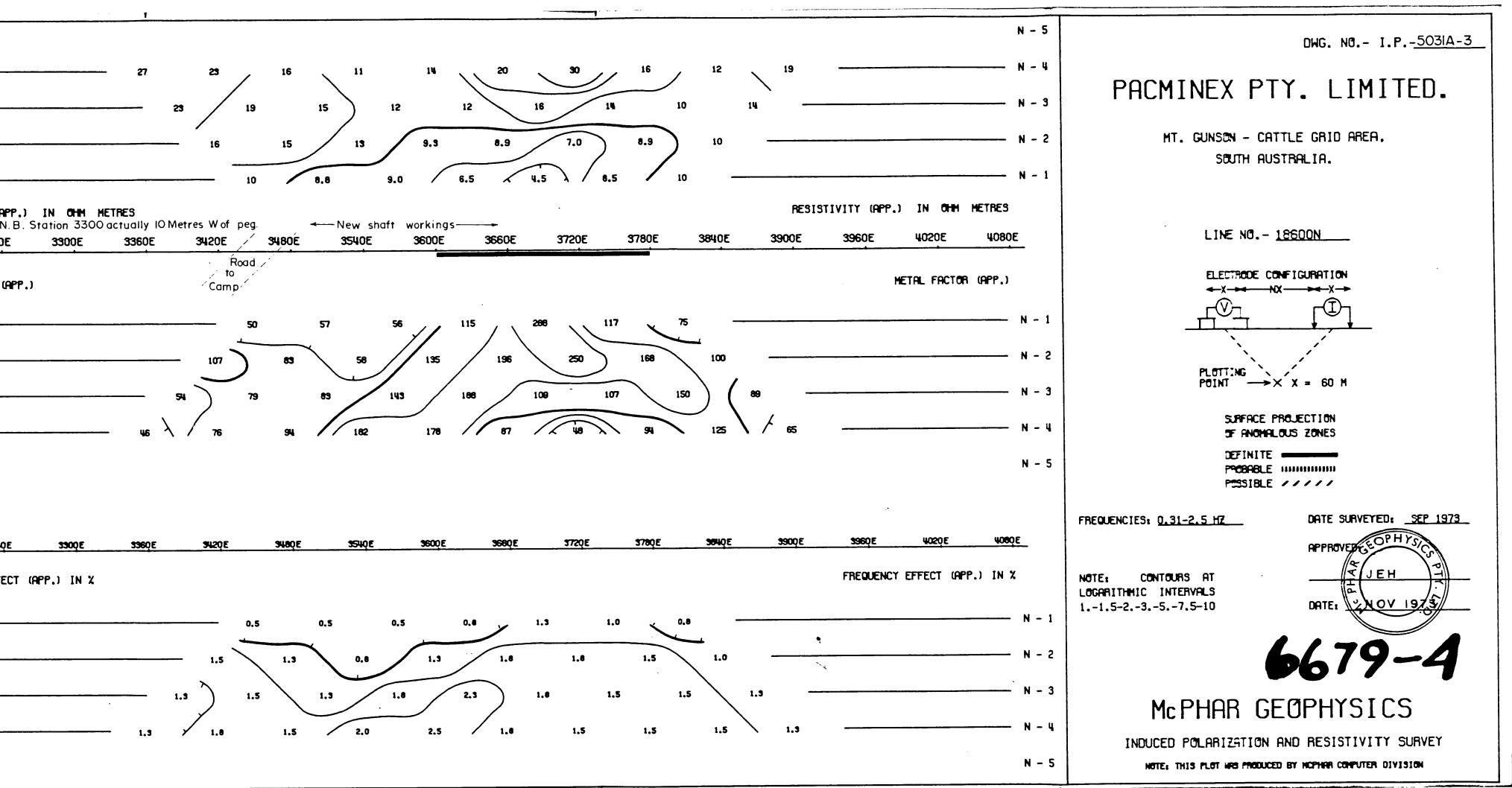




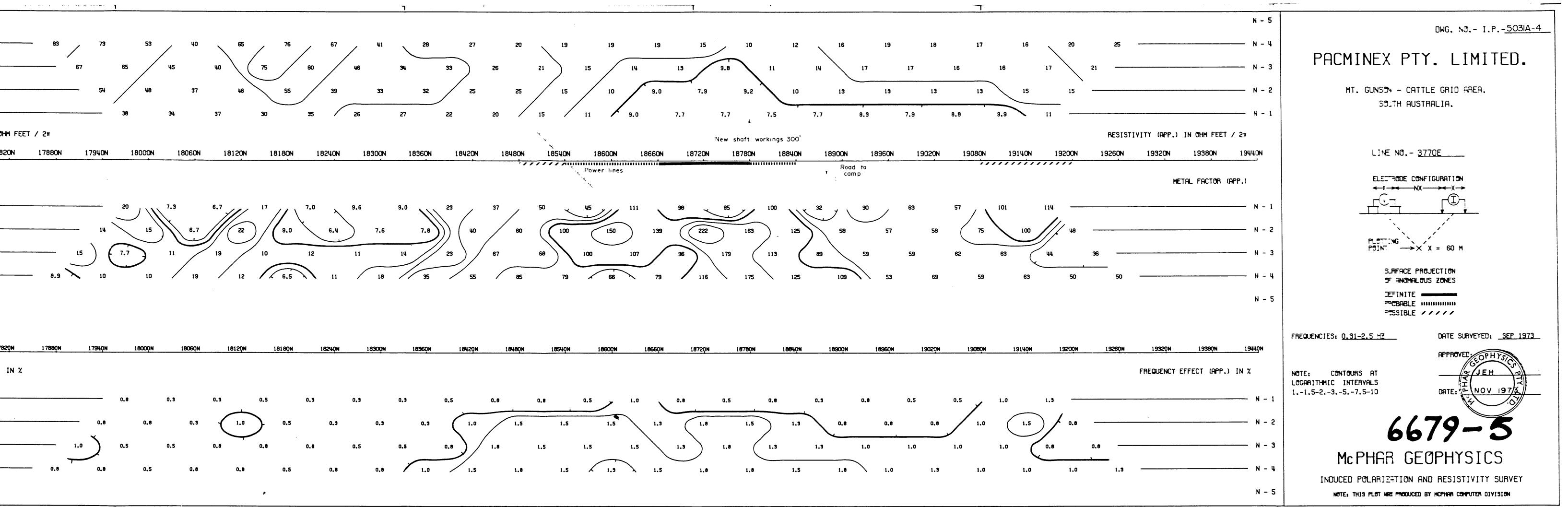
	1	
		N - 5
		N – 4 –
		N - 3
		N - 2
		N - 1
		RESISTIVITY (APP.) IN OHH
		2420E 2480E 2540E
		METAL FACTOR (APP.)
		N - 1
		N - 2
		N - 3
		N - 4
		N - 5
		<u>2420E 2480E 2540E</u>
		FREQUENCY EFFECT (APP.) IN %
		N - 1
		N - 2
		N - 3
		N - 4
		N - 5



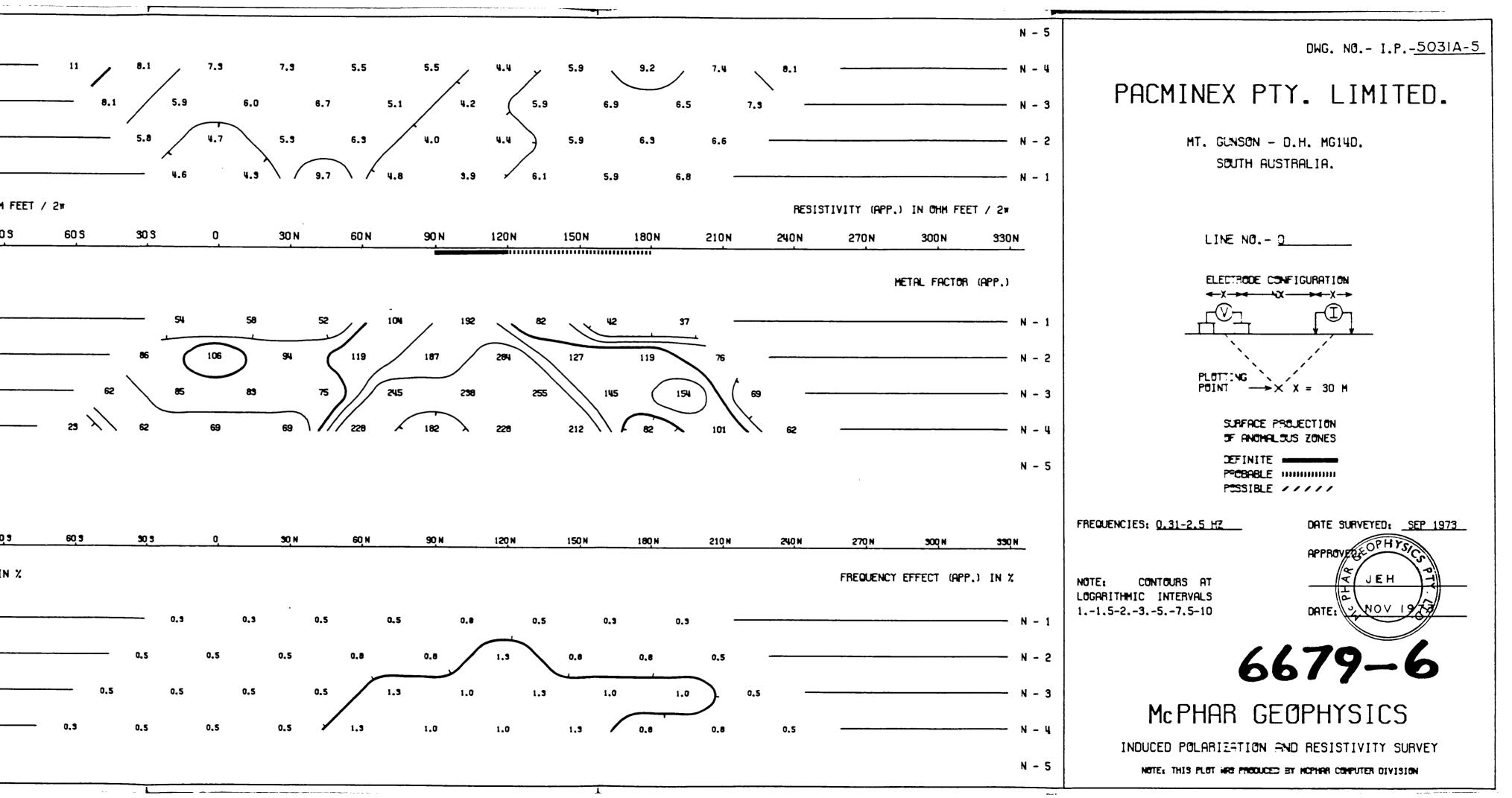
	N - 5
	N-4
	N - 3
	N - 2
	N - 1
	RESISTIVITY (APP
	N.E 3180E 3240E
	HETAL FACTOR (AP
	N - 1
	N - 2
	N - 3
-	N - 4
	N - 5
	N - J
	3180E 3240E
	FREQUENCY EFFECT
	N - 1
	N - 2
	N - 3
	N 4.
	N - 5



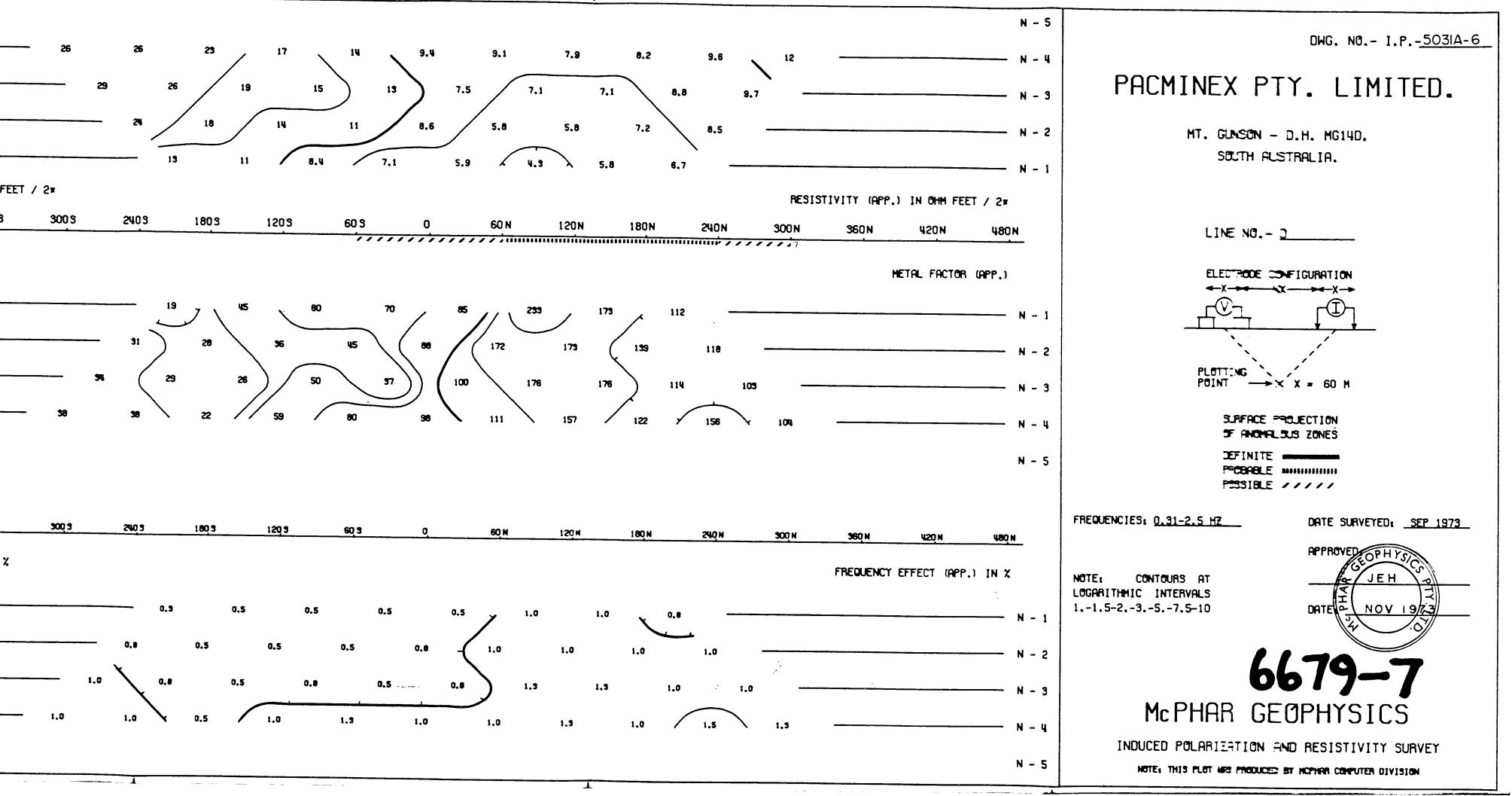
N - 5
. N - 4
N - 3
N - 2
N - 1
RESISTIVITY (APP.) IN OHM F
17700N 17760N 17820N
METAL FACTOR (APP.)
N - 1
N - 2
N - 3
N - 4
N - 5
17700N 17760N 17820N
FREQUENCY EFFECT (APP.) IN
N - 1
N - 2
N - 3
- N - 4
N - 5



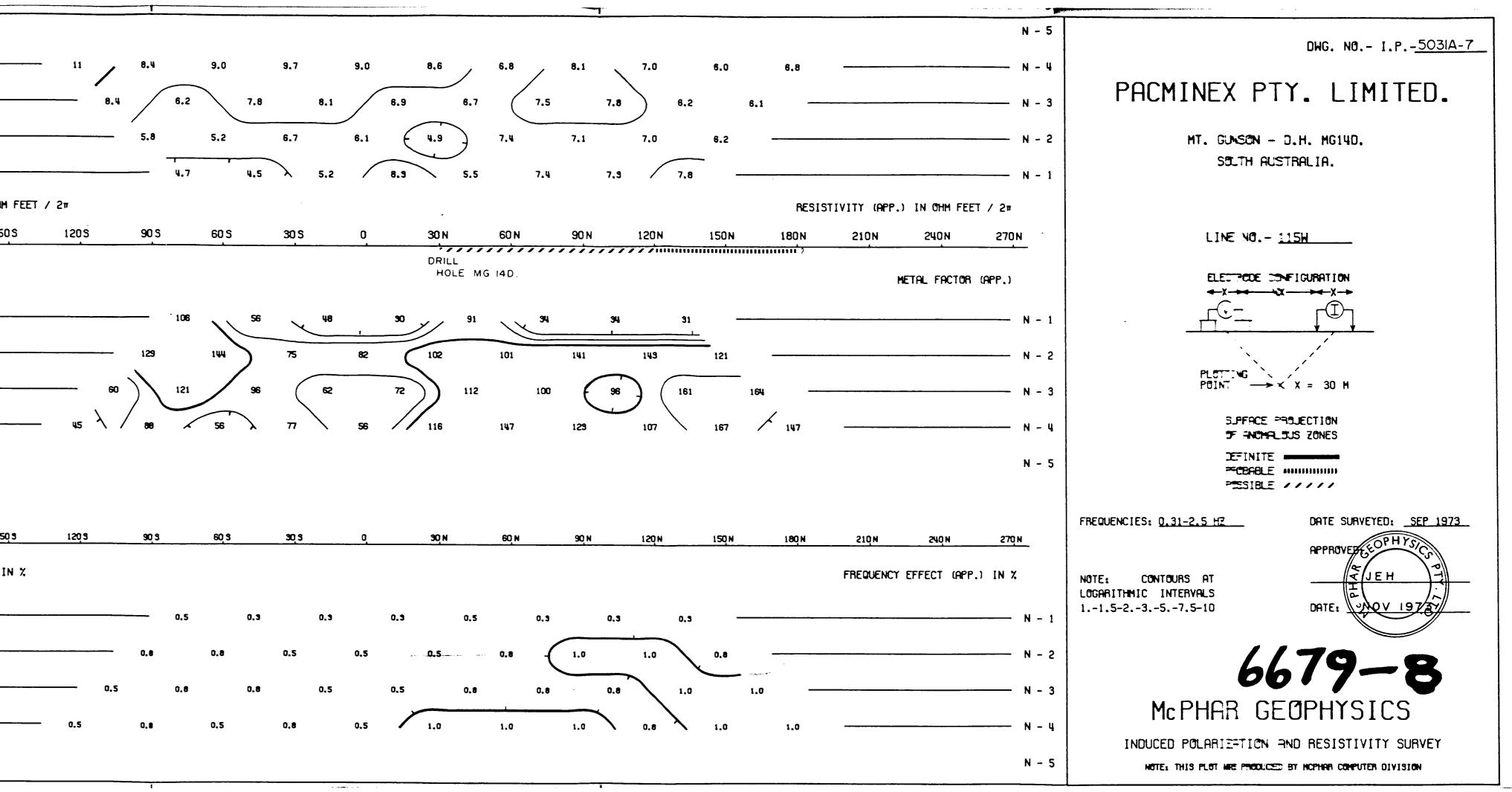
	 ۲	
	N -	5
	N -	ų
	N -	3
	N -	2
	N -	1
		RESISTIVITY (APP.) IN OHM F
		1505 1205 905
		METAL FACTOR (APP.)
	N -	1
•	N -	2
	N -	3
	N -	4
	N -	5
		150 9 120 9 90 9
		FREQUENCY EFFECT (APP.) IN ;
	N -	1
	N - 3	2
	N - 3	3
	N - 1	4
	N - 5	5

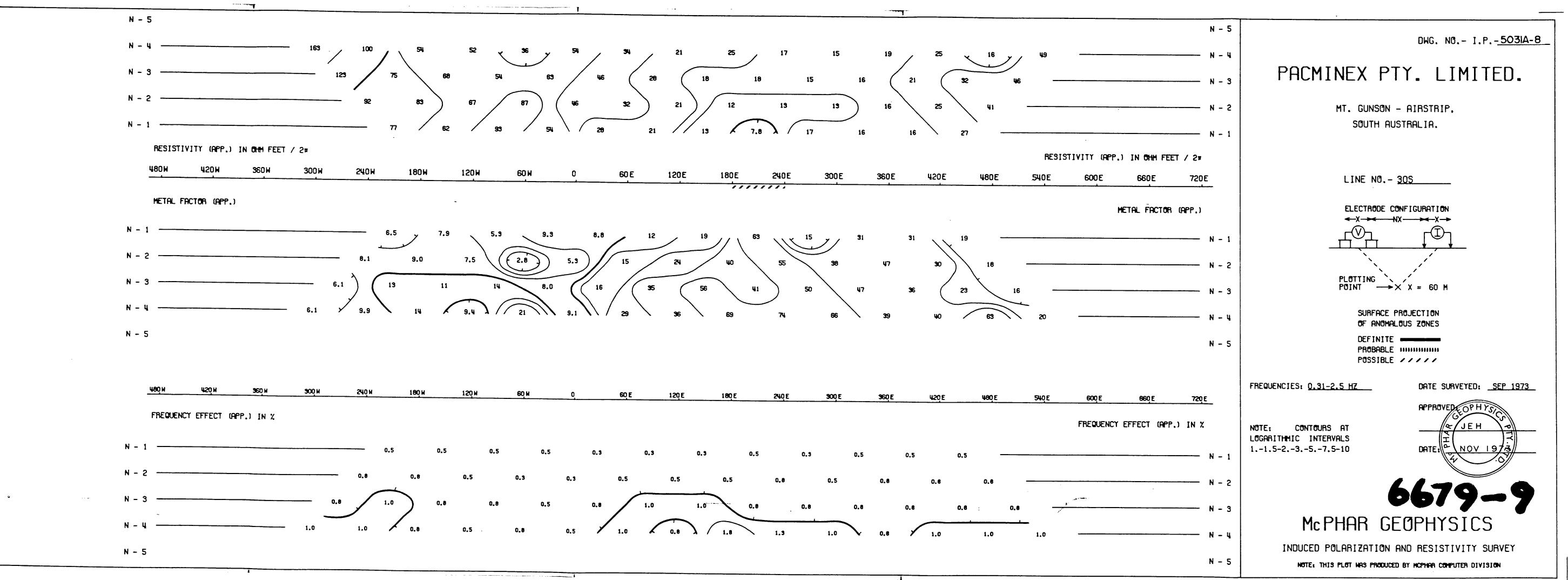


	F	
		N - 5
		N 11
		N - Y
		N - 3
		N - 2
		N - 1
		RESISTIVITY (APP.) IN OHH FEE
		4803 4203 3603
		METAL FACTOR (APP.)
		N - 1
		N - 2
-		N - 3
		N - 4
		N - 5
		480 3 420 3 560 3
		FREQUENCY EFFECT (APP.) IN X
		N - 1
		N - 2
		N - 3
		N - 4
		N - 5
	 	·····



			······································	
				N - 5
				N - 4
х ,				N - 3
				N - 2
				N - 1
				RESISTIVITY (APP.) IN CHM (
				210S 180S 150S
				METAL FACTOR (APP.)
	-			N - 1
				N - 2
				N - 3
				N - 4
				N - 5
:				
				2103 1803 1505
				FREQUENCY EFFECT (APP.) IN
				N - 1
		a to the second s		N - 2
) I				N - 3
				N - 4
				N - 5
-				 ······································





-

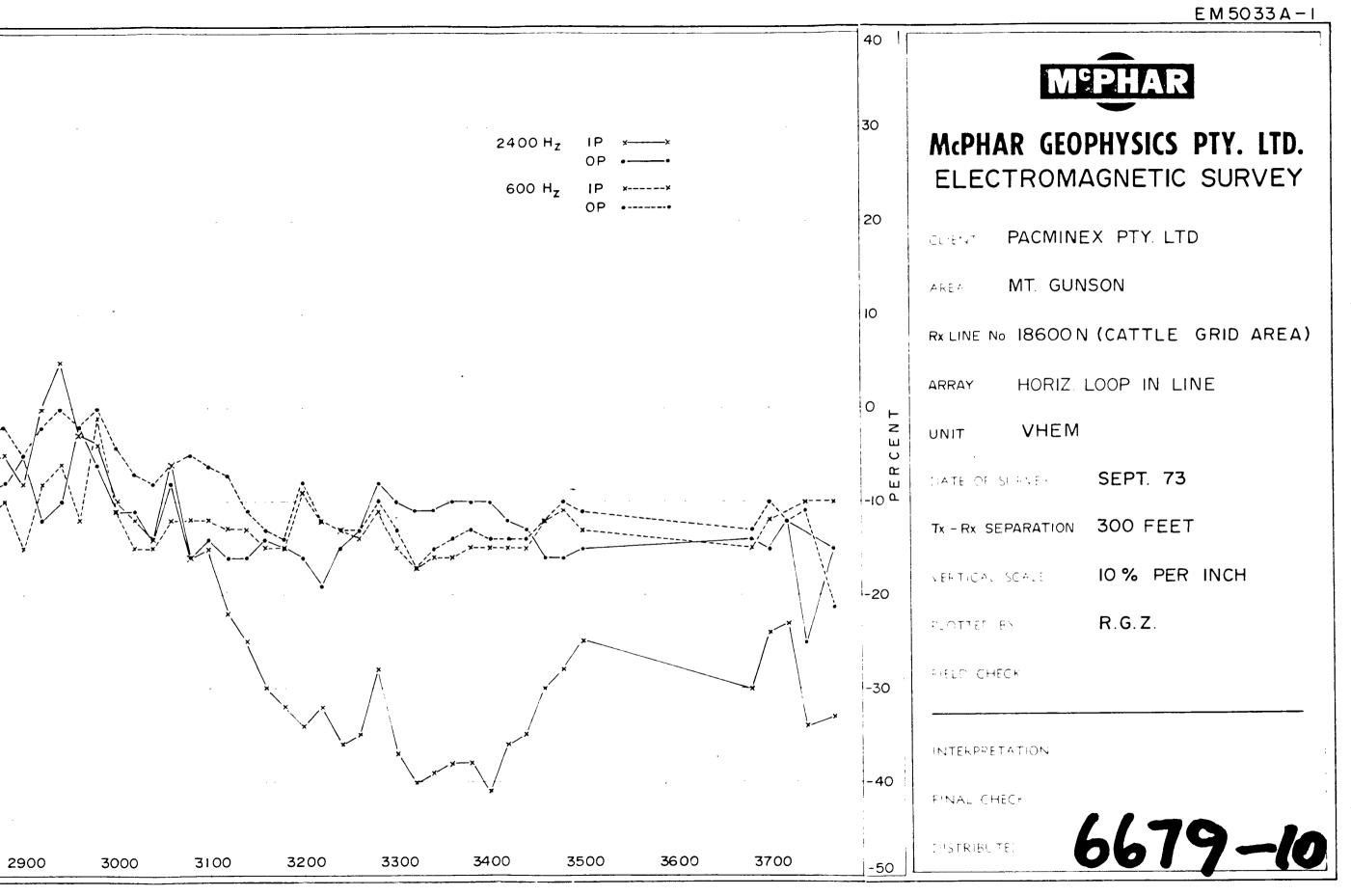
-

. .

_ _

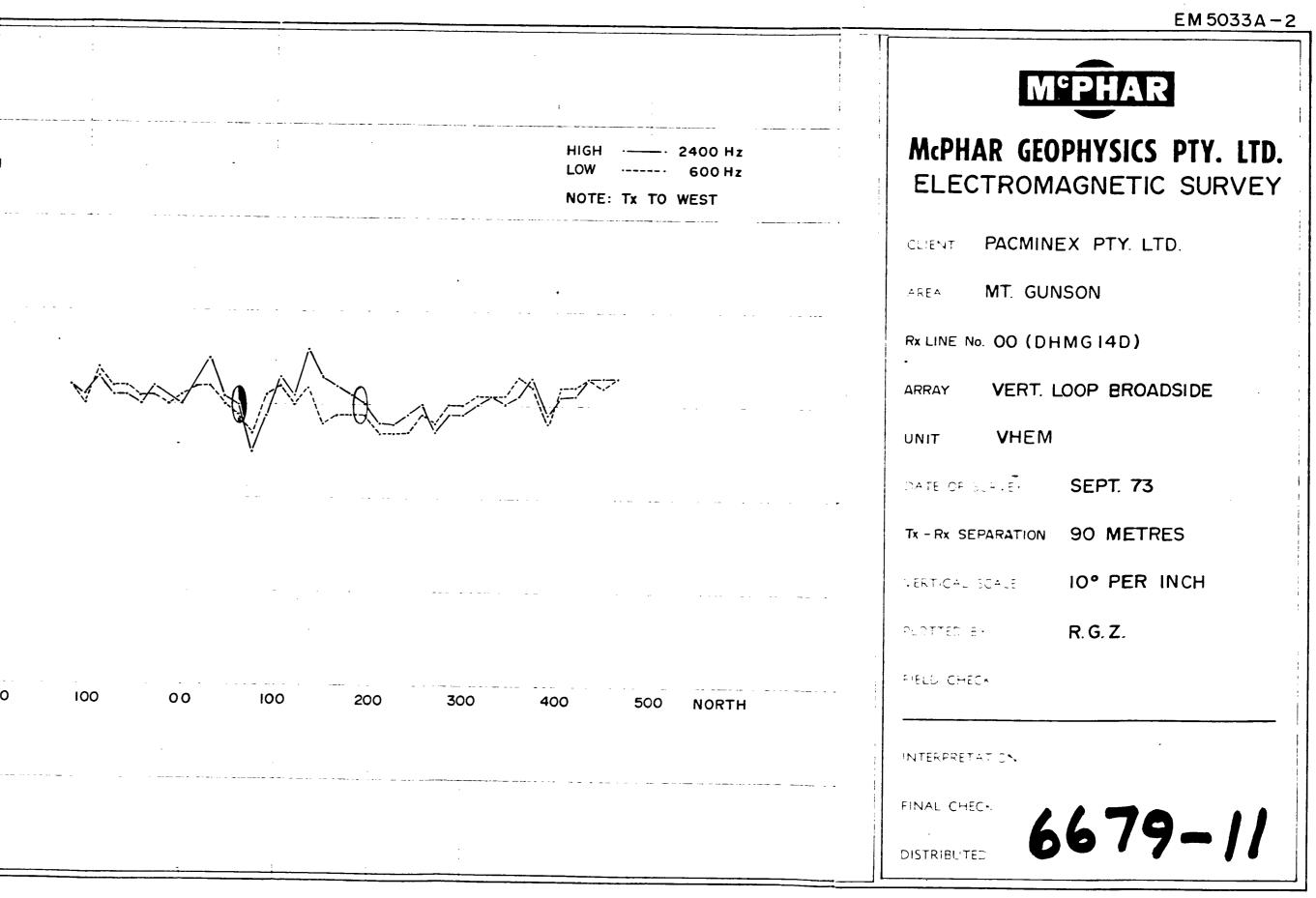
. <u>.</u>

2600 2700 2800

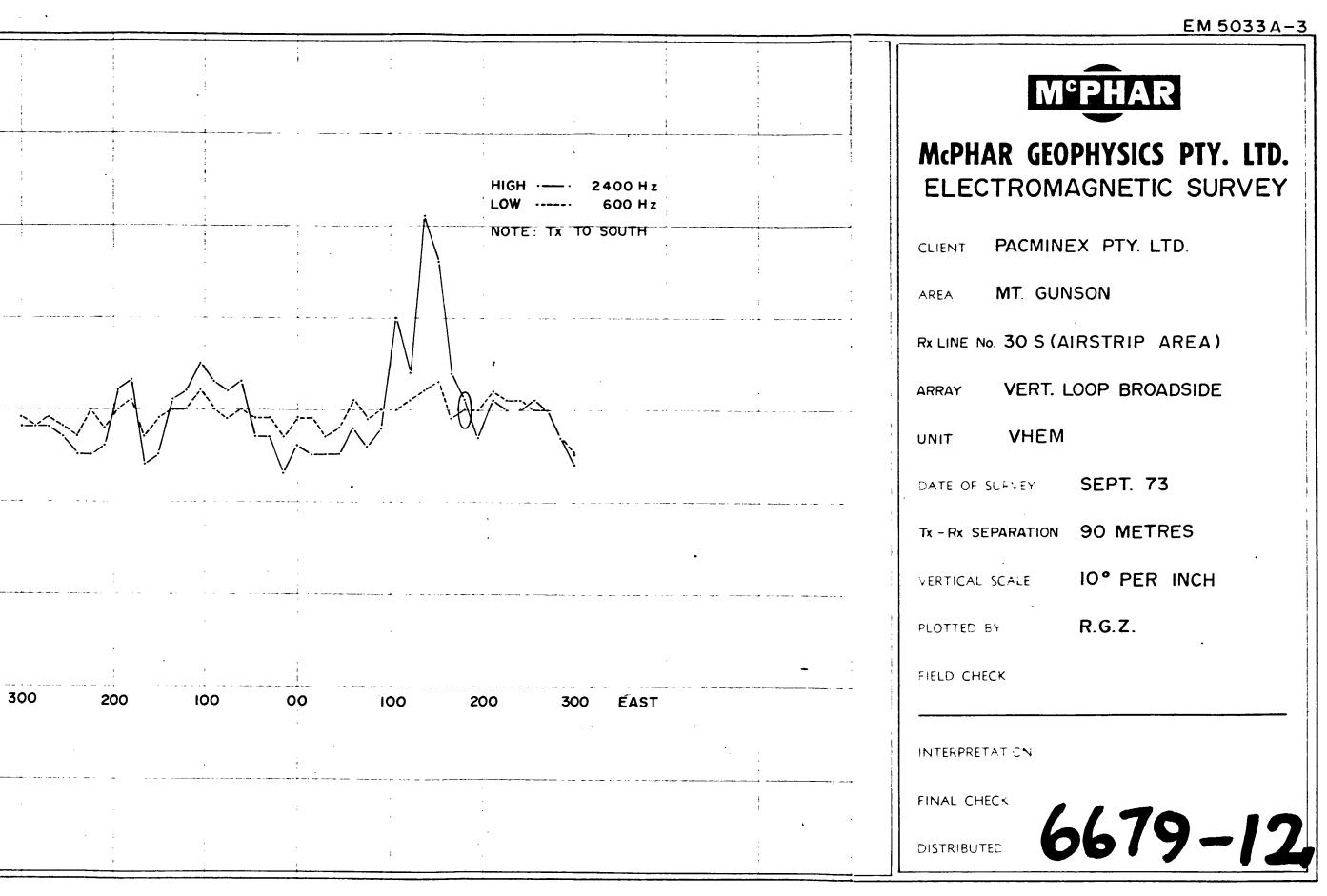


SOUTH 20 10 3 3 4 00 10 10 10 10 20 10 20 10 20 10 20 10 20 10 20 20 20 20 20 20 20 20 20 20 20 20 20				
SOUTH 20 				
SOUTH 20- -00-				
20 - 				
20- 10- 3 4 00- 3 10- 10- 20- 10- 20- 10- 20- 10- 20- 20- 20- 20- 20- 20- 20- 2			SOL	JTH
- 0- - 0 - 0 - 0 - 0 - 0 - 0 - 0				
10 - 9 9 00 - 6 10 - 20 20 NORTH SOUTH 200)
10 - 9 9 00 - 6 10 - 20 20 NORTH SOUTH 200				
10 - 9 9 00 - 6 10 - 20 20 NORTH SOUTH 200				
10 - 9 9 00 - 6 10 - 20 20 NORTH SOUTH 200				
а а ио го го го го го го го го го го го го го			HC	>-
а а ио го го го го го го го го го го го го го				
й оо в 10- 20- 20- холтн 200тн 200			S	
а 10- 20- SOUTH 200			9 T B	
а 10- 20- SOUTH 200			AN OC) -
10 - 20 - NORTH SOUTH 200				
20 20 NORTH SOUTH 200	•		ā	
20 20 NORTH SOUTH 200		_		
20 NORTH SOUTH 200			10) -
NORTH SOUTH 200				
NORTH SOUTH 200				
NORTH SOUTH 200				
NORTH SOUTH 200			- 20)
NORTH SOUTH 200				
SOUTH 200			NOR	TH
SOUTH 200				
			500111	200
			•	

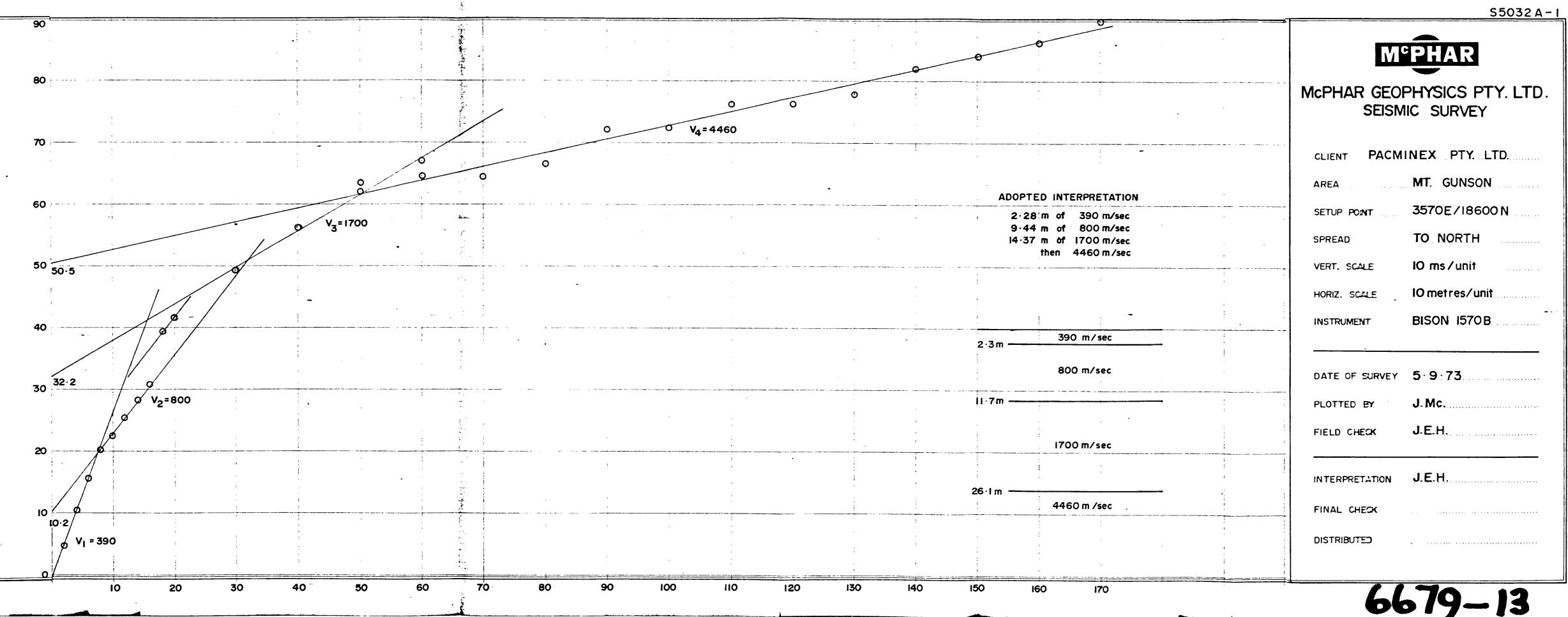
· •

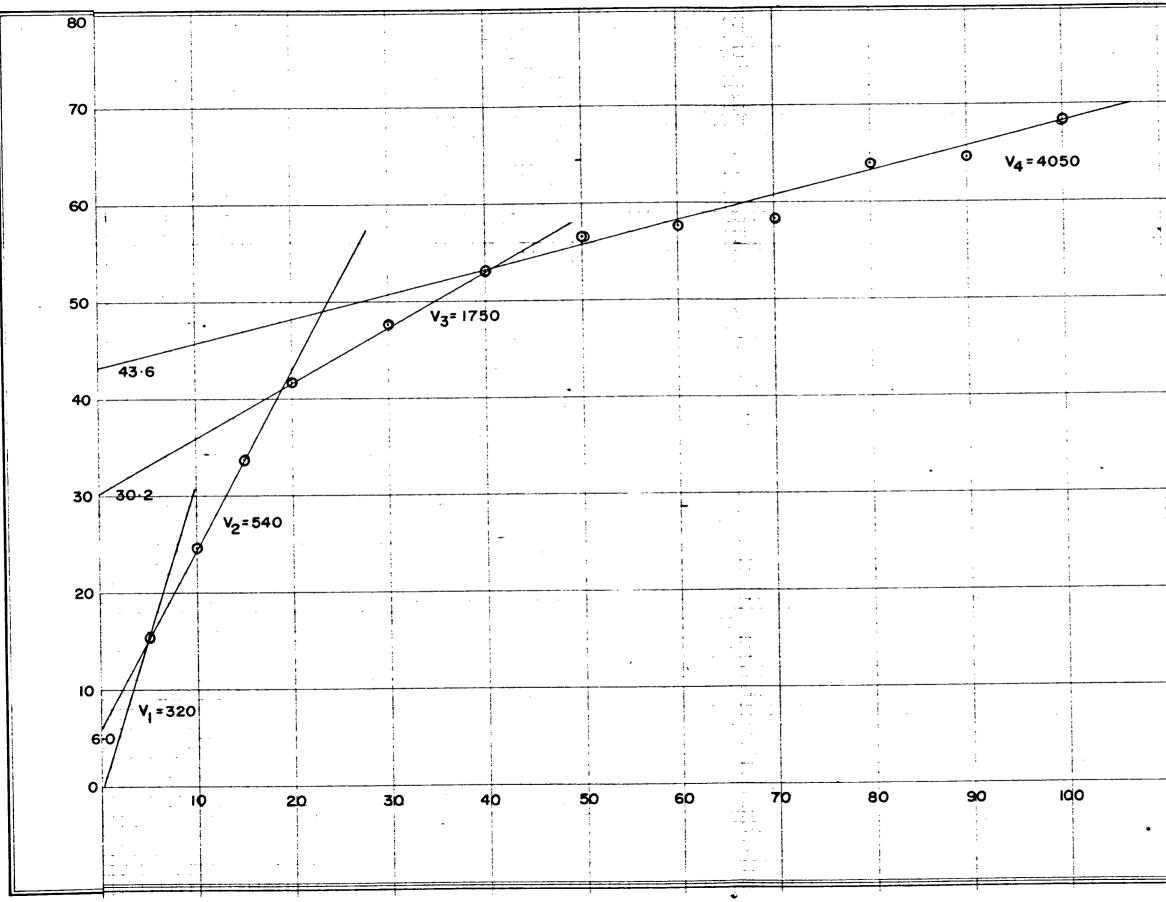


 		· · · · · · · · · · · · · · · · · · ·			·					
, ; }				}	· · ·	·····	······································		······································	
! .		: !	1 1	1) ,	•			:	
· ·		1		1 1 1			:		:	
; 	; 		<u> </u>	<u>i</u>	i 		•			
		• •		; ; ;					•	
•		1					:			
		к				1	:		WEST	
· ·····		· · · · · · · · · · · · · · · · · · ·		• •	;		• •			
			•	2	• •		:			
				•						
		· ···	: 1 	1 	° † • • • = • • • • • • • • • • • • • • • •	••• •• •• •• •• ••	• • • • • • • •			
					t ¦					
					,					
		•								
·····			* ••··•	, • <u></u>					n -00 -	
			!						- 00 - ת ע נ	
									Z A	
	•		·						<u>- +0</u> e	
· ·				1				· · · · · · · · · · · · · · · ·		
				i	•					
			4	, , 1 ,						
		· · · · · · · · · · · · · · · · · · ·	4 2 4	•	•. • • = • • • • • • • • •	• · · · · · · · · · · · · · · · · · · ·	• ··•······	· · · · · · · · · · · · · · · · · · ·	20°-	
			· *							
			•	•						-
			1			-				. /
		· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·		<u>.</u>	•	<u></u>		30°-1	WEST 3
			1		1	-			EAST	
			:	1						
							1 			
	:	1		۱ -		• •	: .			
	:		• •			.				
					: :		• • •		•	

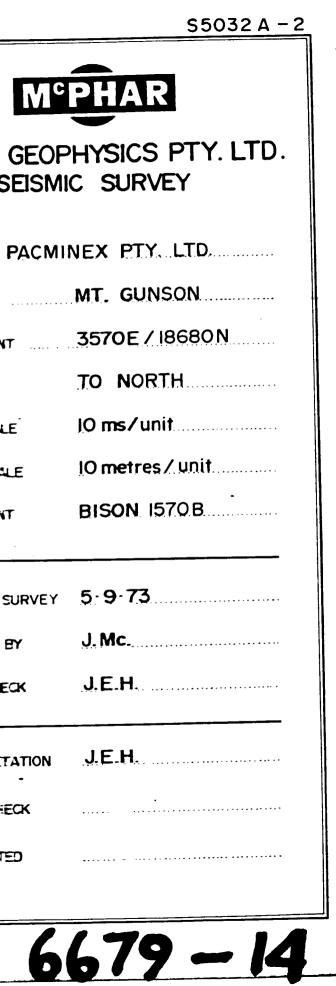


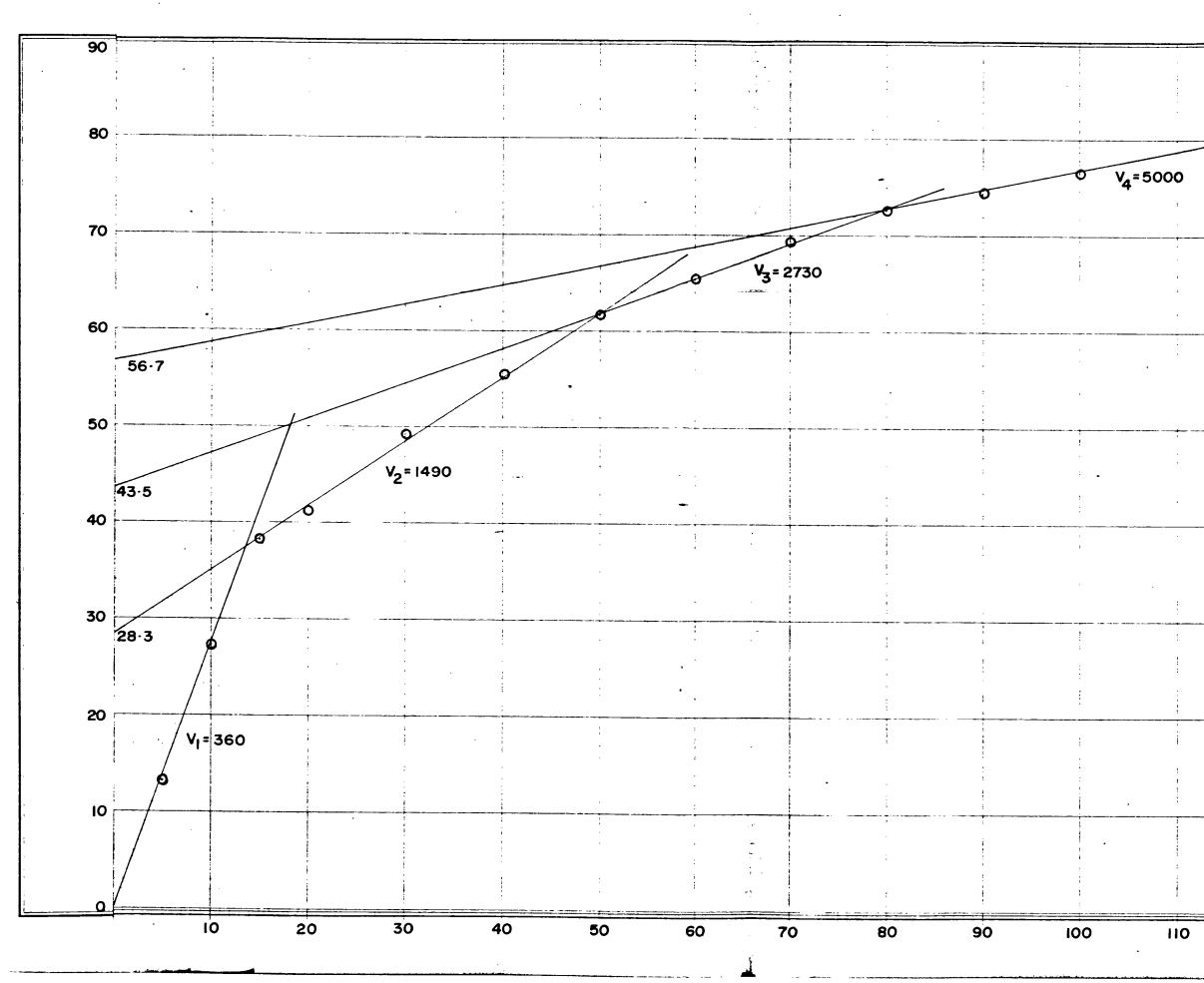
·····



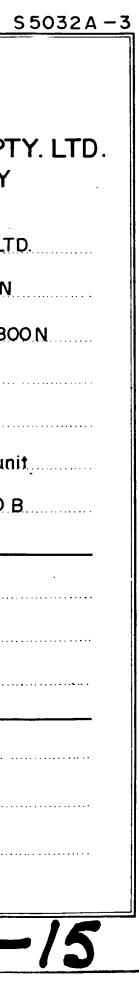


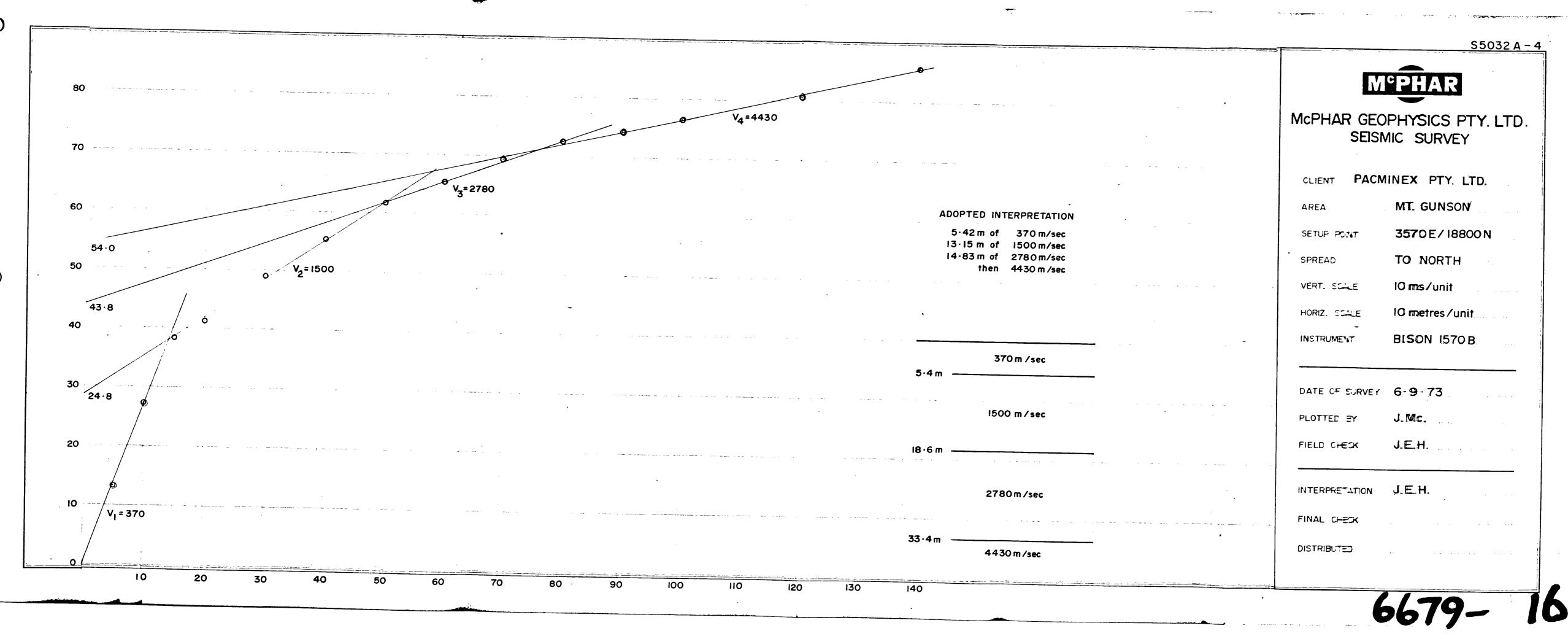
			<u> </u>						Mc	PHAR
-			•				-		McPHAR GEOF	PHYSICS PTY
	:		- - -				-			IC SURVEY
	· -		:	1	-		-			
						-			CLIENT PACMI	NEX PTY. LTD.
									AREA .	MT. GUNSON
	1 1		• 2.38	m of 320 m					SETUP PONT	3570E / 18680
		· ·	4·42 12·18	m of 540 m	n/sec			-	SPREAD	TO NORTH
				then 4050 r			•		VERT. SCALE	<u>IO ms/unit</u>
		-		- 		• • •			HORIZ. SCALE	10 metres / unit
	t			· · ·	1	1 1 1 1			INSTRUMENT	BISON 1570B
			2·4 m	320 m/sec			·	-		
				540 m/sec	2 4 4 4	-			DATE OF SURVEY	5.9.73
		• •	6·8 m							J. Mc.
				1750 m/sec			•		PLOTTED BY	
	•	:	19.0 m				2 4 8 7 7 7		FIELD CHECK	J.E.H.
				4050 m/sec			, , , , ,			J.E.H.
					1 (2) 2) 2) 2) 2) 2) 2) 2) 2) 2)	- - -	•		INTERPRETATION	<u>, y. L. 1</u> I.
	, :			1	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	·		FINAL CHECK	• •·····
	; ; ;							-	DISTRIBUTED	·····
		1 1 1	-							
	•	!	1	1 	1				₹ ↓	



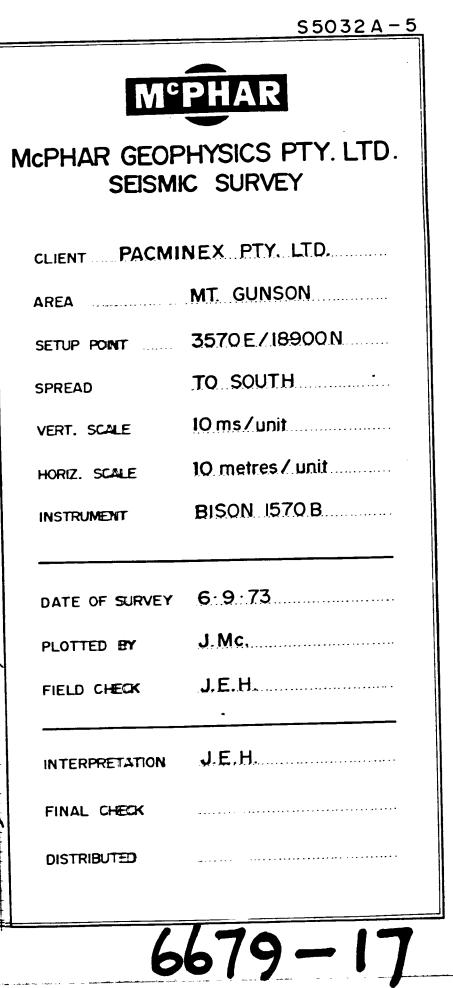


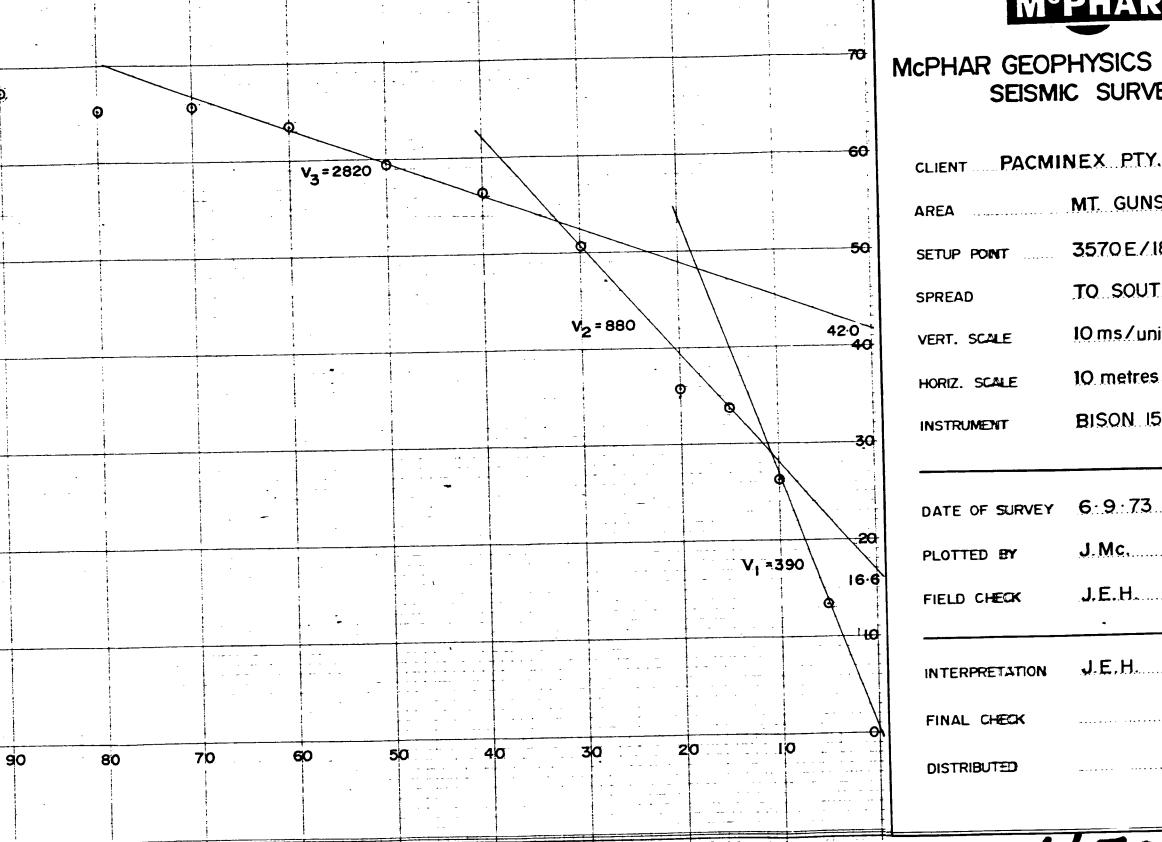
:		•			1 - - -		Μ	PHAR
0				· · · · · · · · · · · · · · · · · · ·	:		_	PHYSICS PTY.
· · · ·	•	ADOP	TED INTERPRETATION	:	-		SEISIV	IIC SURVEY
		12 · 97	5 m of 360 m/sec 7 m of 1490 m/sec				CLIENT PACM	INEX PTY. LTD.
	• •	-	m of 2730 m/sec then 5000 m/sec	!		· ·	AREA	MT. GUNSON
							Setup point	3570E/18800.N
•	:		<u></u>		•	· · · · · · · · · · · · · · · · · · ·	VERT. SCALE	10 ms/unit
	•	5.3m -	360 m/sec		;	· · ·	HORIZ. SCALE	10 metres / unit
· · · · · · · · · · · · · · · · · · ·			1490 m/sec	-	· · · · · · · · · · · · · · · · · · ·	-	INSTRUMENT	BISON 1570 B
	-	18·2 m				-	DATE OF SURVEY	6-9-73
	-				•		PLOTTED BY	J.Mc.
	•		2730 m/sec			•	FIELD CHECK	J.E.H.
							INTERPRETATION	J.E.H.
		36·1m —	5000 m/sec			-	FINAL CHECK	·····
:	*						DISTRIBUTED	<u></u>
120	130	140	<u> </u>	1			6	679-1

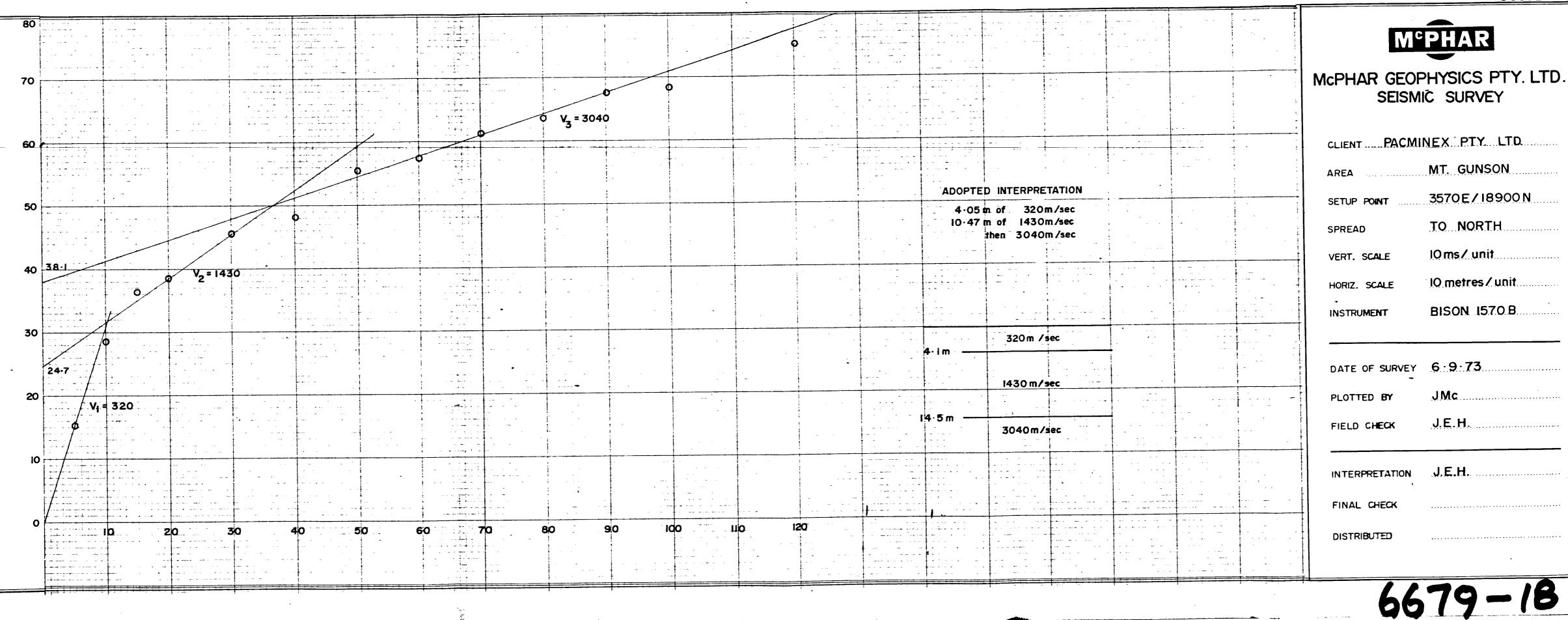


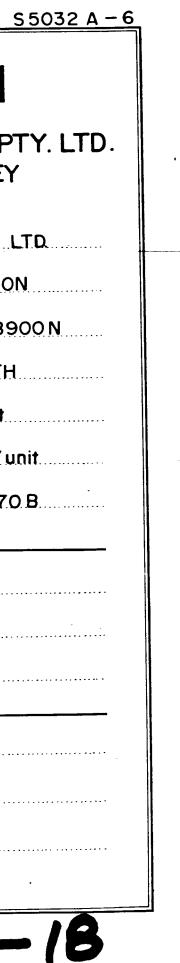


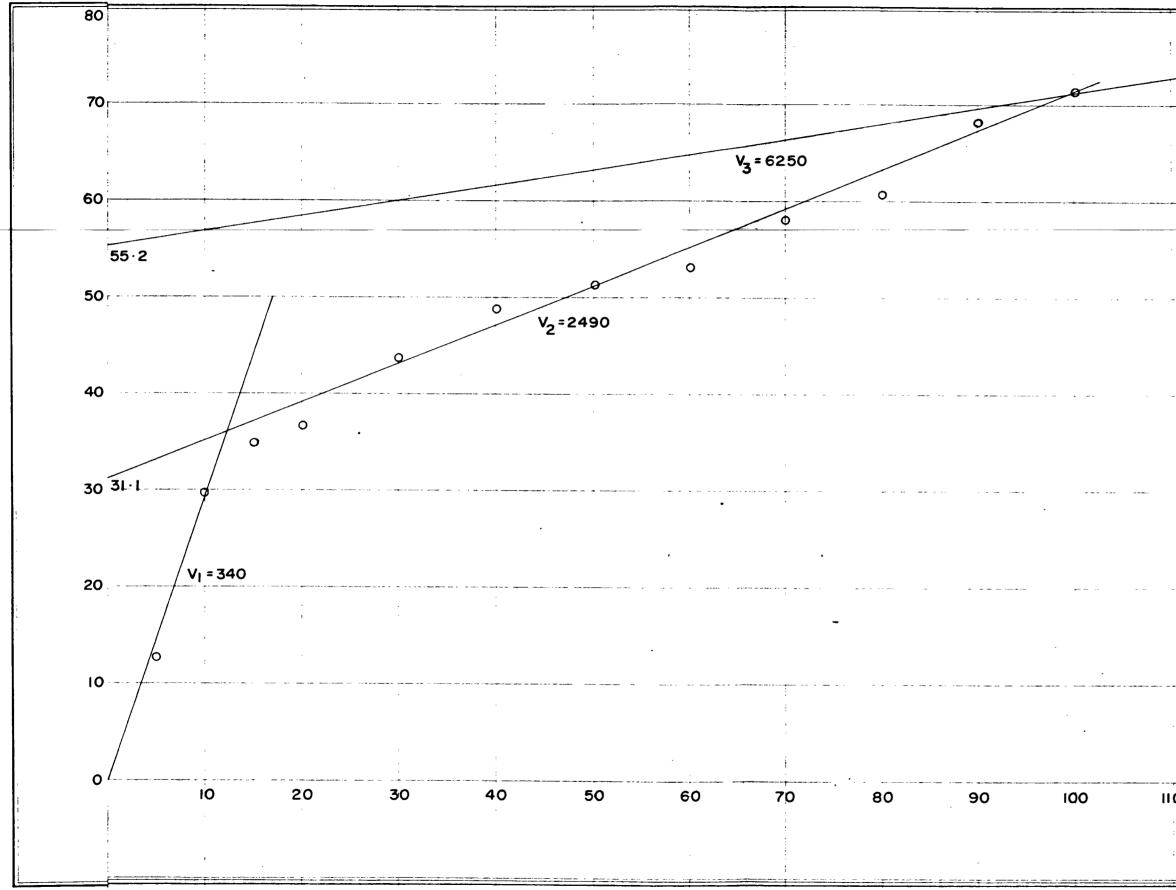
						(3) 				
-			-						•	-
		· ·		· · · · · ·						
						-	ADOPTED	INTERPRET	ATION	
			-		-		3-61 m 10-96 m the	of 880 m	/sec -	
-	•								-	
							3.6 m —	390 m∕se 880 m∕se		
	-					\$. 	14·5 m	2820 m/se		
				· · · ·						
									IQ	9_
					; ;					









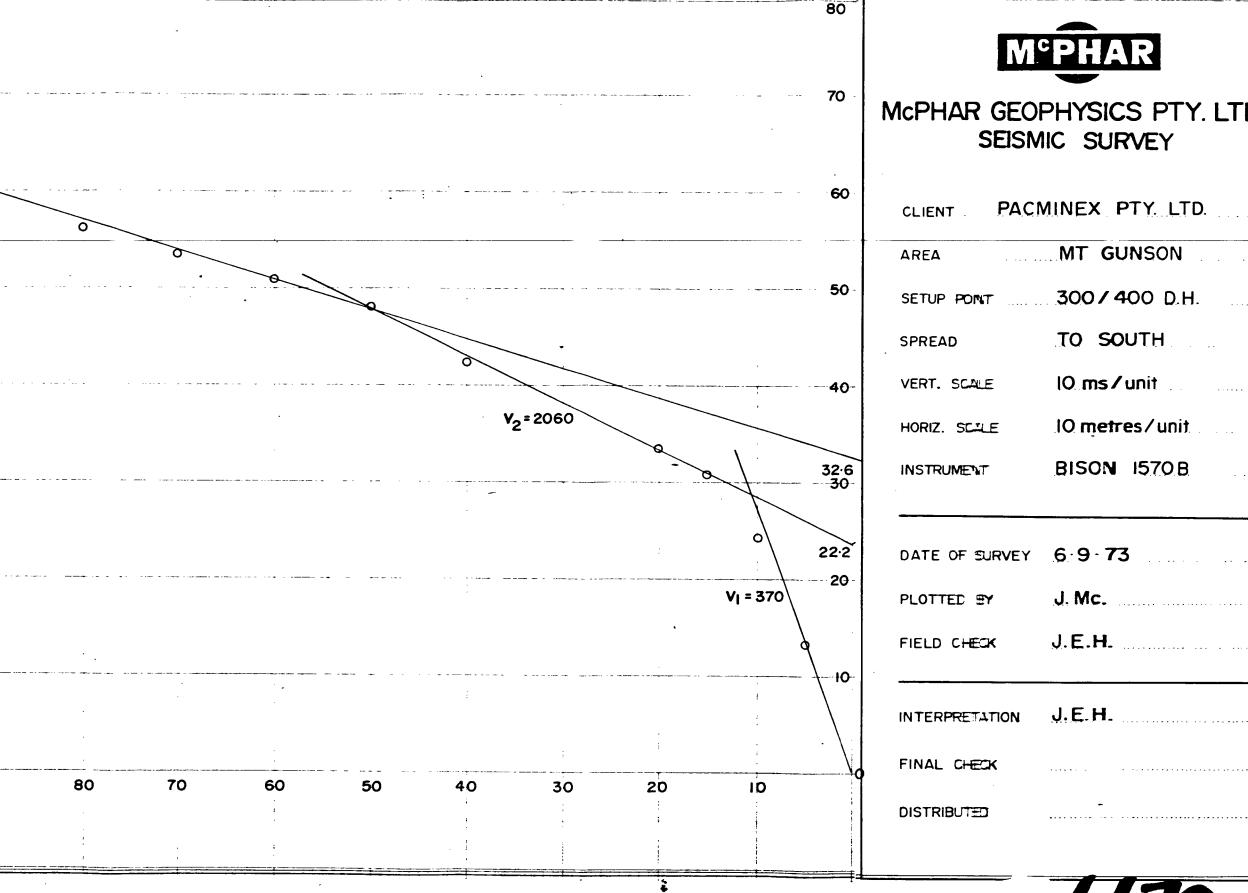


S 5

			•	· · · · · · · · · · · · · · · · · · ·					
:	0		- 1		· · ·	•		M°	PHAR
								McPHAR GEOF	
			·			:	4 • •		IC SURVEY
:		:	:	۰	· ·				
				1 - 3		• ·	:	CLIENT PACN	INEX PTY. L
								AREA	MT. GUNSON
				ADOF	TED INTERPRETATION)N			3570 E/1900
		,			34 m of 340 m/sec 35 m of 2490 m/sec			SETUP POINT	3370E/1900
				32.	then 6250 m/sec			SPREAD	TO NORTH
								VERT. SCALE	IO ms/unit
					340 m/sec			HORIZ. SCALE	10 metres/un
				5·3m —	<u></u>			INSTRUMENT	BISON 1570
•	••••••						•		-
		•					۰	DATE OF SURVEY	5.9.73
								DATE OF SURVET	J J(.J
	•		•		2490 m / sec		1	PLOTTED BY	J. Mc,
				i	: :		-	FIELD CHECK	J.E.H.
		•	; 	1 1 					
		:	:				i :	INTERPRETATION	J.E.H.
			:	37·7 m ~				FINAL CHECK	
0	120	130	140	•	6250 m / coc			FINAL GREAN	
			!		:		:	DISTRIBUTED	
ι.				- - -	•				
					<u> </u>				.79_
	-								n/7-

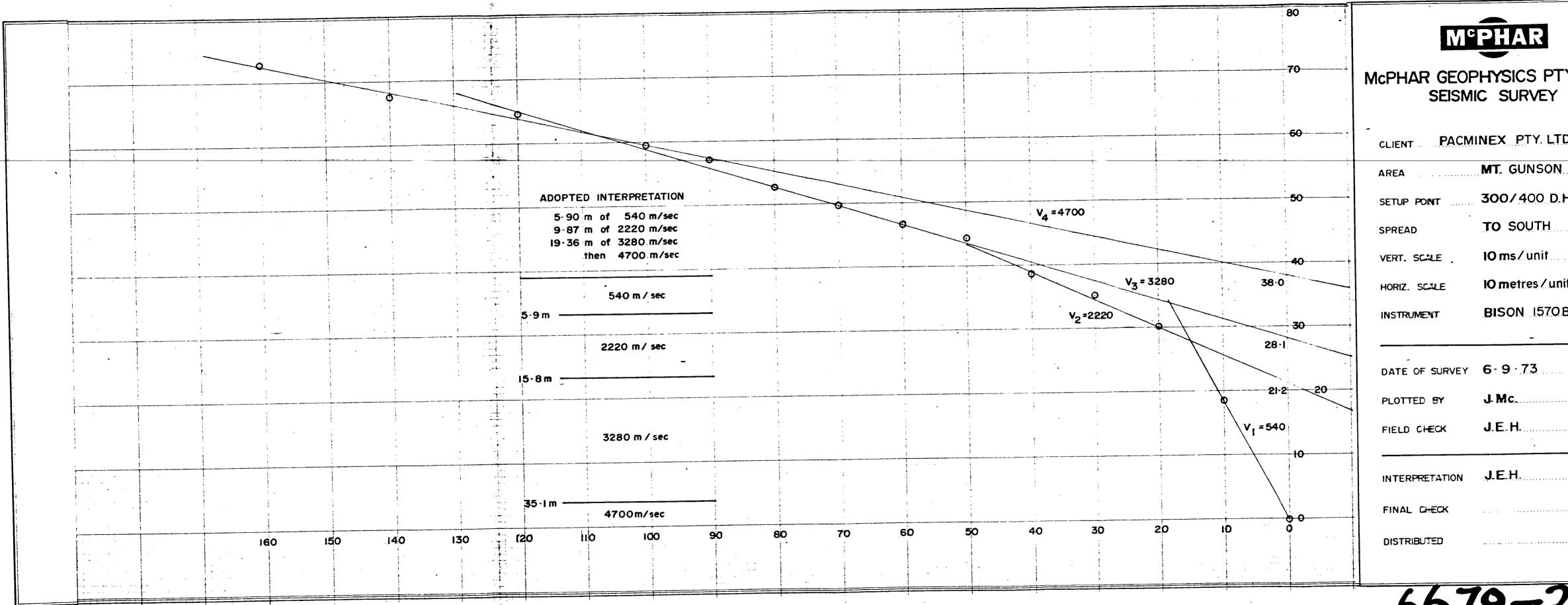
، د د ب ورو و میکورو و د در و میکورو و د در و میکورو و م	agaan taan taan ahaa sa
5032A - '	7
·	
Y. LTD.	
ΓD.	
······································	
D.N.	
····· ·	
t	
8	
. .	
<u> </u>	
	
	E .
10	
17	

					:	9 7 -	٠		:		
	!					:					
		-	۰.						,		
	r			·							
	1				\$ •	i	,	TO			
		1				·			V3=327	0 0	
	1 		······································				· · · · · · · · · · · · · · · · · · ·		.		
	1	1									
		:									
.	*										
						ADOP	TED INTERPRETATIO	N	.		
						4-:	20 m of 370 m/sec				
						13-	5 m of 2060m/sec				
	·			•			then 3270m/sec				
	, ,		· ·			•					
		1	i				:				
						INTERPRE	ETED SECTION CORR	ECTED			
			- 				FOOT STATION INTE		•		
		1 1 	• •	·		-	;	· · · · · · · · · · · · · · · · · · ·			
	:	1		-			300 m/ sec				
		1 2		1 1	•	3·4m —	· · · · · · · · · · · · · · · · · · ·				
		1			•						
	·	; ; ;	÷	·			1440 m / sec	•			:
	ł					,	4		· · · · · · · · · · · · · · · · · · ·		
				ŧ		14 6 m —	· · · · · · · · · · · · · · · · · · ·				
						• :	2690 m/ sec		•		
	·								;		
, ,	Í							· · · · · · · · · · · · · · · · · · ·			· ·- ·- ·- · · · · · · · · · · · · · ·
	•			,	i	•				•	
				1							
			-	, 1		د :	-	•	1		
				1	1			120	110	100	90
	-				1		. 1	:		4	
	-				4 1	, ,					
					4 1 1				4 3	:	,



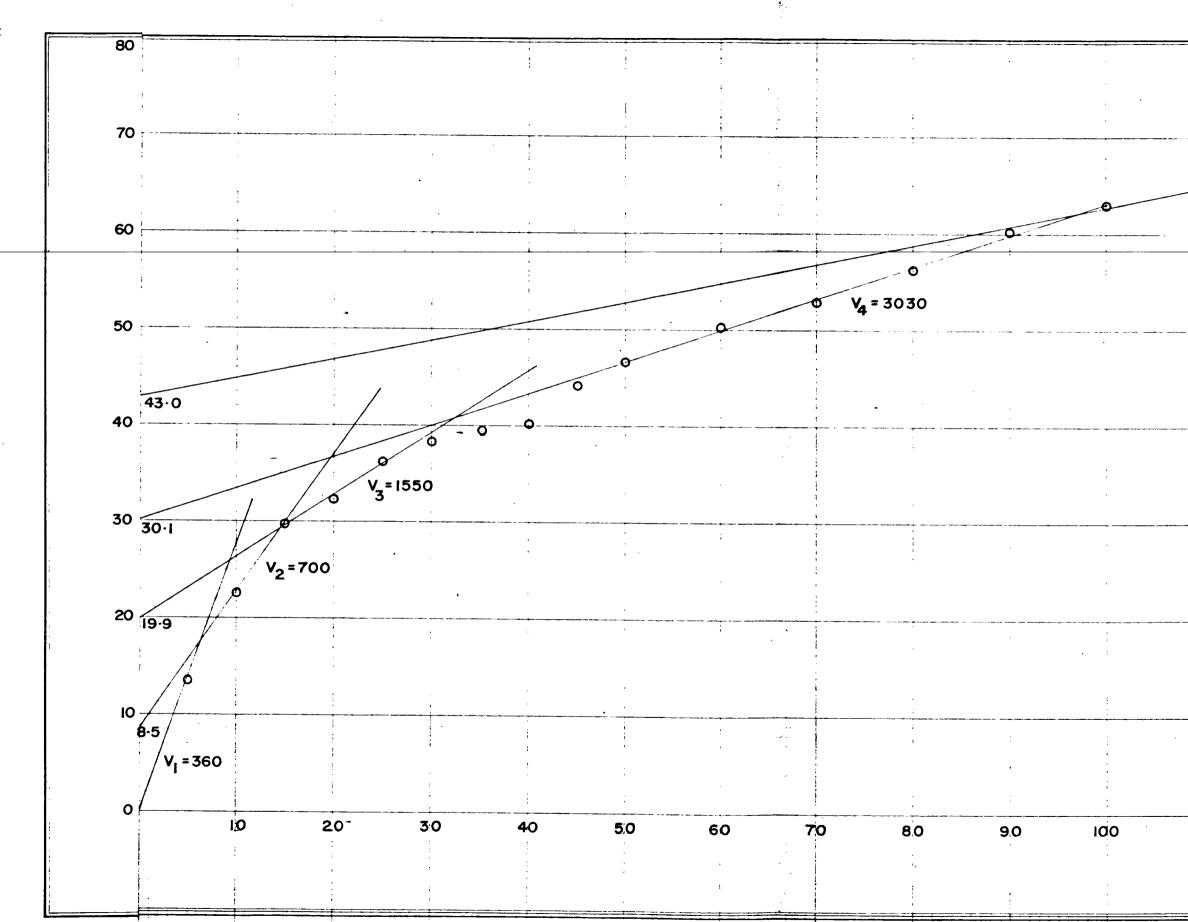
.

5032A-8	1
Y. LTD.	
⁻ D	
-	
·	
· · · · · · · · · · · · · · · · · · ·	
7-7	

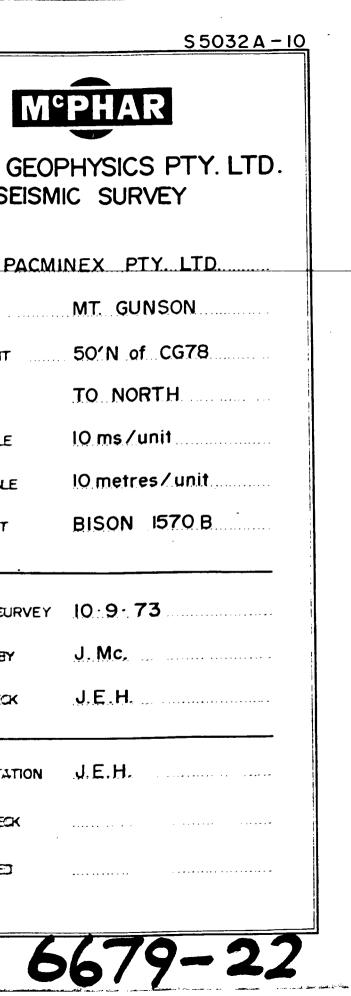


6679-21

<u>5032 A - S</u>	€
Y. LTD.	
D.	
Η,	
·	
it	
B	
·····	



· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·		-				· · · · · · · · · · · · · · · · · · ·		
									SEISN	IIC SURVEY
:			ADOPTED		TATION				AREA	MT. GUNSC
			I • 78 m 4 • 03 m 8 • I 9 m t	of 700	m/sec			,	SETUP POINT	50'N of CO
	· ·	ł	INTERPRETED FOR 27 FOO	T STATION	INTERVAL			:	HORIZ. SCALE	10 ms/unit 10 metres/u BISON 157
:	:		l·5 m ─── 4·8 m ───	<u>300 m /s</u> 580 m /s	sec			1 • •	DATE OF SURVEY	10-9-73
			11·5 m	2490 m/:	sec		1		PLOTTED BY	J. Mc, J.E.H.
							· • • •		INTERPRETATION	J.E.H.
	•			<u></u>		1	:		DISTRIBUTED	······································
			· · ·				: :		1	

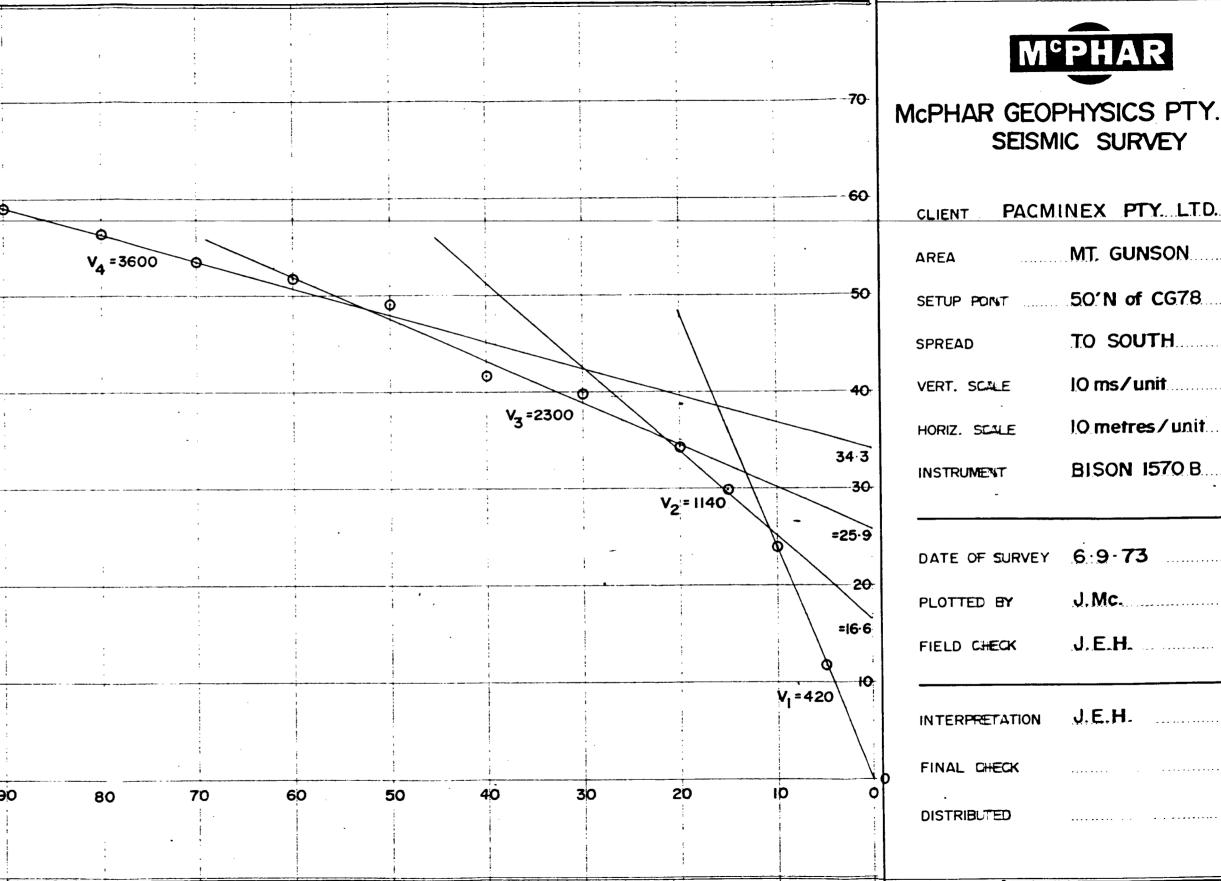


•		-			· · · · · · · · · · · · · · · · · · ·						
		- 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2			· · · · · · · · · · · · · · · · · · ·						:
		· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·		:	}				•	
						1 			:	0	;
			÷		1						¢
		2		-	- - - -	2 8 8			:		
		i					•	ADOPTE	D INTERPRET	ATION	
	-			• • 1			• •	5-48	m of 420 m m of 1140 m m of 2300 m	/sec	• • • •
			:					•	then 3600 m		
		 ₹	· · · ·	,	• •		-				:
		· · · · · · · · · · · · · · · · · · ·	•	· •	4 • •	•	· · ·		ED SECTION CO DOT STATION		:
	· · · · · · · · · · · · · · · · · · ·				•	•			345 m/sec		
	, f 1	•			: : .		- • } •	7.6m	940 m/sec	: 	
	, , ,	;	· ·	• • •	· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·			•		
	• 1 1				;	· ·	• • •	- - 	1890 m/sec		
			•		•	• • •		16·7m	2960 m / sec		
	-	•		• • E	: .		۱.		2300111736	•	
			1 † †	:	1	4 • •					
	₽ } ₽			: : :		;	· · · ·		· · ·		
2 0 1				:		•		-		IQO	9
- -						f - -					
		 		; ;	: - <u>FCEF</u> F	: . 				·	at and a second
							-				

• • • •

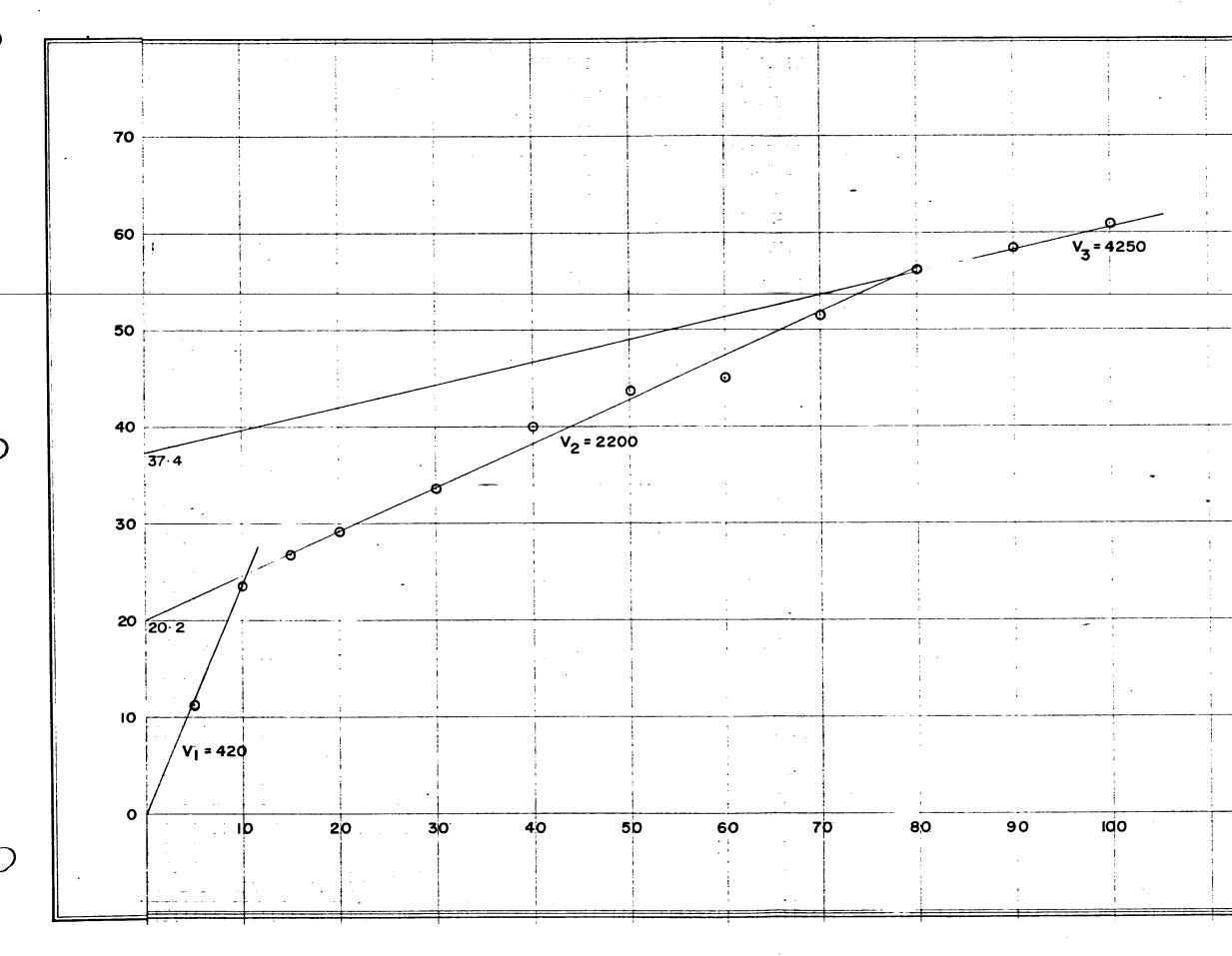
.

and the second states

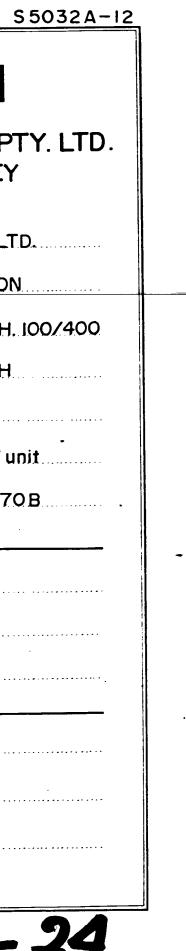


6679-23

<u>)32A – I</u>	
. LTD.	
)	
	•.
••••••	
•	
<u> </u>	
······	
• • • • • • • • • • • • • • • • • • • •	
· · · · · · · · · · · · · · · · · · ·	
2	



								M°	PHAR
:							 		PHYSICS PTY. LTD. IC SURVEY
•	:		· · · · · · · · · · · · · · · · · · ·				 	CLIENT PACMI	NEX PTY. LTD.
		· · · · · · · · · · · · · · · · · · ·	4∙32 2I∙2	D INTERPRE m of 420 m m of 2200 m then 4280 m	m/sec m/sec			setup point	60' N of D.H. 100/400 TO NORTH
		-	INTERPRETE FOR 27 FO	D SECTION OT STATION		· · · · · · · · · · · · · · · · ·		VERT. SCALE HORIZ. SCALE INSTRUMENT	IO ms/unit IO metres/unit BISON 1570B
-	•	• • •	3.5m ←	345 m/s	ec			DATE OF SURVEY	6 - 9 - 73 -
		•	· · · · · · · · · · · · · · · · · · ·	1810 m/s	Sec .	- -		PLOTTED BY FIELD CHECK	J.Mc. J.E.H.
•	•		21·0 m ——	3520 m∕s	sec			INTERPRETATION	J.E.H.
	• •						•	DISTRIBUTED	·····
		! 						66	79-24



V ₂ =2220 o 100 90 80					and the second se					
N ₂ =2220 o N ₂ =2220 o 100 90 80		4								
V ₂ =2220 o					•					
V ₂ =2220 o V ₂ =2220 o 100 90 80			· ···· - · · · · · · · · · · · · · · ·		e		×			
V ₂ =220 o 100 90 80										
V2=2220 8								Ø		
V ₂ =2220 0 100 90 80									a	
									V =22	20
100 90 80									. 2	
B0 90 80	·	·····	• • • • • • • • • • • • • • • • • • • •		•				• • • • • • • • • • • • • • • • • • •	
00 90 80										
08 0e 00l										
100 90 B0	· ·		· · · · · · · · ·			<u>.</u>				
100 90 B0										
100 90 80										
08 06 001				· · · · · · · · · · · · · · · · · · ·	- • • • • • • •			-		
100 90 80				· · · · · · · · · · · · · · · · · · ·	- • • • • • • •			-	·	
100 90 80				· · · · · · · · · · · · · · · · · · ·	- • • • • • • •			-		
100 90 80	-	• • • • • • • • • • • • • • • • • • •	-	· · · · · · · · · · · · · · · · · · ·				- 		
100 90 80	-	• • • • • • • • • • • • • • • • • • •	-	· · · · · · · · · · · · · · · · · · ·			 	-		
100 90 80 I		• • • • • • • • • • • • • • • • • • •	-	· · · · · · · · · · · · · · · · · · ·						•
100 90 80 I	-	• • • • • • • • • • • • • • • • • • •	-	· · · · · · · · · · · · · · · · · · ·			<u>-</u> .	-		
IOO 90 80 1	-	• • • • • • • • • • • • • • • • • • •	-	· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	•
100 90 80		• • • • • • • • • • • • • • • • • • •	-	· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	• •
		• • • • • • • • • • • • • • • • • • •	-			· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	·····		
			-			· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·			
			-			· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·			80

.

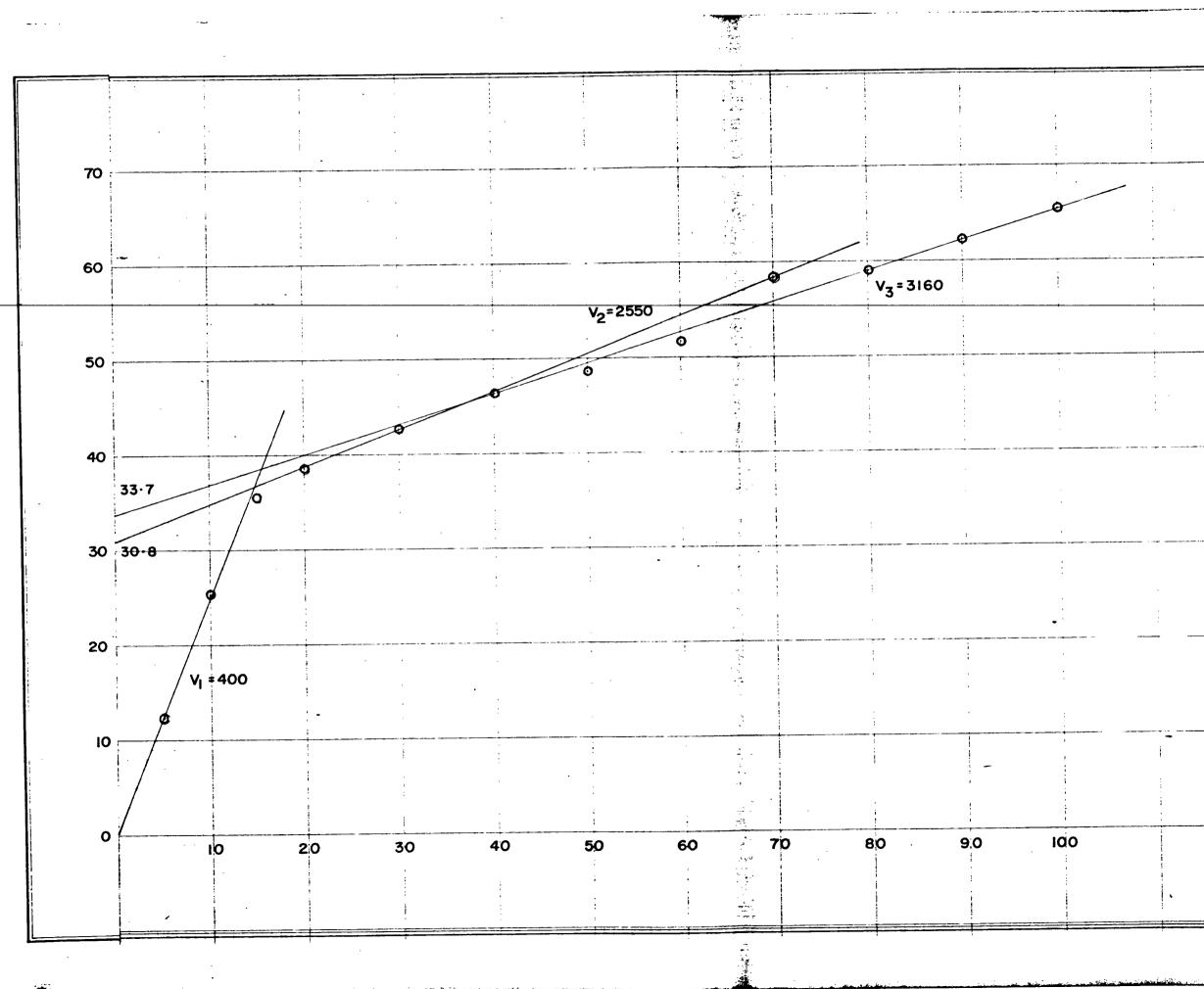
.

			<u>, , , , , , , , , , , , , , , , , </u>				<u>\$5032A-1</u>
							70 MCPHAR GEOPHYSICS PTY. LTD. SEISMIC SURVEY
=2220 0					···· ·· ··· ·· ·· ·· ·· ·· ·· ·· ·· ··	(60 CLIENT PACMINEX PTY. LTD.
a a							AREA MT. GUNSON
	8	•				·	50 SETUP POINT
		ँ					SPREAD TO NORTH
	•		0	8	·		40- VERT. SCALE IO ms/unit
					````		HORIZ. SCALE IO metres/unit
						3	30- INSTRUMENT BISON 1570 B
				-		ð	DATE OF SURVEY 6.9.73
	•					\	PLOTTED BY J.MC.
							FIELD CHECK J.E.H.
		•		- <u>-</u>			INTERPRETATION J.E.H.
				:			FINAL CHECK
80 70	<b>60</b>	50	40	30	20	10	DISTRIBUTED
					•		

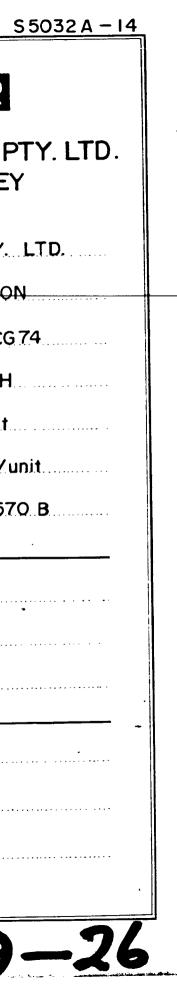
-

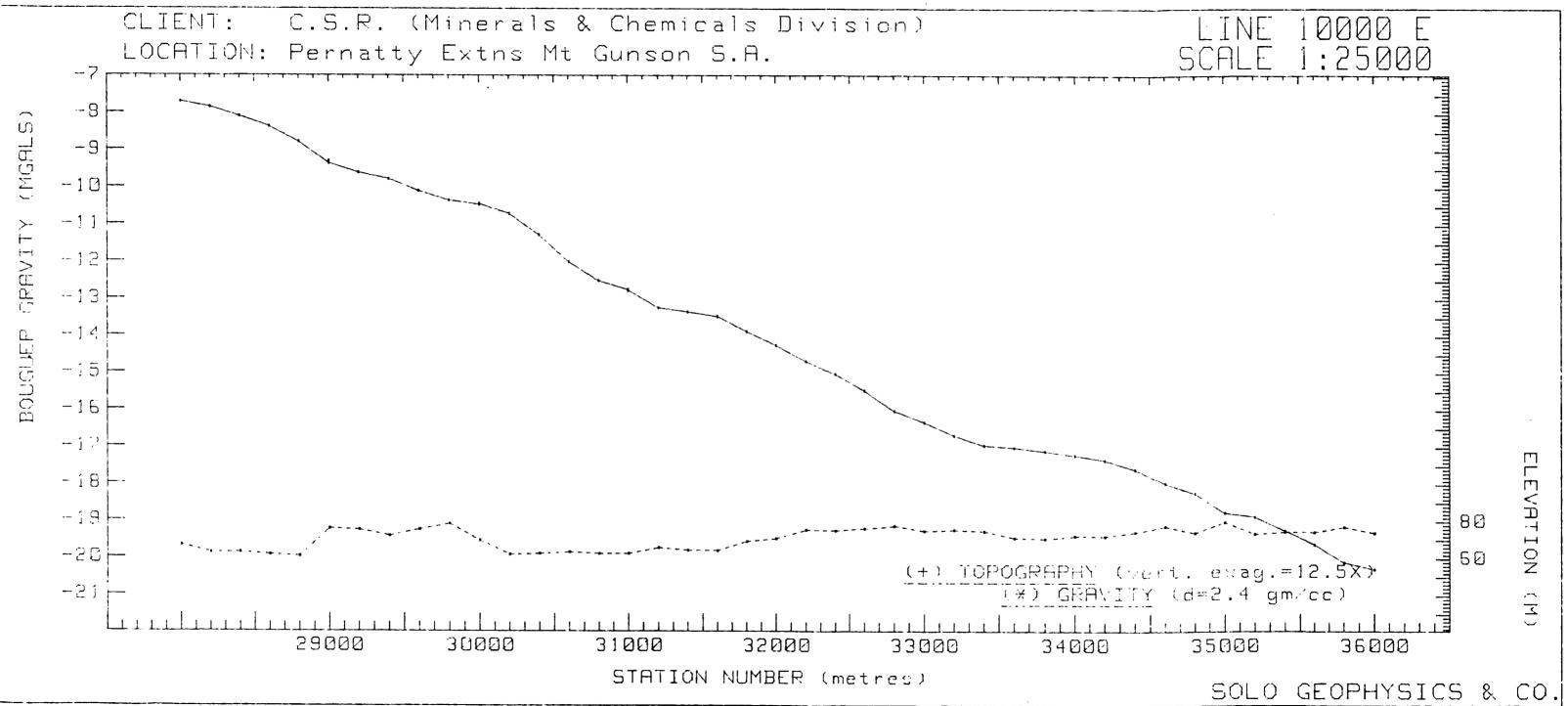


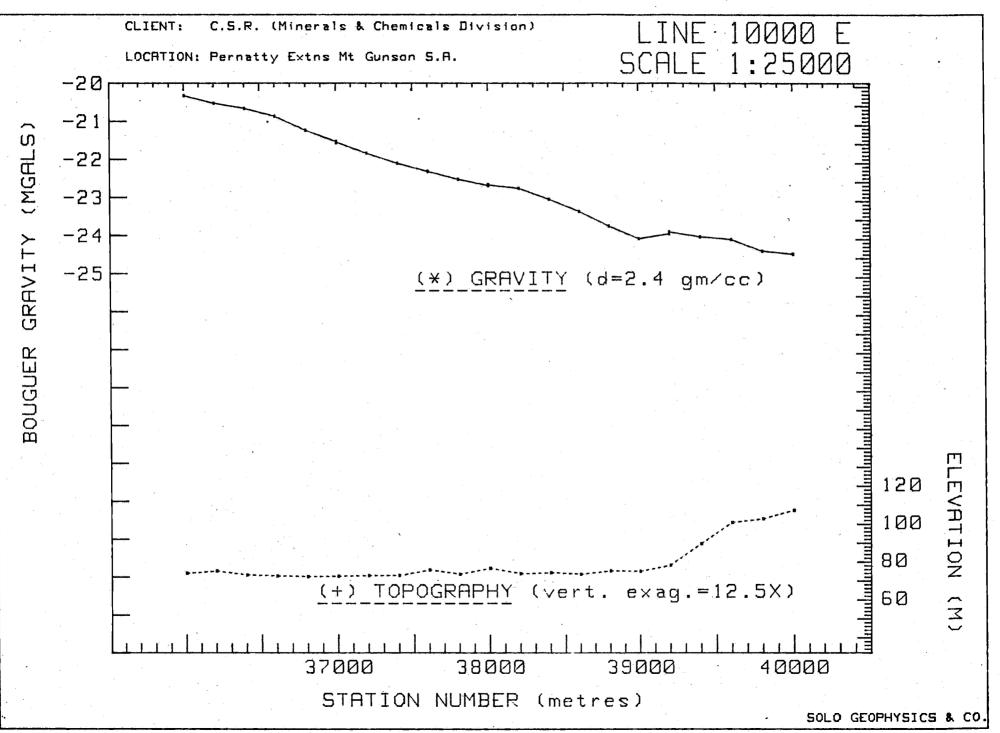
------

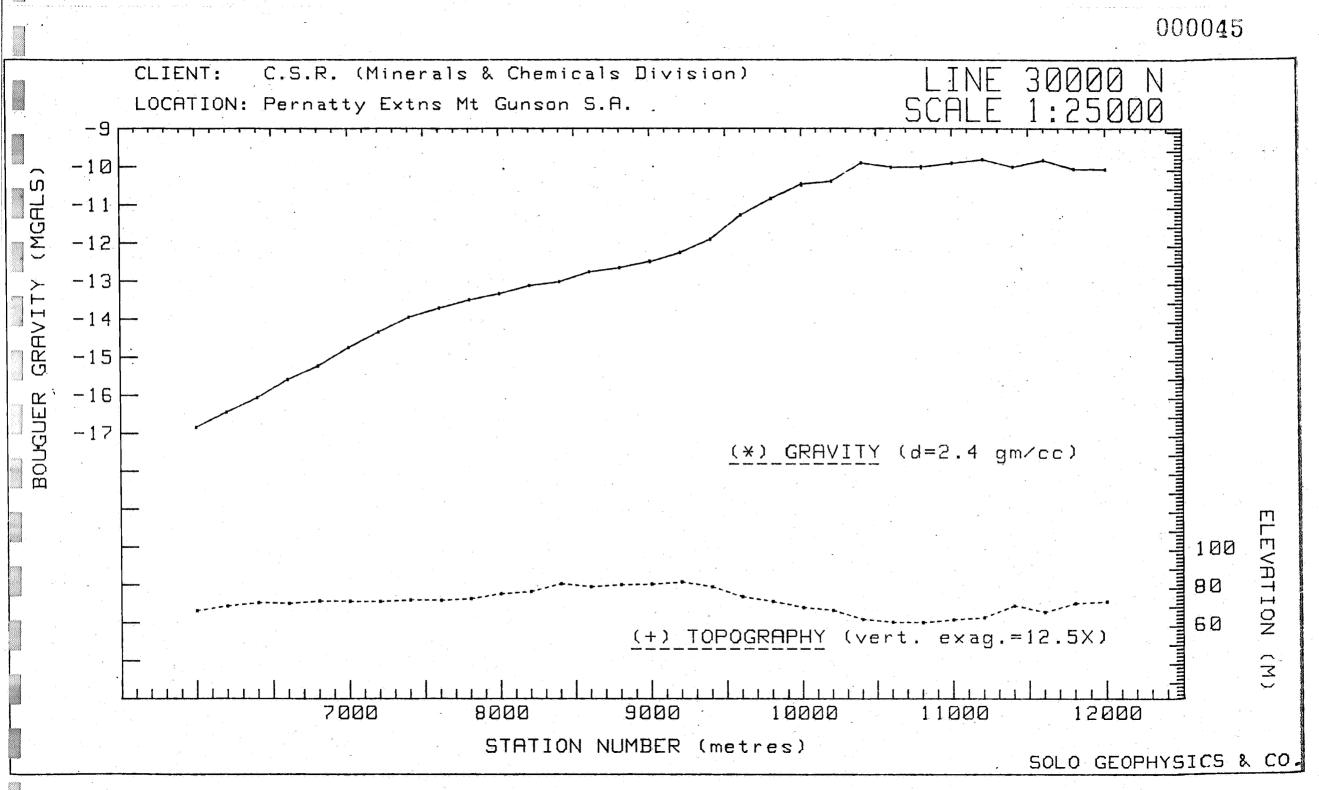


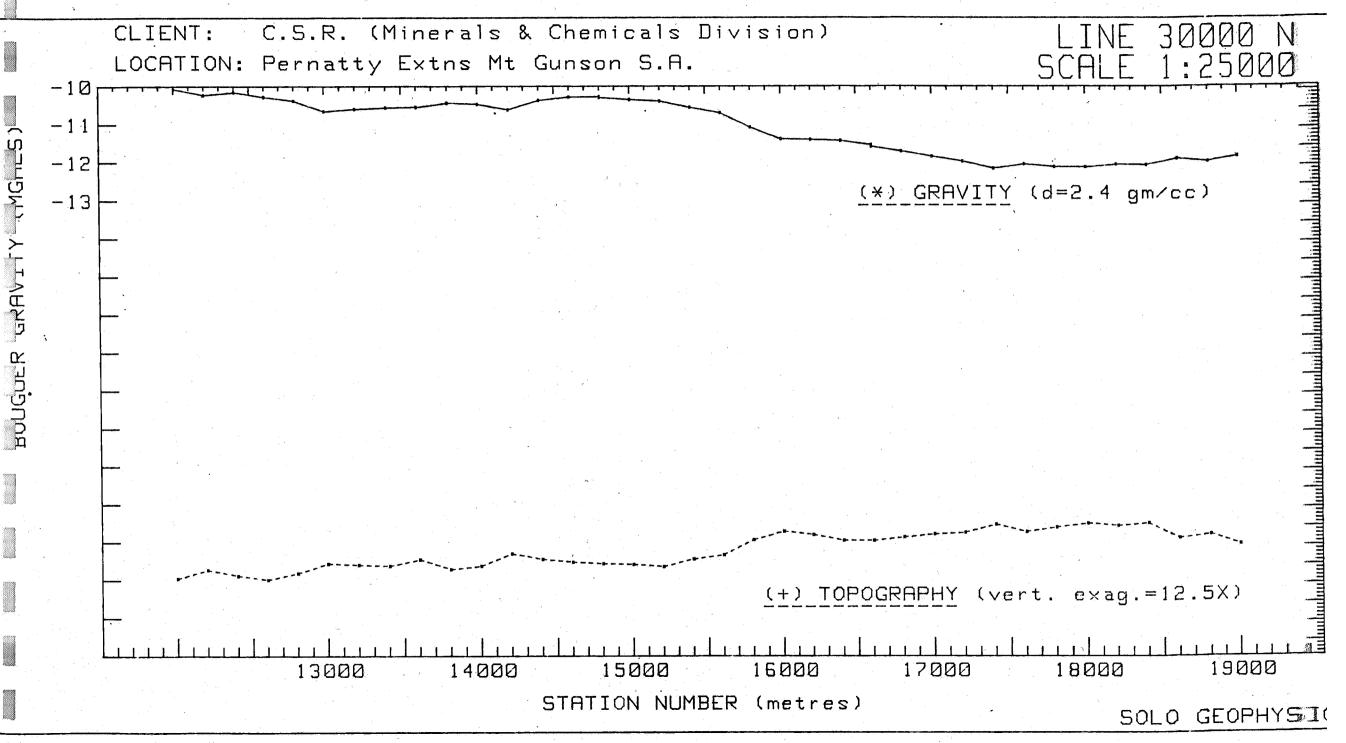
	· · ·						:		M°	PHAR
			۱ 							
	•		:	:					McPHAR GEOF SEISM	IC SURVEY
						:				
	<u>.</u>		· · · · · · · · · · · · · · · · · · ·			•			CLIENT PACM	INEX PTY. LTC
	•	i				·	; ; <del>;</del>	•	AREA	MT. GUNSON
		:	ADOPTE		TATION	, , 1				
				m of 400		, , ,	1		SETUP POINT	40'S of CG74
		•		m of 2550 then 3160		· · ·			SPREAD	TO NORTH
			:		:			•	VERT. SCALE	10 ms/unit
	-		INTERPRETE		CORRECTED	) )	1		HORIZ. SCALE	10 metres/unit.
		•	FOR 27 FO				· · ·	•	INSTRUMENT	BISON 1570 B
-		· · · · · · · · · · · · · · · · · · ·		330 m /	sec		· ·			
			5·1 m	2100 m/s	sec				DATE OF SURVEY	6·9·73
			-i0·0·m	2600 m /	sec		:	· · · · · · · · · · · · · · · · · · ·	PLOTTED BY	J.Mc.
		• • •		· · ·		:	, , , ,	; · · ·	FIELD CHECK	J.E.H.
	<u> </u>				· · · · · · · · · · · · · · · · · · ·				INTERPRETATION	J.E.H.
•			•	2 : : : : : : : : : : : : : : : : : : :	: : : :	, , , ,			FINAL CHECK	
	:			•						
	1				1		1		DISTRIBUTED	•••••
	: :	•		1	}					
				<u>.</u>						170
				- <b></b> X			<u>a an an air an </u>	and the second	. 155 - 155	-679-

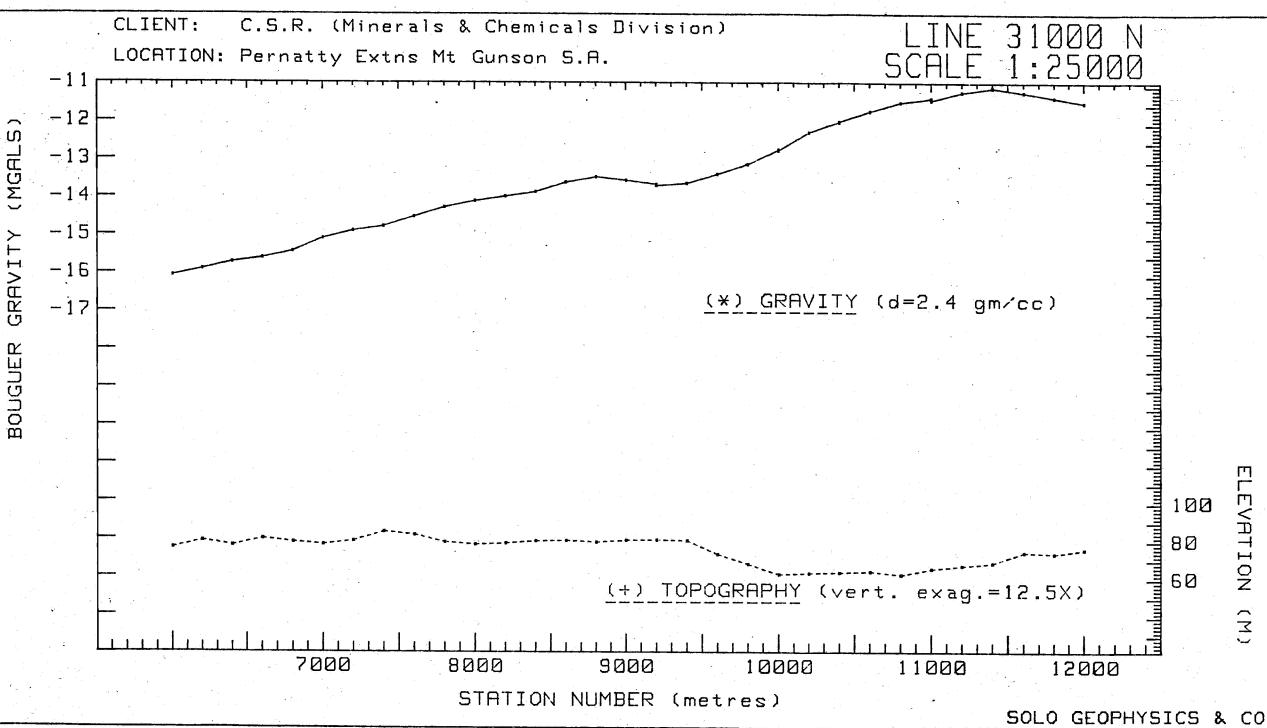


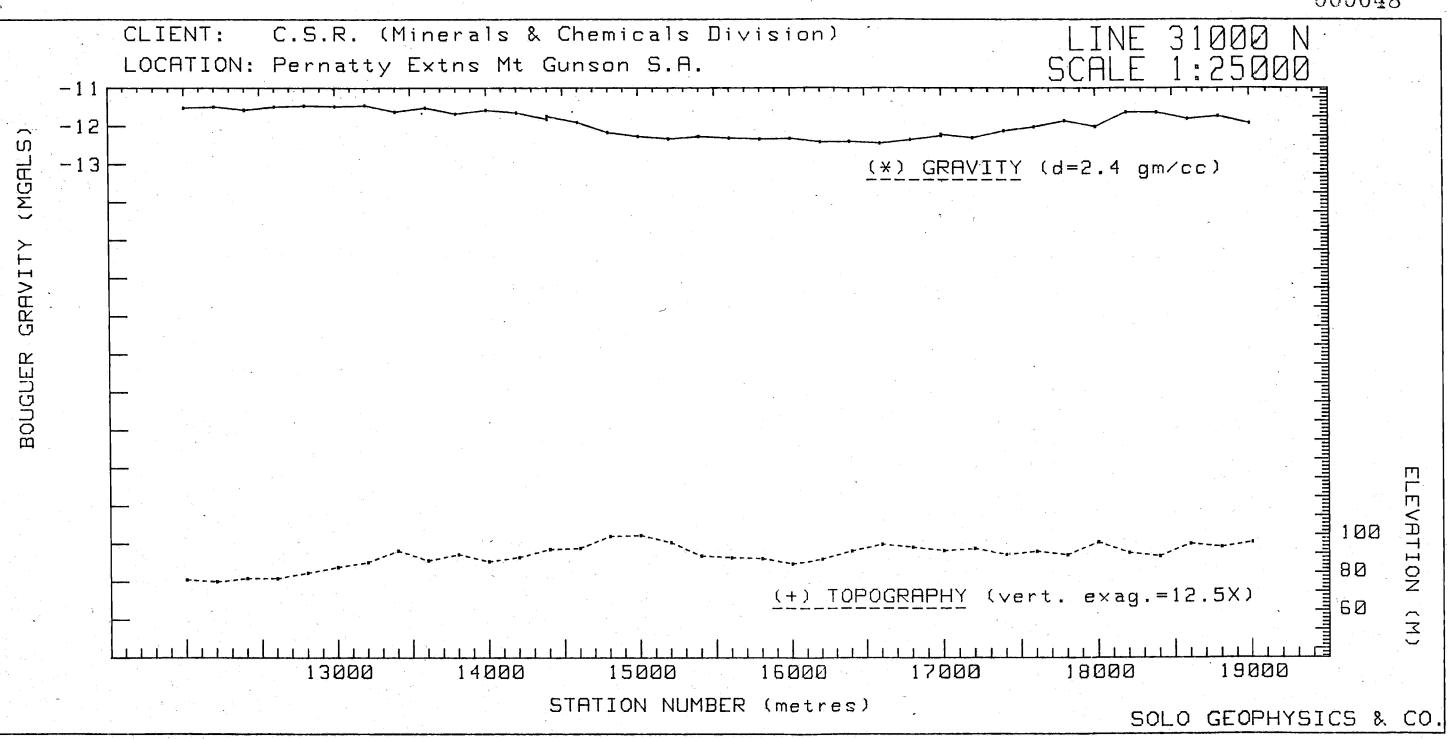


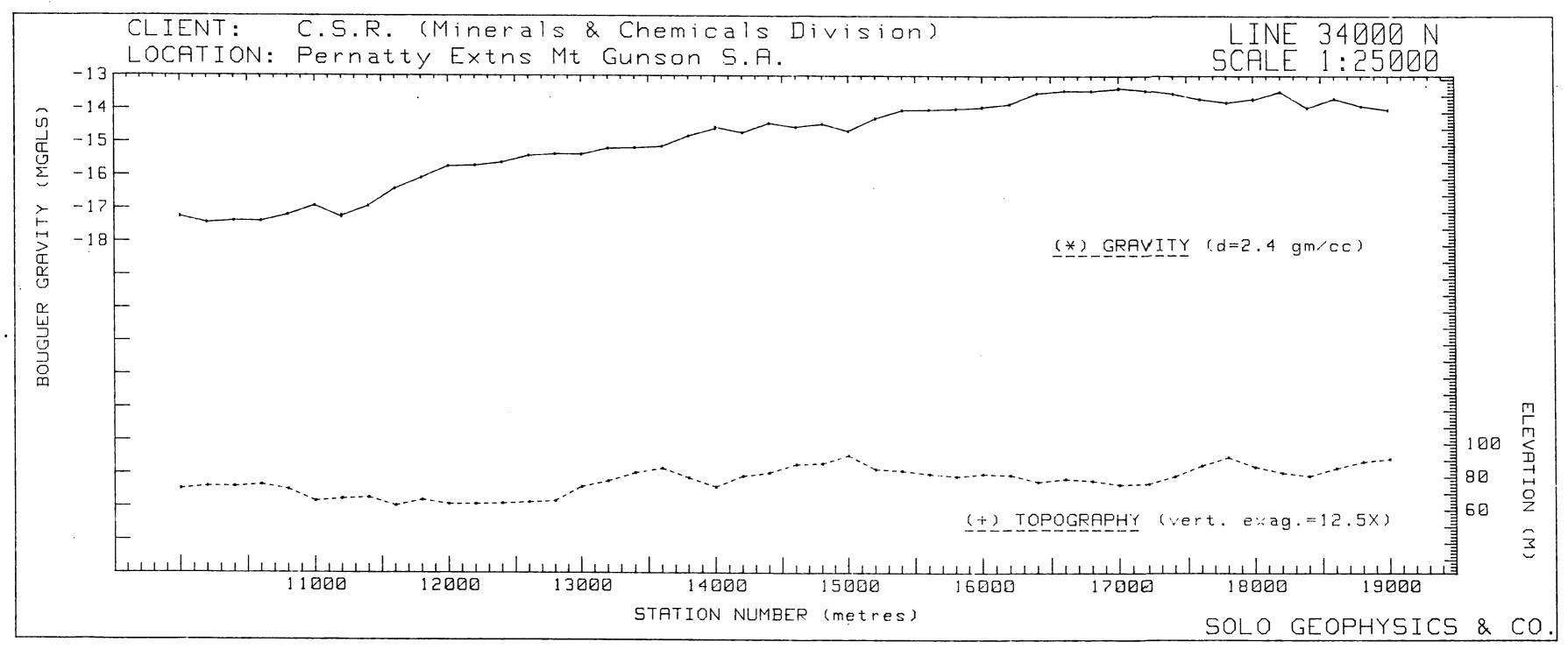


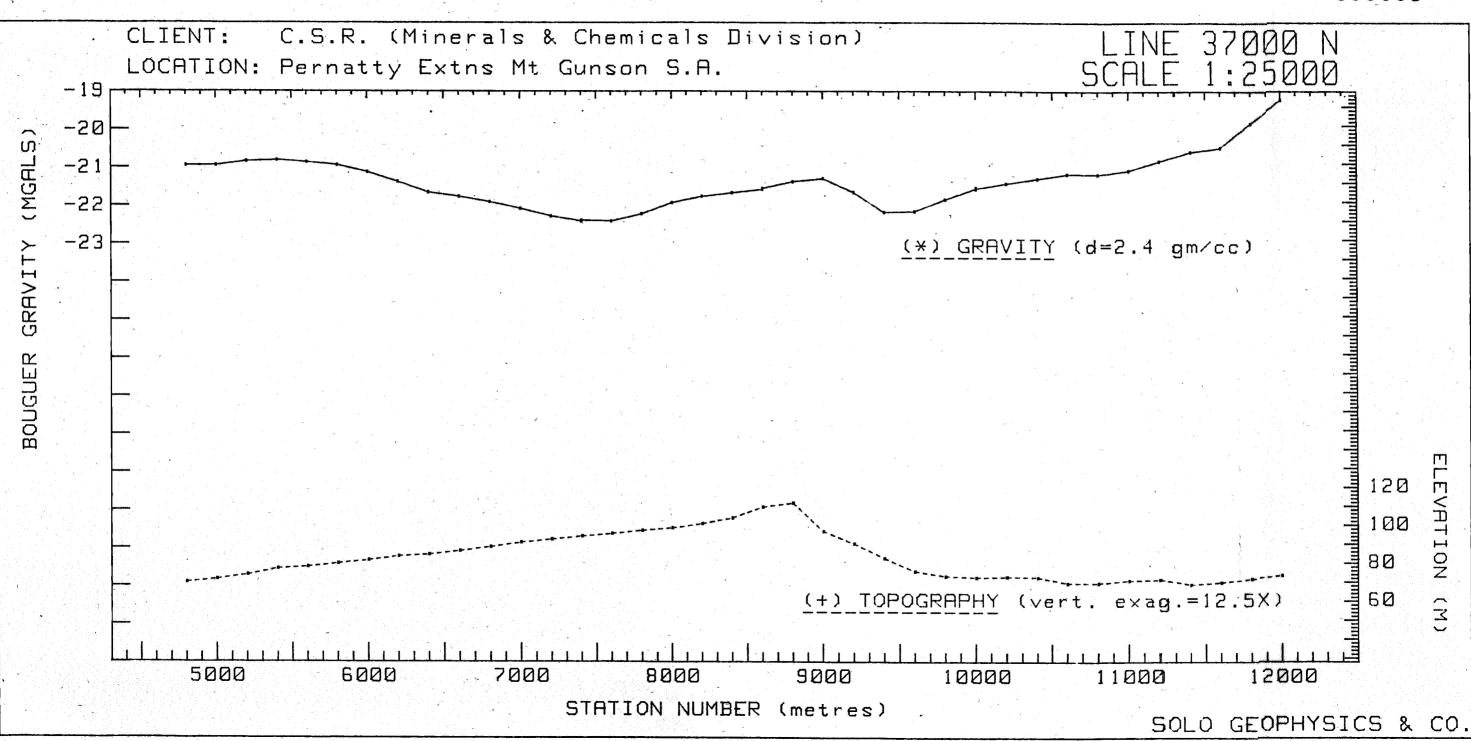


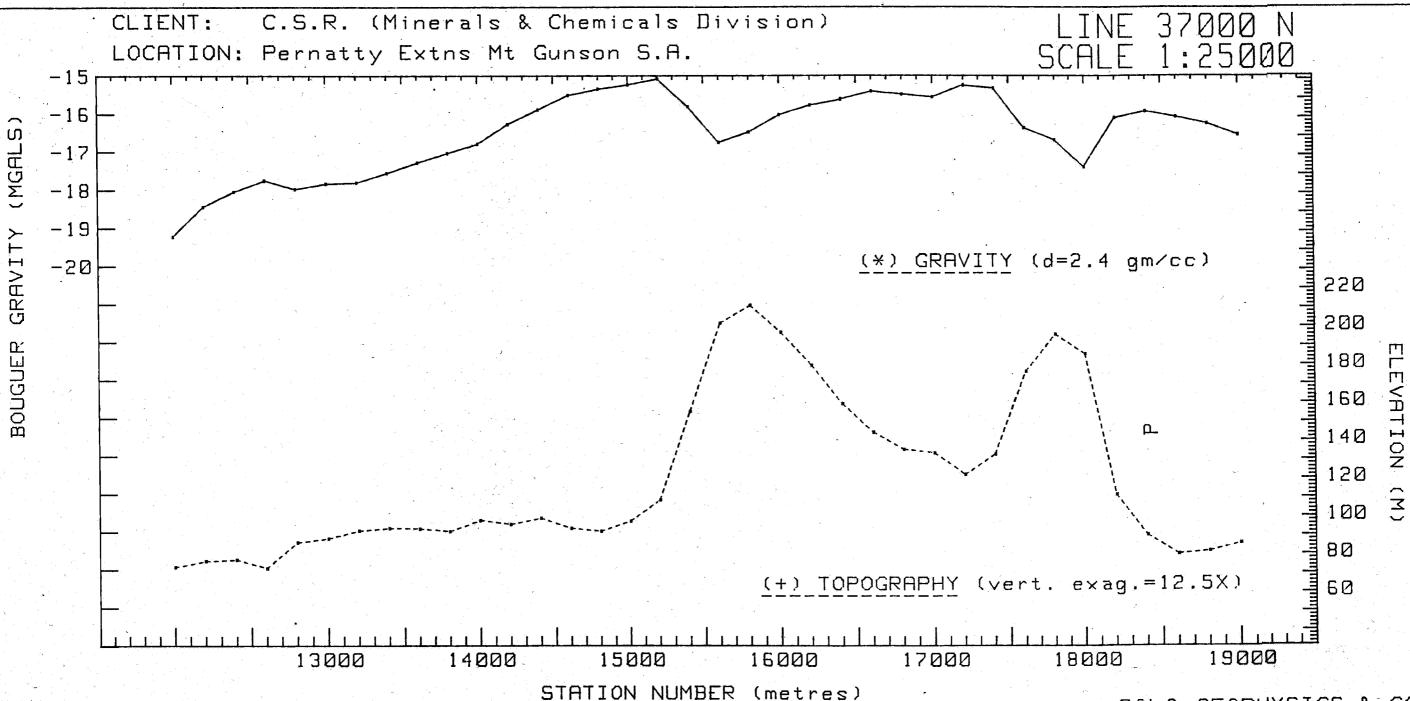






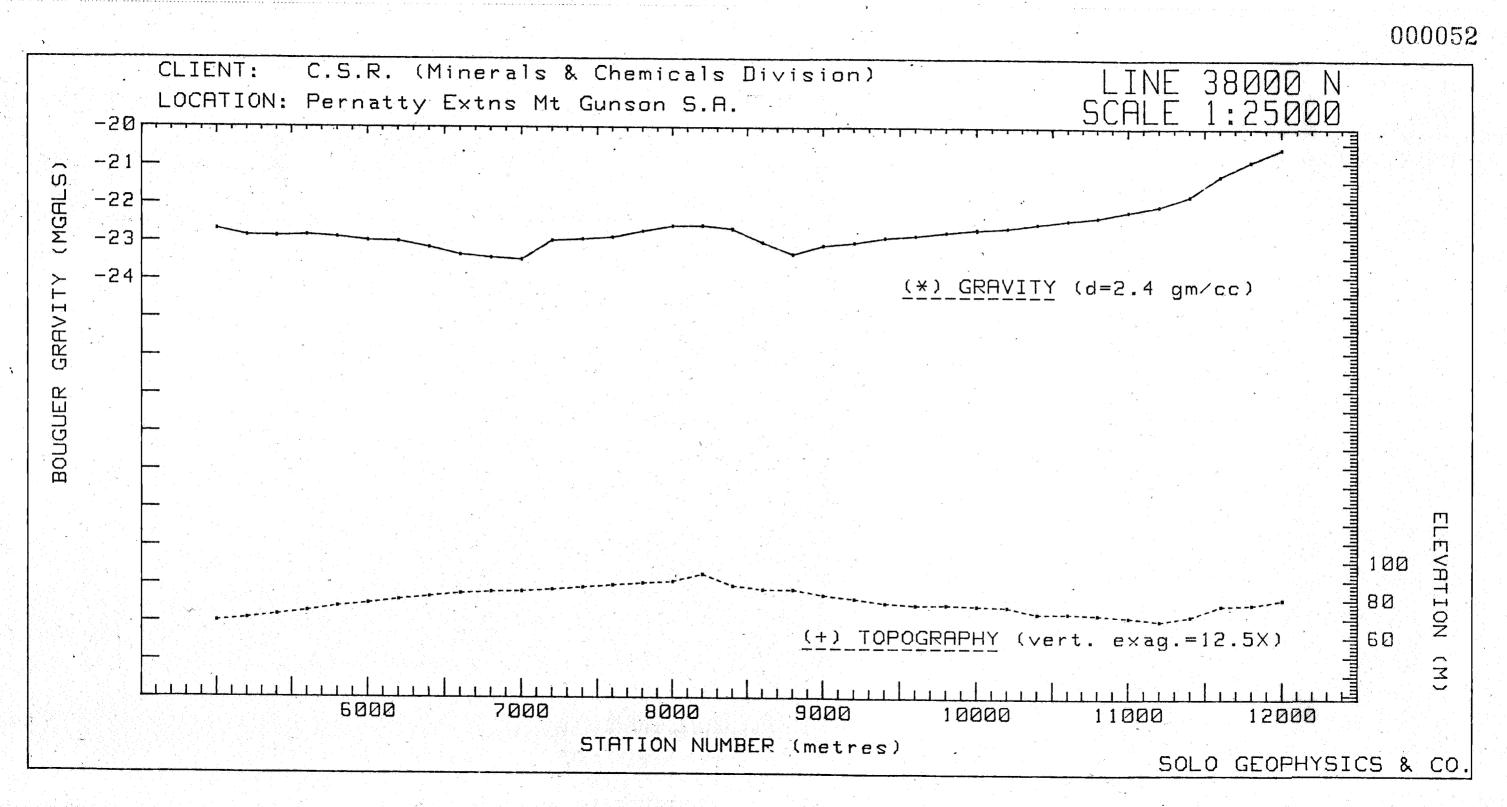


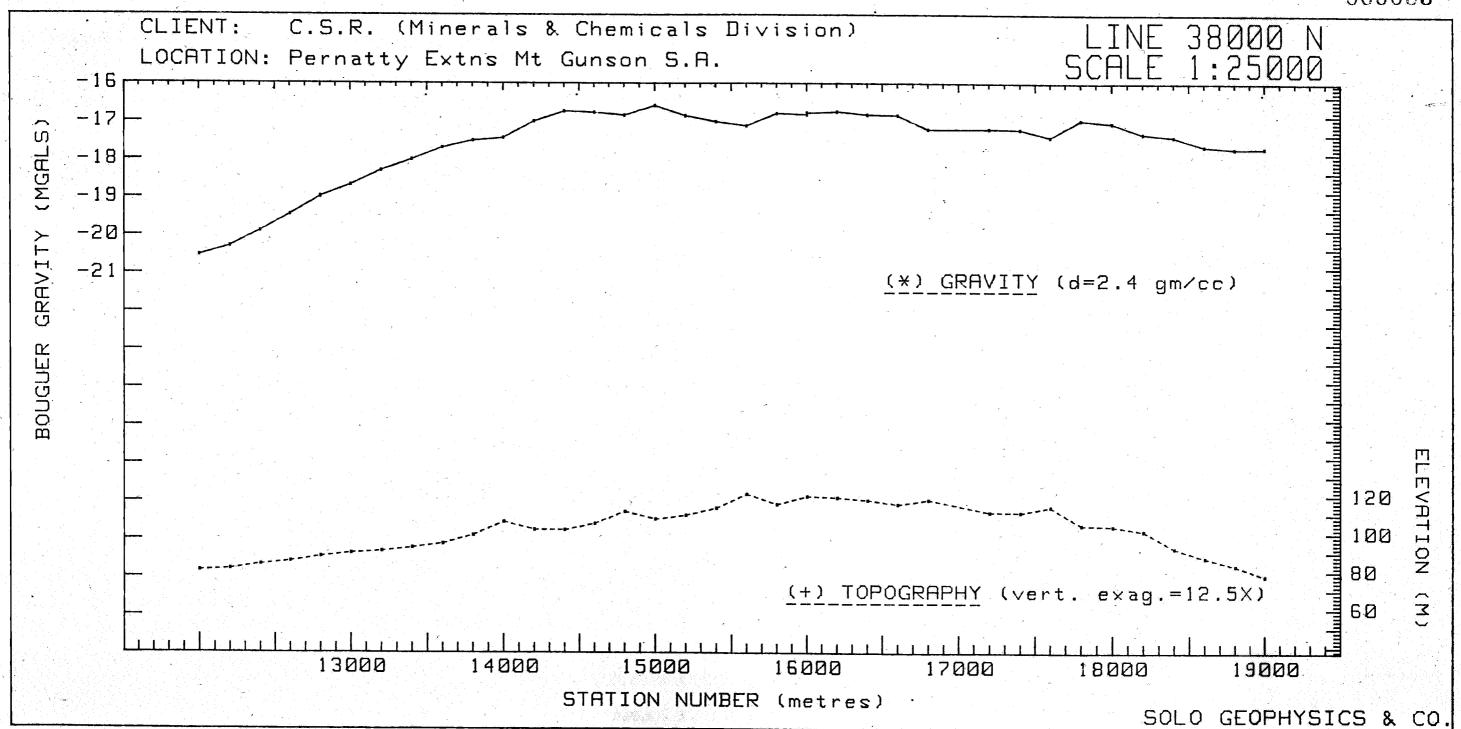


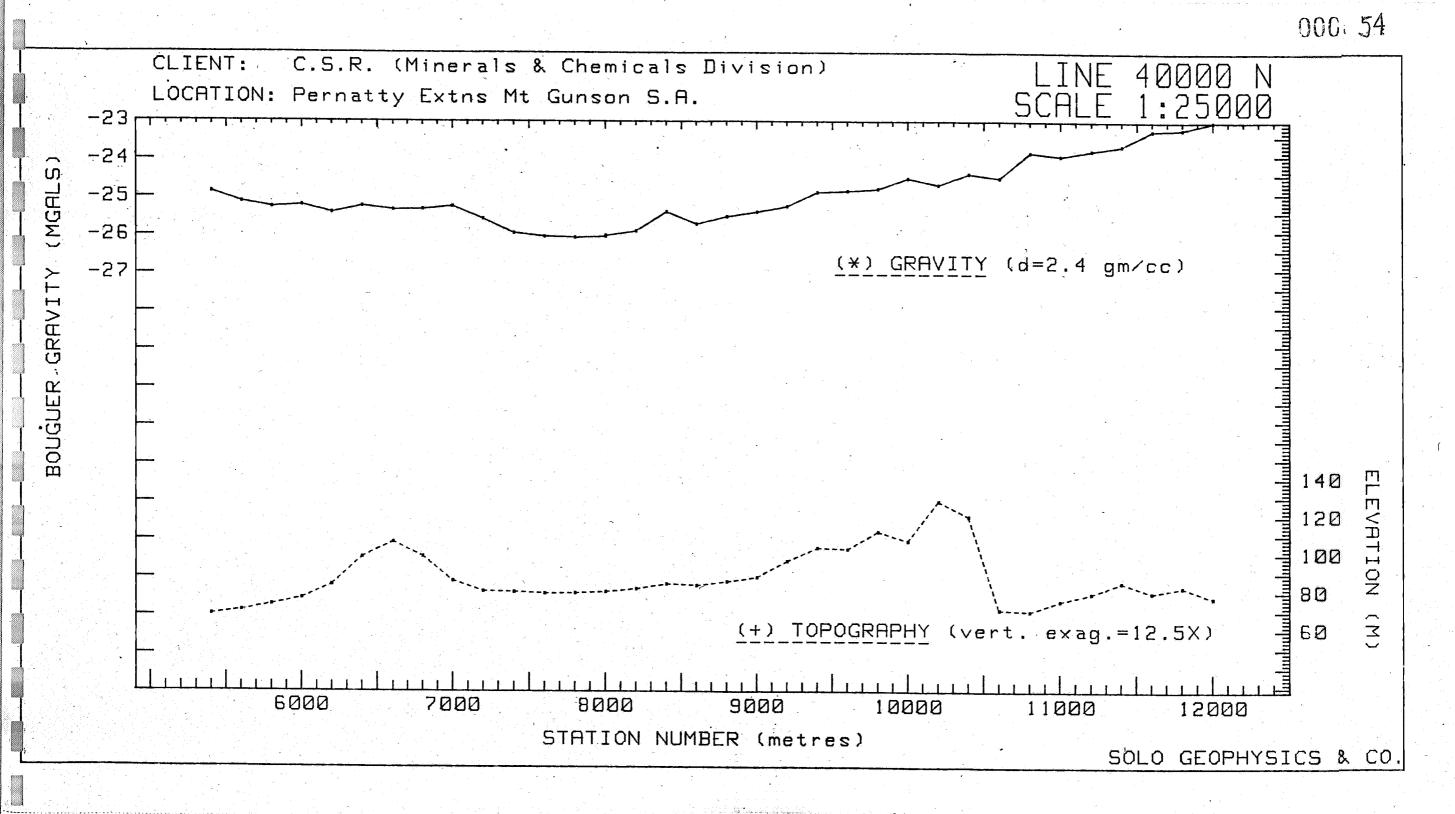


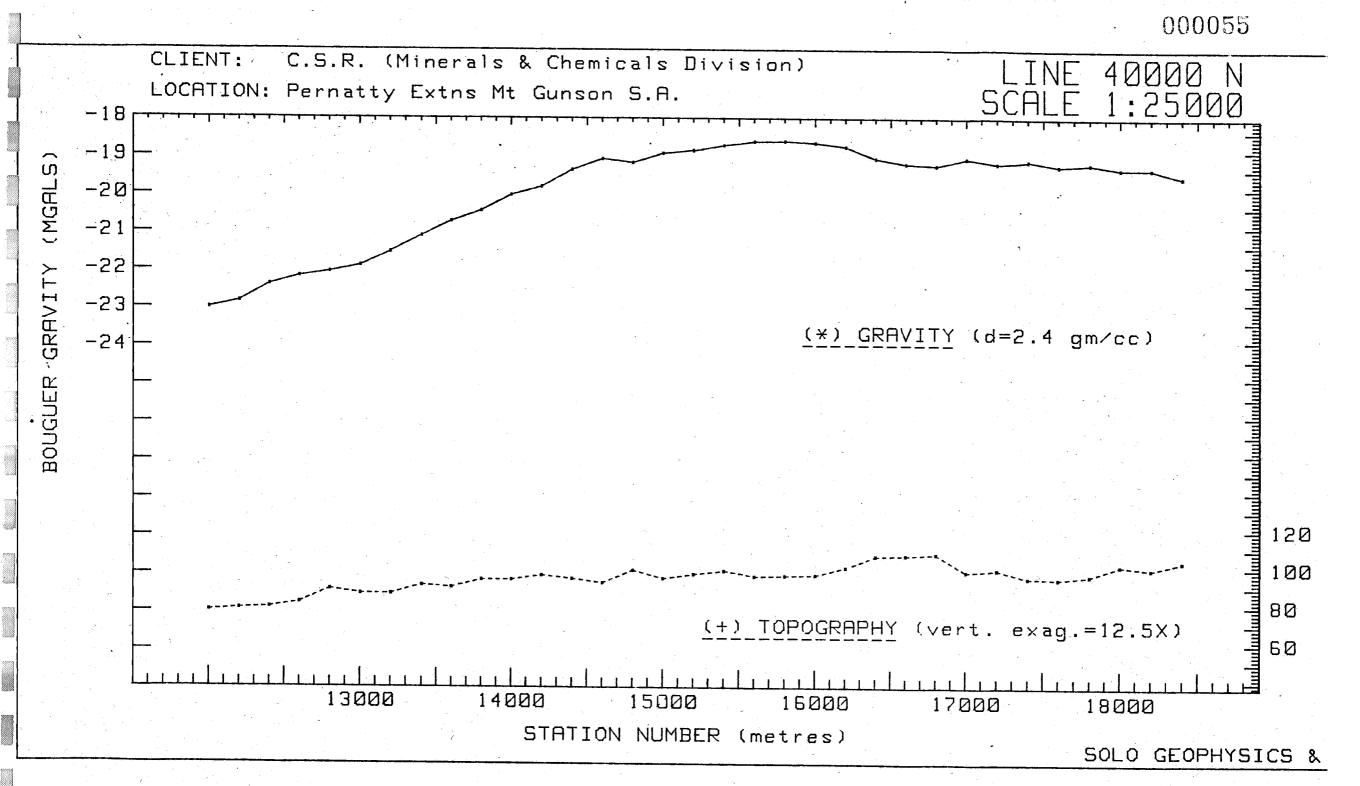
· _ `

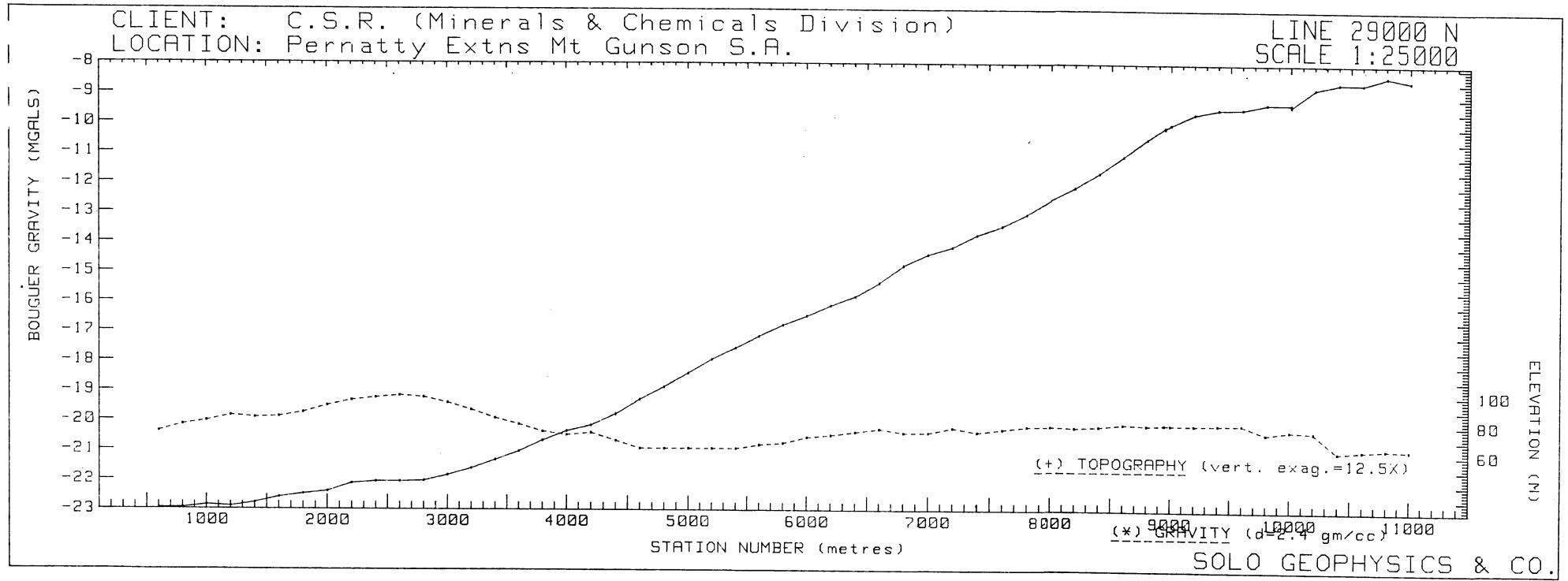
SOLO GEOPHYSICS & CO.



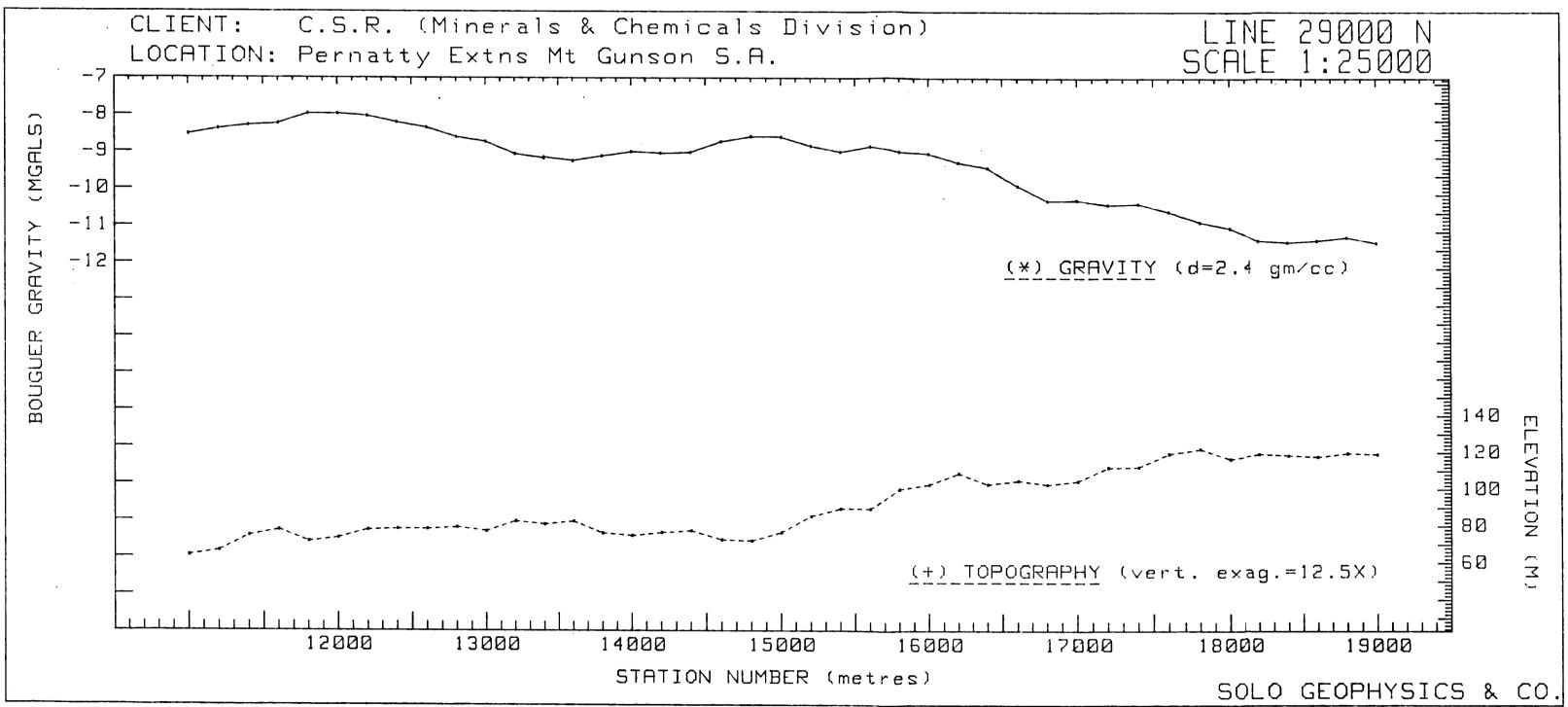


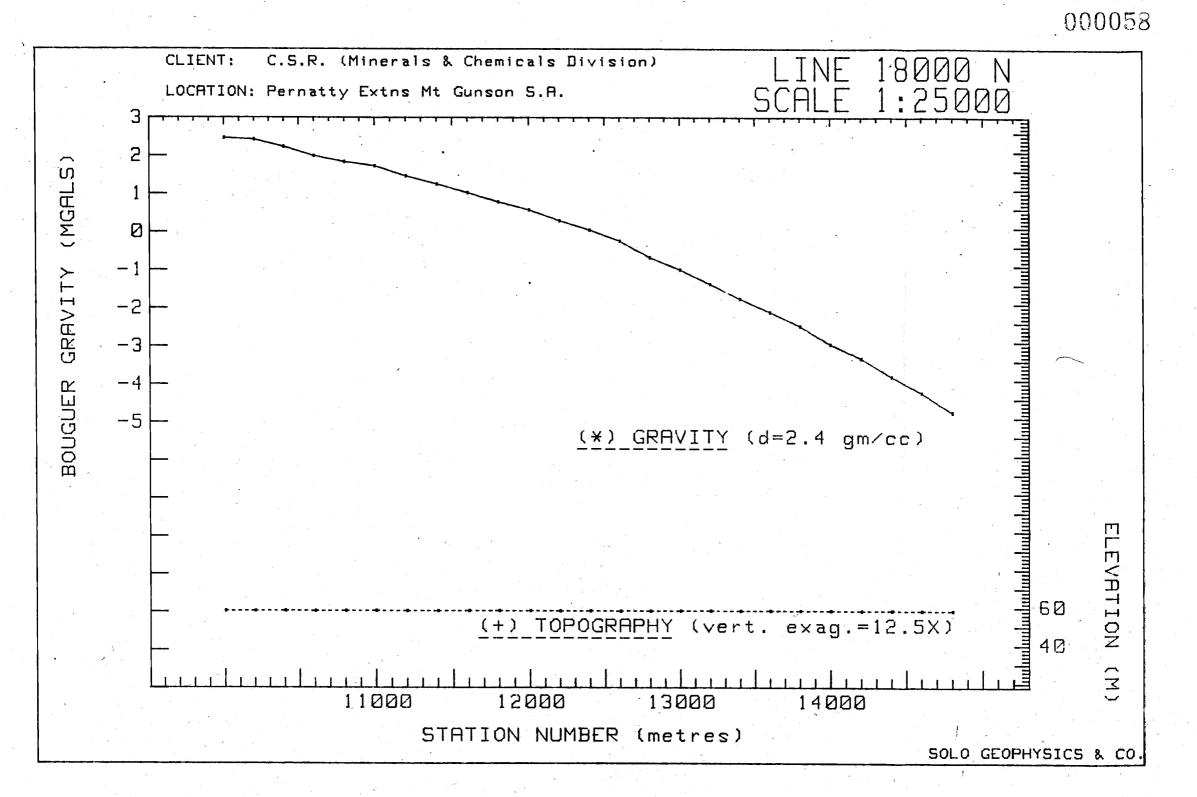




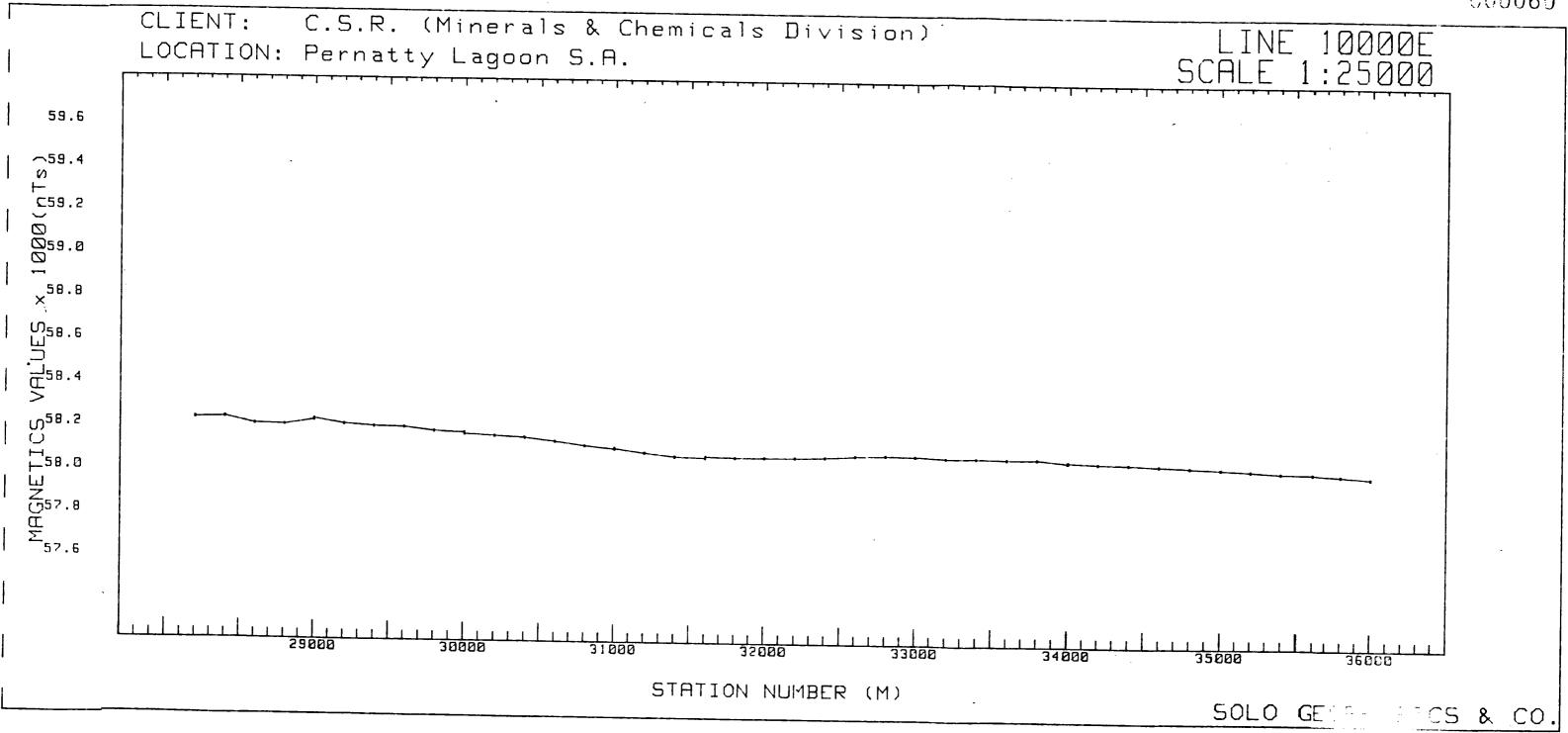


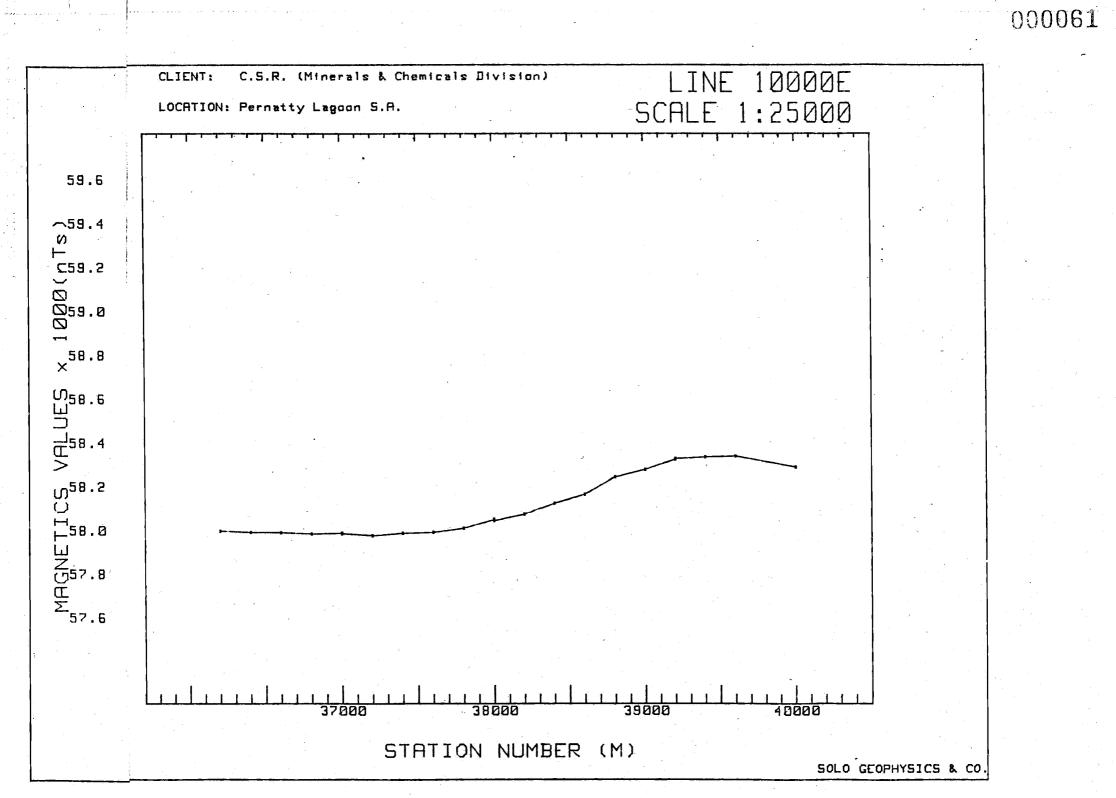
00005<mark></mark>5

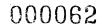


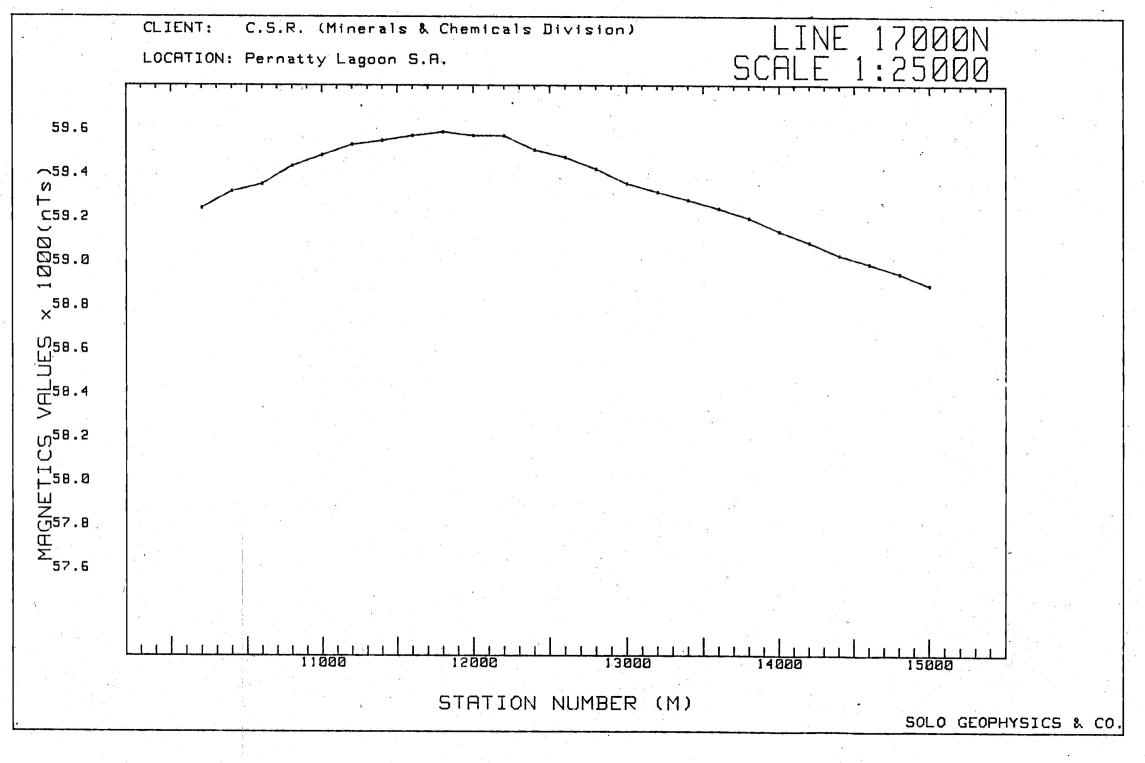


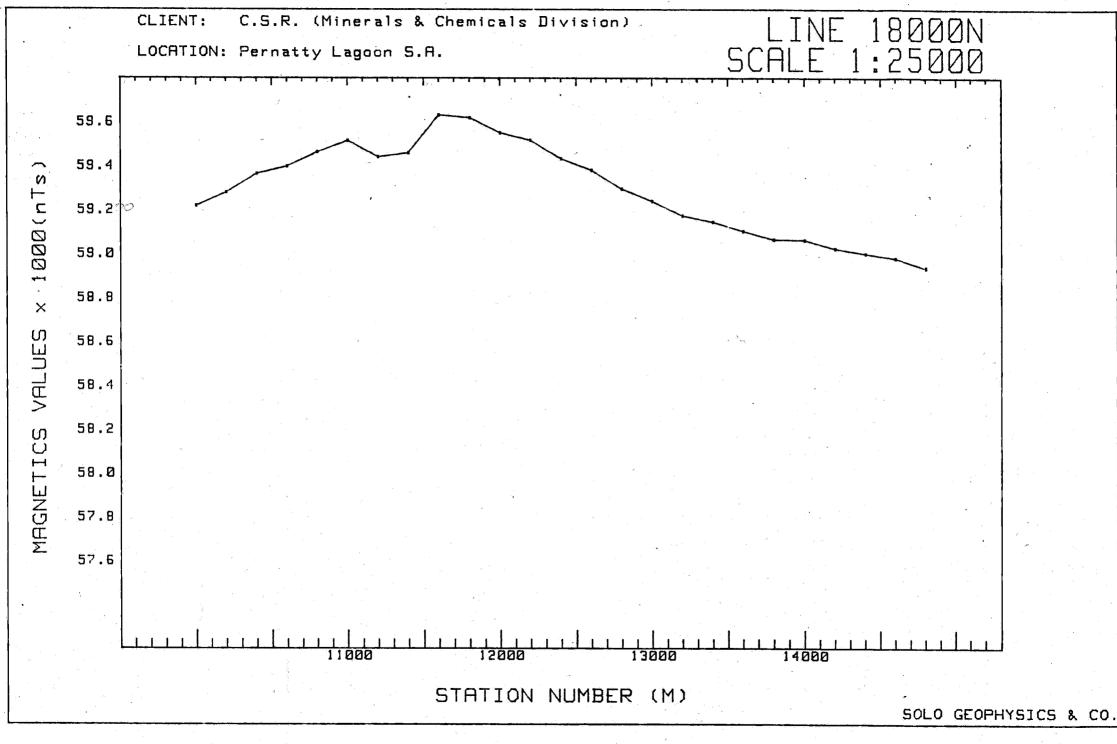
#### CLIENT: C.S.R. (Minerals & Chemicals Division) 7000 NF Ν LOCATION: Pernatty Extns Mt Gunson S.A. SC :25000 3 2 (MGALS) 0 -1 GRAVITY -2 -3 BOUGUER -4 -5 gm/cc) (*) GRAVITY (d=2.4)ELEVATION (+) TOPOGRAPHY (vert. exag.=12.5X) ŝ 11000 12000 13000 15000 14000 STATION NUMBER (metres) SOLO GEOPHYSICS & CO.

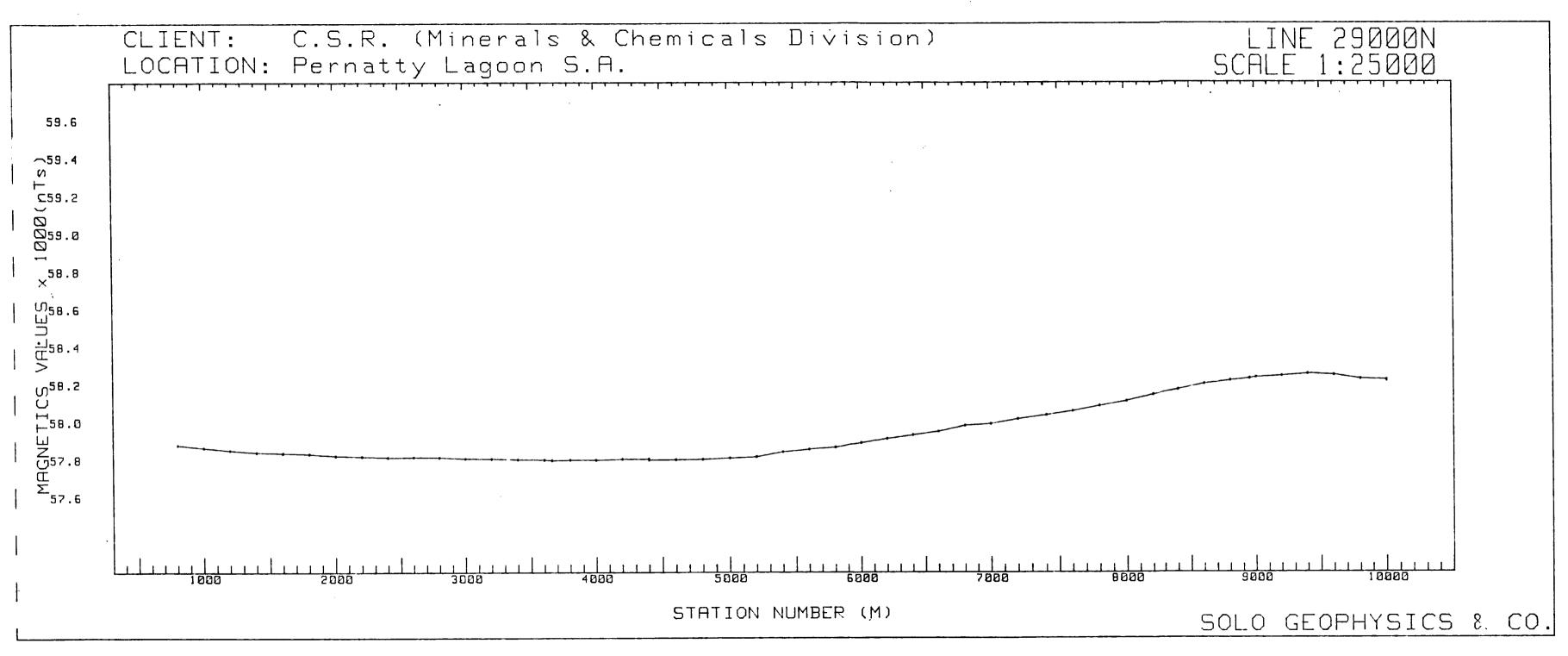


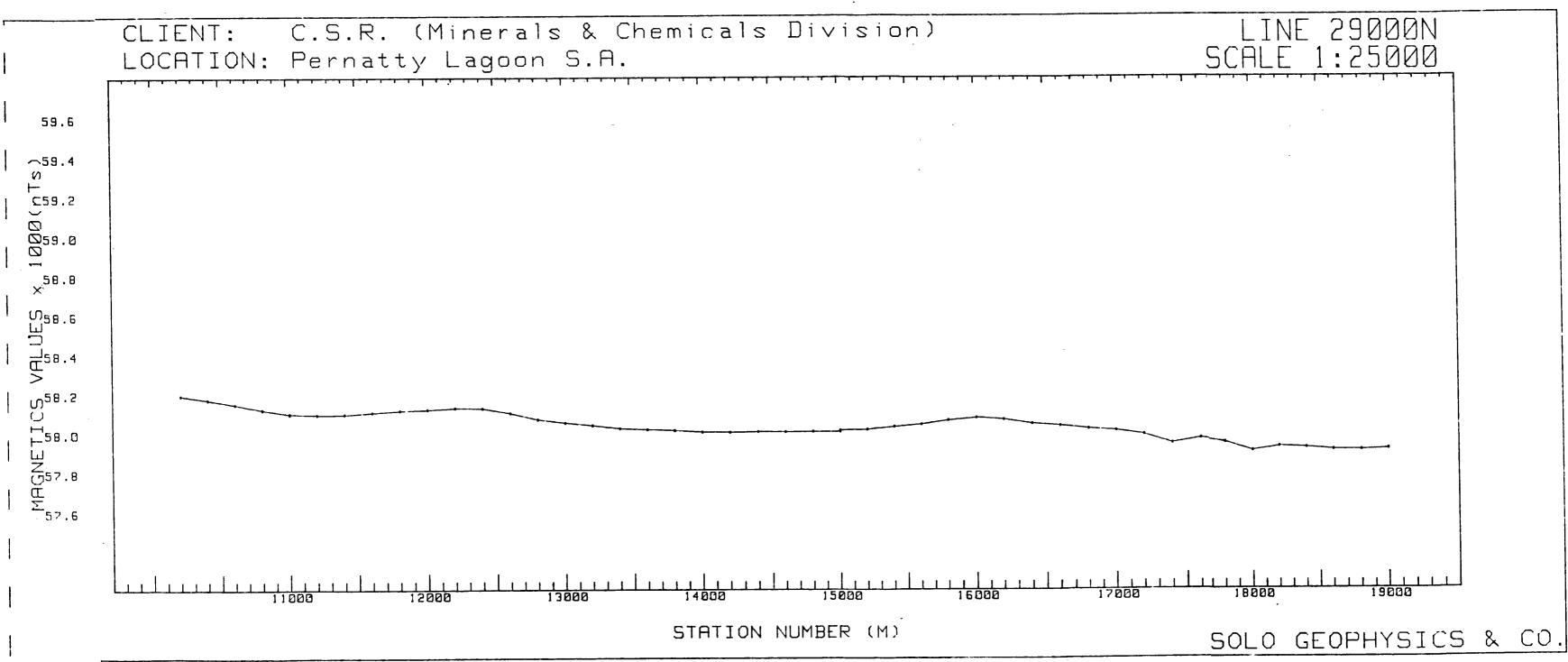


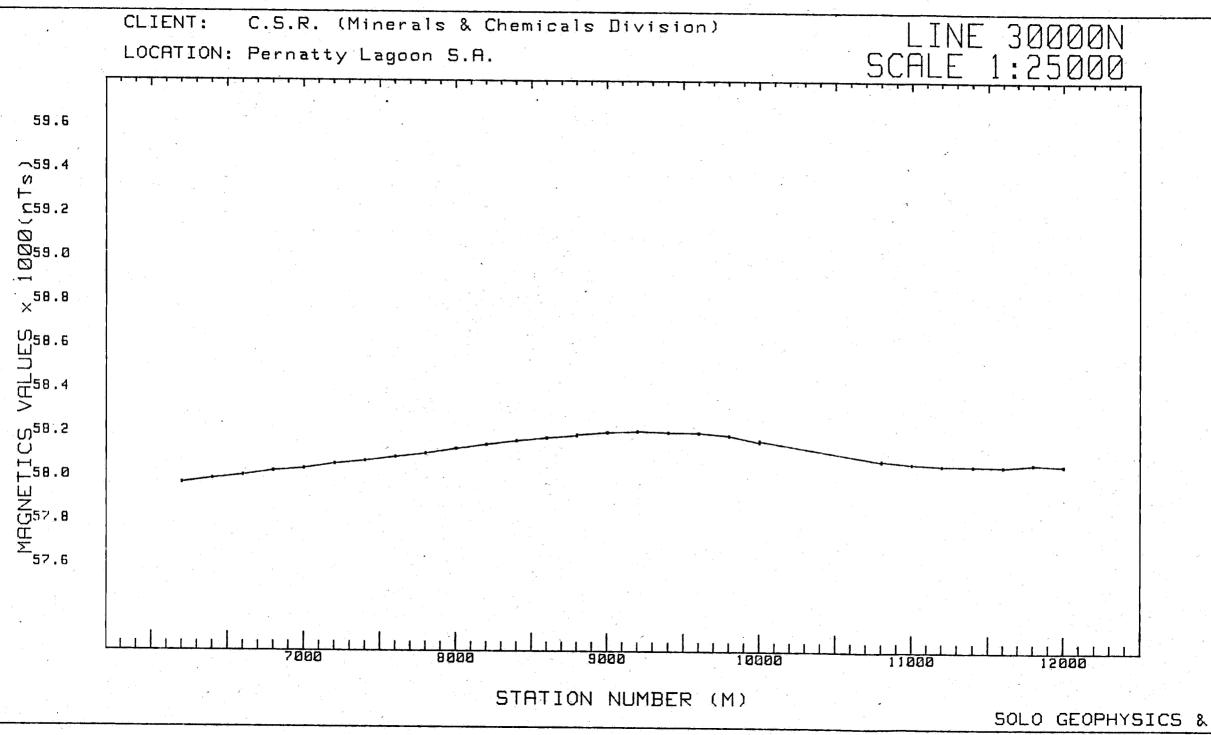


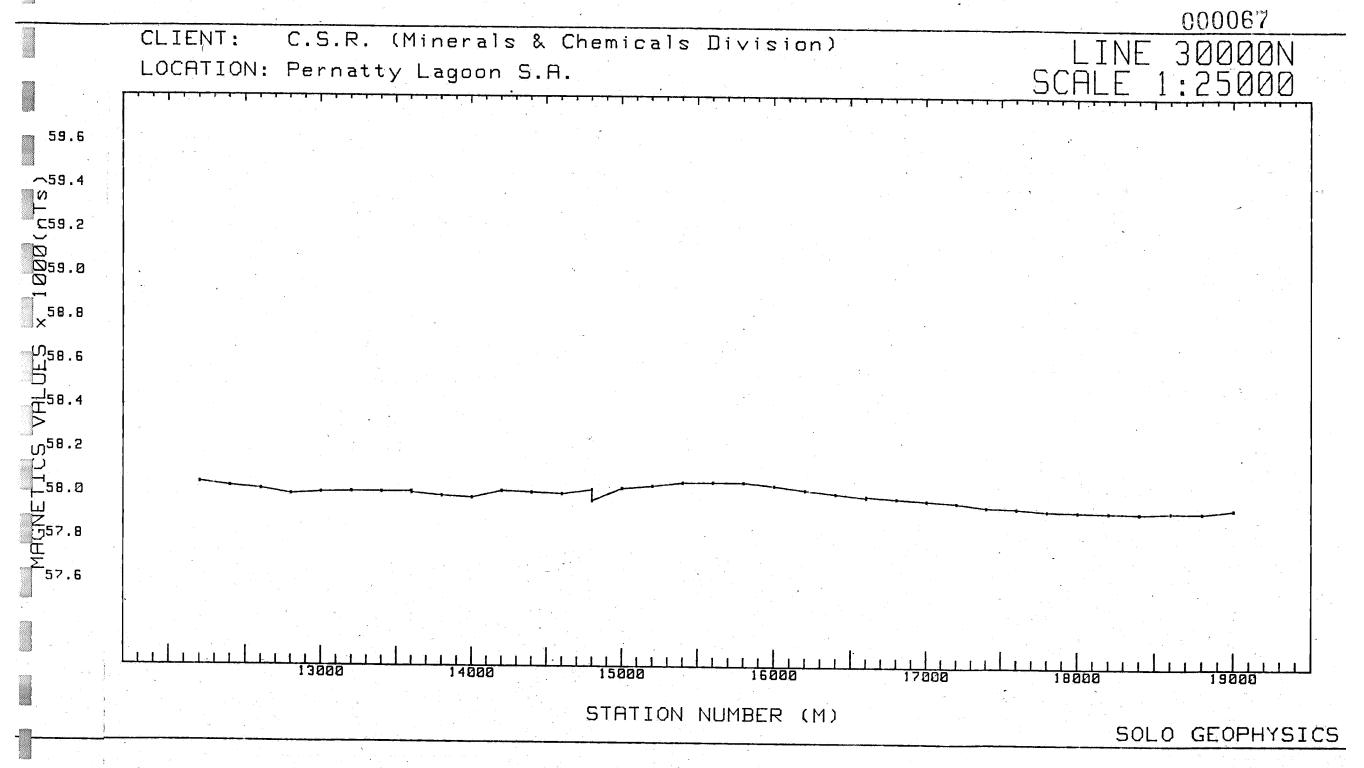


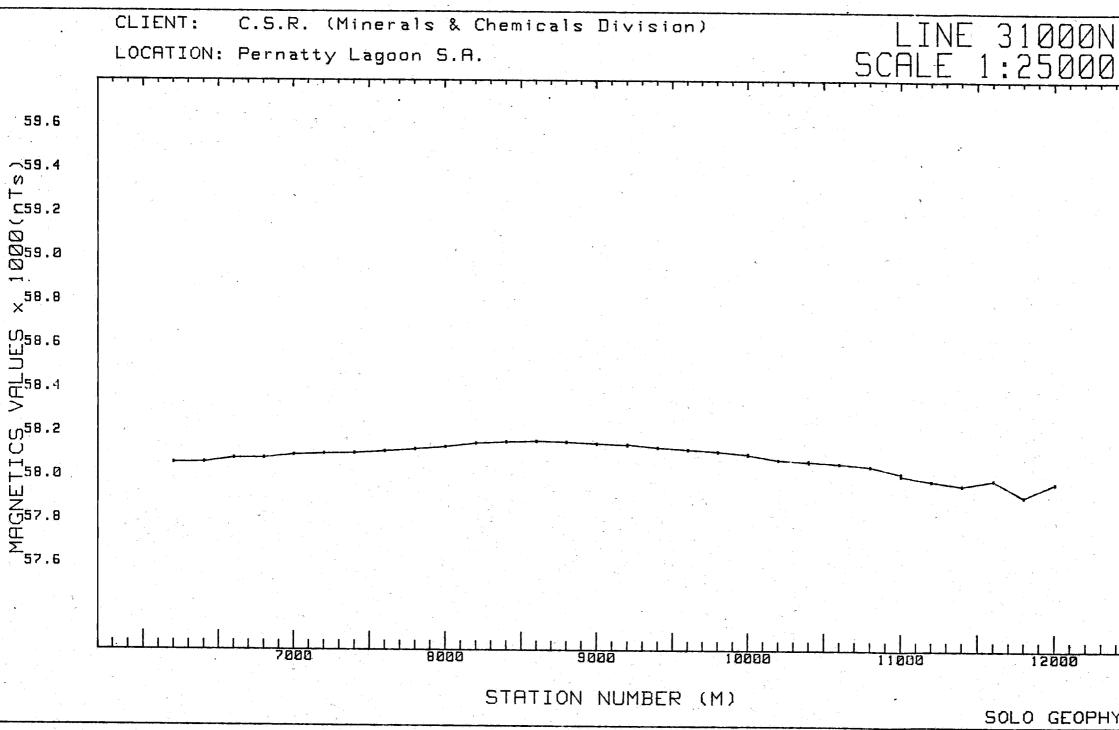




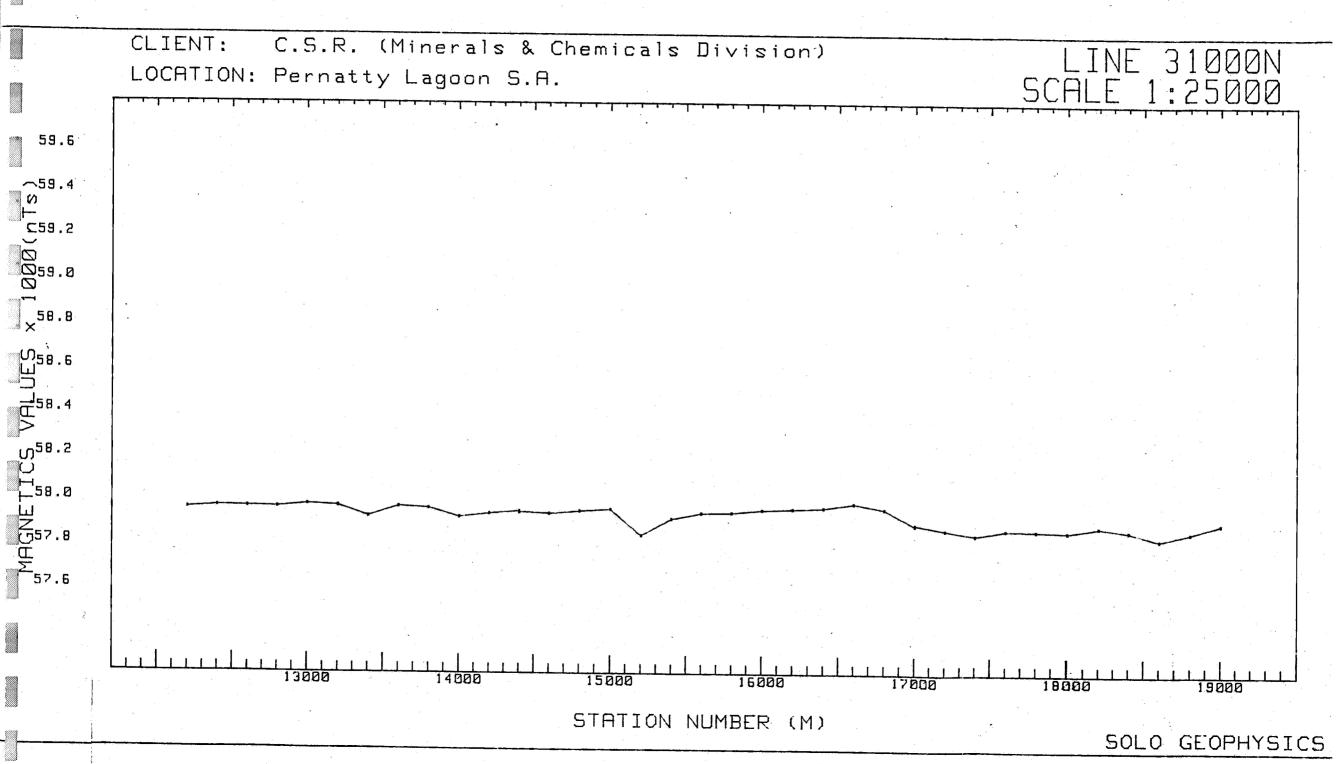


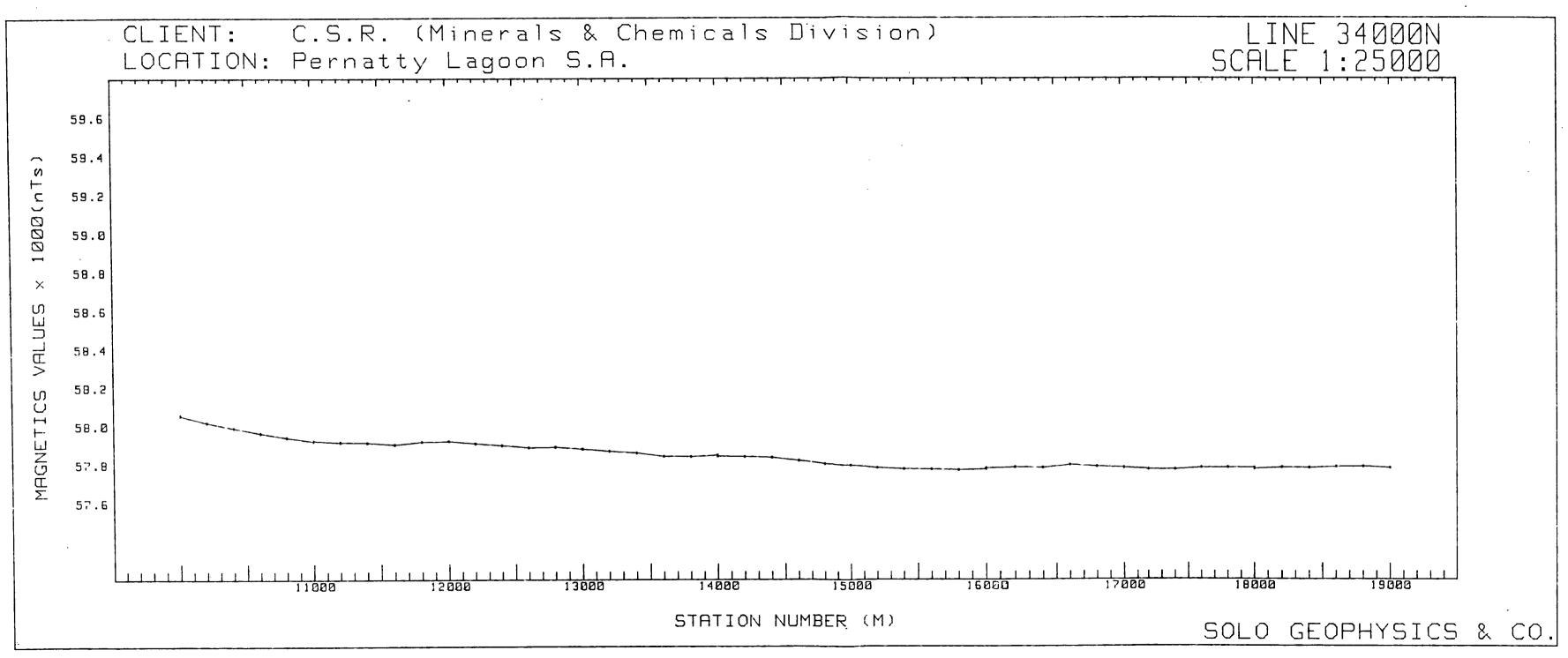






SOLO GEOPHYSICS & CC

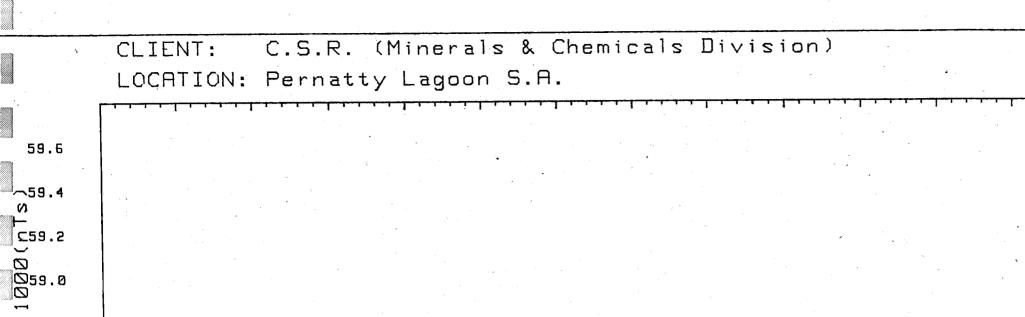




5

37000N

:25000



7000

6000

×^{58.8}

い_{58.6} コロ 158.4

ဟ^{58.2} ပ

U U U U U U 57.8 U E 57.6

STATION NUMBER (M)

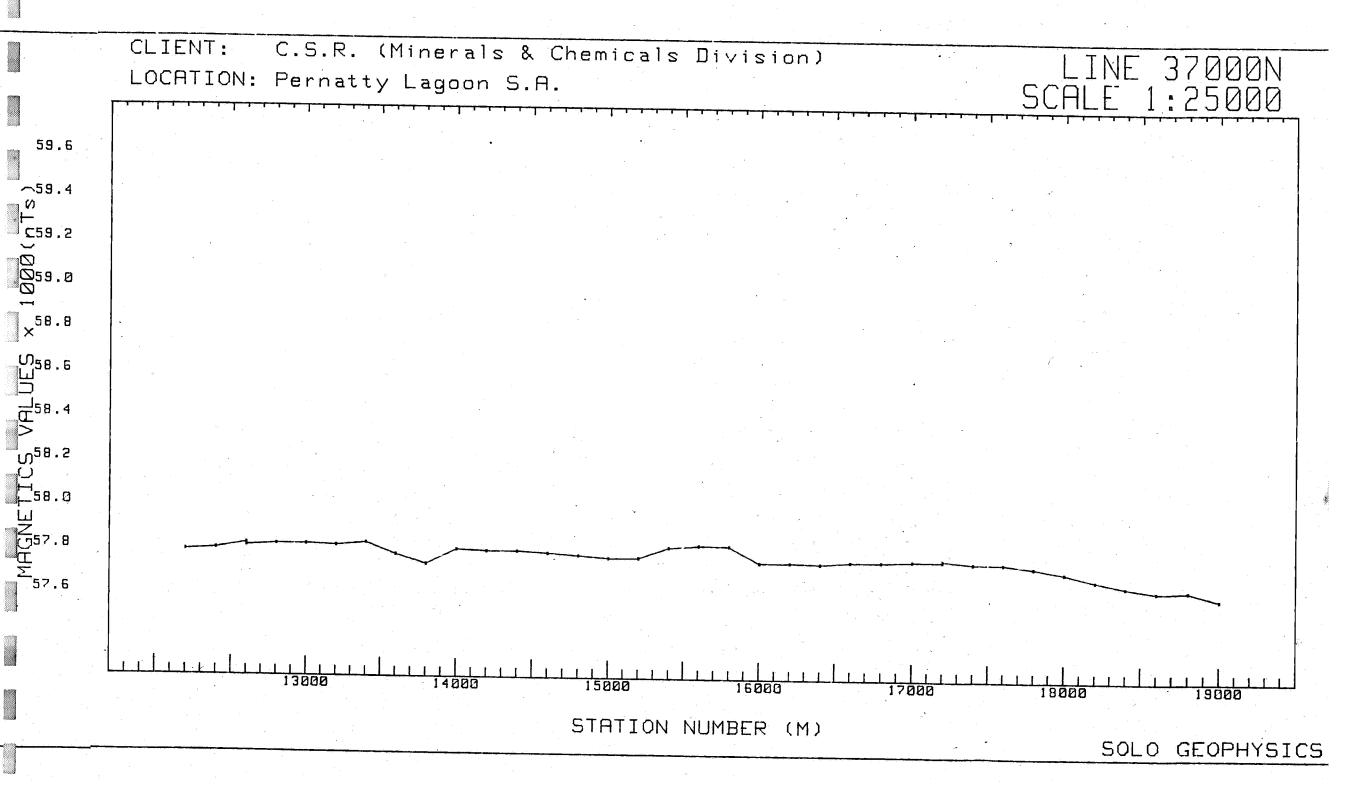
9000

8000

SOLO GEOPHYSI

11000

10000

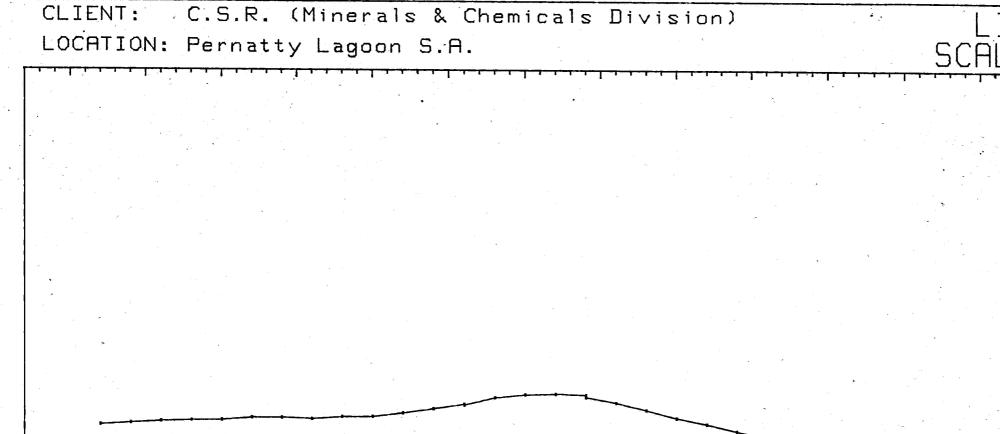


INE

38000N

:25000

12000



1 1 1 1 1 1

STATION NUMBER (M)

9000

1 1 1

7000

6000

59.6

~59.4

<u>5</u>59.2

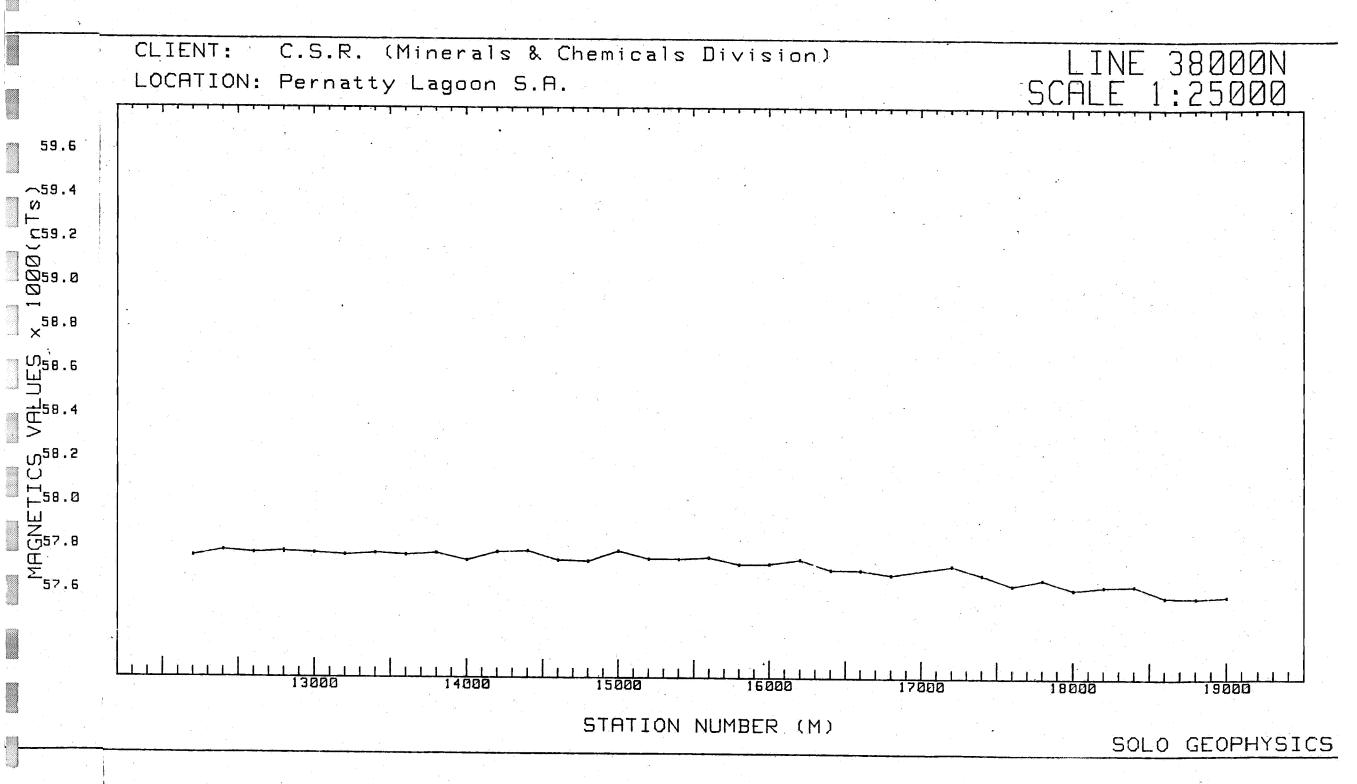
0 259.0

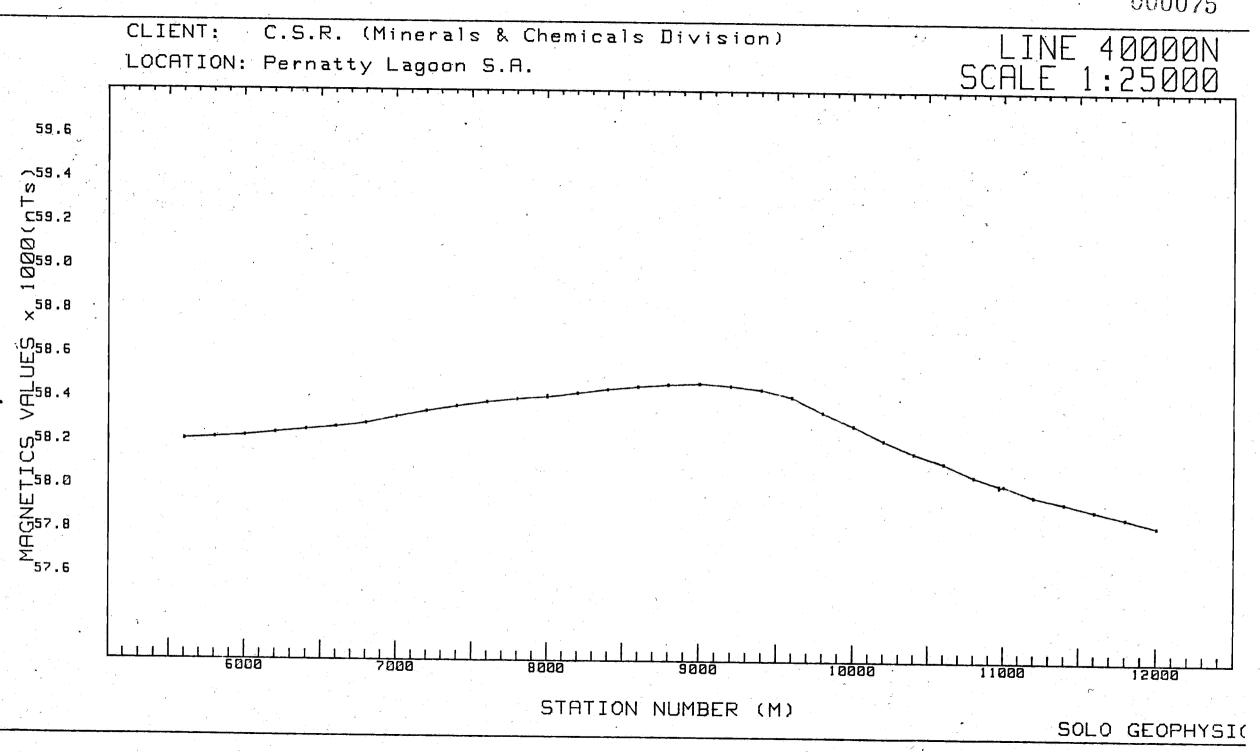
×58.8

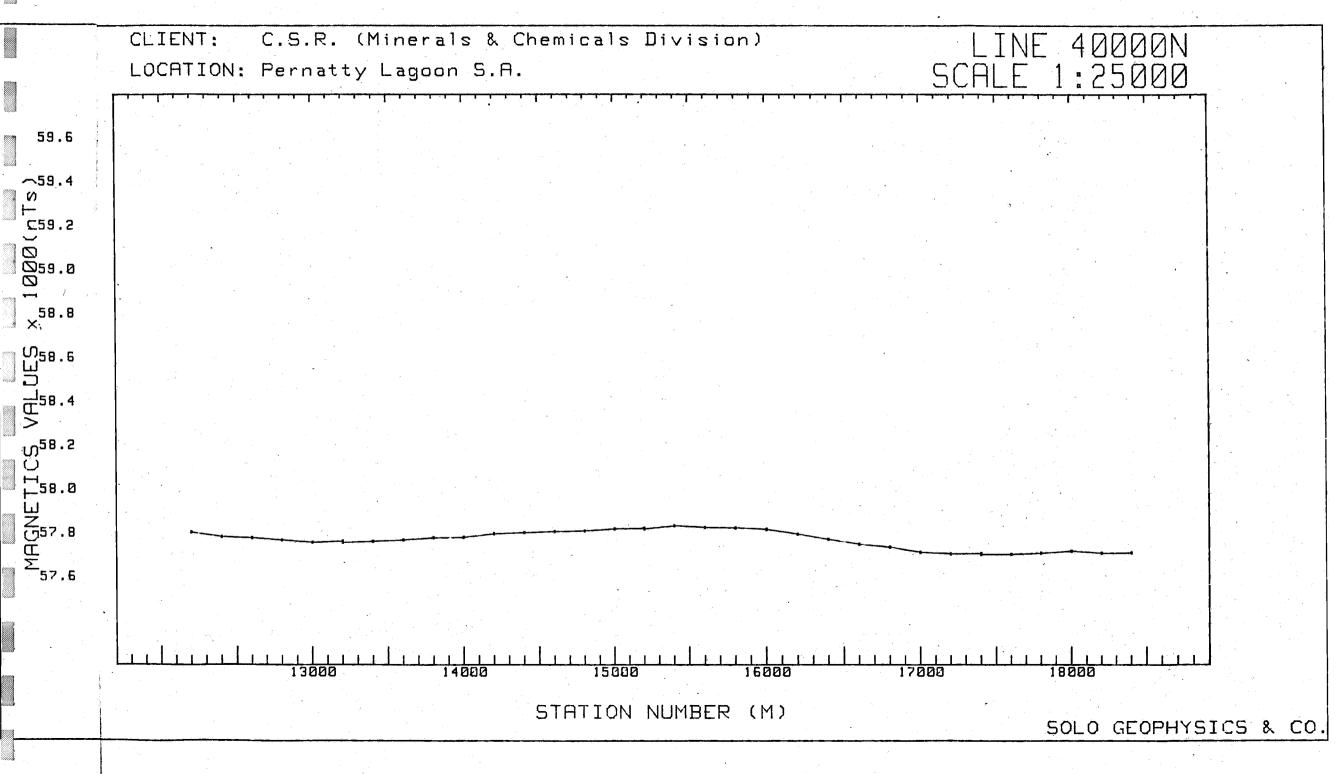
058.6 U D J58.4

SOLO GEOPHYSICS

11000







MT. GUNSON MAGNETIC SURVEY 12.9.83. TRAVENSE TIE IN READINGS. 000077

STN	KEASING.
SOLO GEOPHYSICS GAID	
19000 N 5000 E	58 324
19000 N 4600 E	58342
HAULAGE RD TRAVERSE	
50 EAST	58 332
100 *	58 329
MG. 87 TRAVERSE	4
50 EAST	58209
100 "	58221
PIDE LINE THAVEASE	
So EAST	58156
100 "	58156
AIR STRIP TRAVERSE.	
SO EAST	58062
100 "	58061

MT. GUNSON MAGNETIC SURVEY 12-9-83.

# HAULAGE ROAD TRAVERSE.

STN	KEADING.	
O EAST	58341	
50	58346	
100	58341	
150	58 341	
200	58339	
250	58340	
300	58344	
350	58 347	
400	58354	
450	58372	
500	58388	
550	58410	
600	58 405	
650	58 398	
700	58,390	
750	58387	
800	58-376	
850	58354	
900	58365	
950	<b>1</b> 800	
1000	50277	
1050	10	
1100	58380	
1150	58387	
1200	58395	
1250	58403	
1300	58414	
1350	58426	
1400	58435	
1450	58 446	
1500	58 458	
1550	58 477	
1600	58 487	
1650	58 504.	
1150.	58390.	
	•	

MT. GUNSON MAGNETIC SURVEY 12.9-83

MG. 87 TRAVERSE

	STN	READING.	
	200 WEST	58 213	
	150 "	58 215	
e en	100 "	58 213	
	50 "	58 210	
en e	O EAST	58 219	
······································	50	58 225	i iç çir şirinin iş
· · · · · · · · · · · · · · · · ·	100	58 227	
· · · · · · · · · · · · · · · · · ·	150	58 228	
	200	58 234	
n general and a symptocity and the second	250	58 243	
	300	58253	
	350	58-267	
	400	58 284	
	450	58 301	
	500	58337	
	550	58 338	
	600	58 335	
	650	58 336	•
· · ·	700	50329	
	-	58 325	
	0.	58323	
		58322	
		58 323	
		58 322	
		58 325	
	to Co	58330	
	1100	58338	
· · · · ·	1150	58346	
•	1200	58 354	
	1250	58 364	
		58.374	
	1300	50 379	
	1300	0001	

MT. GUNSON MAGNETIC SURVEY 12-9-83

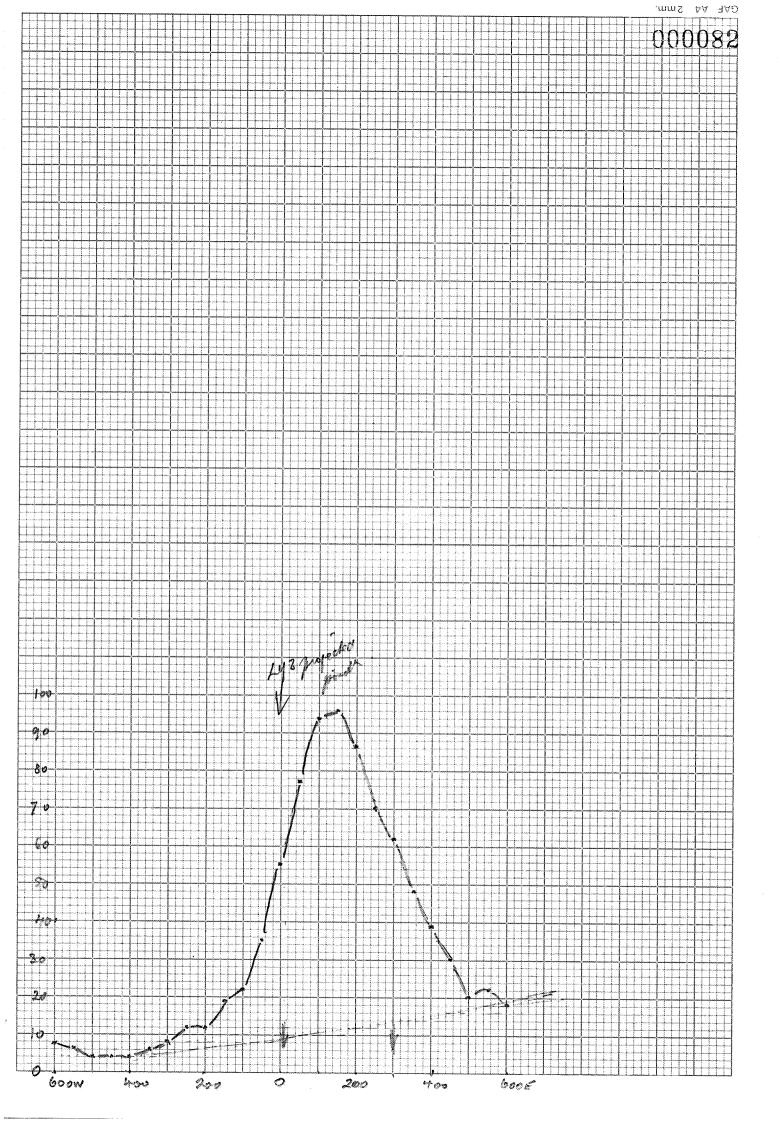
PIPE LINE TRAVERSE

	STN	READING	
	0	58 168	
	50	58 167	
	100	58 170	
	150	58 167	
	200	58 166	
an tan an an an an an an	250	58 179	
	300	50 170	
	350	50 12/1	•
	400	50 187	
· · · · · · · · · · · · · · · · · · ·	450	58 190	
· · · · · · · ·	500	58 202	
	550	58 216	
	600	50 242	
	650	58 277	e de la companya de l La companya de la comp
	700	58 311	
	750	58 311	
	800	58312	
	850	58 306	
	900	58301	
	00	58293	
	1000	58 287	
	1-6-	58 291	
an a	1100	58 292	
a da an	Al ma	58 297	
т. 	1200	58 299	
	1250	58 308	
an a	IRAA	58 308	
	1350	58 321	
	1400	58327	
	1400	58325.	

MT GUNSON MAGNETIC SURVEY 12-9-83

AIN STRIP TRAVENSE.

STN	READING
•	58065
0	
50	58068
100	58069
150	58 075
200	58 0 80
250	58 083
300	58 0 85
350	58 092
400	58 100
450	58 111
500	58 1/8
550	58 137
600	58 153
650	58 174
700	58 201
750	58237
800	58 274
850	58 301
900	58 301
950	58 298
1000	58296
1050	58 291
1100	58 293
1150	58 296
1200	58 298
1250	58 299
1300	58 299
1350	58 311
1400	58 316
1450	58 329
1500	58 328
Ð	58067



	Minerals Divisio	RECEIVED A SEPTIMENT A	000083
то	P.R. Gidley	NTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTTT	WJL/sg1/401 (1) -> DGT/
FROM	W.J. Langron	DATE	September 13, 1983 JLC
		"BLIND DYKE"	WJL/sg1/401 () -> DGT/ September 13, 1983 JLC Yo fellowup (E) file Gunson 401.

Apropos of the buried feature to the west of and parallel to the MG14 dyke, Gunson - reference the perspective plot of ground magnetics (downward continued) which we generated recently.

During the course of the Lake Torrens Joint Venture Meeting on 2nd September, Mr. Peter Haskins of Aquitaine Australia Minerals mentioned what could be a similar case tested by Aquitaine in Joint Venture with Esso on their E.L. 1015 (Roxby Hill), subsequently relinquished.

Hole SSL/1001 was sited on a weak magnetic linear with the Sturtian trend and a 3 mgal gravity anomaly. The hole entered a "blind dyke" at 300 m from surface and stayed in the dyke material for 100+ m. There was a little pyrite in the dyke with mafics of somewhat unusual composition.

The report on this work (including assays, petrology) is on open-file and the core is stored in the SADM& core library.

Our Adelaide staff should inspect this core and the report. Measurements of magnetic susceptibility on the core could be useful in our overall study of Shelf data.

W.J. Langron

cc - DAB/DGT/JLC (Adelaide) - RJF

- DJC/File

MT GUNSON MAGNETIC SURVEY

RVEY 12-4-83

# AIN STRIP TRAVENSE.

STN	READING.
0	58065
50	58068
100	58 069
150	58 075
200	58 080
250	58 083
300	58 085
350	58 092
400	58 100
450	58 111
500	58 118
550	58 137
600	58 153
650	58 174
700	58 201
750	58237
800	58 274
850	58 301
900	58 301
950	58 298
1000	58296
1050	58 291
1100	58 293
1150	58 296
1200	58 298
1250	58 299
1300	58 299
1350	58 311
1400	58 316
1450	58 329
1500	58 328
0	58067

MT. GUNJON MAGNETIC SURVEY 12-9-83

.1

## PIPE LINE TRAVERSE

STN	READING
0	58 168
50	58 167
100	58 170
150	58 167
200	58 166
250	58 172
300	58 170
350	58 174
400	58 182
450	58 190
500	58 202
550	58 216
600	58242
650	58 277
700	58 311
750	58 311
800	58312
850	58 306
900	58301
950	58293
1000	58 287
1050	58 291
1100	58 292
1150	58 297
1200	58 299
1250	58 308
1300	58 308
1350	58 321
1400	58327
1400	58325.

•

.

MT. GUNSON MAGNETIC SURVEY 12-9-83.

000086

•

HAULAGE ROAD THAVERSE.

STN	READING.
O EAST	58341
50	58346
100	58341
150	58 341
200	58339
250	58340
200	58344
350	58 347
400	58 354
450	58372
500	58388
550	58410
600	58 405
650	58 398
700	58,390
750	58387
800	58-376
850	58354
900	58365
950	58370
1000	5837Z
1050	58374
1100	58380
1150	58387
1200	58395
1250	58403
1300	58414
1350	58426
1400	58435
1450	58 446
1500	58 458
1550	58 477
1600	58 487
1650	58 504.
1150.	58390.
	<b>/</b>

.

MT. GUNSON MAGNETIC SURVEY 12.9.83. TRAVENSE TIE IN READINGS. 000087

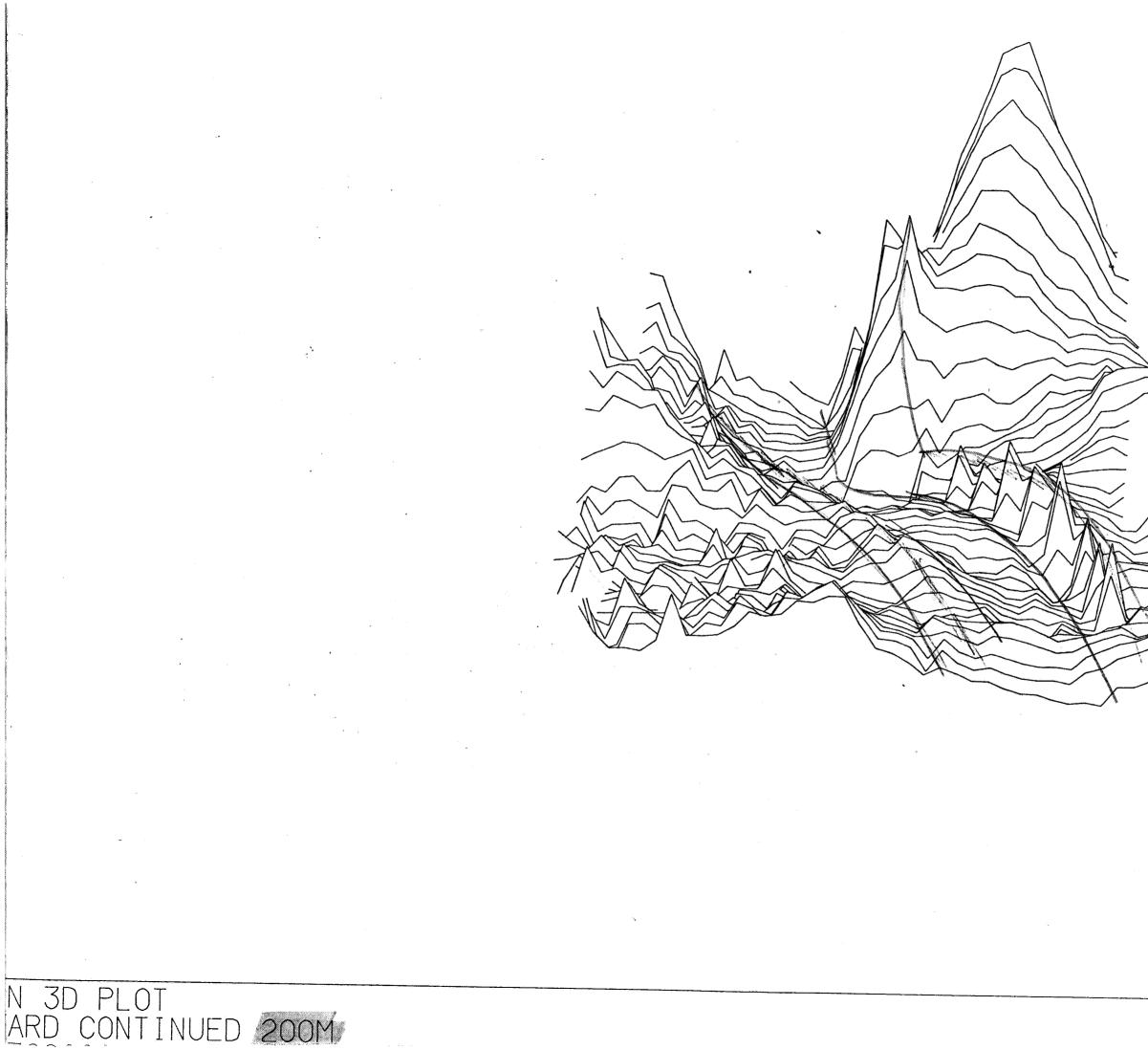
STN	KEASING.
SOLD GEOPHYSICS GAID	
19000 N 5000 E	58 324
19000 N 4600 E	58342
HAURAGE RD TRAJERSE	
50 BAST	58 332
/00 *	58 329.
MG. 87 TRAVERSE	
SO EAST	58209
100 "	58221
PIDE LINE TRAVERSE	
So EAST	58156
/00 "	58156
AIR STRIP TRAVERSE.	÷
SO EAST	58062
100 -	58061
	•

MT. GUNSON MAGNETIC SURVEY 12.9-83

880000

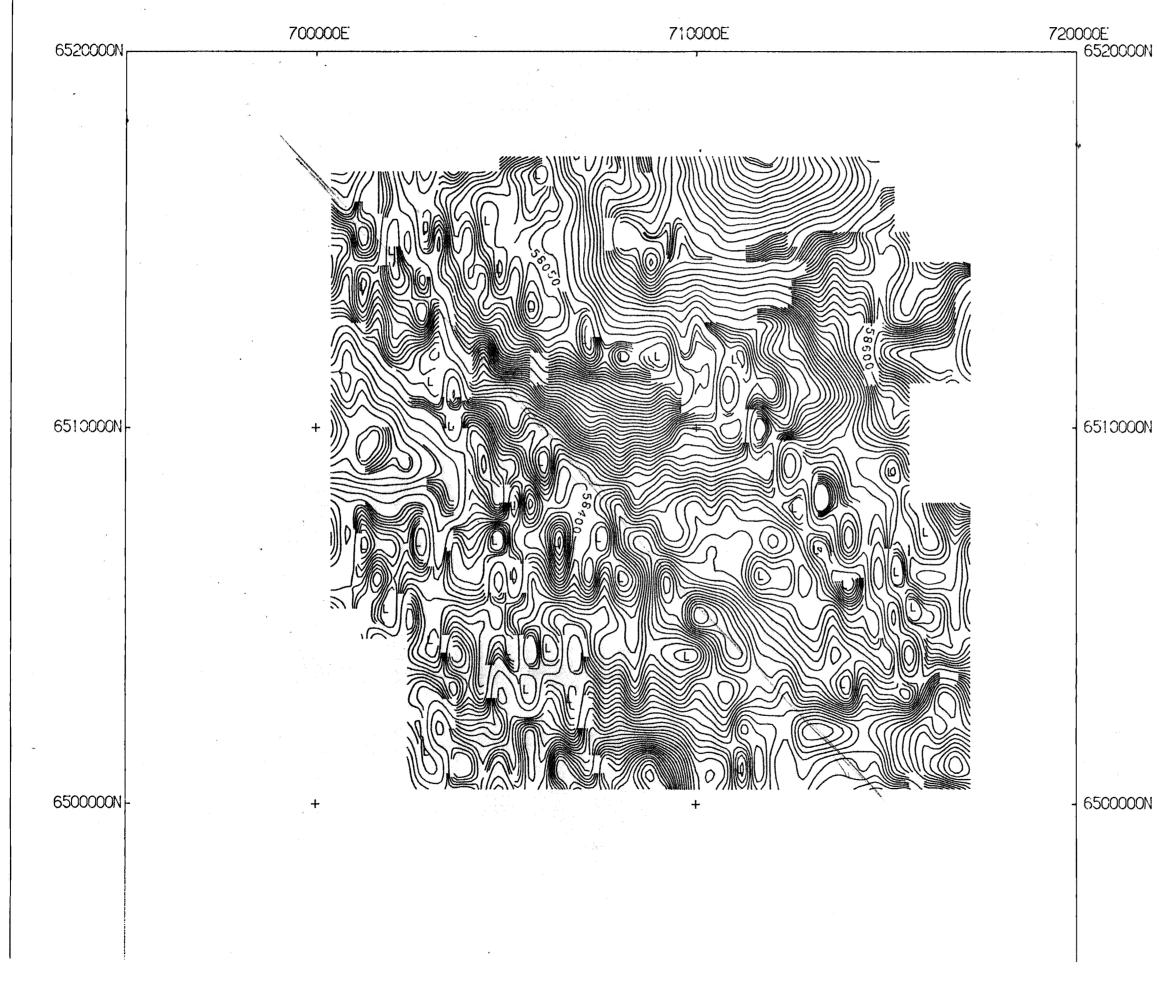
# MG. 87 TRAVERSE

~ I	A . (
STN	READING
200 WAST	58213
150 "	58 215
100 m	58 213
50 "	58 210
O EAST	58 219
50	58 225
100	58 227
150	58 228
200	58 234
250	58 243
300	58253
350	58-267
400	58 284
450	58 301
500	58337
550	58 <b>33</b> 8
600	58 335
650	58 336
700	58 329
750	58 325
800	58323
850	58322
900	58 323
950	58 322
1000	58325
1050	58330
1100	58338
1150	58346
1200	58 354
1250	58 364
1300	58.374
1300	58379



. . . . . . . .



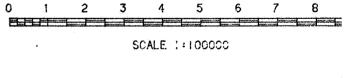


### DATA SPECIFICATIONS

000090 1 KM & 0.5 KM LINE SPACING: 200 METRES STATION SPACING: DATE ACCUIRED: JUNE-SEPTEMBER 1982 ACQUIRED BY: SOLO GEOFHYSICS ADELAIDE S.A.

#### PROCESSING SPECIFICATIONS

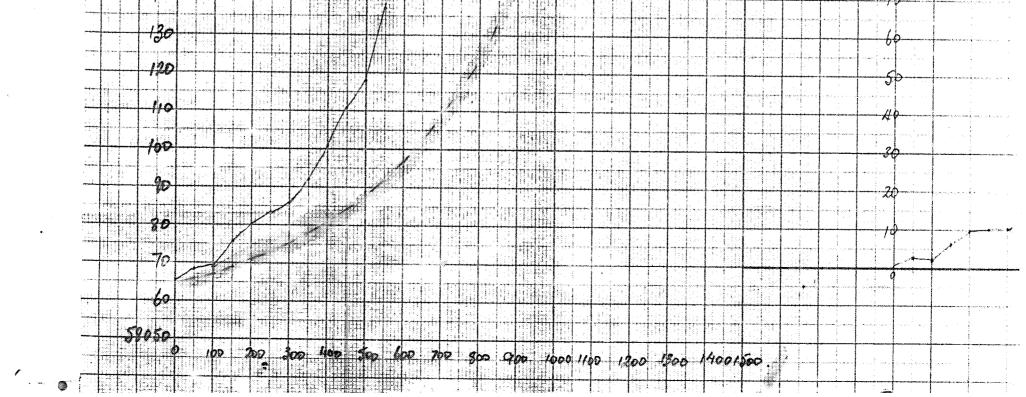
GRID SIZE :	5Cm X 5	-
REGIONAL :	CRIDDED DATA DOWNWARD CONTINUED	2
RESIDUAL :	CRIGINAL GRID MINUS DOWNWARD	
	CONTINUED DATA	





GRID NOTATION REFERS TO AUSTRALIAN MAP GRID ZONE 53

					BCAN						PRITISH MADE							MA	ET	1C		Suk									
	340								₩	n N N N N N N N N N N		i de secondo de secondo				1.00	F	TIR	1 2 2	STI	RIP	-	TA	AUF	RSE				*****		
4	10				1.44												-				1.		÷7			•		1		ana ana ana na 1971. T	
	32																							••••••						•	ς.
					1				ti-		• • • • • •	-	-				• • • • • • • • • • •				•	A		en e	1						
++	325											-		4					1973						1		_				a kanga k
	ting the set	1EI 1							rigi			d th			0.0 <b>00.0</b>				i 1900-mark 1	a	- 1	4		i e e colonnario E	er a harmad a ge	2 	w				
	310												1					-			11		-							, en estanos e	
Lau - Jan - La	300	<u> </u>												-					ф		11			nganan jarraman jarrama	•	n sa			1		
										an air an		1.		/		7			-		141			t. . n. mail means						n, 1989-19-19-19-19-19-19-19-19-19-19-19-19-19	#1000000000000000000000000000000000000
	290					<u>i de la com</u>	1						$\downarrow$				~				1				ļ					ana an i	
y., <b>.</b>			• • • • • • •	÷-		-+-	╞┅╢╍		57.9°			4	1	a for a scar	₩4 * 6 ¢	÷	•••••			en en en en en	4	en e		an starting							
*****	280					••••				<del></del>	-		∦							-r	ļ								• • • • • • •	γ.,	
1979 - A. 199	270	ne siste och en en S						ر به موقع <mark>معا</mark> ر ا		e	e le p	dyak.	1	1		••• •	2012200	a ta ka saya	i contra	l f		e normalija L		20 - 2 <b>1</b> 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	in dia.	-			1		
en manie i ranne i ranne	2.10									*****			†					1											•.•.•• ()	an an an tairte	
	260									anser a l'algera		1				and and a	** 1.5.5. 2	•		7				analana J	n na sinana J	· · · · · · · · ·					
i 13., mijerim		د. مربع ومشعده					(*		÷			$\left  \right $								<i>[</i>									•.•	n, 6 m n, 5 m 1	
	250		1										Ì			110										1		; ;		parameter of the state of the state	And and a second
	and tailed						に北口					1-	erenter e		hanaaq	****	anjaran karap	-	_/					a de la serie	an article				į		
	-tho			+	-+						-	1							1									+70-	•••••••	es, e se se se	
	230			111		t luli						1	, strang				2 •		T-T-		×		i	in the second se		· · · · ·	1.000		1		
	*30				1.1.1	743					$\uparrow \uparrow$	1						11	<del>د زر د</del> ر				-+-				•	160		ang si si	
	-220										11						2 <b>4</b> 5 <b>7 7 7 7 7</b>	t	artige L					en edenami T	in na terren 1 1	an ann a' san		150-			
	9 <b>9</b>			-	++++						11.		a a Se <del>rie</del> r		++++		: : ••••			178-March (0.101-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-								100-		1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 -	
	-210										<b> </b>												_				1	iko.		r. 4.445 10,000 10 4	40, Y
								- ++++	++-+-	÷, e	1-		in an								معدد المعرف	, viene i su		***		e e por l'anga					
	-200								+++		1						Y	1 1										130-			Marina ( Marina
	190			111						$\uparrow \uparrow$														ner konstan j	i malana.		-		1		
11.143 1	10																1			****						1	1	120		Na Maria (Marina ang Karangan Sang Karangan) Karangan Sang Karangan Sang Karangan Sang Karangan Sang	17 S. M. M. M.
	180																					filmen (m.			****	1 Pass 48	1	110		(	
-				-		-444		i <b> </b>							 													110	******** ¥ 7,8*	• 3.• 4.000 · 4.00	* 54 *
	170	<u>.</u>					<b>F</b>	A Sarte		1							-					i						100-			
				er en						$\left\{ \right\}$		-	s ever					line +			Ang a	. emotion	, <b> </b> ,	a Antonio antonio Antonio antonio	i ver i sere e	х ж.					
	-160									4	-				1.3379				-									90-		i nagana t	· •
									1	+		•••••					· .							• •	and the second second second	no se	- N - N.				
	120							5.8	11		1					$\ $											1	Şþ		allinia itarpo panto nagingang	<b></b>
	1/10										1.000			1											A A Andrea granating			••••		-	
	1 1			1	- 17		题出出		T			1		1.61			1	1								+	+	7þ—		والراجية والمتحمية	



\$

VETIC RAVERSE	SURI	IE1		/	12.	9 -	83														1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 -				
RAVERSE		-														-			-  +						Ē
										• • • • • • • • • •		1.1			•• <del> </del>								+++++++++++++++++++++++++++++++++++++++		
																						44-4 - 4-4			-
and the set of addition of a set of a s																									
,		-														n)r			•••• ••• •••			-			
<ul> <li>A second s</li></ul>	a di ta parti a su di ta p												,   , , ,				erti								
						•	-		+++	**															, . 
n i tavar sir s merenadar		70																							
		,		n an							$\left  \right $	$\left\{ \cdot \right\}$		•	-					-			-		
		land and			1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.					- 7	/	$\backslash$													
n n Shridh <b>i</b> way synyawyy ngy n		\$0									<b>İ</b>		$\overline{\langle \cdot \rangle}$		1										
n - nan - nandara ana ana ana ana		£10					•			1															
		<del>30</del>					-									) ) j 									
an a		10				•	++-		+++++++++++++++++++++++++++++++++++++++	1				V	-										
e (1. a e (1. a e (1. a		10		· · · · · · · · · · · · · · · · · · ·					1	4															
· · · · · · · · · · · · · · · · · · ·		90							$\parallel$																
t suiste terme	9	o							1						ţ÷										
	\$	`p							# _				engente de la factoria. La constante de la constante de		¥.										مین <del>د و</del> د ا د کر
2 	7	þ									T							***							
e e e e e e e e e e e e e e e e e e e	6										T					$\overline{\mathbf{A}}$		·							
	5	<b>b</b>			*****			1		~~ • ~ • • • • • •					ļ		$\overline{\mathbf{A}}$						ŗ		14 11 11
	#	a ser a contractor	the state of the second state of	a , e , el planadare e		-	1							~			$\left  \right $								
		ti sana. A	a series a series	ا سیاسہ (یوجہ ا	n dan ay									****											
	-		and the second			K				*								Å							
n in ering of the sold dery on d					7												•••• ••• •••								  
1997 - 1998 - 1998 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 -	/c	<b>}</b>			<b>.</b>									-											
andre and a support of the support o					<b></b>				<u>}</u>						4					14	90				, ; , , , , , , , , , , , , , , , , , ,
n de service metalementes métalementes de la constante de la const				ev vi [*] en pa					$\mathbf{z}$	1	K.			12											
БО.	n na series and series		The second secon							-		1			1										
•		n an an an an san an a						1 1		4				1					I			[ <b>**</b> ]			4.44

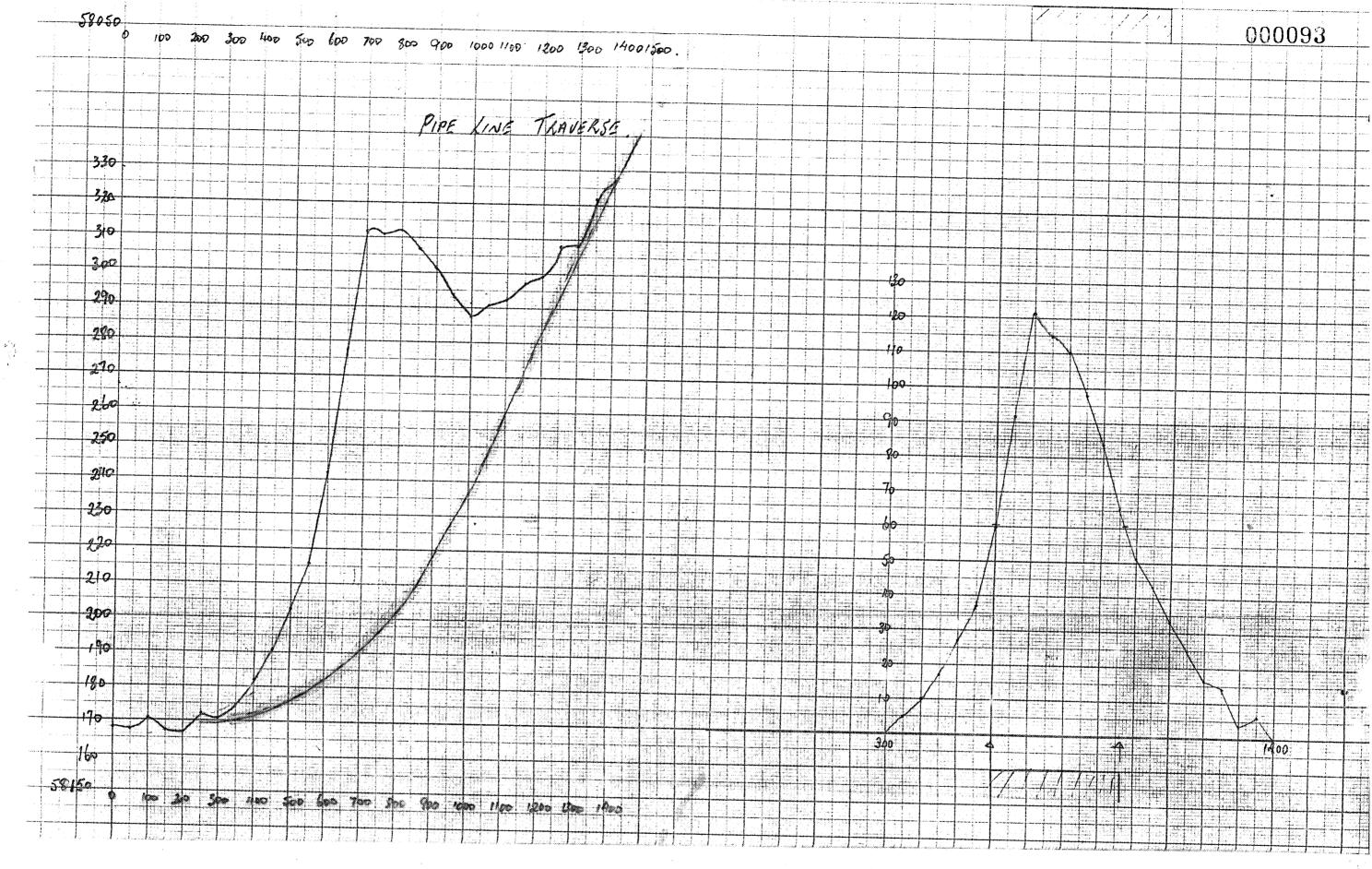
ų,

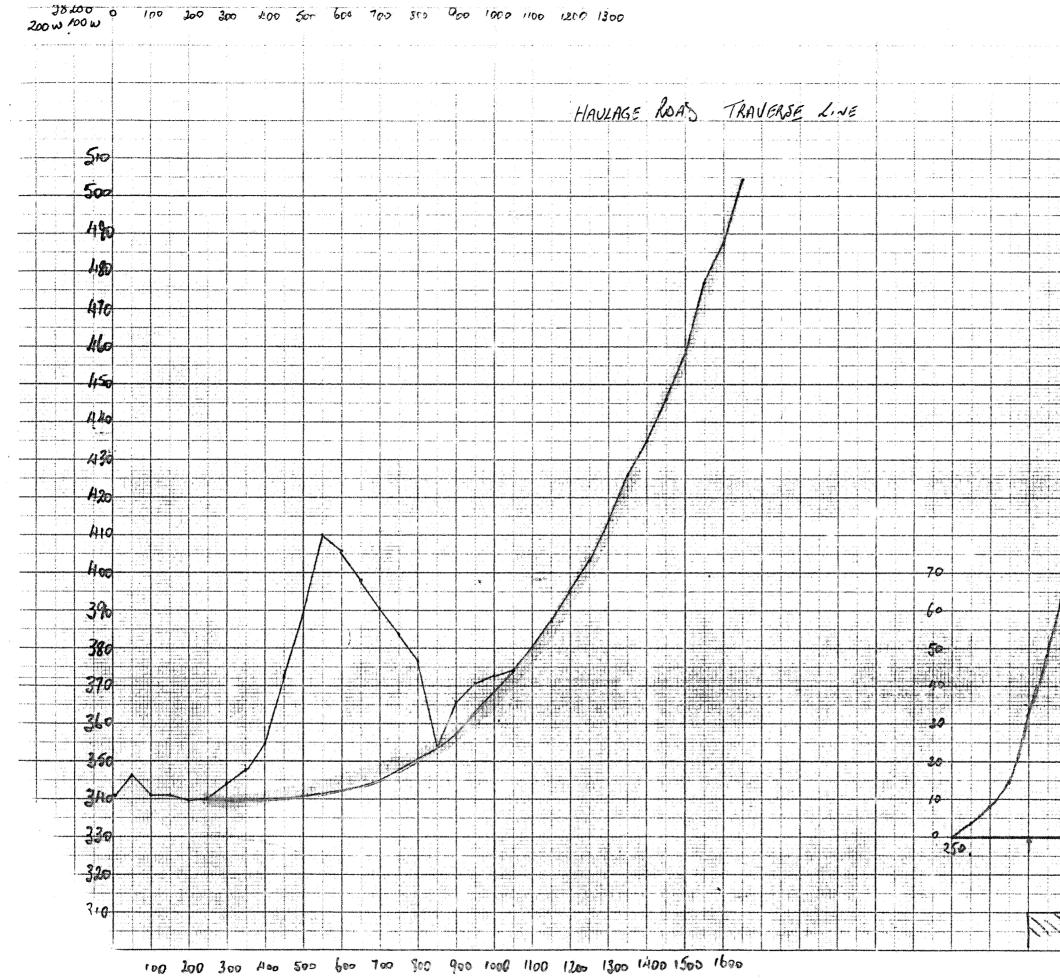
1 ÷ ( . h: 123.4 9. L. S 130 n y man y ana s tine time ~~~}; **** jja. e e california E 4 . . ł a tangan a -. . ana din ي. ساينې ŝ. -------..... · · · · · · · · · · · · 1.1 ·•••• • • • • • 1 -----..... .... . . . . . 180---------anatoria B la ser la s 1 e por al filosome 20 • 10,000 and 10,000 و موتيد بالد من . . a fara tas Ĭ0

1. N. a si si di si a a si ..... in the first spectrum of the second se ł

bo. ..... . 

· h ana yan 





100 200 300 200 500 600 700 500 000 100 1200 1300

14 4/// 000094 • ...... • d. - 4 400 30 4 5 걸렸 **a**tar 14. 神经 湖田 44 ----ninan (nganan) mananga yan mananga yang t de la composición d La composición de la c 귀단 ing in 무다 . 12 đĒ 3 3 ÷Ŀ ard cia 144.44  $T_{-}$ 143 1050 550-i fizi Data & Dry Est W. Natsen Supervises J.L. Centes 11

