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EL 1974 CHARLOTTE WELL

ANNUAL AND FINAL REPORTS FOR THE PERIOD 1/8/94 TO 3/6/96

Submitted by

CRA Exploration Pty Ltd 1996

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ENVELOPE 8962

TENEMENT:

EL 1974, Charlotte Well

TENEMENT HOLDER:

CRA Exploration Pty Ltd

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CRA EXPLORATION PTY LIMITED A.C.N. 000 057 125

SUBJECT:

SECOND AND FINAL REPORT FOR EXPLORATION LICENCE 1974

CHARLOTTE WELL, SOUTH AUSTRALIA FOR THE PERIOD ENDING

7TH MAY, 1996

AUTHOR:

S.P. NEWBERY

DATE:

JUNE, 1996

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CRAE REPORT NO.:

22182

CRA EXPLORATION PTY. LIMITED

ANNUAL REPORT FOR CHARLOTTE WELL EL 1974, SOUTH AUSTRALIA, FOR THE PERIOD ENDED 31ST JULY, 1995

Gairdner SH 53-15, South Australia

AUTHOR:

M.G. BARLOW/ W.A. STEWART

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1. SUMMARY

Charlotte Well EL 1974 was granted to CRAE on August 1994. Exploration in the past twelve months has concentrated on the Pinery Dam and Pascoe Well prospects, with base metals as the primary commodity.

The Pinery Dam prospect was first identified by BHP in the 1970s. Drilling in 1977 failed to intersect rocks that could explain the magnitude of the magnetic source and it appears likely that the holes terminated in intrusive dykes.

Ground magnetics undertaken in 1994 over the Pinery Dam anomaly were designed to define the anomaly geometry and facilitate the placement of a series of holes to fully test the body.

Three holes were aimed directly over the body and intersected doleritic rock at 13m. While susceptibility measurements of 4000 * 10⁻⁵ SI were recorded, they cannot adequately explain the magnetic anomaly. Holes drilled to the periphery of the anomaly intersected Gawler Range Volcanics.

The second area of interest was the Pascoe Well prospect, where a north east trending graben had been interpreted from the recently acquired A4 SAEI aeromagnetic data. A mineralisation setting broadly similar to Mt Gunson was interpreted and exploration work was aimed at targeting trapping mechanisms for migrating fluids, such as unconformity surfaces and bounding faults. The concept was tested with across-strike traverses of gravity, ground magnetics, CSAMT and a series of TEM soundings.

While the gravity and ground magnetics confirmed the general graben geometry, there was some disparity between the two data sets as to the exact positions of the bounding faults. Ten line kilometres of CSAMT and 20 TEM soundings were undertaken across zones of interest but only weak conductors were detected.

Despite the lack of encouraging results from the electrical geophysics, five holes were drilled along the traverse to test various aspects of the graben and to test a discrete magnetic anomaly on the northern edge of the northern horst. No significant results were obtained.

2. INTRODUCTION

Charlotte Well EL 1974 was granted on August 1st 1994. The tenement covered an area of approximately 2406 square kilometres, 70 km to the west of Woomera, South Australia. The EL was reduced to 230 square kilometres after the first year of exploration. Plan SAa 6255 shows the location of the tenement as well as the current EL boundaries.

EL 1974 covers the northern part of Lake Gairdner. Lithologies are dominated by Proterozoic rhyolites and dacites. Pandurra Formation onlaps the basement to the west, and is unconformably overlain by Adelaidean Tent Hill Formation. Numerous north-west trending dykes of the Gairdner Dyke swarm intrude the basement and Pandurra Formation. Occasional north-east trending dykes can also be discerned in the magnetics. Jurassic/Cretaceous Sediments overlay basement and Adelaidean to the north.

The area was flown with magnetics as part of the A4 South Australian exploration initiative (SAEI) in April/May 1993. Exploration interest focussed on a north east trending graben, identified from the airborne magnetics and referred to as the Pascoe Well prospect. A reevaluation of the BHP Pinery Dam prospect was also undertaken.

3. CONCLUSIONS

Additional ground magnetic work and drilling at the Pinery Dam prospect has failed to adequately explain the very large magnetic source at this site. No further work is warranted however, due to the unprospective nature of the rock (dolerite) intersected.

Gravity and magnetics at the Pascoe Well grid defined a possible graben structure in basement. If sagging and compaction of suitable sediments within the graben had occurred then potential exists for base metal mineralisation in geochemical and structural trap sites of migrating fluids.

Strategic zones within the graben were tested with CSAMT and TEM soundings. No significant conductors were recorded. It was also shown that the area is not particularly amenable to these techniques due to very conductive, near-surface conditions.

A fence of five drill holes placed across the graben intersected the Tent Hill and Pandurra Formations at similar depths. The data indicated that graben formation had been predepositional to these sediments and that the traverse was on the extreme edge of the basin. No significant results were obtained and no reducing sediments were intersected.

4. INVESTIGATIONS

Exploration focussed on two prospect areas:

Pascoe Well

A NE-trending graben 8 km wide with basement highs to the NW and SE was interpreted from aeromagnetics (MESA, 1993). The graben is in the vicinity of a number of unconformities between Gawler Range Volcanics, Pandurra Formation, Adelaidean Tent Hill Formation and Jurassic/Cretaceous sediments (Blisset, 1977). The Pandurra/Adelaidean basin deepens eastwards.

The setting is broadly similar to that at Mt. Gunson and it was conceived that mineralisation may be trapped geochemically by suitable sediments (e.g. reducing) within the Pandurra Formation or Tent Hill Formation on the edges and tops of the interpreted horst structures. The graben is a potential focus for fluids deriving from sagging and compaction within the graben and from the deeper basin to the east. The unconformity surfaces, graben faults and boundary faults are suitable conduits for such fluids. This concept was tested and defined by a variety of geophysical methods and drilling.

Pinery Dam

Interpretation of aeromagnetics (MESA, 1993) identified a discrete magnetic anomaly, $3.5 \, x$ 1.5 km, near Pinery Dam. This anomaly was previously recovered with ground magnetics by BHP (1977) and drill tested with one hole. Dolerite was intersected at 23m depth, and the main magnetic mineral was ilmenite. It was possible that the hole intersected one of the many Gairdner Dykes rather than the cause of the anomaly.

The anomaly was followed up in this reporting period with ground magentics and drilling.

4.1 Ground Magnetics

A total of 22 line kilometres of ground magnetics were recorded to test magnetic anomalies identified from the A4 SAEI aeromagnetic data. The data were recorded over seven grids and two north south traverses across a postulated half graben at the Pascoe Well prospect. Locations are shown on plan SAa 6504.

Plans SAa 6488 and 6328 show magnetic profiles for traverses 7700E and 8000E across the Pascoe Well graben respectively.

Between stations 16800 and 18400N on line 8000E, the traverse follows a buried pipe line and the data is contaminated by high frequency noise. Spikes at 12400, 19200 and 8200 on the same line, relate to intrusives across the magnetic basement and are possibly responses associated with various dykes.

Overall, the data confirms a basement high on the northern edge of the traverses with a rapid increase to magnetic basement to the south at stations 49000N and 18800N on lines 7700E and 8000E respectively. Line 8000E also shows that the basement appears to be shallower towards the southern margin of the traverse, in agreement with the proposed graben model.

Ground magnetic profiles for the grids labelled A to F are included as Plans SAa 6492 to 6497. They were targeted at various dykes on the up block portion of the Pascoe Well graben. In all cases the aeromagnetic targets haves been identified and represent magnetic anomalies of 100 to 200nT on the ground. All the anomalies with the exception of E appear to have depth to tops of between 50 and 75m. The depth to the top of the source for E appears to be slightly deeper at 150 to 200m below surface.

Eight line kilometres of ground magnetics were completed across the southern part of the Pinery Dam anomaly, presented on plan SAa 6491. Ground magnetics and drilling was undertaken at this site by BHP in 1977, but previous work failed to adequately explain the high magnetisation. The new grid was designed to provide additional, detailed mapping of the anomaly boundaries for a planned 'fence' of drill holes to positively identify the causative body (see the section on drilling in this report).

Due to the very shallow nature of the target, the magnetics clearly outline the boundaries of the body. Modelling suggests that the susceptibility exceeds 10000 * 10-5 SI, twice that recorded in the BHP hole. Demagnetisation and/or remanence may need to be invoked.

4.2 Gravity

One hundred and sixty gravity stations were recorded at 100 m intervals along lines 7700E and 8000E on the Pascoe Well grid. Bouguer gravity and elevation profiles are presented in plans SAa 6489 and 6490 for line 7700E and plans SAa 6329 and 6330 for line 8000E. Data listings and processing sequence are provided in Appendix II.

The data has been reduced with a Bouguer reduction density of 2.3 g/cc. This was found to be the optimum in reducing correlation between elevation and the gravity profile. It is also considered to be realistic in view of the fairly thick sequence of overburden and weathered material present.

Line 8000E shows basement block highs on the northern and southern edges of the traverse. While both the gravity and magnetics put the northern edge of the southern block near stations 8000 to 8400E, there is a disparity of over 3 km between the data sets for the southern contact of the northern block. One possible explanation is that the northern block is composed of banded volcanics with only the most northern half being magnetic.

Assuming a depth to basement on the northern block of 50 m (based on the magnetic modelling to the top of the dykes) and a density contrast of 0.3 -0.4 g/cc, modelling suggests that the depth to basement in the centre of the graben is at least 150 m from surface.

4.3 Controlled Source AMT (CSAMT)

Three sections of scalar CSAMT were recorded along line 8000E, shown on plan SAa 6503. CSAMT was employed in an attempt to define the geometry of the postulated graben and also to detect any electrical contrasts associated with mineralisation. In this regard, the contacts between basement highs and lows (based primarily on the gravity data) and the 0.5 mgal high between stations 12800 and 14000N were the primary targets for surveying. The sections surveyed were as follows:

- 1. 17275-19200E at 25m stations
- 2. 11600-17275E at 50m stations
- 3. 7600-10000E at 50m stations

The work was recorded by Zonge Engineering P/L of Fullarton, S.A. in October and November 1994. Recording details are provided in Appendix III. Sections of the raw data: impedance phase, Cagniard resistivity, and the static-corrected resistivity, and the contractors interpretation are contained in Appendix IV. Details of the static correction methodology are provided in Appendix V.

Plans SAa 6352 to 6353 show smooth model inversions for the CSAMT traverses. The proprietary inversion process is briefly explained in Appendix V.

Referring to the inversions and raw data, the following conclusions can be made:

- 1. The depth of penetration is limited to 200 m and normally about 100m.
- 2. A three layered geology is evident.
- 3. The first layer, or near surface has a variable conductivity and effectively maps topography; topographic highs, particularly dunes are resistive with lows being relatively conductive.
- 4. The second layer varies in thickness between 25 and 100m and is extremely conductive $(\rho < 5 \Omega.m)$. This has produced recording conditions where the near field occurs at very shallow depths.
- 5. A third, more resistive layer is evident along the entire traverse with resistivities of approximately 10Ω .m. With such a small resistivity, this is unlikely to be basement and probably represents either weathered basement or overlying sediments. It is shallowest between 18100 and 18600N with another slightly deeper section between 16500 and 17100N.
- 6. There are numerous single station anomalies (such as at 16300N) that possibly relate to near surface heterogeneities and should be disregarded.
- 7. Only one anomaly can be identified; a conductive feature centred on 17150N with a depth to source of 100m.

4.4 TEM

In-loop TEM soundings were also undertaken along line 8000E to detect conductive targets along or near faults associated with the graben geometry. The first set of soundings were recorded with a 100 * 100m transmitter centred on 18450, 17950, 17450, 16950, 16450, 15450, 14950, 14450, 13950, 13450, 12950 and 12600N. Work was recorded by Zonge Engineering P/L in November 1994 with details provided in Appendix III.

Decay curves for the loop placements are presented in Appendix VI. No conductors were identified but it was felt that the with the very conductive overburden, the loop moment was not large enough to provide sufficient sampling of the late time response.

The 100m soundings at 17950, 18450, 18850 and 18950 and 19050N appear to be contaminated by near surface IP effects, evident as the negative early time response.

A second set of TEM soundings were performed by the same contractor using a 200*200m loop, with the primary aim to test the CSAMT anomaly centred on 17150N. Transmitter placements were centred on 16450, 16850, 16950, 17050, 17150, 18450, 18950 and 19050N. Decay curves are presented in Appendix V.

No conductors or anomalous zones were identified. However, the larger transmitter has extended the useable data window by 20 msec out to 60 msec after turnoff. Note also that the IP effect on the 100*100m transmitter data at stations 18450, 18950 and 19050N has been removed with the larger transmitter geometry.

4.5 Drilling

4.5.1 Pascoe Well

One diamond hole (RC/DD94CW6) and four RC holes (RC94CW7 to RC94CW10) were drilled to test across the graben (plans SAa 6328, 6358, 6488). None of the holes intersected Gawler Range Volcanics and all ended in Pandurra Formation (Appendix VII).

Hole RC/DD94CW6 was drilled to obtain a stratigraphic section in the centre of the graben. Holes RC94CW7, RC94CW9 and 10 were drilled to test various portions of the interpreted horst and weak CSAMT conductors at 17150N and 18925N. Hole RC94CW8 was drilled to test a discrete magnetic anomaly on the northern edge of the northern horst. No significant assays were returned and no reducing sediments were intersected.

4.5.2 Pinery Dam

A fence of five vertical aircore holes (AC94CW1, AC/DD94CW2, AC94CW3-5; plan SAa 6491) were drilled across the anomaly for a total of 213m to identify the cause of the anomaly. Hole AC/DD94CW2 included a diamond tail (11.5m).

Doleritic rock was intersected in AC94CW1, AC/DD94CW2 and AC94CW3 corresponding to the magnetic anomaly (Appendix VII). Gawler Range Volcanics were intersected peripheral to the anomaly in holes AC94CW4 and AC94CW5 (Appendix VII). No significant assays were returned.

Two samples of the doleritic rock from the diamond tail of AC/DD94CW2 were submitted for petrological description (Appendix VIII). Sample 1156565 was collected from the interval 43.00 to 43.10m and sample 1156566 was collected from the interval 53.45 to 53.65m.

Susceptibility measurements from the doleritic rock did not match that predicted by modelling (max. 4000×10^{-5} SI). Magnetic remanence may explain this.

4.6 Diamond Indicator Sampling

As part of CRAE regional diamond sampling program, eight 40 kg bulk samples were collected from the top 20m of holes RC/DD94CW6, RC94CW7, RC94CW9 and RC94CW10 for observation of kimberlitic indicator minerals. Chromites were reported in two samples from the top 10m of CW9 and CW10 with negative results for all other samples submitted (Appendix I).

M.G. BARLOW

MGB/dt Reports/Charlotte Well

REFERENCES

Blisset, A.H., 1977. S.A. Geological Series Sheet SH5315 Gairdner. Department of Mines SA.

MESA, 1993. SAEI Geophysical 1:250 000 series, part sheets SH5311, SH5315 and SI5303. South Australian Department of Mines and Energy.

LOCATION

Gairdner

SH53-15

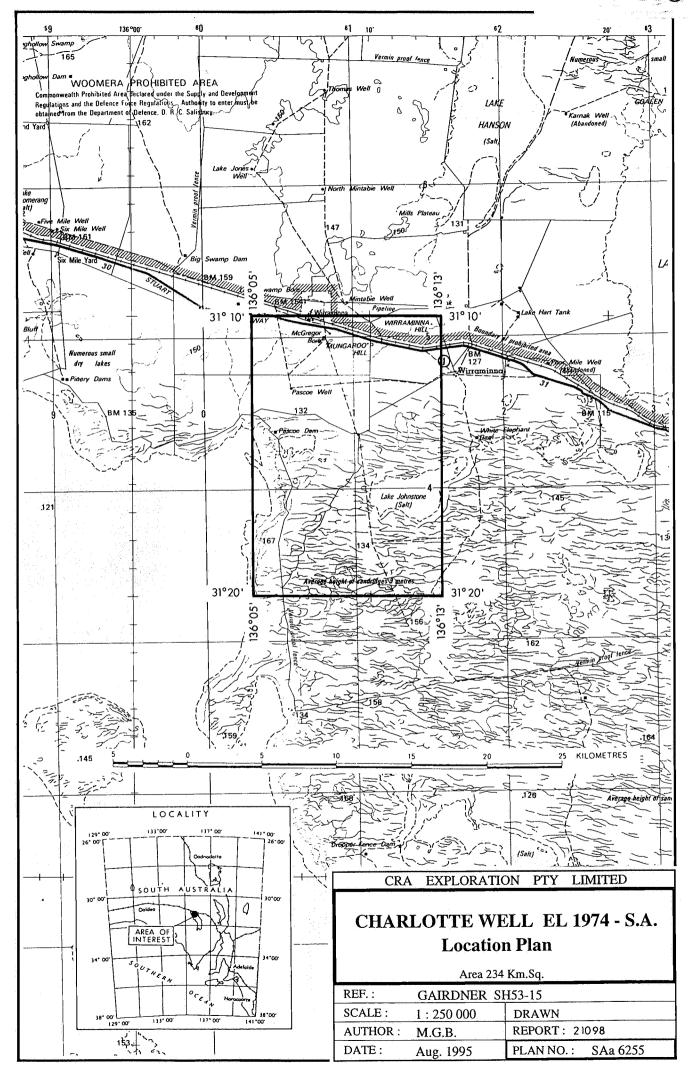
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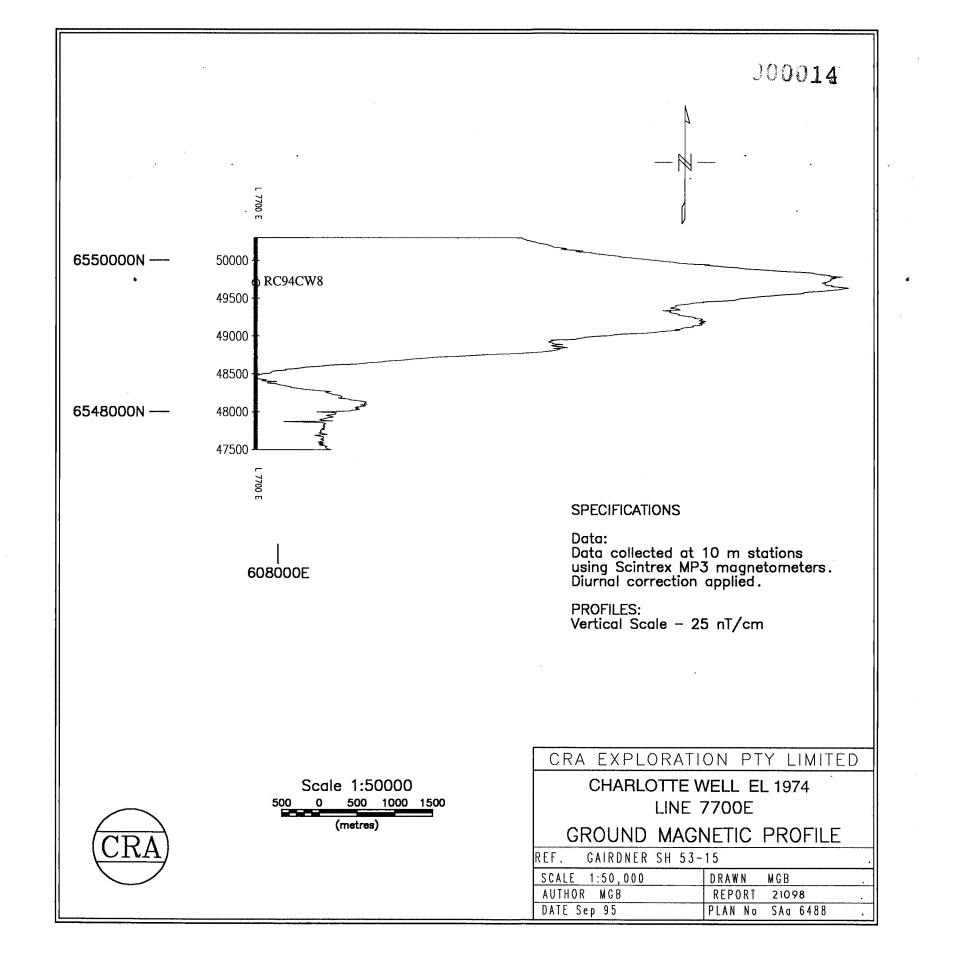
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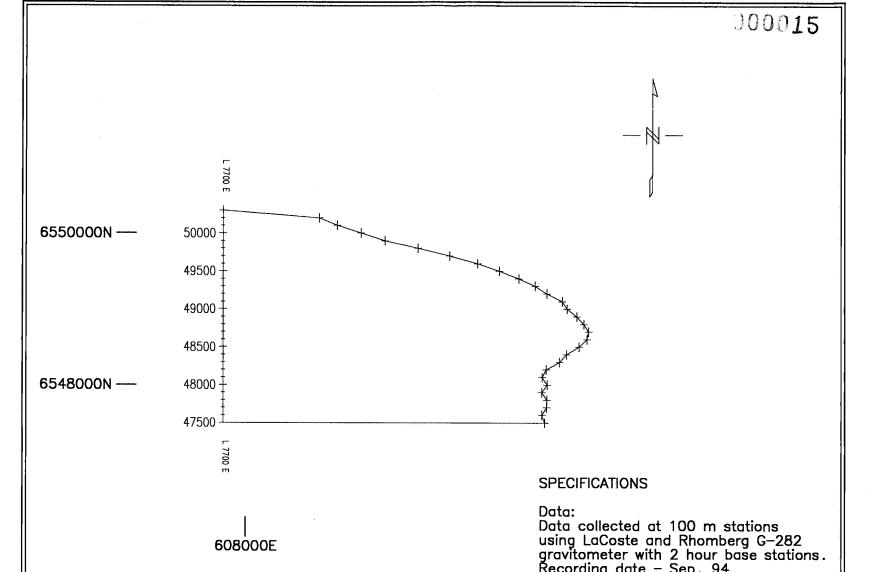
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LIST OF DPO'S

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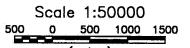






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using LaCoste and Rhomberg G-282
gravitometer with 2 hour base stations.
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Operator - MGB
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Profiles: Vertical Scale - 0.5 mgal/cm



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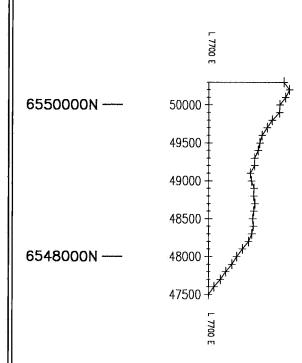
CHARLOTTE WELL EL 1974 LINE 7700E

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AUTHOR MGB	REPORT 21098 .
DATE Sep 95	PLAN No SAa 6489 .







608000E

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Profile: Relative elevation Vertical scale – 5 m/cm

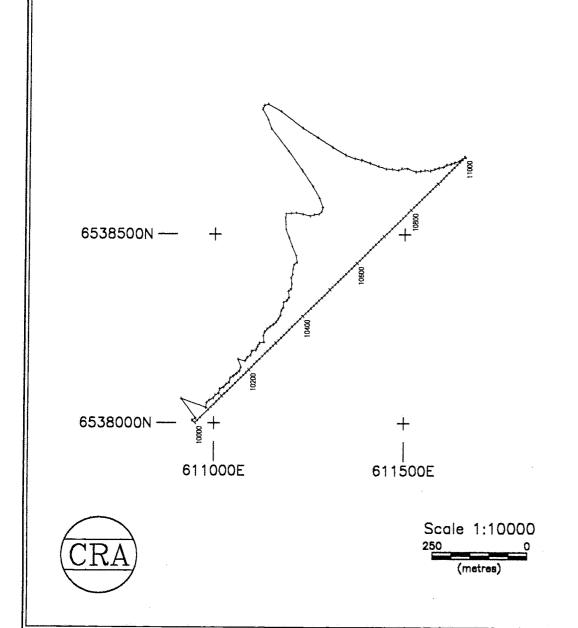


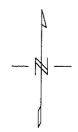
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CHARLOTTE WELL EL 1974 LINE 7700E ELEVATION PROFILE

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AUTHOR MGE	}	REPORT	21098	
DATE Sep 95		PLAN No	SAa 6490	





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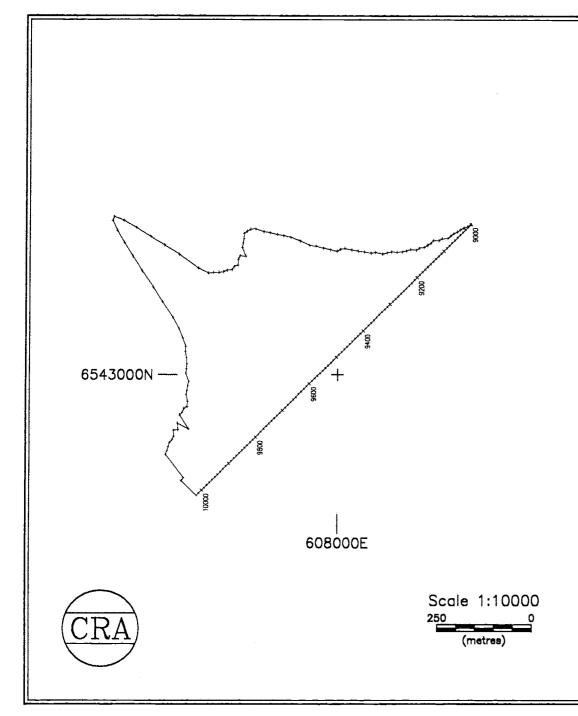
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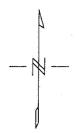
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CRA EXPLORATION PTY LIMITED

CHARLOTTE WELL EL 1974 GRID D

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AUTHOR MGB	REPORT 21098 .
DATE Sep 95	PLAN No SAG 6492 .





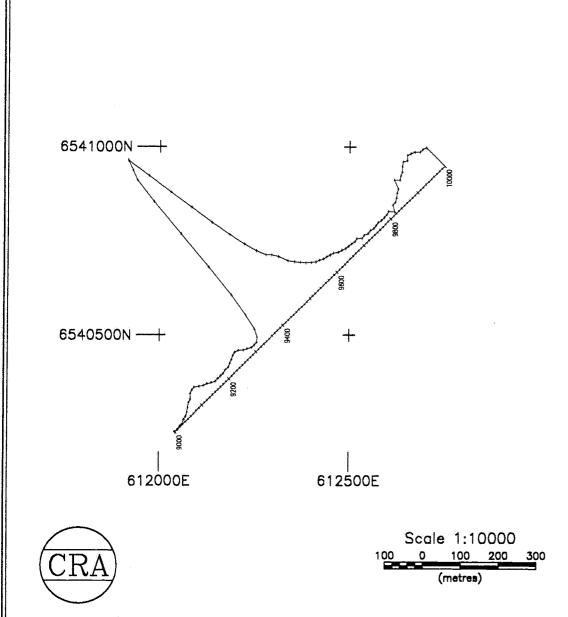
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Data collected at 10 m stations
using Scintrex MP3 magnetometers.
Recorded August 1994.
Diurnal correction applied.

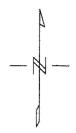
PROFILES: Vertical Scale - 50 nT/cm

CRA EXPLORATION PTY LIMITED

CHARLOTTE WELL EL 1974 GRID C

REF. GAIRDNER	SH 53-15
SCALE 1:10,000	DRAWN MGB .
AUTHOR MGB	REPORT 21098
DATE Sep 95	PLAN No SAG 6494 .





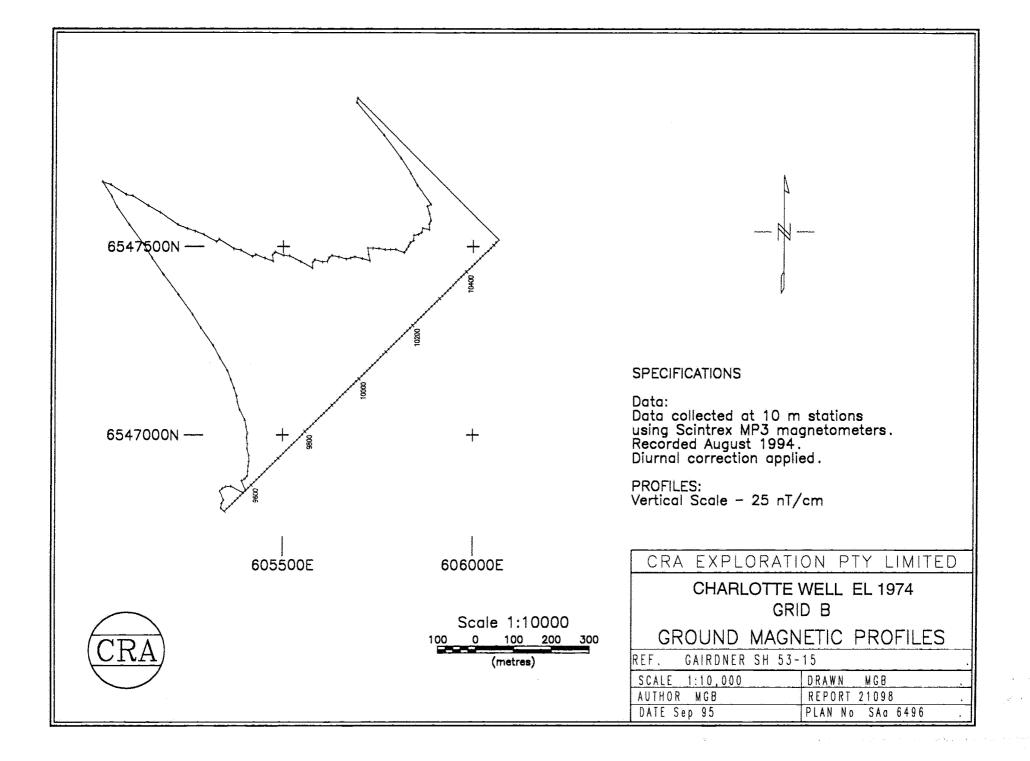
Data:
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using Scintrex MP3 magnetometers.
Recorded August 1994.
Diurnal correction applied.

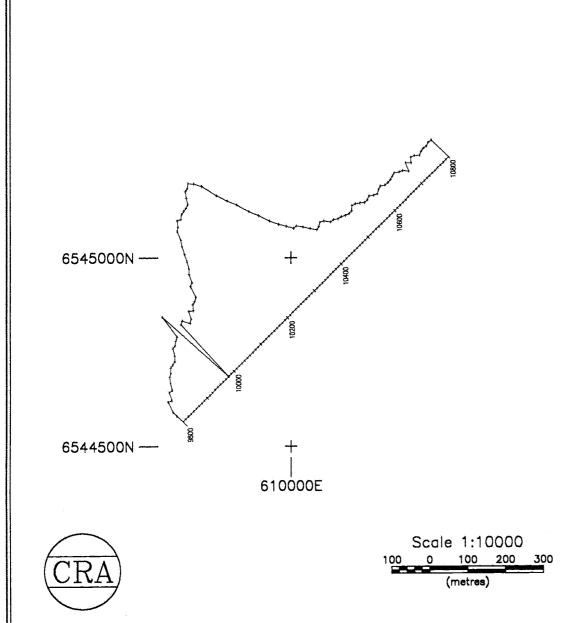
PROFILES: Vertical Scale - 50 nT/cm

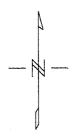
CRA EXPLORATION PTY LIMITED

CHARLOTTE WELL EL 1974 GRID F

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AUTHOR MGB	REPORT 21098 .
DATE Sep 95	PLAN NO SAO 6495 .







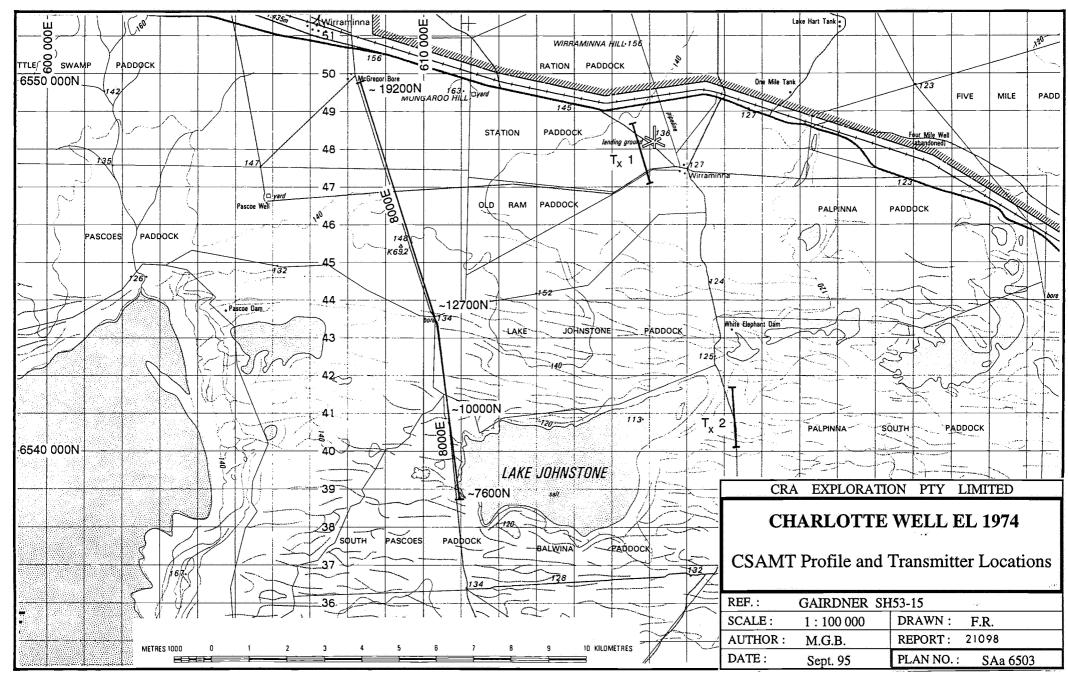
Data:
Data collected at 10 m stations
using Scintrex MP3 magnetometers.
Recorded August 1994.
Diurnal correction applied.

PROFILES: Vertical Scale - 25 nT/cm

CRA EXPLORATION PTY LIMITED

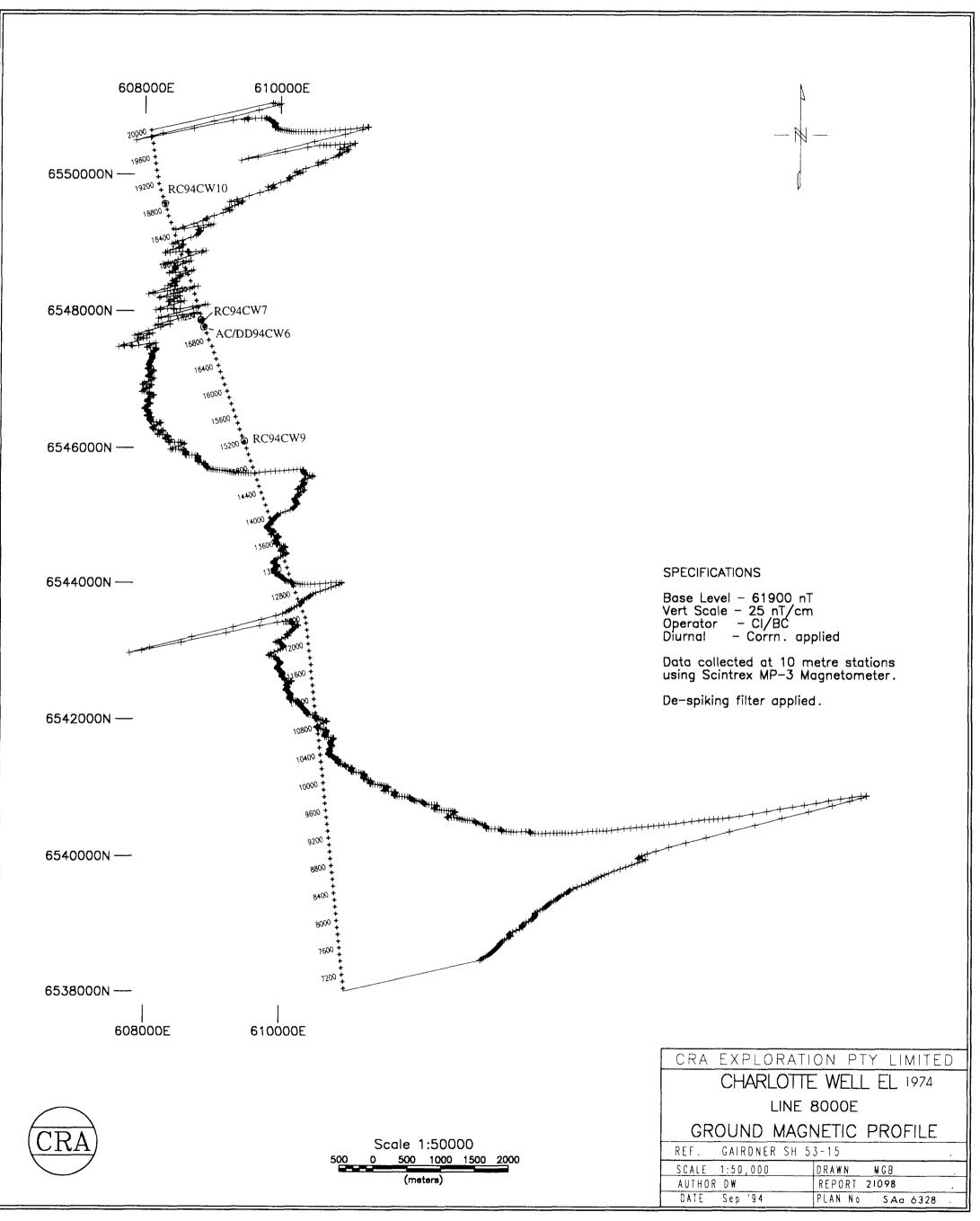
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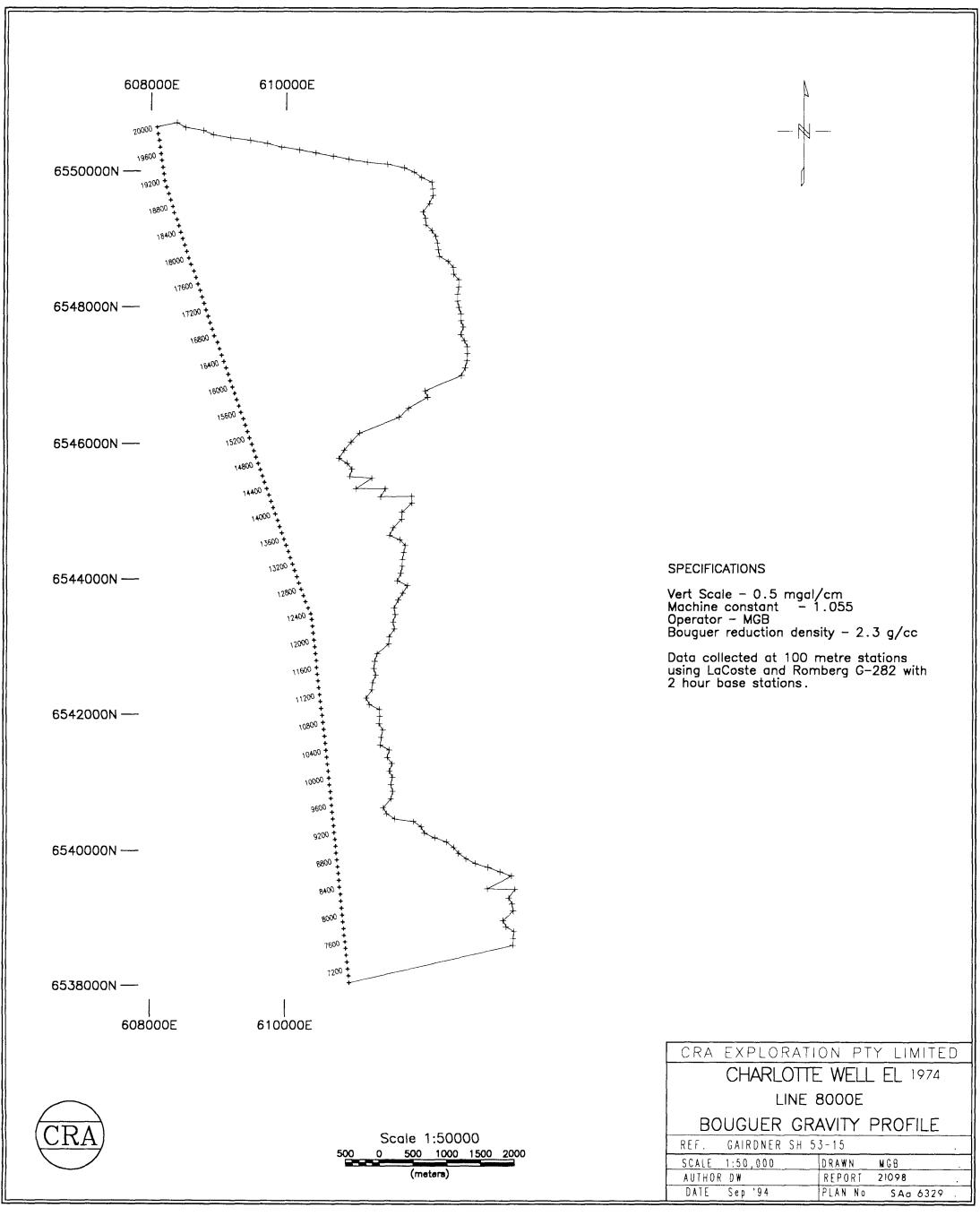
REF.	GAIRDNER	SH	53-	15			
SCA	LE 1:10,000			DRAWN	MGB		
AUTI	HOR MGB			REPORT	21098		
DAT	E Sep 95			PLAN No	SAa 6	497	

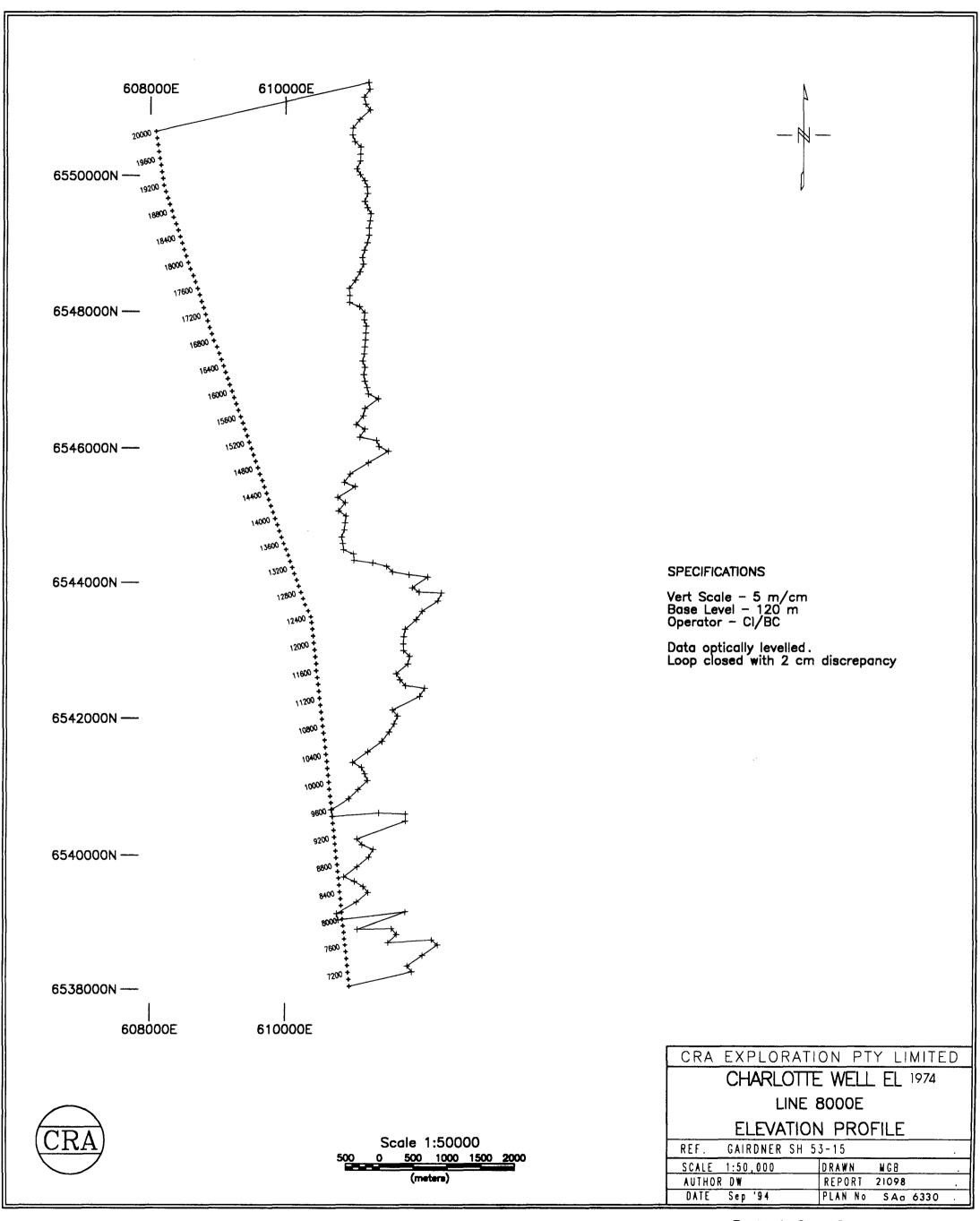


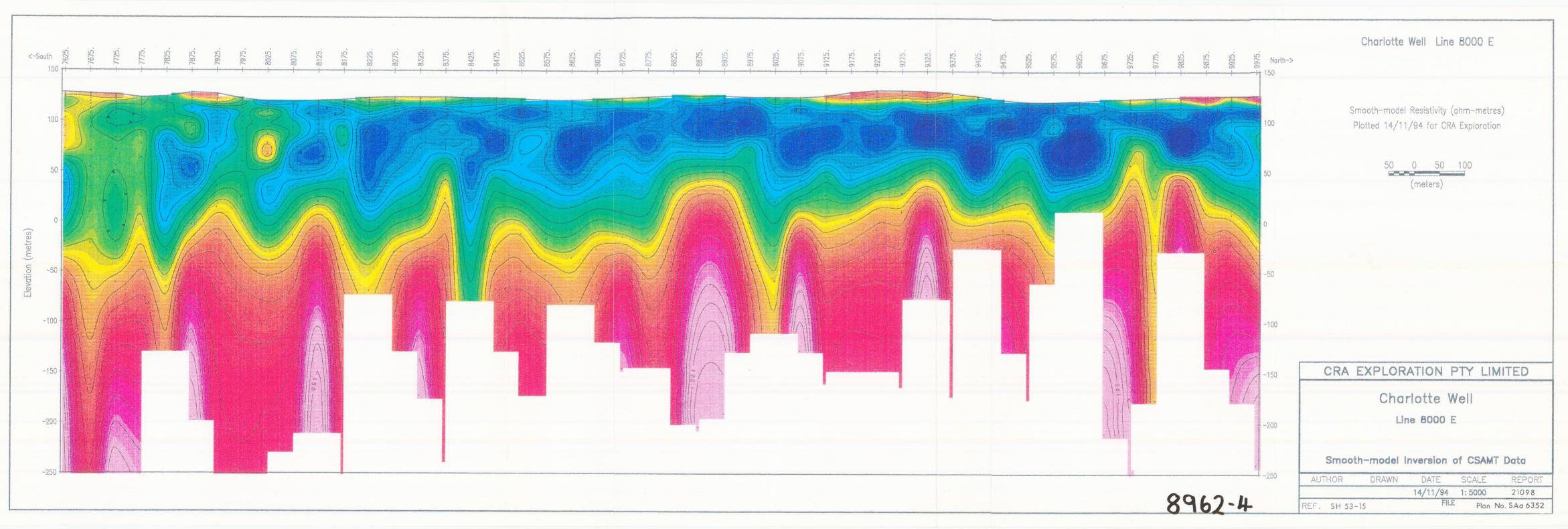
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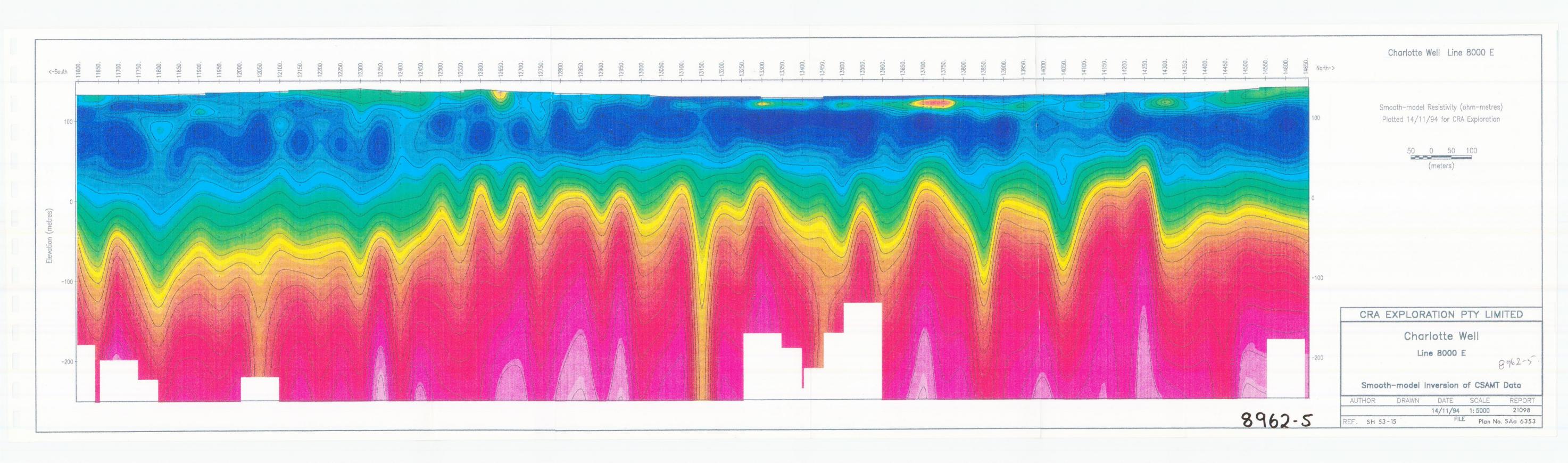
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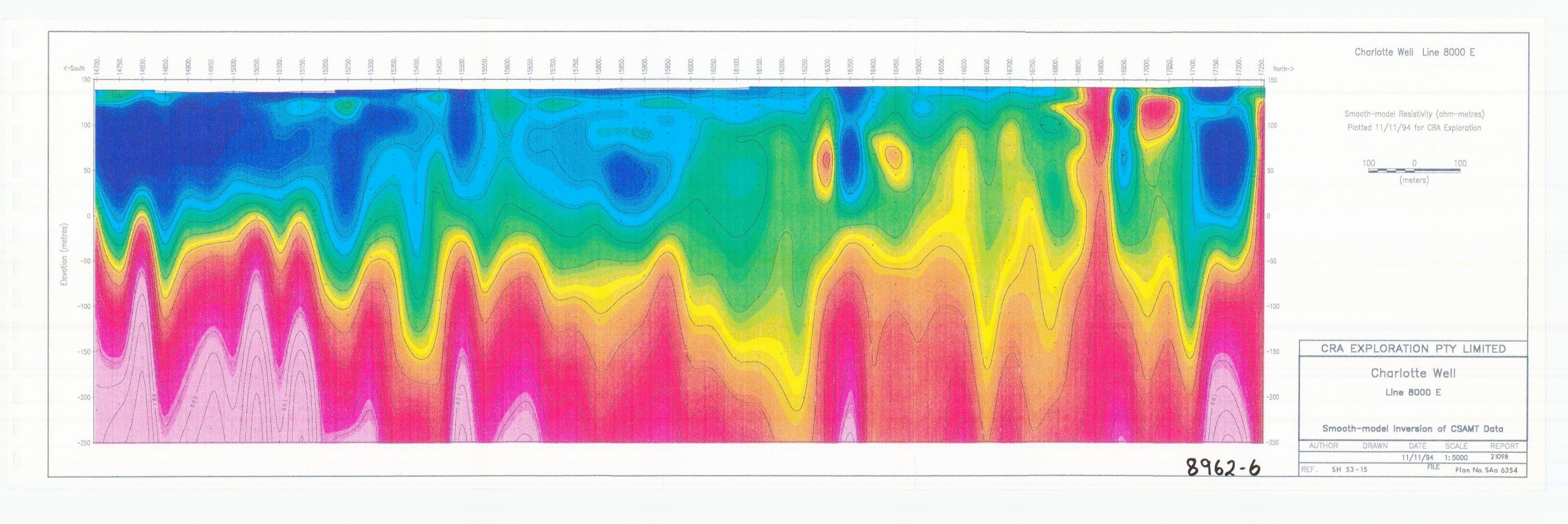


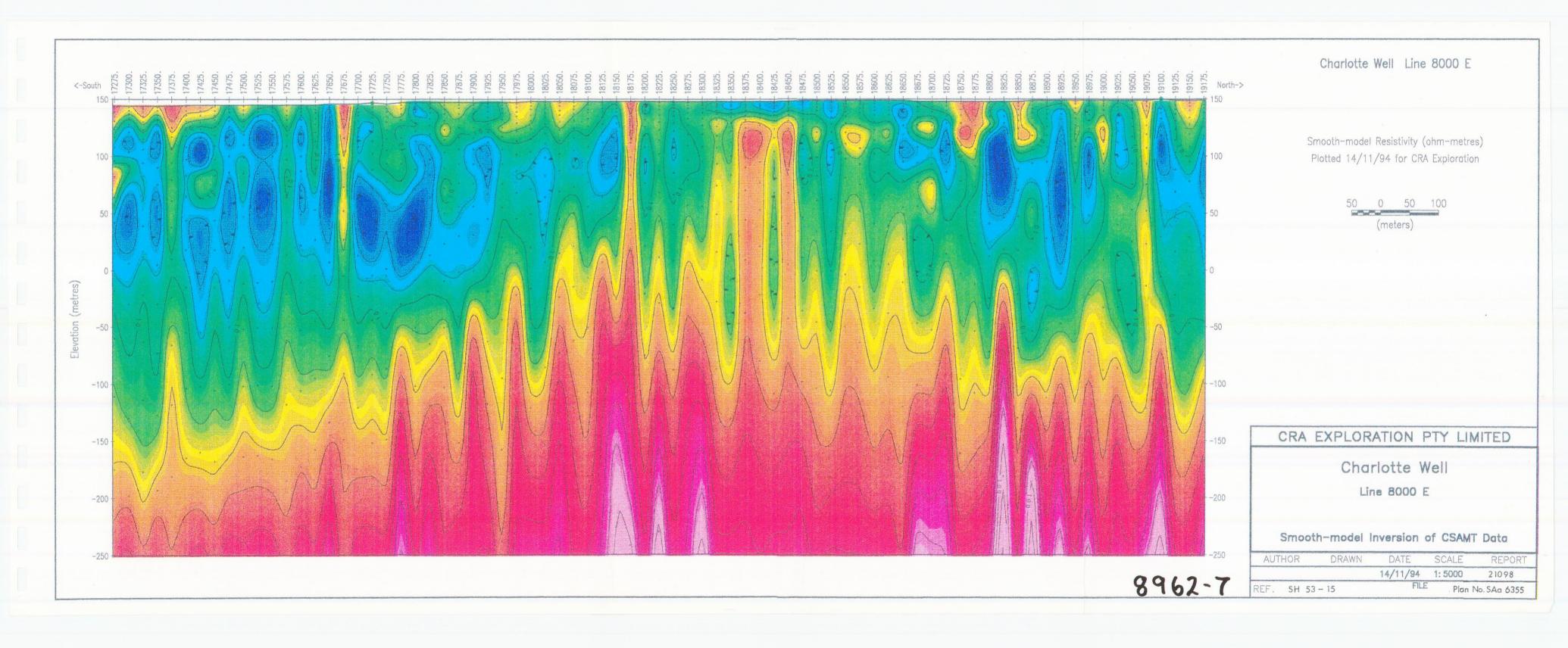


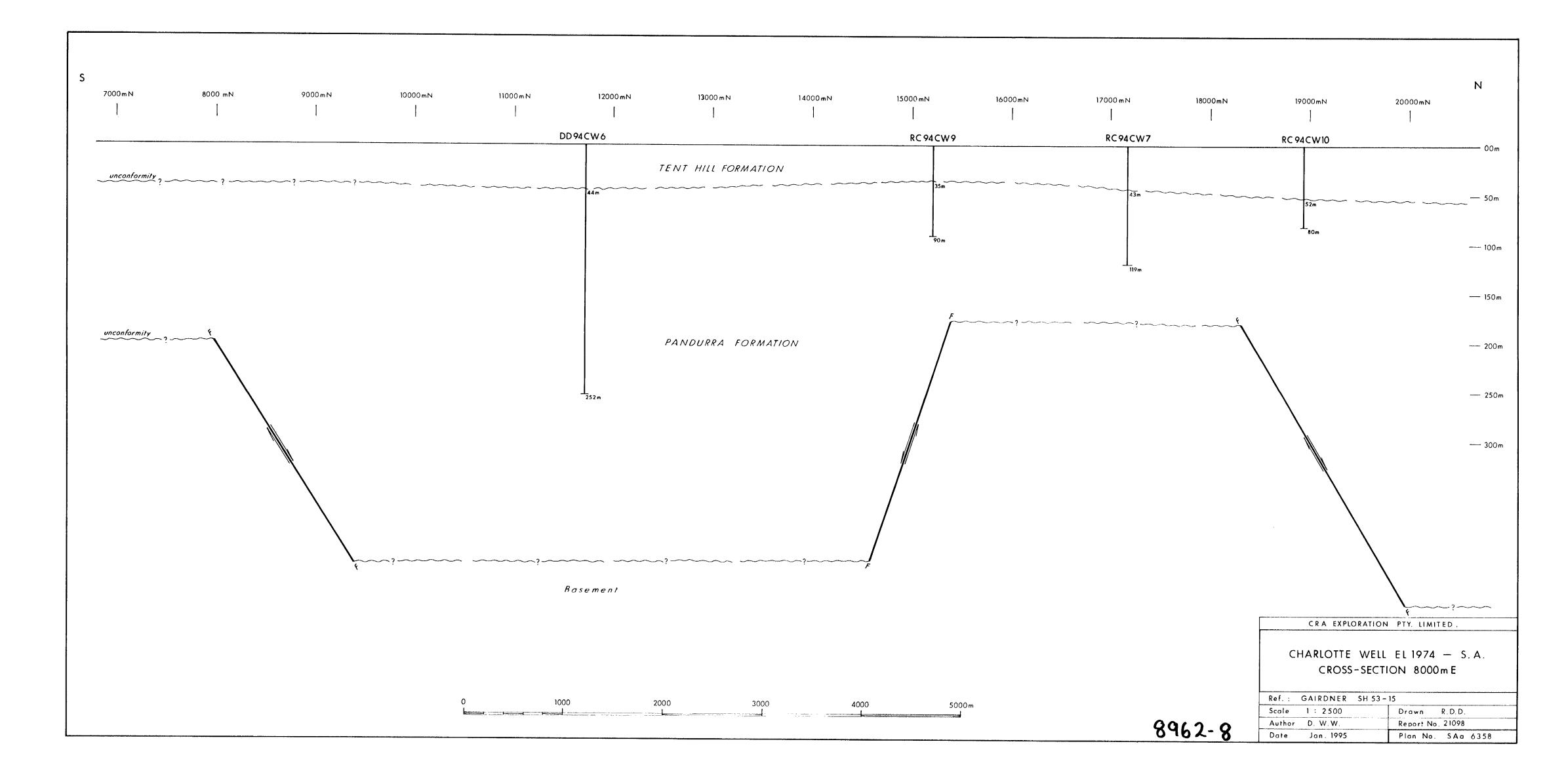


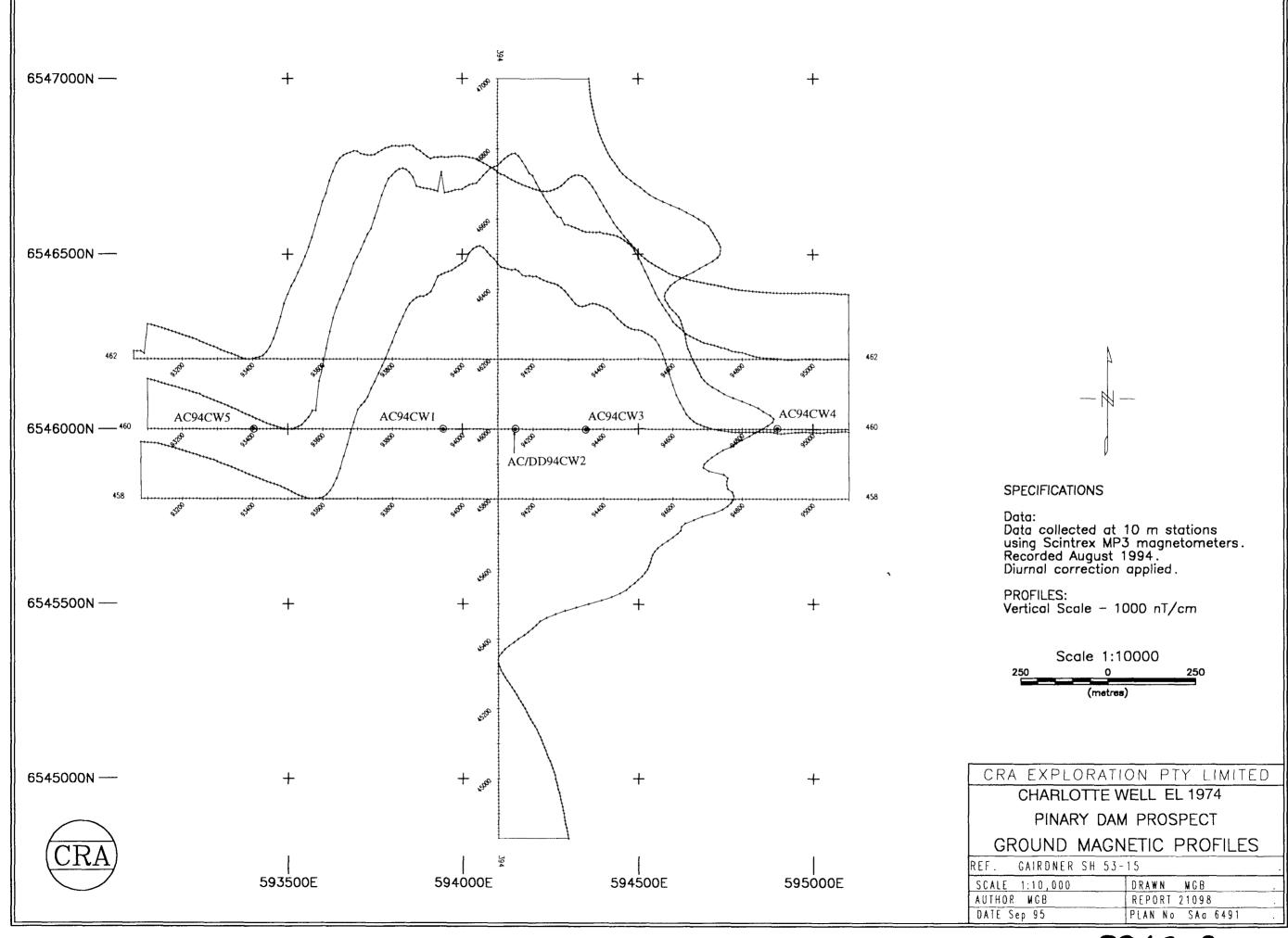












APPENDIX I Diamond Indicator Sampling

SAMPLE NO	DRILLHOLE	EASTING	NORTHING	100 SHEET	DPO	REPORT	RESULT
3943308	RC/DD94CW6	608875	6547750	LAKE HART	54363	O13/95	Negative
3943309	RC/DD94CW6	608875	6547750	LAKE HART	54363	O13/95	Negative
3943310	RC94CW7	608800	6547875	LAKE HART	54363	O14/95	Negative
3943311	RC94CW7	608800	6547875	LAKE HART	54363	O15/95	Negative
3943312	RC94CW9	609475	6546100	LAKE HART	54363	O13/95	1 Ch
3943313	RC94CW9	609475	6546100	LAKE HART	54363	O14/95	Negative
3943314	RC94CW10	608275	6549600	LAKE HART	54363	O14/95	4 Ch
3943315	RC94CW10	608275	6549600	LAKE HART	54363	O13/95	Negative

APPENDIX II Gravity Data Files, Lines 7700E and 8000E

GRAVITY READINGS WERE CORRECTED FOR METER DRIFT	/ NAM Gra	vity Line 80	000E, CI	narlotte Wel	1. 08.09 94		1	1	T	
FREE AIR CORRECTION WAS APPLIED USING DENSITY OF 2 3grams/cc	1				., 00.00.07			 		
FREE AIR CORRECTION WAS APPLIED USING DENSITY OF 2 3grams/cc	/ GRAVITY	READING	S WERE	CORREC	TED FOR M	ETER DRI	FT			
FREEE AIR CORRECTION WAS APPLIED USING DENSITY OF 2.3grams/cc	/ GRAVITY	READING	S WERE	CORRECT	TED FOR L	ATITUDE L	JSING	ISOGAL 65		
BOUGER CORRECTION WAS APPLIED USING DENSITY OF 2 3grams/cc	/ FREE AIR	CORREC	TION W	AS APPLIE	D USING 20	ah/R	1	T = 3-3-3-3		
PAR FREE .3086	/ BOUGER	CORRECT	TON WA	AS APPLIED	USING DE	NSITY OF	2.3gra	ms/cc		
PAR GMT 10	/ PAR FRE	E;.3086								<u> </u>
PAR BASE STATION: A: 606066. 6550652. 960000.	/ PAR ZON	E ; 53.			*****		 	·	:	
PAR METER; : 1.055	/ PAR GMT	; 10.				.,				
FMT (A1, 1X, F9.4, 1X, F8.3, 1X, F7.3, 1X, F8.1, 1X, F9.1, 5(1X, 12.2), 2(1X, F1.3))	/ PAR BASI	E STATION	; A : 60	8086. 6550	652. 98000	0.				
FMT (A1, 1X, F9.4, 1X, F8.3, 1X, F7.3, 1X, F8.1, 1X, F9.1, 5(1X, 12.2), 2(1X, F1.0.3))	/ PAR MET	ER;:1.05	5				1			
FEOH										
FEOH	/ FMT (A1,1	1X,F9.4,1X,	F8.3,1X	,F7.3,1X,F8	3.1,1X,F9.1,	5(1X,I2.2),2	2(1X,F	(0.3)		
Line 8000	/ EOH									
Line 8000	/ Easting No	orthing Stat	lion Rav	_G Elevation	n Bouguer	G Time Da	ate Drif	Corr Base	! !	
608086.1 6550652 20000 2939.422 152.208 601.8 7.36 08.09.94 980000 608100.3 6550553 19900 2939.591 152.231 601.917 7.41 08.09.94 980000.7 608128.8 6550355 19700 2940.273 151.301 602.308 7.52 08.09.94 980000.9 608143.1 6550256 19600 2940.468 151.822 602.559 7.59 08.09.94 980000.9 608143.1 6550256 19600 2940.468 151.822 602.559 7.59 08.09.94 980001.1 608157.3 6550157 19500 2941.363 150.139 602.842 8.05 08.09.94 980001.1 608157.3 6550157 19500 2941.1662 148.961 603.083 8.11 08.09.94 980002.4 608185.8 6549959 19300 2941.958 148.763 603.287 8.16 08.09.94 980002.7 608200.1 6549860 19200 2942.225 148.961 603.083 8.11 08.09.94 980003.2 608260.2 6549765 19100 2942.272 149.552 603.761 8.27 08.09.94 980003.2 608260.4 6549669 19000 2942.729 149.159 603.997 8.33 08.09.94 980003.2 608260.4 6549669 19000 2942.729 149.159 603.997 8.33 08.09.94 980003.2 608230.2 6549765 19100 2942.372 149.552 603.761 8.27 08.09.94 980003.2 608303.8 6549479 18800 2943.547 148.881 604.204 8.38 08.09.94 980003.2 608330.8 6549479 18800 2943.784 148.306 604.737 8.52 08.09.94 980003.9 608341.4 6549193 18500 2943.784 148.306 604.737 8.52 08.09.94 980004.7 608381.2 6549288 18600 2943.784 148.306 604.737 8.52 08.09.94 980004.7 608481.6 6549089 18400 2944.445 148.666 605.067 9.03 08.09.94 980004.7 608481.6 6549089 18400 2944.445 148.666 605.067 9.03 08.09.94 980005.3 608441.6 6549089 18400 2944.445 148.666 605.067 9.30 08.09.94 980005.3 608411.6 6549089 18400 2944.445 148.666 605.067 9.30 08.09.94 980005.3 608411.6 6549089 18000 2944.636 147.795 605.26 9.38 08.09.94 980005.3 608502.1 6548907 18200 2944.636 147.795 605.26 9.38 08.09.94 980005.6 608502.1 6548907 18200 2944.634 148.011 605.23 29.43 08.09.94 980005.6 608502.1 6548907 18200 2944.636 147.795 605.26 9.38 08.09.94 980005.6 608502.6 6548621 17900 2944.644 148.011 605.23 29.43 08.09.94 980005.6 608502.6 6548621 17900 2944.644 148.011 605.23 29.43 08.09.94 980005.6 608683.6 6548431 17700 2945.258 144.691 605.075 10.01 08.09.94 980005.6 608693.8 6548641 17500 2945.575 144.595 605.067 10.24 08.09.94	Line 8000						T			
608066.1 6550652 20000 2939.422 152.208 601.8 7.36 08.09.94 980000 2 60810.3 6550553 19900 2939.591 152.231 601.917 7.41 08.09.94 980000 2 608114.5 6550454 19800 2940.091 151.272 602.176 7.47 08.09.94 980000.7 608128.8 6550355 19700 2940.273 151.301 602.308 7.52 08.09.94 980000.9 608143.1 6550256 19600 2940.468 151.822 602.559 7.59 08.09.94 980001.1 608157.3 6550058 19400 2941.136 150.139 602.842 8.05 08.09.94 980001.1 608157.3 6550058 19400 2941.136 150.139 602.842 8.05 08.09.94 980001.8 608157.5 6550058 19400 2941.662 148.961 603.083 8.11 08.09.94 980002.7 608200.1 6549959 19300 2941.955 148.963 603.287 8.16 08.09.94 980002.7 608200.1 6549969 19200 2942.225 148.958 603.544 8.22 08.09.94 980003.2 608230.2 6549765 19100 2942.372 149.552 603.761 8.27 08.09.94 980003.2 608230.2 6549765 19100 2942.372 149.552 603.761 8.27 08.09.94 980003.2 608230.2 6549765 19100 2942.372 149.552 603.761 8.27 08.09.94 980003.2 608230.2 6549765 19100 2943.774 148.881 604.204 8.38 08.09.94 980003.5 608230.8 6549479 18800 2943.512 148.006 604.449 8.35 08.09.94 980003.9 608303.8 6549479 18800 2943.784 148.306 604.737 8.52 08.09.94 980004.4 608343.1 6549384 18700 2943.784 148.306 604.737 8.52 08.09.94 980004.7 608341.4 6549193 18500 2944.145 148.366 604.737 8.52 08.09.94 980004.9 608411.6 6549193 18500 2944.636 148.443 605.15 9.09 08.09.94 980005.1 608641.6 6549098 18400 2944.636 147.683 605.274 9.32 08.09.94 980005.3 608502.1 6548907 18200 2944.636 147.683 605.274 9.32 08.09.94 980005.6 608502.1 6548907 18200 2944.636 147.683 605.27 9.33 08.09.94 980005.6 608502.1 6548037 18200 2944.636 147.683 605.087 9.33 08.09.94 980005.6 608502.1 6548037 18200 2944.636 147.795 605.26 9.38 08.09.94 980005.6 608502.1 6548037 18200 2944.636 147.683 605.08 10.07 08.09.94 980005.6 60868.3 654833 17600 2944.636 147.586 605.086 10.07 08.09.94 980005.6 60868.3 654833 17600 2944.636 147.586 605.086 10.07 08.09.94 980005.6 60868.3 654833 17600 2944.641 148.091 605.075 10.19 08.09.94 980005.6 608788.9 6548049 17300 2944.636 147.533 605.081 10.07 08.09.94 9800				2939.422	152.208		7:35	08.09.94	980000	A
608100.3 6550553 19900 2939.591 152.231 601.917 7:41 08.09.94 980000.2 608114.5 6550454 19800 2940.091 151.272 602.176 7:47 08.09.94 980000.7 608128.8 6550355 19700 2940.273 151.301 602.308 7:52 08.09.94 980000.9 608143.1 6550256 19600 2940.468 151.822 602.559 7:59 08.09.94 980001.1 608157.3 6550157 19500 2941.136 150.139 602.842 8:05 08.09.94 980001.8 608157.3 6550157 19500 2941.662 148.961 603.083 8:11 08.09.94 980002.4 608158.8 6549959 19300 2941.662 148.961 603.083 8:11 08.09.94 980002.4 608200.1 6549860 19200 2942.225 148.986 603.544 8:22 08.09.94 980003.2 608230.2 6549765 19100 2942.372 149.552 603.761 8:27 08.09.94 980003.2 608260.4 6549669 19000 2942.729 149.189 603.997 8:33 08.09.94 980003.2 608230.8 6549479 18800 2943.512 148.006 604.449 8:45 08.09.94 980003.5 608320.8 6549479 18800 2943.512 148.006 604.449 8:45 08.09.94 980003.4 608343.1 6549384 18700 2943.784 148.306 604.737 8:52 08.09.94 980004.4 608343.1 6549384 18700 2943.784 148.306 604.737 8:52 08.09.94 980004.9 608411.4 6549193 18500 2944.328 148.436 605.05 9:09 08.09.94 980004.9 608411.4 6549193 18500 2944.328 148.433 605.15 9:09 08.09.94 980005.3 608411.6 6549068 18400 2944.328 148.443 605.15 9:09 08.09.94 980005.6 608411.6 6549068 18400 2944.328 148.443 605.15 9:09 08.09.94 980005.6 608411.6 6549098 18400 2944.328 148.443 605.15 9:09 08.09.94 980005.6 608632.2 6548812 18100 2944.636 147.795 605.26 9:38 08.09.94 980005.6 608502.1 6548907 18200 2944.666 147.795 605.26 9:38 08.09.94 980005.6 608502.1 6548907 18200 2944.666 147.795 605.26 9:38 08.09.94 980005.6 608502.2 6548812 18100 2944.666 147.795 605.26 9:38 08.09.94 980005.6 608502.1 6548047 17900 2944.781 146.618 605.007 10:10 08.09.94 980005.6 608637.9 6548526 17800 2944.788 146.618 605.007 10:10 08.09.94 980005.6 608728.5 6548240 17500 2945.572 144.552 605.067 10:24 08.09.94 980005.6 608728.5 6548240 17500 2945.572 144.552 605.067 10:24 08.09.94 980005.6 608728.5 6548240 17500 2945.572 144.552 605.067 10:24 08.09.94 980005.6 608728.5 6548240 17500 2945.572 144.552 605.067 10:24 08.09.94	608086.1	6550652	20000	2939.422	152.208	601.8				
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608562.4 6548716 18000 2944.708 147.566 605.146 9:49 08.09.94 980005.7 608592.6 6548621 17900 2944.741 147.083 605.02 9:55 08.09.94 980005.8 608637.9 6548526 17800 2944.878 146.618 605.008 10:01 08.09.94 980005.9 608668.1 6548431 17700 2945.028 146.058 604.989 10:07 08.09.94 980006.1 608698.3 6548335 17600 2945.289 145.301 605.046 10:13 08.09.94 980006.4 608728.5 6548240 17500 2945.495 144.691 605.075 10:19 08.09.94 980006.6 608788.9 6548049 17300 2945.773 143.753 605.051 10:30 08.09.94 980006.9 608819.1 6547954 17200 2946.022 142.732 605.041 10:37 08.09.94 980007.2 608849.3 6547859 17100	608532.2	6548812	18100	2944.644						
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608668.1 6548431 17700 2945.028 146.058 604.989 10:07 08.09.94 980006.1 608698.3 6548335 17600 2945.289 145.301 605.046 10:13 08.09.94 980006.4 608728.5 6548240 17500 2945.495 144.691 605.075 10:19 08.09.94 980006.6 608758.7 6548145 17400 2945.572 144.552 605.067 10:24 08.09.94 980006.7 608788.9 6548049 17300 2945.773 143.753 605.051 10:30 08.09.94 980006.9 608819.1 6547954 17200 2946.022 142.732 605.041 10:37 08.09.94 980007.2 608849.3 6547859 17100 2946.416 141.529 605.142 10:42 08.09.94 980007.6 608879.5 6547763 17000 2946.572 141.233 605.185 10:48 08.09.94 980007.8 7608086 6550652 20000 2939.187 152.208 10:58 08.09.94 980007.9 608909.7 6547668 16900 2946.643 140.907 605.161 11:09 08.09.94 980007.8 608939.9 6547573 16800 2946.505 142.101 605.21 11:14 08.09.94 980007.8 608987.1 6547478 16700 2946.452 142.394 605.162 11:21 08.09.94 980007.7	608637.9	6548526	17800	2944.878						
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608758.7 6548145 17400 2945.572 144.552 605.067 10:24 08.09.94 980006.7 608788.9 6548049 17300 2945.773 143.753 605.051 10:30 08.09.94 980006.9 608819.1 6547954 17200 2946.022 142.732 605.041 10:37 08.09.94 980007.2 608849.3 6547859 17100 2946.416 141.529 605.142 10:42 08.09.94 980007.6 608879.5 6547763 17000 2946.572 141.233 605.185 10:48 08.09.94 980007.8 / 608086 6550652 20000 2939.187 152.208 10:58 08.09.94 980007.9 608909.7 6547668 16900 2946.643 140.907 605.161 11:09 08.09.94 980007.9 608987.1 6547478 16700 2946.452 142.394 605.162 11:14 08.09.94 980007.7	608728.5									
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C00040.4 CE 47004 40000 00 10 F00	608987.1	6547478	16700	2946.452						·····
	609019.1	6547384	16600							

609051.1	6547291		2946.558	141.987	605.077	11:32	08.09.94	980007.8	
609083.1	6547198		2946.682	141.586	605.067	11:37	08.09.94	980008	
609115.1	6547105	16300	2946.803	141.227	605.064	11:43	08.09.94	980008.1	
609147.1	6547012		2946.907	140.811	605.032	11:49	08.09.94	980008.3	
609179.2	6546919	16100	2947.049	140.379	605.034	11:54	08.09.94	980008.4	
609211.2	6546826	16000	2947.149	139.803	604.966	12:01	08.09.94	980008.5	
609243.2	6546733	15900	2947.217	139.811			08.09.94	980008.6	
609275.2	6546640	15800	2947.378	139.312			08.09.94	980008.8	
609307.3	6546547	15700	2947.431	139.176	604.966	12:18	08.09.94	980008.9	
609339.3	6546454	15600	2947.447	139.192			08.09.94	980008.9	
609371.3	6546361	15500	2947.458	139.079			08.09.94	980008.9	
609403.3	6546268	15400	2947.196	140.243			08.09.94	980008.6	
609435.4	6546175	15300	2947 163	137.889			08.09.94	980008.6	
609467.4	6546082	15200	2947.336	137.321			08.09.94	980008.8	
/ 608086	6550652	20000	2938.953	152.208	7-05-05		08.09.94	980000	
/ 608086	6550652	20000	2938.932	152.208	and the second		08.09.94	980000	
609499.4	6545989	15100	2947.343	135.871	603,879		08.09.94	980008.9	
609531.4	6545896	15000	2947.032	136.885			08.09.94	980008.5	1
609563.5	6545803		2946.718	135.798			08.09.94	980008.2	
609595.5	6545710		2946.191	137.978			08.09.94	980007.7	
609627.5	6545617		2946.115	138.035			08.09.94	980007.6	
609659.5	6545524		2945.848	139.161			08.09.94	980007.3	
609691.5	6545431		2946.671	135.801			08.09.94	980008.2	
609723.6	6545338		2947.378	132.741			08.09.94	980008.9	
609755.6	6545245		2947.638	131.464			08.09.94	980009.2	
609787.6	6545152		2947.725	132.787			08.09.94	980009.3	
609819.6	6545059		2948.122	129.814	602.755		08.09.94	980009.7	
609851.7	6544966	~	2948.416	130.612	603.166		08.09.94	980010	
609883.7		13900	2948.645	129.293	603.063		08.09.94	980010.2	[
609915.7	6544779		2948.966	130.081			08.09.94	980010.6	
609947.7	6544686		2949.093	129.632			08.09.94	980010.7	
609979.8	6544593	13600	2949.071	129.202			08.09.94	980010.7	
610011.8	6544500		2949.243	128.463			08.09.94	980010.9	
610043.8	6544407	13400	2949.185	128.312			08.09.94	980010.8	L
610075.8	6544314	13300	2949.218		603.004			980010.9	
/ 608086	6550652		2938.932	152.208			08.09.94	980000	Α
610107.9	6544221		2949.164	129.255	603 129		08.09.94	980010.8	
610139.9	6544128		2949.323	129.016			08.09.94	980011	
610171.9	6544035		2948.828	131.553			08.09.94	980010.4	
610203.9	6543942		2948.481	133.376			08.09.94	980010.1	
610236.1	6543849		2948.415	133.873			08.09.94	980010.1	
610268.1	6543756		2947.985	136.099			08.09.94	980009.5	
610300.1	6543663		2947.475	138.581	602.894		08.09.94	980009	
610340.1	6543570		2948.201	135.822	603.007		08.09.94	980009.8	
610380.1	6543485		2948.023	136.459	602.891	,	08.09.94	980009.6	···
610392.1	6543400		2947.355	139.731			08.09.94	980008.9	
610404.2	6543299		2947.493	139.052			08.09.94	980009	
610416.3	6543198		2948.073	136.532	602.744		08.09.94	980009.6	
610428.4	6543097		2948.302	135.531	602.698		08.09.94	980009.8	
610440.5	6542996		2948.743	133.717	602.704		08.09.94	980010.3	
610452.6	6542895		2948.802	133.371	602.617		08.09.94	980010.4	
610464.7	6542794		2948.893	133.177	602.596		08.09.94	980010.5	
/ 608086	6550652		2938.989	152.208			08.09.94	980000	A
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610844.1 6539153 8100 2955.133 119.249 603.904 12:49 09.09.94 980017.3 610854.2 6539052 8000 2955.331 119.379 604.071 12:55 09.09.94 980017.5 610864.4 6538951 7900 2953.029 129.416 603.691 13:01 09.09.94 980015.1 610874.6 6538849 7800 2954.961 122.029 604.101 13:07 09.09.94 980017.2 610884.8 6538748 7700 2953.913 127.088 603.994 13:14 09.09.94 980016.1 610894.9 6538647 7600 2953.879 127.787 604.037 13:21 09.09.94 980016.4 610915.3 6538546 7500 2954.227 126.416 604.045 13:27 09.09.94 980016.4 610925.5 6538343 7300 2952.771 133.735 603.915 13:40 09.09.94 980014.9 610945.8 6538141 7100 2953.855 128.857 603.996 13:52 09.09.94 980016.1	/ 608086	6550652	20000	2938.723	152.208		12:29	09.09.94	+	Α
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APPENDIX III

Instrumentation, Recording Procedures and Data Quality,

CSAMT and TEM Survey, Charlotte Well

(Zonge Engineering & Research Organization)

SELECTED EXTRACTS FROM:

CSAMT SURVEY REPORT

Charlotte Well/Kalabity Prospect for

CRA Exploration Pty. Limited

Issue Date: 19 April, 1995

Executive Summary

In December of 1994 and January of 1995, at the request of Mike Barlow of CRA Exploration, Zonge Engineering and Research Organization performed controlled-source audio-frequency magnetotelluric (CSAMT) surveys on two separate prospects in South Australia. The first survey was on the Charlotte Well prospect, located near Glendambo in the mid-north of the state. The second survey was situated on the Kalabity Station, near the town of Olary, in the state's eastern pastoral region.

One long CSAMT line was run over the Charlotte Well area, with the majority (7.1 kilometres) surveyed using 50 metre station spacing. The remainder of the line (1.9 kilometres) was surveyed using 25 metre station spacings. The second phase of the survey, at Kalabity, consisted of six lines totalling 40 kilometres, most of which was read using 50 metre station spacing. 1.5 kilometres were surveyed using 25 metre station spacings. On both surveys, follow-up transient electromagnetic (TEM) soundings were made over areas of interest.

Project Logistics

Survey Overview

On the 27th of October 1994, a Zonge Engineering crew, led by Jeff Cashmore, began CSAMT production on the Charlotte Well prospect. Only one long line, line 8000E, was read using two transmitter locations (see figure 1 for line locations). This work was followed up by in-loop TEM soundings over several areas as an independent means of checking the CSAMT data (and the inversion process). This portion of the survey was completed on the 8th of November, 1994. The electric field was oriented approximately perpendicular to strike on line 8000E.

During the Charlotte Well phase of this survey four days of production were lost due to problems with the alternator. At least one full day of production (over the course of a few days) was also lost due to problems with the GDP-32. That unit finally failed completely, so production was switched to a three channel GDP-16 for two days until an eight channel GDP-16 could be shipped up. Production rates for the three channel receiver were quite comparable with those for the eight channel.

During the second phase of this survey 1.5 days of production were lost due to transmitter problems. One day of production was also lost due to inclement weather.

Field Procedures

For the CSAMT, electric-field components parallel to the transmitter antenna were usually measured at each station using 50 metre long grounded dipoles. Where better lateral resolution was needed, 25 metre grounded dipoles were used. In either case, magnetic field components perpendicular to the transmitter antenna were measured using an inductive coil.

For the data taken at 50 metre station spacings, four electric field and one magnetic field measurements were read simultaneously at each setup. At Charlotte Well, the 25 metre stations spacing data was taken using seven electric-field and one magnetic-field measurements simultaneously at each setup. Data were collected at discrete frequencies ranging from 8192 hertz down to frequencies ranging between 32 hertz and 1 hertz. The lower frequency was chosen so that data was taken at least two frequencies into the near-field. This was occasionally difficult to determine, as the location of the notch frequency was often quite variable along a line, and could be somewhat difficult to recognise, especially in the field.

For the TEM, the transient magnetic field was measured "in-loop", i.e. with the receiving antenna (antennae) set up at the centre of the transmitting loop. At Charlotte Well all TEM data were taken at 0.5 hertz, comparing data from both 100 metre and 200 metre transmitting loops. Only Hz data was taken, using the Zonge coil alone.

Field Instrumentation

A Zonge Engineering GGT-25 transmitter was used to generate source fields for the CSAMT and TEM surveys. Power was provided by a trailer-mounted, ZMG-30 motor generator, CSAMT transmitting bipoles were approximately 1.5 kilometres long, running parallel with the traverse line.

An eight channel GDP-32 was used at the beginning of this survey at Charlotte Well to record data. It became apparent that this receiver was not working properly, and needed to be replaced. These problems were not related to and did not affect the data quality. This unit was switched first with a three channel GDP-16 (being the only receiver available), and then with an eight channel GDP-16. The remainder of the data taken on this survey (during both stages) were taken using an eight channel GDP-16.

For the CSAMT, the electric field receiver dipoles were grounded by coppersulfate porous pots. Three different models of coil were used to sense the magnetic field during the first phase of this work. These included the Saarloos coil, an EMI model BF-10 and a Zonge ANT-1B. During the second phase of the work only the Zonge ANT-1B was used.

For the TEM at Charlotte Well, the Zonge TEM/3 antenna was used to measure transient magnetic field.

The data were downloaded each evening from the receiver's solid-state memory to a portable computer. Final processing, modelling and plotting were completed in Zonge Engineering's Adelaide office.

Data Quality

This section is a general overview of the data quality for the work performed on this survey. Since each survey line used a different transmitting bipole, data quality varied greatly. More detailed discussion of data quality for each line will be found in the Data Presentation section of this report.

Following standard Zonge Engineering field procedures, the receiver operator repeated each measurement at least twice. If variation in apparent resistivity was greater than 5 percent, additional repeats were recorded.

Overall, the data quality for these surveys was at least acceptable. Data were generally the worst in areas where the resistivities were extremely low, i.e. ranging in value from 1 to 10 ohm-metres. Signal levels are very low in this type of ground, thus making readings substantially noisier. It is also worth noting that, if for example, individual resistivity readings range from 1 to 1.5 ohm-metres (repeatable to about 50 percent), it may not be worthwhile for the operator to use a great deal of time taking enough data to get the variation percentage down to an apparently "acceptable" level.

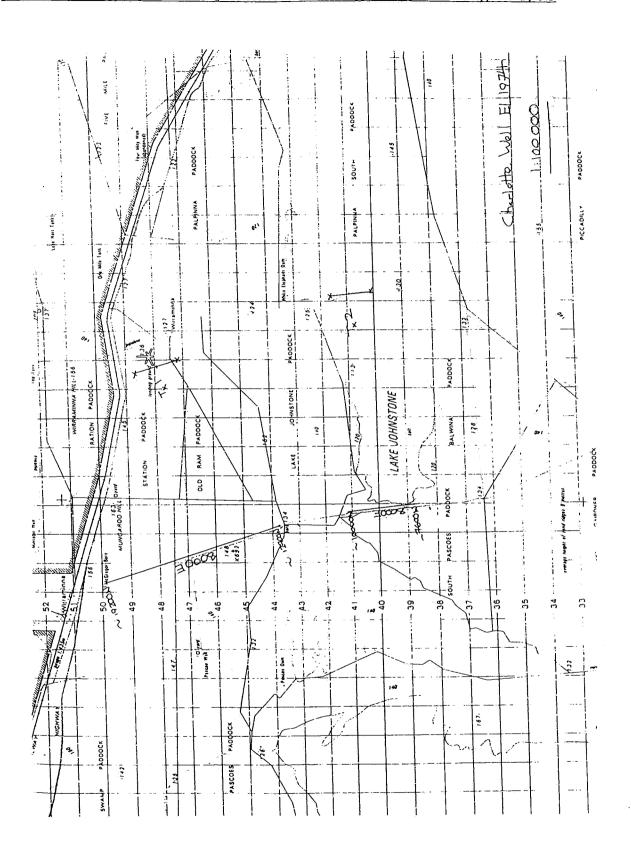


Figure 1: Location Map for Charlotte Well, line 8000E (from Michael Barlow).

APPENDIX IV

Raw Plot Files and Contractors Report, CSAMT, Line 8000E

(Zonge Engineering & Research Organization)

CHARLOTTE WELL/KALABITY CSAMT

Zonge Engineering - January, 1995

Charlotte Well

All eastings and northings used in this report are local coordinates.

The survey at Charlotte Well was comprised of one line, divided into two separate sections. Line 8000E was read in late October and November of 1994. The southern section of the line extended from 7600N to 10000N. The northern section of the line extended from 11600N to 19175N.

Line 8000E: CSAMT

All of the data for the southern section of the line, and for the northern section of the line from 11600N to 17250N were taken at 50 metre station spacings. From 17275N to 19175N, all of the data were taken at 25 metre station spacings. Most of the data on this line were taken down to 4 hertz, although from 17800N to the northern end of the line at 19175N, data were taken down to 1 hertz.

Two transmitter locations were used for this line. The first, used for the southern part of the line, was centred approximately 7.5 kilometres east of the line at 15500E, 88000N. The second transmitter location, used for the northern part of the line, was also 7.5 kilometres east of the line, centred at 15500E, 16000N. Both transmitter antennas were approximately 1.5 kilometres long.

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The northern transmitting bipole produced currents of 20 to 24 amperes for frequencies from 1 hertz to 256 hertz. At higher frequencies, the transmitter current was limited by the intrinsic impedance of the transmitter antenna wire, dropping gradually to between 1 and 3 amperes at 8192 hertz. The southern transmitting bipole produced 10 to 12 amperes for frequencies from 4 hertz to 256 hertz. Currents then dropped gradually to between 1.5 and 2 amperes at 8192 hertz.

The near-field notch came in fairly consistently and strongly on this data set at around 16 hertz. Since most of the data was taken to 4 hertz, the full frequency range was inverted.

Resistivities along this line were generally very low, with values that ranged from one to five ohm-metres for most of the southern section of the line, and high values only around 20 ohm-metres near the northern end of the line. These low resistivities, combined with the low currents produced by the southern transmitting bipole combined to make the data from the southern section of the line fairly noisy, as measured by variation in the repeatability of the resistivities. Variations between apparent resistivity repeats were generally on the order of 5 to 30 percent, with any given frequency varying up to 50 to 100 percent. frequency data were slightly noisier due to weaker signal strength, although this was not entirely consistent either. 256 hertz and 512 hertz were both noisier than most. These two frequencies are very close to the fifth and ninth harmonics of standard 50 hertz power line signal, and are therefore often noisier than the rest.

The quality of the phase data followed a similar pattern to the resistivity data, being generally fairly noisy, with the noisiest data usually at the highest frequencies (as well as at 256 hertz and 512 hertz).

Data quality, from the northern section of this line are generally better than from the southern section, especially for the 50 metre data (taken using the Saarloos coil). Resistivity variations were generally better than 15 percent, with much of the data better than 5 percent. As expected, variation was worse for the higher frequency data, with variation up to 50 to 100 percent for the 8192 hertz data. As with the southern section of the line, it appears that this data was somewhat affected by power line noise. For this part of the line, 256 hertz, 128 hertz and 64 hertz were slightly noisier than the rest.

Again, the noise in the phase data followed the same pattern as the resistivity data, with the noisiest data at the highest frequencies, and at the frequencies affected by power line noise.

While the 25 metre data at the far north end of the line is only slightly more variable than the other data from the rest of the line, there is another problem with the data quality from this area. When examined closely, the resistivity and phases on the black-and-white pseudosection for this part of the line can be seen to group into units of seven. This grouping is also apparent on the colour inversion section for this part of the line. This data was taken reading seven electric field readings (dipoles) and one magnetic-field reading (magnetic coil) per setup. The grouping pattern suggests that the problem is not in the electric field measurements, but is most likely in the magnetic field measurement, as this is the one reading that is common to all seven resistivity calculation. It appears that the EM1 coil was reading inconsistently

from setup to setup, while still maintaining some measure of repeatability within a setup. Historically this coil has been one of our best and most accurate, and we are uncertain for the reason for this problem. While the data on this northernmost end of this line is not of the highest quality, I would suggest that it is still basically correct. Nevertheless, this is a problem that we will have to be more vigilant for in the future.

APPENDIX V

Technical Notes Accompanying CSAMT Smooth Model Inversion
& Static-Corrected Profiles
(Zonge Engineering & Research Organization)

CHARLOTTE WELL/KALABITY CSAMT

Zonge Engineering - January, 1995

Technical Notes

Static Effects

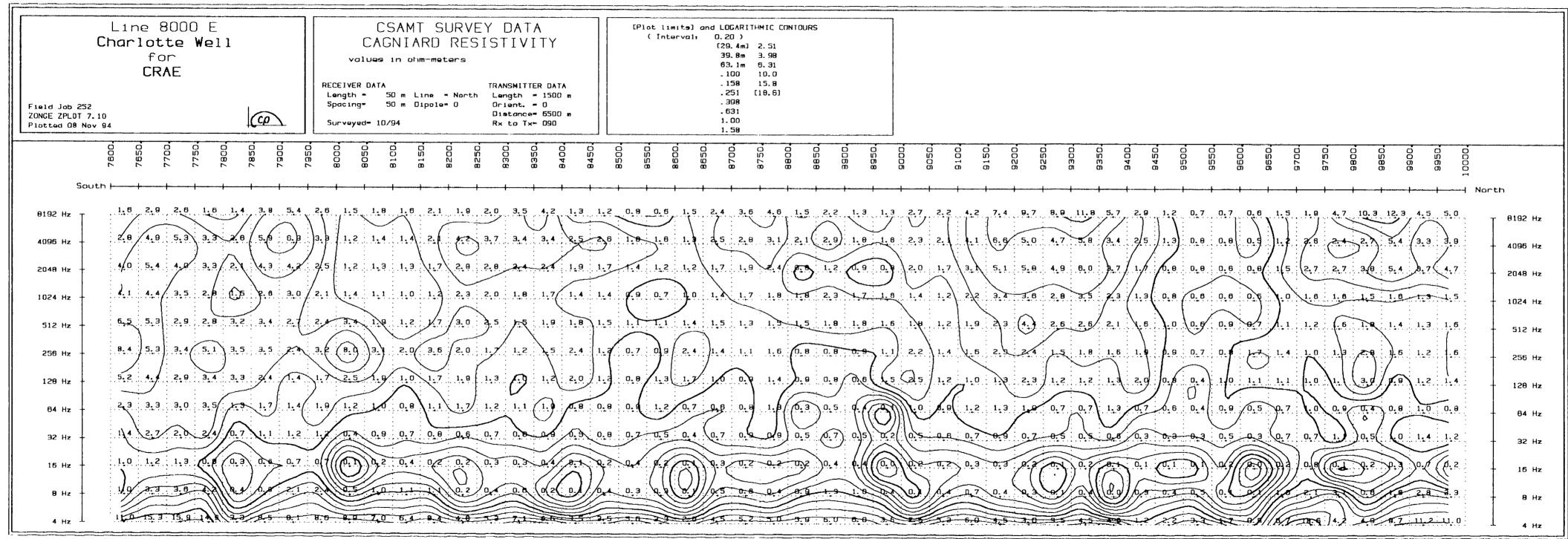
Static-shift effects can be caused by both topography and near-surface inhomogeneities that are too small to be resolved by the 8192 hertz data. Small, near-surface features cause an offset in the sounding curves, but do not change curve shape. Static-shift corrections were calculated by an adaptive static-correction method that uses a non-parametric, robust-moving-average filter to estimate corrected resistivity values. The static-correction often removes residual powerline noise variation as well as topographic effects. The static-correction procedure also removes the effects of small-scale, near-surface geology. Both Cagniard apparent resistivity and static-corrected apparent resistivity pseudosections are useful for interpretation. Cagniard apparent resistivity data have more station-to-station variation, but near-surface geologic effects are preserved. Both topographic and near-surface geologic effects are suppressed in the static-corrected data, enhancing the interpretation of deeper and broader scale geology.

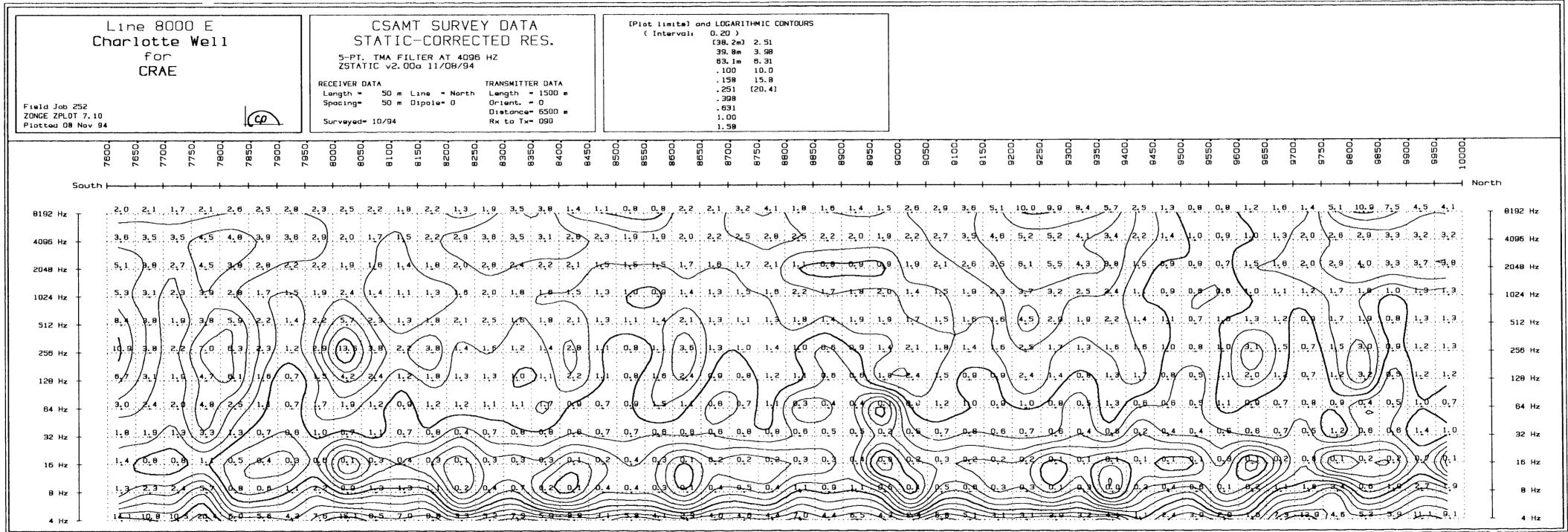
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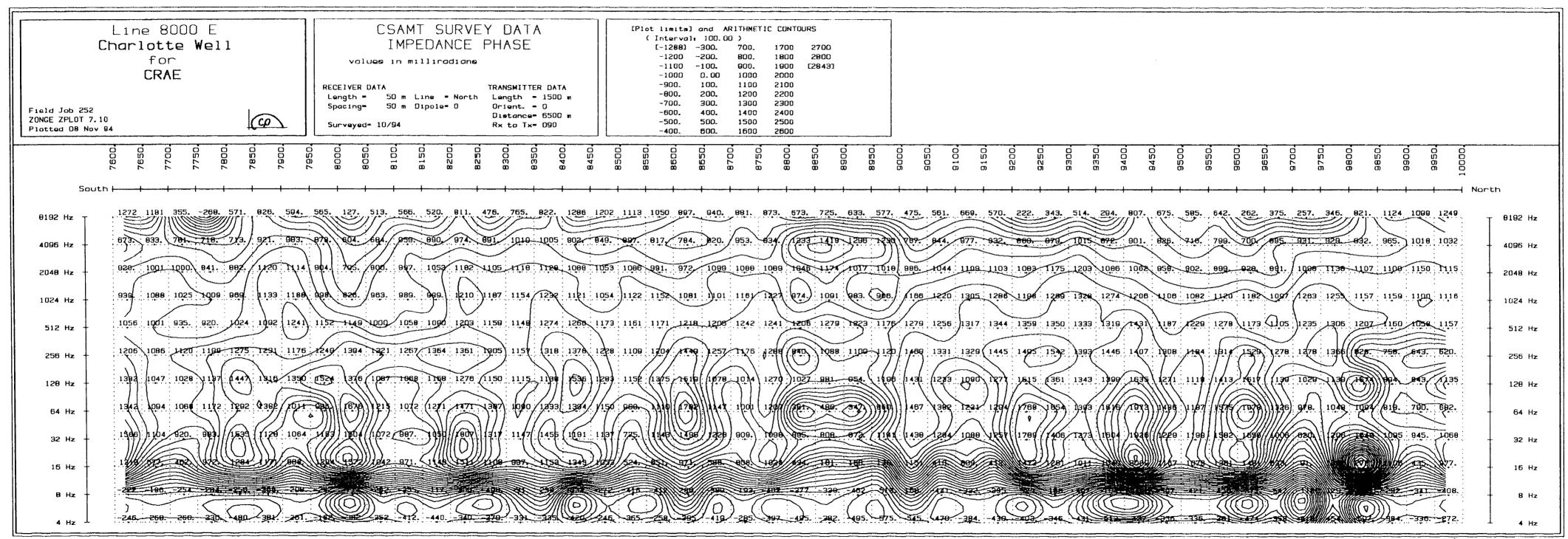
Smooth-Model Inversion

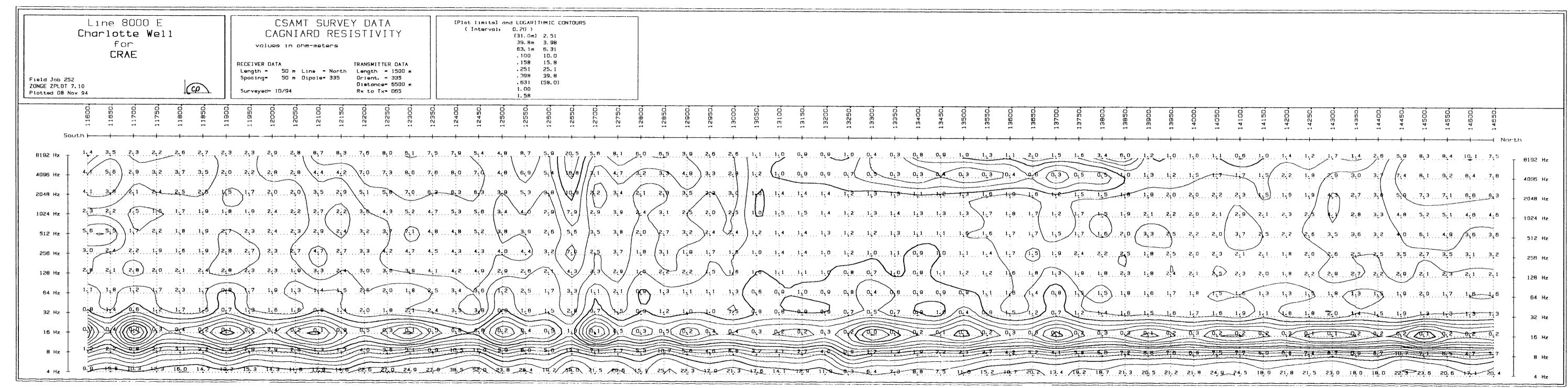
The static-corrected apparent resistivity and impedance phase data were modelled using a smooth-model inversion routine. The inversion algorithm is designed to produce an economical inversion of entire CSAMT data sets. Instead of predicting sharp boundaries between layers, which can be misleading, smooth-modelling produces a smoothly-varying resistivity cross-section, a cross-section that graphically represents the diffuse nature of electrical measurements.

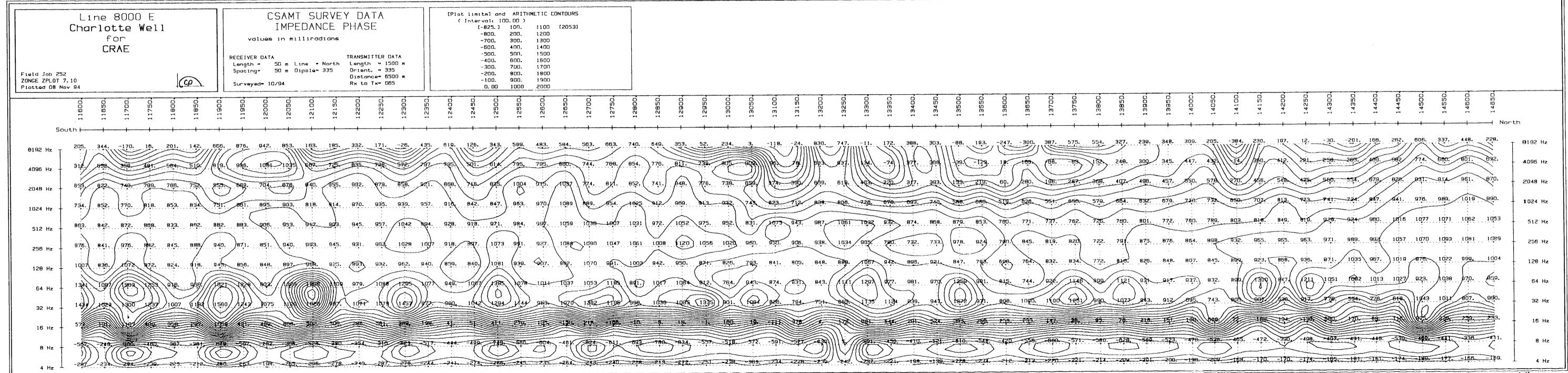
The modelling program calculates a sequence of thin layers that provide a best fit to the data. Seven layers are used for each decade of frequency spanned by the sounding. The calculated resistivities of these layers are then plotted against layer depth to produce the final smooth-model cross-section. Smooth-model resistivity is much more representative of the ground response than apparent resistivity. Near-field and transition-zone data are explicitly modelled by the program. The result is substantially more reliable than the Bostick transformation or other far-field inversion schemes and the result is readily interpretable in geologic terms.



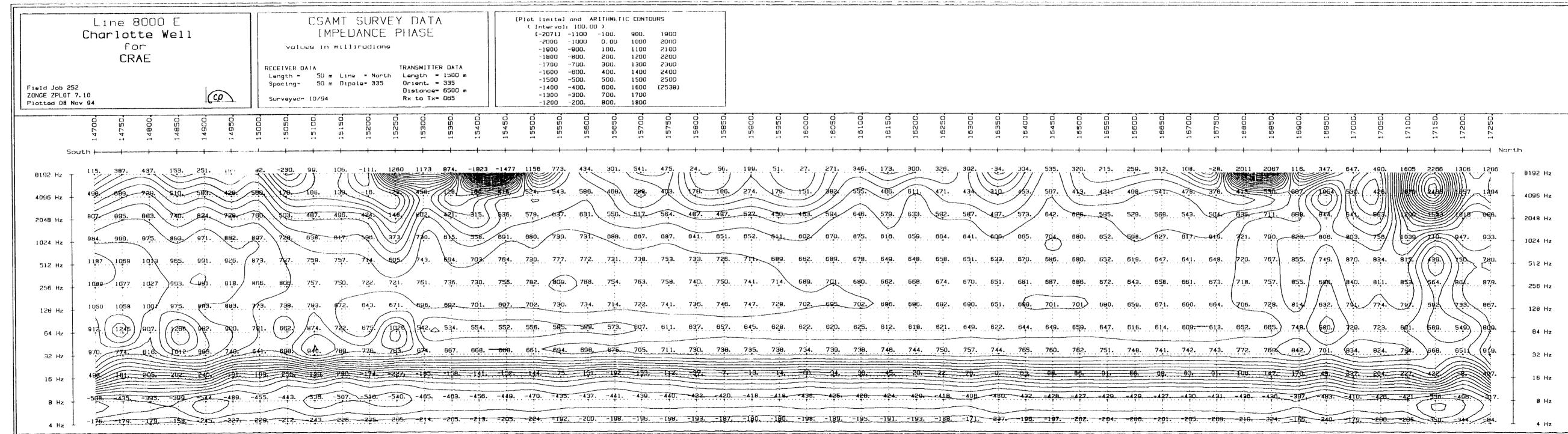


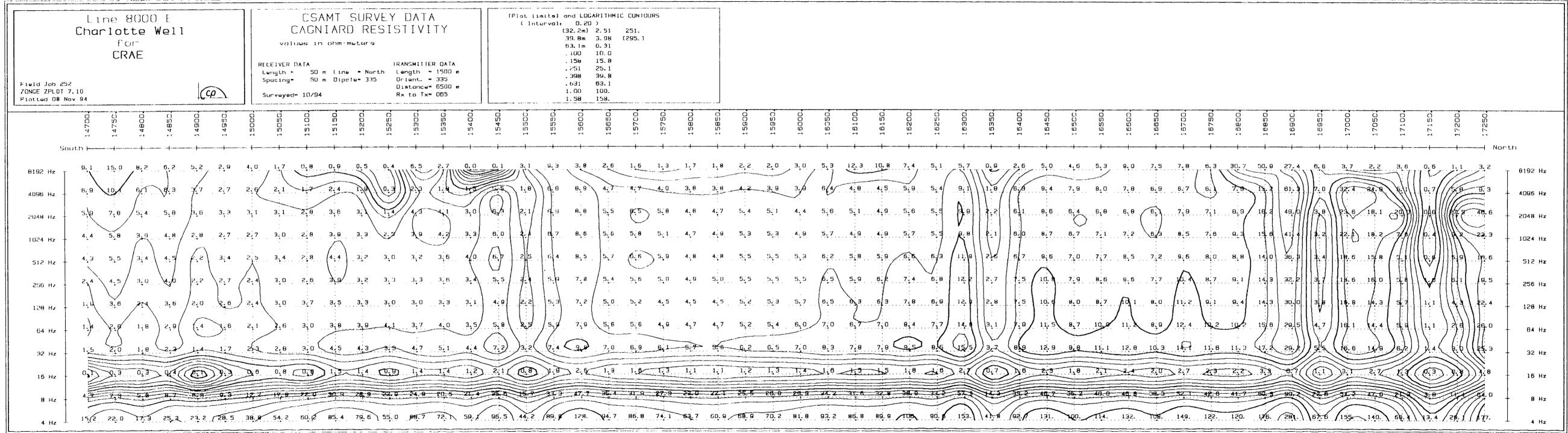




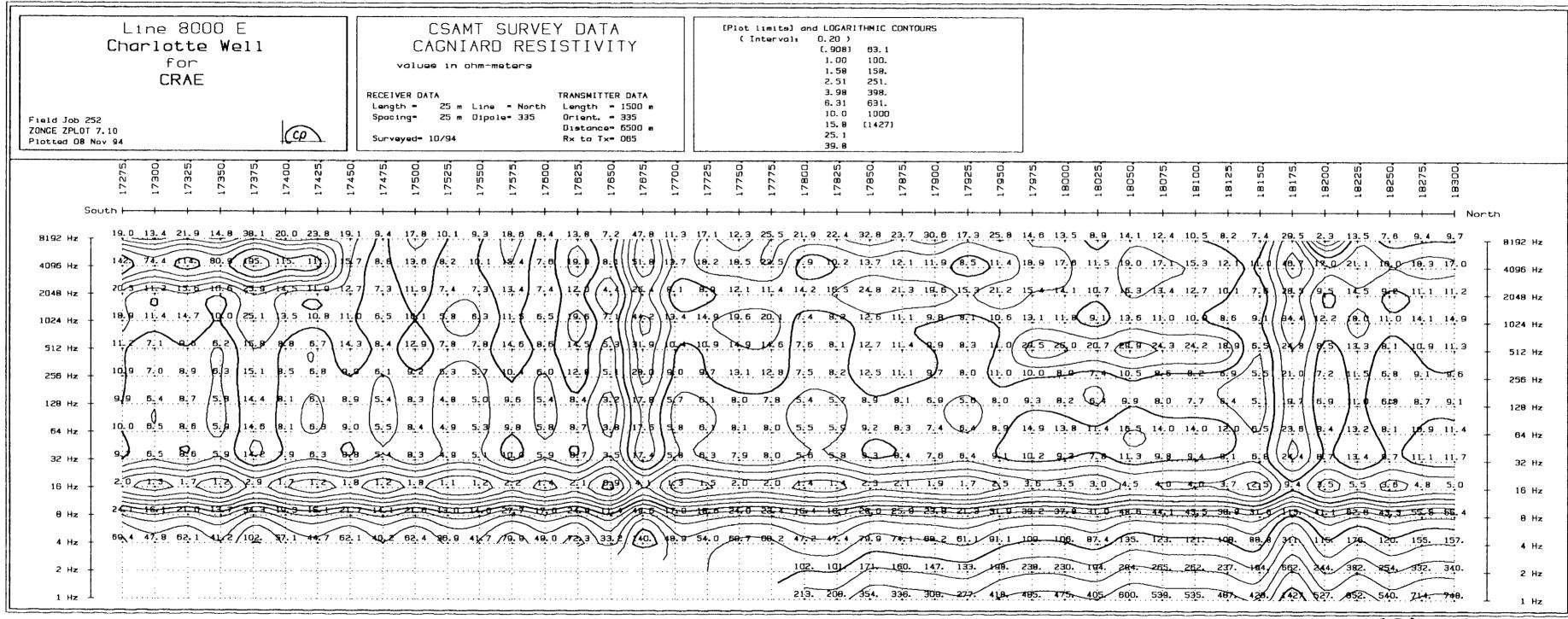


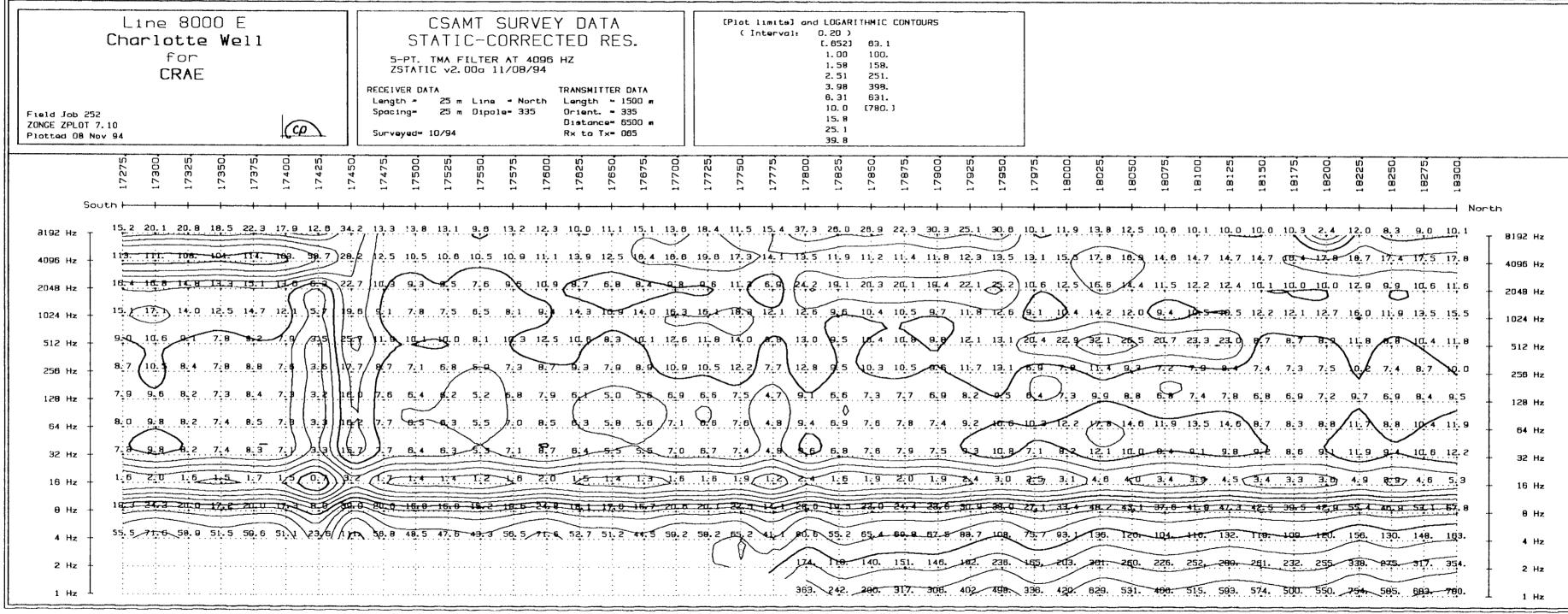
[Plot limits] and LOGARITHMIC CONTOURS CSAMT SURVEY DATA Line 8000 E (Interval: 0.20) [39.5m] 2.51 Charlotte Well 39.8m 3.98 5-PT. TMA FILTER AT 4096 H7 ZSTATIC v2.00a 11/08/94 69.1m 6.31 for .100 10.0 CRAE . 158 15.8 TRANSMITTER DATA . 251 25. 1 8962-15 .398 39.8 Orient. = 335 .631 [55.9] Distance* 6500 m Field Job 252 1.00 ZONGE ZPLOT 7.10 Plotted OB Nov 94 Rx to Tx* 065 Surveyed= 10/94 9182 Hz 4 096 Hz 2048 Hz 1024 Hz 512 Hz 256 Hz 512 Hz 128 Hz 64 Hz 32 Hz 32 Hz 16 Hz 16 Hz 8 Hz 8 Hz

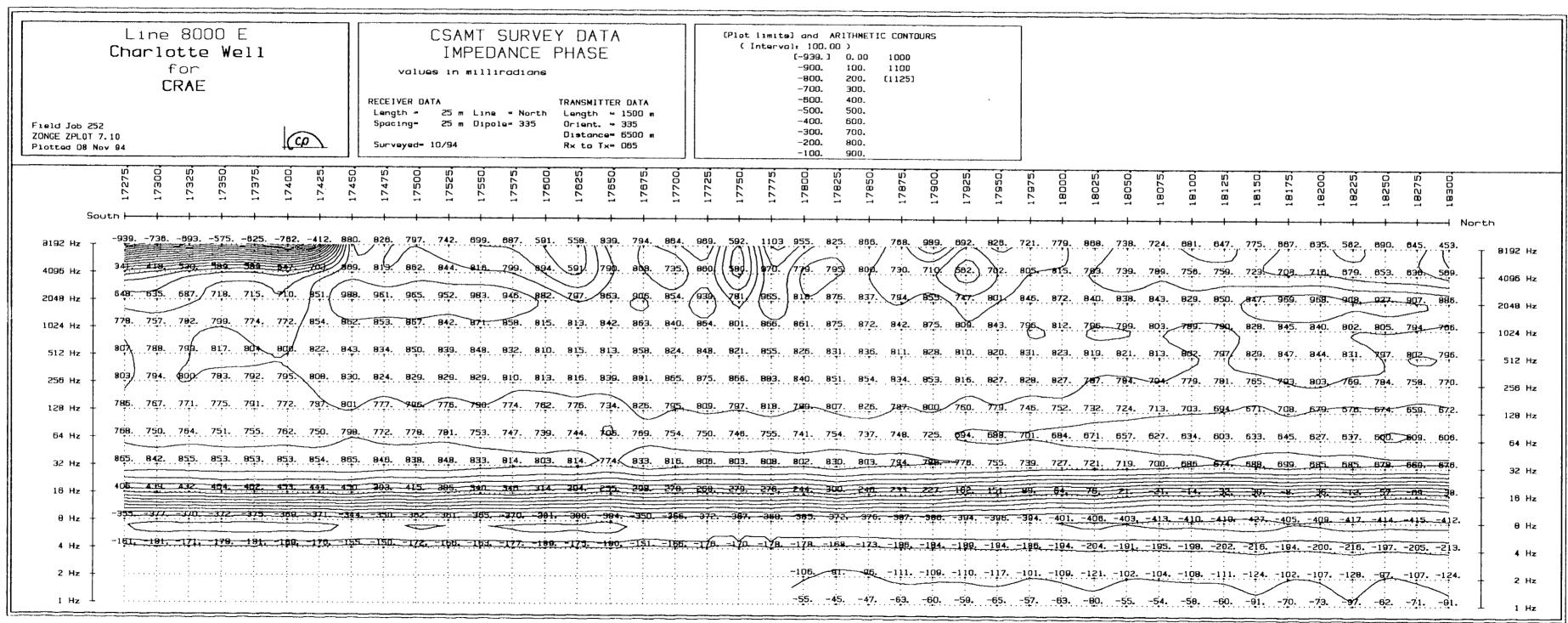


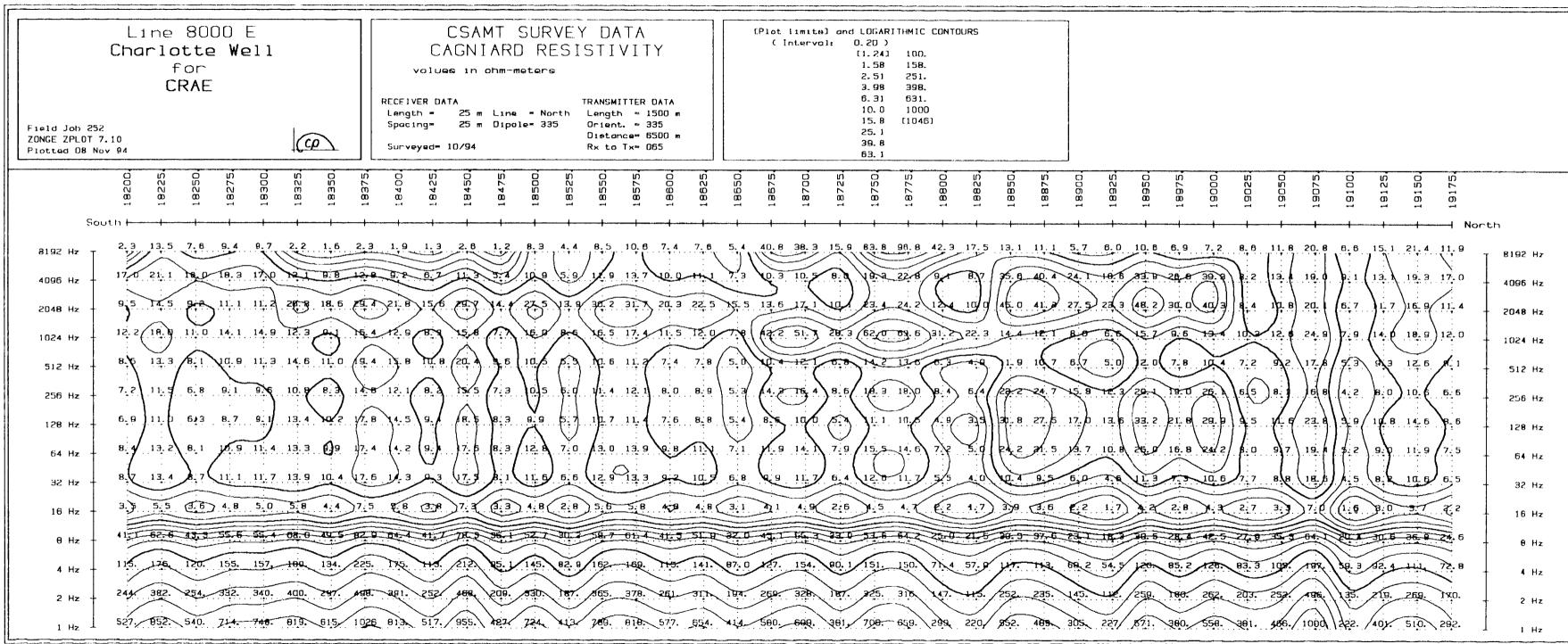


CSAMT SURVEY DATA [Plot limits] and LOGARITHMIC CONTOURS Line 8000 E (Interval: 0.20) STATIC-CORRECTED RES. Charlotte Well [25.4m] 2.51 251. 39.8m 3.98 [352.1 5-PT. TMA FILTER AT 4096 HZ for 63.1m 6.31 ZSTATIC v2.00a 11/08/94 . 100 10.0 CRAE TRANSMITTER DATA RECEIVER DATA 25.1 Length = 50 m Line = North Length = 1500 m Spacing= 50 m Dipole= 335 Urient. = 335 63.1 . 631 Field Job 252 Distance= 6500 m 1.00 100. ZONGE ZPLOT 7.10 8962-18 Rx to Tx# 065 Surveyed= 10/94 1.58 Plotted 08 Nov 94 8192 Hz 4096 Hz 4096 Hz 2048 Hz 2048 Hz 1024 Hz 1024 Hz 512 Hz 512 Hz 256 Hz 256 Hz 128 Hz 120 Hz 64 Hz 32 Hz 32 Hz (10) 16 Hz 16 Hz 8 Hz







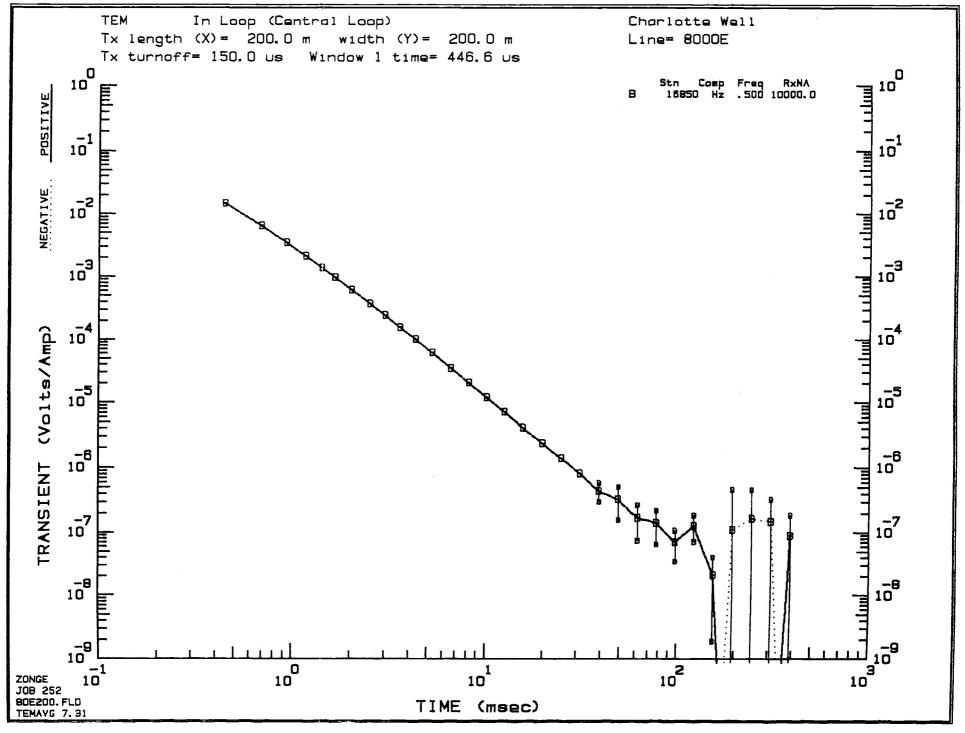


line 8000 F CSAMT SURVEY DATA [Plot limite] and ARITHMETIC CONTOURS (Interval: 100.00) Charlotte Well IMPEDANCE PHASE [~425,] -400. for values in milliradians -300. 700. CRAE RECEIVER DATA TRANSMITTER DATA 0.00 1000 Length = 1500 m Length = 25 m Line = North 100. 1100 Spacing* 25 m Dipole* 335 Orient. = 335 Field Job 252 200. 1200 Distance 6500 m ZONGE ZPLOT 7-10 (cp) 300. [1205] Surveyed= 10/94 Rx to Txm 065 Plotted O8 Nov 94 400. 9175 6 91 964. 1061 1088 987. 1155 1100 1017 1078 1141 1124 1187 934. 1058 893. 1020 1048 1183 964. 984. 1201 1127 1081 1019 1040 1087 1041 8192 Hz 8192 Hz 715. 765. (831. 804. 825. 871. 918. 1006 989 1044 1006 960. 1040 987 1027 1048 4096 Hz 4096 Hz 692 678. 622. 618. 633. 637. 670. 695. 732. 745. 781. 803. 828. 844. 846. 948. 930. d11 1055 1052 1086 1002 947. 1033 1018 1040 103 2048 Hz 2048 Hz 766. 757. 743. 682. 686. 682. 677. 208. 666. 668. 676. 687. 724. 713. 739. 785. 806. 819. 884. 920. 950. 947. 946. 976. 1024 Hz 1024 Hz 751. 745. 719. 702. 716. 719. 736. 770. 747. 770. 771. 768. 769. 784. 758. 787. 803. 838. 860. 884. 906/ 840. 857. 829. 871. 847. 813. 803. 833. 867. 843. 877 908. 912. 921. 512 Hz 512 Hz 803 769. 784. 758. 770. 740. 740. 716. 737. 736. 750. 744. 771. 771. 755. 765. 751. 741. 735. 776. 788. 783. 791. 838. 817. 843. /163. 777. 786. 775. 757. 741. 720. 739. 772. 759. 804. 803. 823. 841 256 Hz 256 Hz 687, 673, 672, 637, 641, 677, 671, 652, 710, 727, 698, 715, 736, 738, 731, 740, 745, 703, 730. 128 Hz 128 Hz 617. 611. 620. 640. 608. 620. 617. 617. 598. 589. 622. 640. 631. 664. 665. 665. 665. 676. 670. 707. 658. 671. 634. 671. 669. 640. 702. 678. 682. 705 64 Hz 64 Hz 670. 684 687 694 706 711 687 708 698 685 691 684 718 732 716 749 753 755 746 747 774 792 801 775 786 770 733 738 722 769 754 785 794 32 Hz 32 Hz 17 29 -11 / -5 4 52 23 45 57 310 22 37 82 15 55 55 59 42 110 59 32 73 61 110 18 96 191 0 16 Hz 16 Hz 408. -417. -414. -415. -412. -414. -413. -412. -408. -398. -402. -395. -419. -404. -402. -404. -407. -404. -407. -404. -405. -405. -405. -407. -404. -407. -404. -407. -404. -407. -404. -407. -408. -407. -408. -4 0 Hz θ Hz -200. -216. -197. -205. -213. -206. -206. -206. -206. -206. -204. -209. -197. -198. -195. -200. -204. -196. -197. -196. -197. -196. -197. -215. -204. -204. -207. -215. -204. -207. -215. -207. -215. -207. -216. -207. -217. -210. -196. -197. -215. -207. -217. -210. -196. -197. -217. -210. -196. -197. -217. -210. -196. -197. -217. -210. -196. -197. -217. -210. -196. -197. -217. -210. -196. -197. -217. -210. -196. -197. -217. -210. -196. -197. -217. -217. -210. -196. -197. -217. -4 Hz 4 Hz -107. -128. -97. -107. -124. -111. -118. -115. -123. -112. -107. -105. -117. -114. -102. -101. -117. -107. -140. -111. -108. -124. -101. -174. 2 Hz 2 Hz

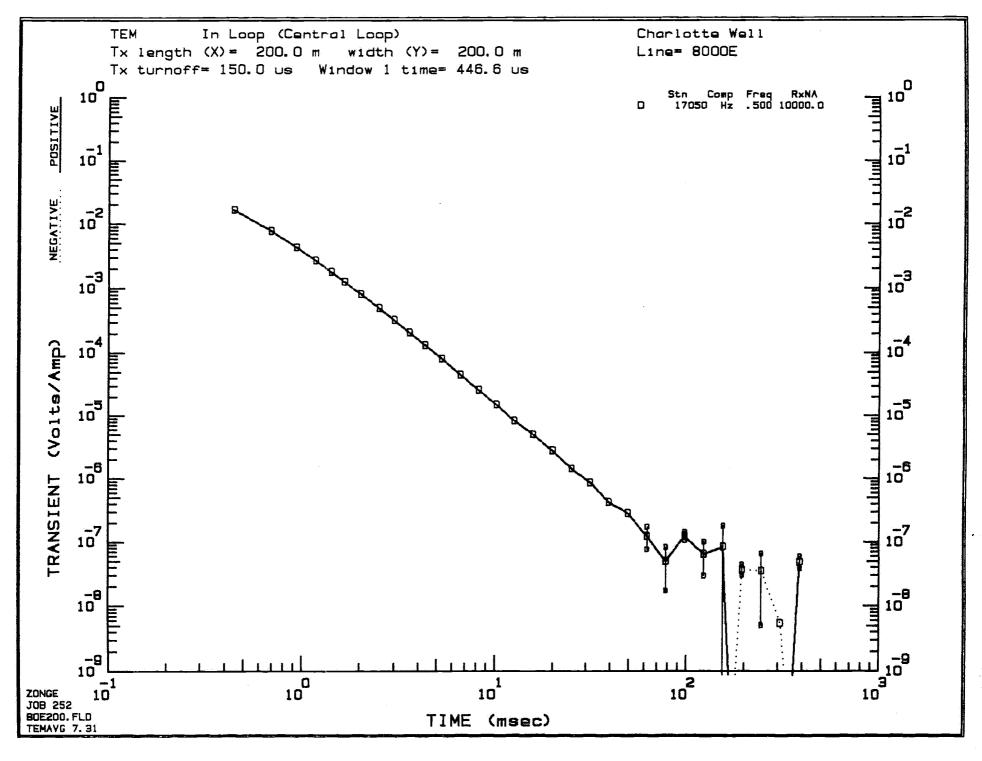
Line 8000 E CSAMT SURVEY DATA [Plot limits] and LOGARITHMIC CONTOURS (Interval. 0.20) STATIC-CORRECTED RES. Charlotte Well [1, 62] 158. 2.51 251. for 5-PT. TMA FILTER AT 4096 HZ 3, 98 398. ZSTATIC v2.00a 11/08/94 CRAE 6. 31 631. [917.] 10.0 RECEIVER DATA TRANSMITTER DATA 15. 8 Length = 25 m Line = North Length = 1500 m 25. 1 Spacing= 25 m Dipole= 335 Orient. = 335 Field Job 252 39. 8 Distances 6500 m ZONGE ZPLOT 7, 10 CP 63. 1 Rx to Tx= 065 Surveyed= 10/94 Plotted OR Nov 94 100. 9125 2.4 1.9 1.9 2.1 1.7 2.0 1.7 8.8 6.8 7.9 8.5 8.1 7.1 7.4 37.3 34.7 26.1 52.7 49.6 73.8 37.7 7.4 7.0 7.5 9.1 8.4 6.8 4.5 18.5 11.7 12.9 10.7 18.4 17.9 11.4 8192 Hz 8192 Hz 10.0 14.0 10.5 10.1 9.4 9.5 13.1 12.2 11.7 15.8 18.7 20.1 25.5 91.8 28.4 28.9 26.3 24.8 17.7 13.3 11.8 14.8 (16.0 16.1 16.3 4096 Hz 4096 Hz 29.5 21.8 24.0 24.2 20.8 22.7 20.1 22.7 21.7 27.8 25.5 22.0 21.3 21.4 12.5 15.5 16.6 14.7 12.4 21.6 21.5 25.5 26.4 36.3 35.5 36.2 29.5 25.2 18.2 10.7 12.5 10.9 14.3 14.1 10.9 2048 Hz 2048 Hz 12.2 14.7 11.9 13.1 13.5 13.5 10.7 12.6 14.3 11.1 12.0 10.7 13.1 13.5 15.2 12.9 12.5 11.3 10. (38,0 46.8 46.4 39.0 32.5 54.4 48.2 1024 Hz 1024 Hz 8.5 10.8 8.8 10.1 10.3 15.0 12.8 15.8 17.5 14.4 15.6 13.4 8.7 8.6 9:0 8:1 7.4 6:8 9:5 11:0 11:1 8:0 7:0 11:0 10:6 8.28 7.7 512 Hz 512 Hz 12.1 13.5 10.9 11.8 10. 8.7 9.3 10.5 9.7 8.6 8.4 7.4 13.1 14.8 14.1 11. 14.6 13.8 16.0 15.6 20.8 18.8 23.1 18.7 16.3 13.9 256 Hz 256 Hz 21.5 18.7 20.3 14.7 12.0 14.5 16.2 12.6 14.2 11.4 8.2 8.9 9.9 9.1 8.3 8.3 7.5 7.9 18.0 17.3 22.5 20.7 26.3 11,5 14,8 \Q.7 128 Hz 128 Hz 10.9 12.8 12.9 14.6 11.6 14.2 \$.8 12.5 13.4 11.6 10.5 10.9 11.9 11.2 10.0 10.5 9.9 12. 1 64 Hz 64 Hz 12.4 13.4 11.3 9.5 10.3 11.8 10.6 10.0 9.9 32 Hz 32 Hz 3.57 4.5 (5.9) 4.5 4.6 6.3 5.2 6.8 6.6 5.1 5.6 4.5 4.0 4.3 5.1 4.7 4.3 4.5 4.2 3.7 4.4 4.2 2.9 2.3 2.2 2.27 3.0 2.5 3.3 2.8 7.7 2.6 16 Hz 16 Hz 41.5 51.0 46.9 51.8 50.2 74.8 57.0 67.8 71.7 56.5 50.8 49.0 45.5 47.1 54.0 49.1 45.2 49.9 50.0 54.2 52.4 23.7 30.4 27.8 31.3 28.0 28.5 50.1 94.0 39.8 31.2 37.3 30.8 22 0 Hz 0 Hz 86. 4 71. 3 81. 2 83. 0 94. 8 83. 8 78. 8 180. 115. 144. 130. 144. 142. 198. 157. 184. 195. 151. 162. 133. 118. 129. 149. 136. 125. 133. 120. 110. 140. 148. 4 Hz 4 Hz 246. 287. 307. 204. 162 256 248. 2 Hz 2 Hz

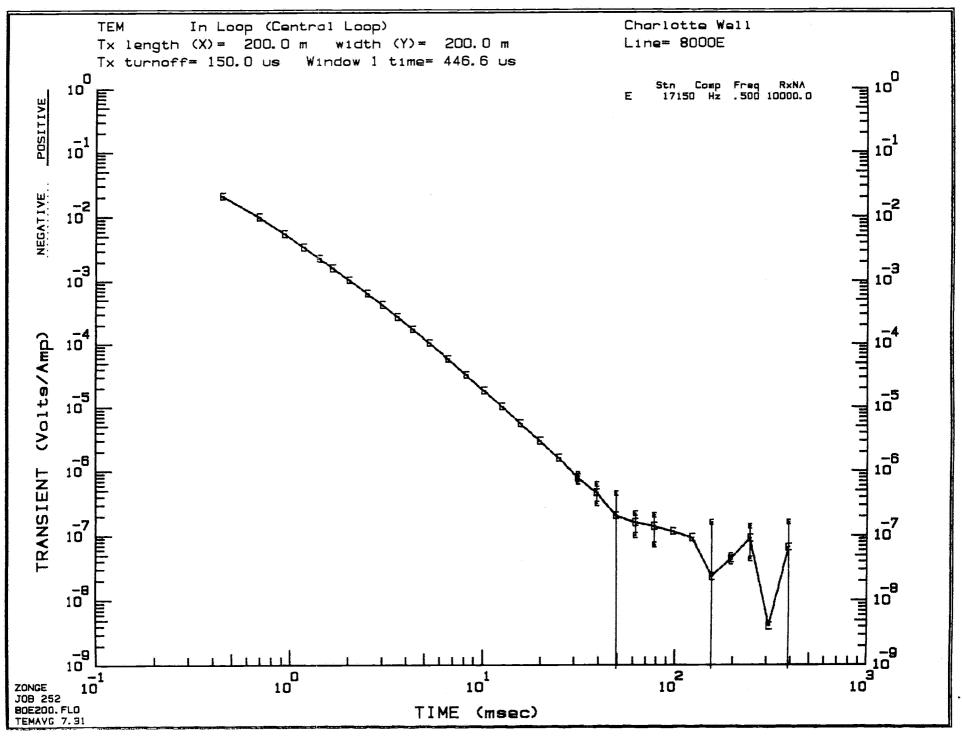
APPENDIX VI

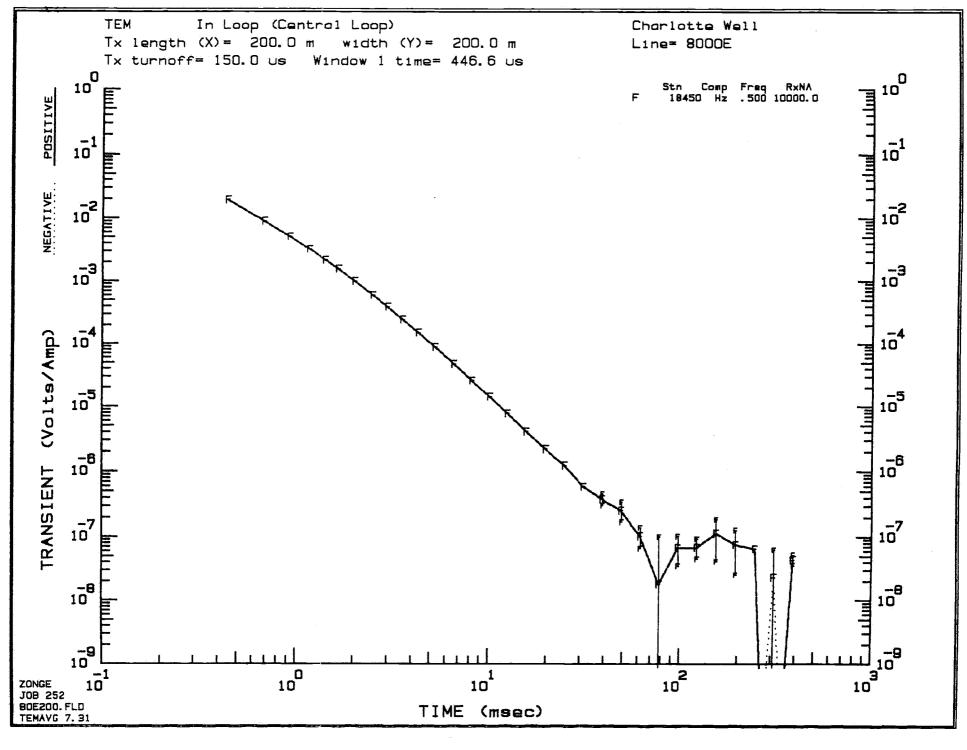
Time Decay Curves for In-loop TEM Survey, Line 8000E

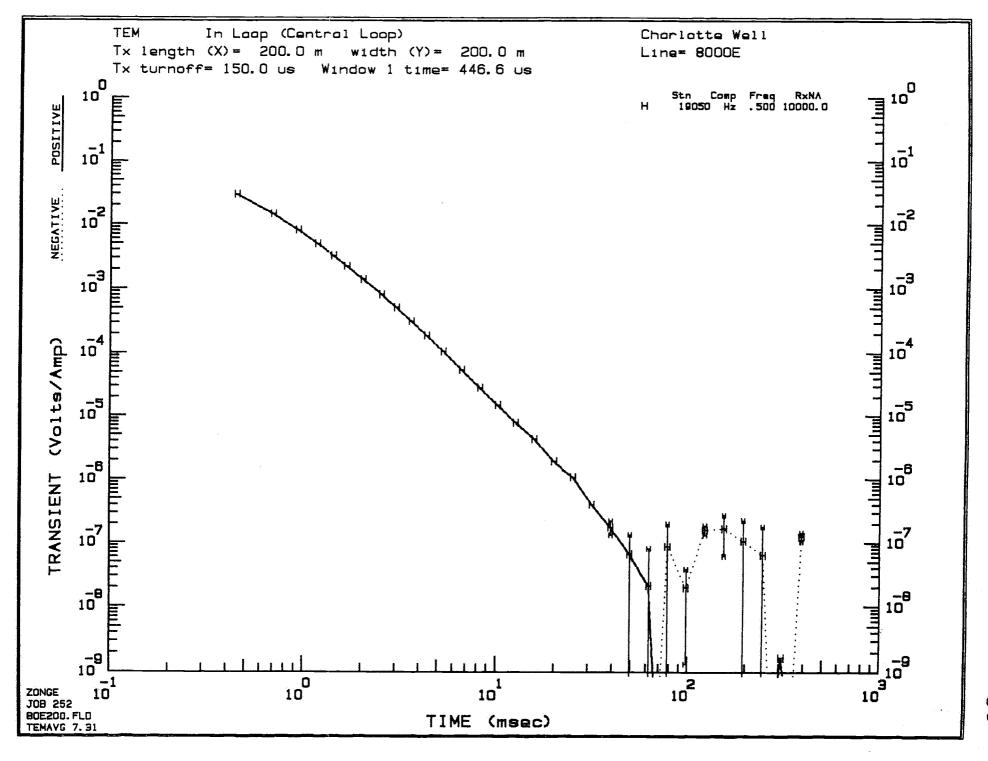


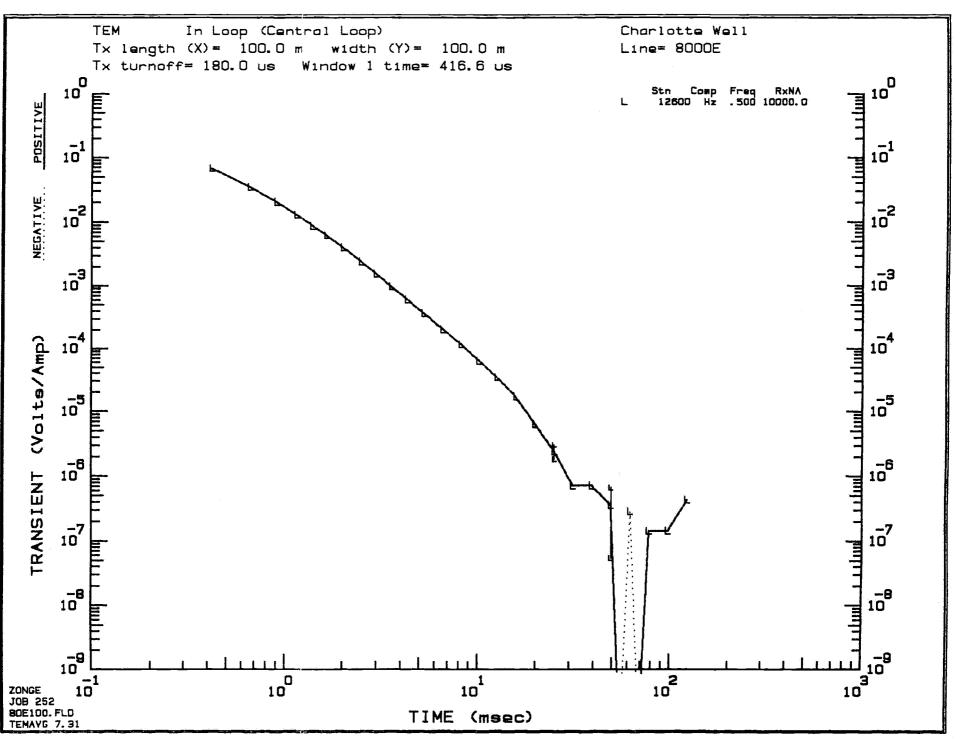
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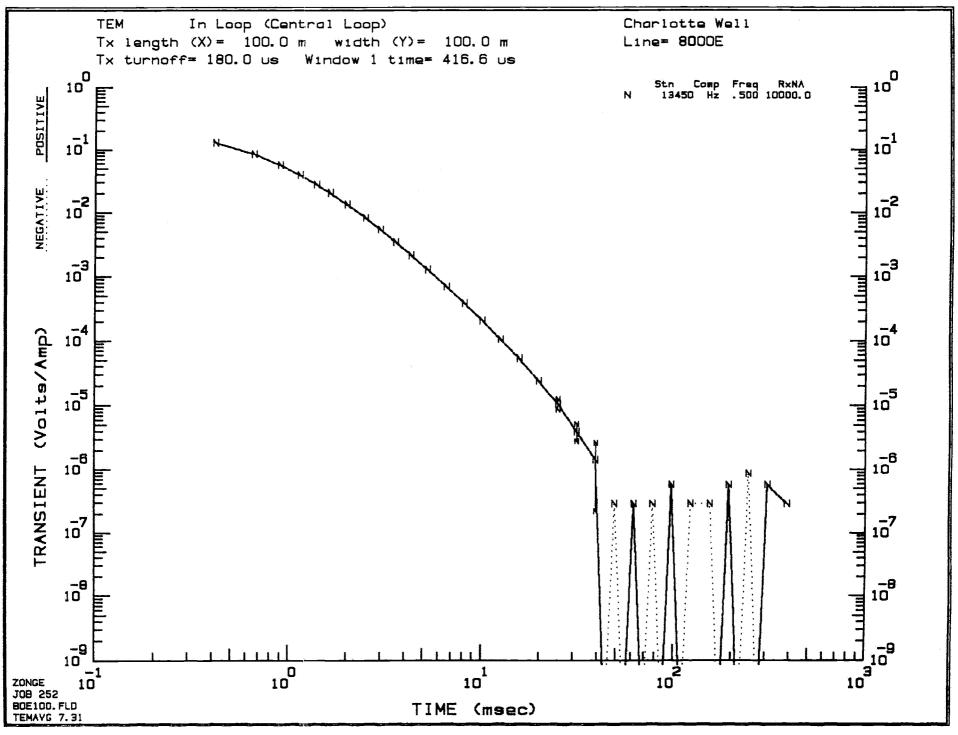


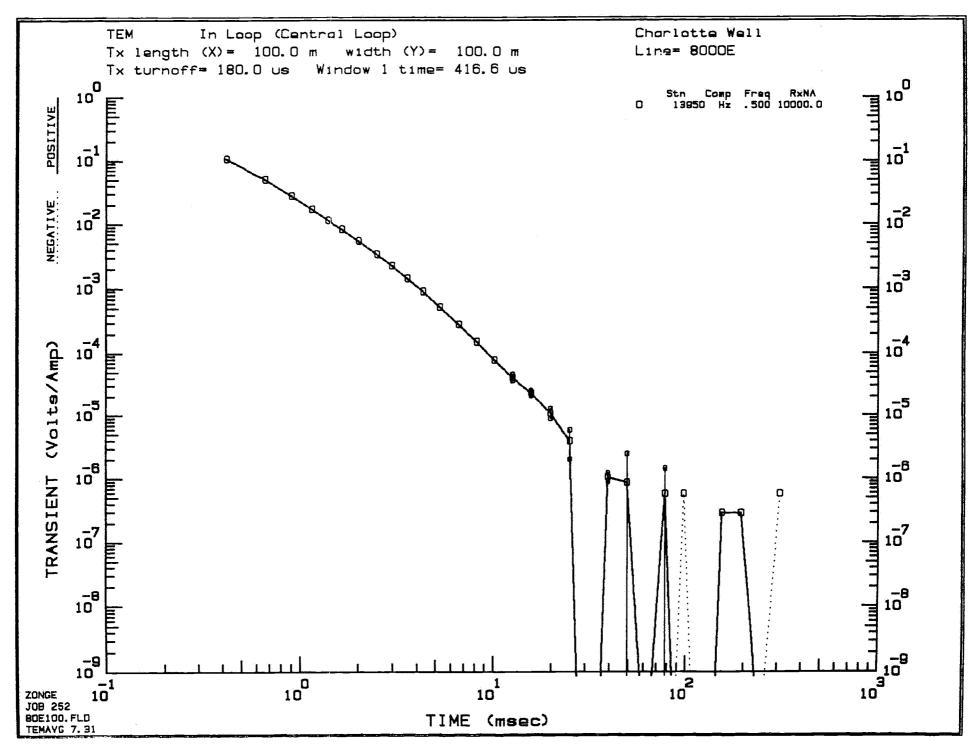


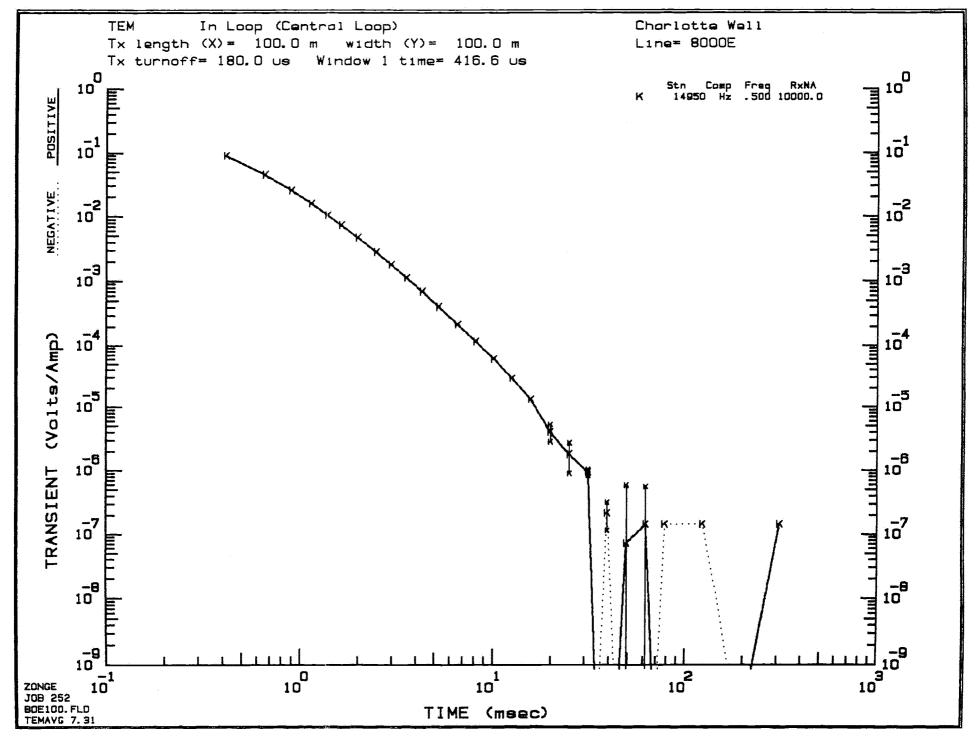


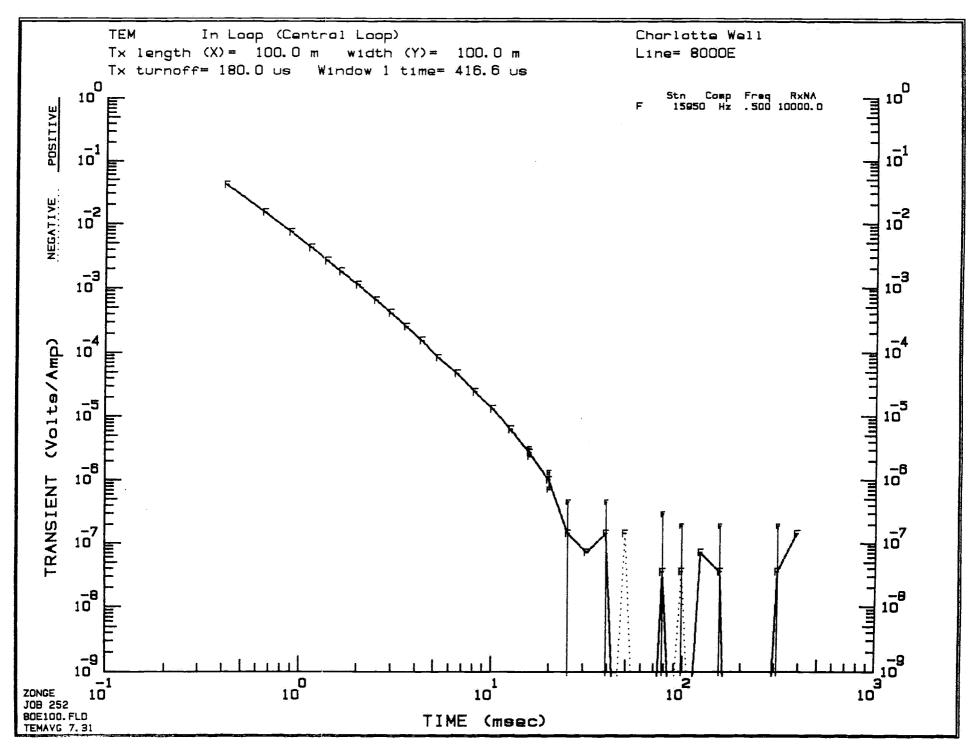


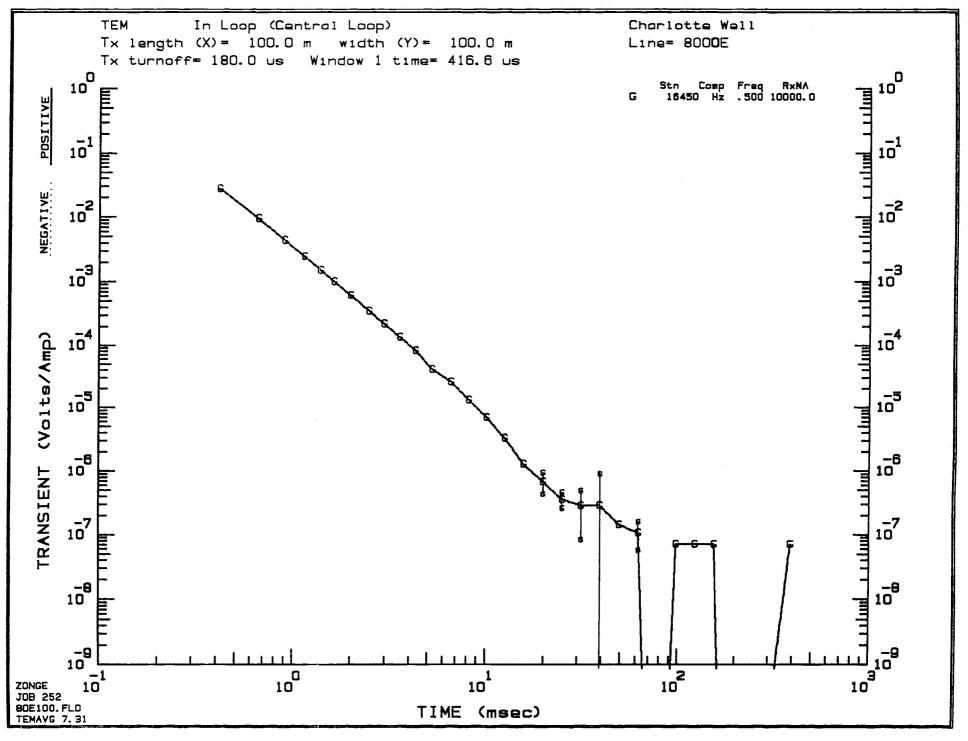




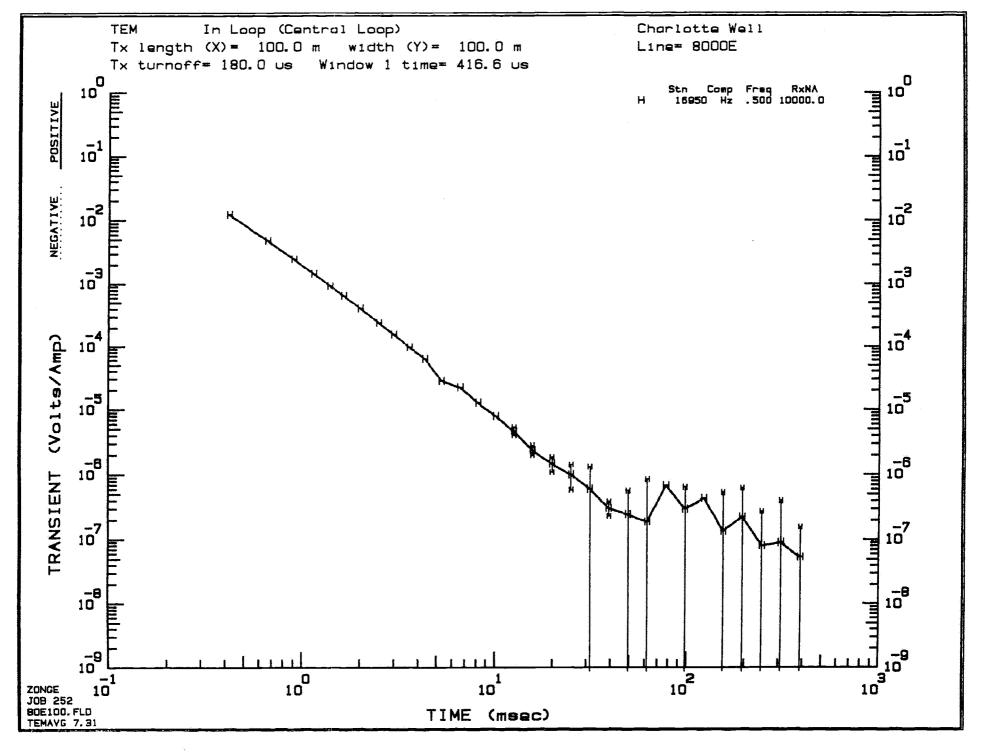






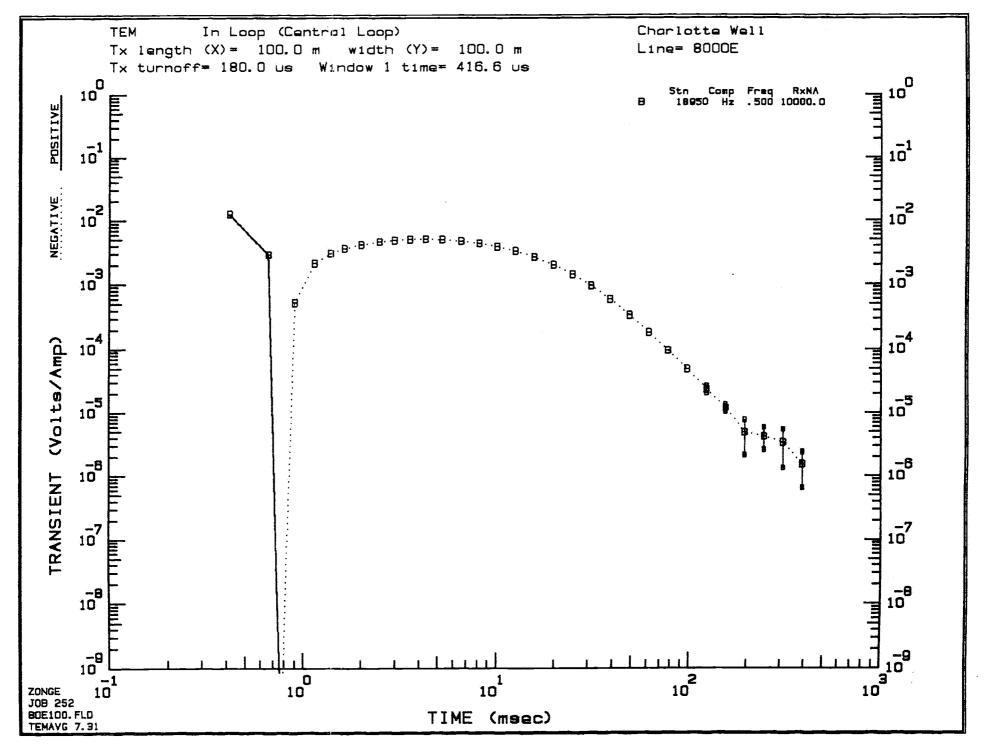


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APPENDIX VII

Lithological Logs and Sample Analyses for 1994 Drill Holes, Line 8000E

CRA EXPLORATION PTY LIMITED

HOLE	AC9	4CW1	CHARLOTTE WELL - EL1974						
PROSPEC AZIMUTH NCLINAT FOTAL DI	ION	PINARY DAM - 90° 48m	NORTHING 6546000(AMG) COMPLETED 8/11/94 ZONE 53 GEOLOGIST WAS	CONTRACTOR DRILLER RIG	3	STRATA JOHN/TI EXPLOR	NY		
		I	GEOLOGICAL DESCRIPTION	RESULTS				*	_
From	То	Summary	Detail	Sample No	From	To	Int	SI	CPS
. 0	. 2	Sand	Red Brown. Sand partly cemented with clay.	3339489	0	2	2	60	. 5
2	4	Sand	Brown, Cemented sand and clayey sand, siliceous.	3339490	2	4	2	20	5
4	5	Sandy Clay	L Brown. Sandy clay and cemented sand.	3339491	4	6	2	20	5
5.	6	Silcrete	Cream Brown. Silcrete with some of the above.	3339492	6	10	4	20	5
6	12	Sand	Cream. Clayey sand.	3339493	10	12	2	20	5
12	1 5	Dolerite	Brown, Weathered dolerite, minor magnetite. Limonitic. Some contamination	3339494	12	13	1	200	5
1.5		Dolerite	Red Brown. Weathered dolerite, minor magnetite. Some red feldspar.	3339495	13	14	1	200	5
19	26	Dolerite	Green Brown. Weathered dolerite, minor magnetite. Some Mn on fractures.	3339496	14	15	1	500	5 5 5
26	38	Dolerite	Green Brown, Mod weathered dolerite, minor magnetite. Some Mn on fractures.	3339497	15	16	1	500	5
38	41	Dolerite	Green Brown, Mod-wk weathered dolerite, minor magnetite, Some Mn on fractures.	3339498	16	17	1	500	5
41	43	Dolerite	Green Brown, Mod weathered dolerite, minor magnetite. Some Mn on fractures.	3339499	17	18	1	300	5
43	47	Dolerite	Green Brown, Mod-wk weathered dolerite, minor magnetite. Some Mn on fractures.	3339500	18	19	1	300	5
47	. 48	Dolerite	Green Brown. Wk weathered dolerite, minor magnetite. Some Mn on fractures.	3339501	19	20	1	300	5 5 5
ВОН				3339502	20	21	1	300	5 5 5
. 1				3339503	21	22	1	300	5
				3339504	22	23	1	400	5
				3339505	23	24	1	600	5
				3339506	24	25	- 1	400	5
				3339507	25	26	1	300	5 5
				3339508	26	28	2	500	5
				3339509	28	30	2	400	5
			A	3339510	30	32	2	1500	5 5
				3339511	32	34	2	900	5
				3339512	34	36	2	1000	5
				3339513	36	38	2	850	5
				3339514	38	40	2	1000	5
				3339515	40	42	2	1000	5
				3339516	42	44	2	1000	5
				3339517	44	46	2	800	5
Ī				3339518	46	48	2	1500	- 5
				ECH		-			
				1					
i i							- 1		
				<u> </u>	1				
\neg				1					

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SAMPLE	Ag	As	Αú	Bi	Ce		Cr	Cu	Fe	K	Mg	Mn	Мо	Na	Ni	Pb	Pd	Pt	Th	Ü Zn
3339489	0	- 1	- 1	0	13	3	230	9	1	0	1	8.0	2	0	10	6		- 5	4	1 20
3339490	0	6	2	0	50	13	170	14	2	. 1	1	140	. 3	0	21	19	1	- 5	7	4 26
3339491	0	12	- 1	0	17	4	190	10	2	1	0	75	3.	0	12	11	- 1	- 5	. 8	2 20
3339492	. 0	. 6	1	0	18	3	130	9	3	. 1	1	85	2	1	9	9	1	- 5	12	2 24
3339493	0	- 1	1	0	11	4	50	8	4	. 1	1	130	1	1	12	9	- 1	- 5	16	3 30
3339494	0	6	- 1	0	.11	. 8	38	11	7		. 1	330	2	1	11	9	- 1	- 5	16	3 40
3339495	0	6	. 1	0	. 9	10	28	14	. 11	0	0	450	3	1	8	7	- 1	- 5	12	3 38
3339496	0	. 4	- 1	0	9	.11	26	17	10	0	0	740	1	1	5	5	- 1	- 5	9	2 65
3339497	0	4	- 1	. 0	11	15	26	19	10	0	. 0	760	1	1	10	8	- 1	- 5	9	2 110
3339498	0	4	- 1	. 0	. 1, 1	15	. 22	17	. 9	0	0	620	1	1	. 7	8	1	5	8	2 80
3339499	0	- 1	1	0	13	18	22	22	10	. 1	0	740	3	1	.8	. 11	- 1	- 5	9	2 90
3339500	. 0	4	- 1	0	1,1	17	24	22	10	1.	0	720	2	. 1	. 8	9	- 1	- 5	8	2 80
3339501	0	4	- 1	O	21	20	16	24	10	1	.1	580	. 2	. 1	11	7	- 1	- 5	. 7	2 75
3339502	0	- 1	- 1	.0	44	. 20	20	28	12	1	. 1	880	2	1	. 14	9	- 1	- 5	7	2 120
3339503	0	4	1	0	50	22	26	. 28	11	. 1	1	740	2	. 1	11	16	1	- 5	8	2 95
3339504	0	4	- 1	0	. 75	20	22	28	10	1	1	760	1	2	11	21	- 1	- 5	7	2 100
3339505	. 0	4	- 1	0	90	24	22	32	9	. 1.	. 1	880	.1	2	13	21	- 1	- 5	8	3 120
3339506	0	- 1	- 1	0	60	24	24	30	9	1	1	800	. 1	.1	13	12	- 1	5	. 6	3 110
3339507	0	4	- 1	0	6.5	23	18	30	1.0	1	1	900	. 2	2	14	11	- 1	- 5	7	4 110
3339508	0	4	- 1	0	65	26	16	36	9	1	1	1150	1	.2	13	10	- 1	- 5	6	2 130
3339509	0	- 1	- 1	0	42	60	20	38	10	1	1	2200	1	2	19	. 8	- 1	- 5	7	2 160
3339510	0	4	- 1	0	48	60	15	36	10	1:	. 1	2600	1	2	20	9	- 1	- 5	7	2 150
3339511	0	- 1	1	0	4 2	49	2.2	30	9	1	1	2000	1	2	20	10	1	- 5	6	2 150
3339512	0	- 1	- 1	0	50	48	22	32	11	. 1	. 1	2600	1	. 2	21	11	- 1	- 5	7	2 160
3339513	0	- 1	- 1	0	50	55	17	32	9	1	. 1	1600	. 1	2	22	9	- 1	- 5	6	2 140
3339514	. 0	- 1	- 1	. 0	49	32	28	32	8	1	1	920	1	. 2	17	9	- 1	- 5	7	2 120
3339515	0	- 1	- 1	0	50	50	22	40	1,1	1		1900	. 1	2	20	10	- 1	- 5	7	2 100
3339516	0	4	1	0	55	38	26	34	9	1	1	1450	1	2	17	9	- 1.	- 5	7	2 120
3339517	0	6	1	0	65	44	22	32	9	2	1	1600	1	2	16	12	- 1	- 5	9	2 120
3339518	. 0	- 1	- 1	0	5 5	35	32	32	9	. 1	1	1300	1	3	16	9	- 1	- 5	8	2 110
SCHEME	ІСЗМ	ІСЗМ	FA3	ІСЗМ	ІСЗМ	IC3M	ЮЗМ	ІСЗМ	ісзм	ІСЗМ	ІСЗМ	ІСЗМ	IC3M	IC3M	ІСЗМ	ІСЗМ	FA3	FA3	ІСЗМ	ІСЗМ ІСЗМ
DL	0	1	1	0	1	0	2	1:	0	Ó	· O.	5	.0	0	2	.0	1	5	0	0 2
UNITS	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	%	%	%	ppm	ppm	%	ppm	ppm	ppb	ppb	ppm	ppm ppm
LAB:AMDEL																				

HOLE	AC/I	DD94	icw:	2			СН	ARLOTTE	WELL .	EL197	74										
PROSPEC	π		PINA	RY DAM	EASTING	G 594150(AMG)		COMMENCED	8/11/94	DPO	54357	AIRCORE	0-42.5m	OXIDISED TO	42m	CONTRACTOR	}	STRATA	\		
AZIMUTH				-	NORTHI	NG 6546000(AMG)		COMPLETED	10/11/94			BQ	42.5-54m	WATER TABLE	-	DRILLER		JOHN /	TINY		
INCLINAT	ION			90°	ZONE	53		GEOLOGIST	WAS							RIG		EXPLOR	ER 200		
TOTAL DE	PTH.			54m	RL.	140m															
. (CORE BLO	OCKS						GEOLOGIC	AL DESCRIPTI	ON								RESUL	TS.		
From	Tö	Rec	%rec	From	То	Summary				Deta	il					Sample No	From	То	Int	SI	CPS
				0.00	2.00	Sand	Orange Brown, Sand, so	ome clay.								3339519	0.00	2.00	2.00	200	4
				2.00	3.00	Sandy Clay	Orange Brown, Sandy of	clay.								3339520	2.00	4.00	2.00	150	40
				3.00	4.00	Sandy Clay	Light Brown. Sandy cl	ay with lumps	of silcrete.							3339521	4.00	10.00	6.00	30	
				4.00	6.00	Silcrete	Light Brown, Silcrete	with cemented	sand.							3339522	10.00	11.00	1.00	700	4
				6.00	10.00	Sandy Clay	Light Brown, Sandy cla	ay.								3339523	11.00	13.00	2.00	250	4 (
				10.00	11.00	Laterite	Red Brown. Laterite c	ap (after dole	rite)							3339524	13.00	15.00	2.00	800	4 (
				11.00	22.00	Mottled Zone	Brown, Highly weather	red dolerite, fe	erruginous in	part.					-	3339525	15.00	17.00	2.00	1500	4 (
				22.00	24.00	Ferruginous Dolerite	Red Brown. Ferruginou	us weathered o	dolerite. Som	iron stai	ned feldsp	ar.				3339526	17.00	19.00	2.00	1500	4 (
				24.00	26.00	Ferruginous Dolerite	Orange Brown, Ferrugi	inous weathere	d dolerite. S	ome iron s	stained fel	dspar.				3339527	19.00	21.00	2.00	1000	.40
				26.00	42.00	Weathered Dolerite	Green Brown, Weather	ed dolerite. Mr	on fractures							3339528	21.00	22.00	1.00	2000	4 (
				42.00	42.50	Dolerite	Grey. Fresh dolerite.									3339529	22.00	24.00	2.00	1000	40
							START DIAMOND TAIL									3339530	24.00	26.00	2.00	2000	40
42.50	44.90	2.30	96	42.50	44.10	Dolerite	Green Grey. Fresh, m	edium to coars	se grained d	lerite with	laths of	leldspar a	nd vesicles	?) filled with qua	rtz	3339531	26.00	28.00	2.00	2000	40
44.90	47.90	3.00	100				and chlorite. Minor py	rite.								3339532	28.00	30.00	2.00	2000	40
47.90	50.90	3.05	102	44.10	44.55	Weathered Dolerite	Brown. Weathered dol	erite.			_					3339533	30.00	32.00	2.00	1500	40
50.90	54.00	3.20	103	44.55	52. <u>5</u> 5	Dolerite	Green Grey. Fresh, m	edium to coar	se grained de	lerite with	laths of	eldspar a	nd vesicles	?) filled with qua	rtz	3339534	32.00	34.00	2.00	2500	40
ECH							and chlorite. Minor py	rite.					<u></u>			3339535	34.00	36.00	2.00	2000	4.0
				52.55	53.55	Altered Dolerite	Band of potassic(?) al	tered dolerite	(pink-brown	colouration) bounded	by calci	te/quartz ve	ins 5mm thick.		3339536	36.00	38.00	2.00	2000	40
							Wk-mod pyrite and tra	ace chalcopyri	le.							3339537	38.00	40.00	2.00	1500	40
				53.55	54.00	Dolerite	Green Grey. Fresh, me	edium to coars	e grained do	lerite with	laths of f	eldspar ar	nd vesicles(?) filled with qua	tz and	3339538	40.00	42.00	2.00	200	40
				EOH			chlorite. Minor pyrite.									3339539	42.00	42.70	0.70	1000	40
								<u></u>								3339699	42.70	44.00	1.30	3000	40
							<u> </u>									3339700	44.00	46.00	2.00	1500	40
																3339701	46.00	48.00	2.00	3000	40
								<u> </u>								3339702	48.00	50.00	2.00	3000	40
																3339703	50.00	52.00	2.00	4000	40
																3339704	52.00	54.00	2.00	1000	40
																	БОН				
						<u> </u>															
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									44												
SAMPLE	Ag	As	Au	Bi	Ce	Co	Cr	Cu	Fe	K	. Mg	Mn	Мо	Na	Ni	Pb	Pd	Pt	Th	U	Zn
3339519	-0.1	- 1	1	-0.1	16	9.2	280	11	2.42	0.500	0.330	310	2.9	0.510	10	4.3	- 1	- 5	3.50	0.51	32
3339520	-0.1	4	. 1	-0.1	14	5.6	230	9	1.65	0.475	0.560	130	2.2	0.260	10	4.9	1	- 5	3.40	0.75	24
3339521	0.3	4	1	0.2	20	4.8	110	10	2.58	1.100	0.580	95	1.6	0.470	13	14.0	- 1	- 5	12.00	2.00	28
3339522	0.2	10	1	0.3	13	4.5	8.0	16	18.00	0.890	0.550	110	1.8	0.520	9	15.0	- 1	- 5	18.00	2.40	46
3339523	-0.1	- 1	- 1	0.2	4.7	3.0	34	12	10.40	0.245	0.220	65	1.1	0.325	3	6.4	1	- 5	10.00	1.60	26
3339524	-0.1	1	- 1	0.2	5.1	5.9	34	24	12.60	0.335	0.200	140	0.8	0.335	4	6.5	- 1	- 5	9.30	2.00	32
3339525	-0.1	4	- 1	0.1	8.1	6.5	32	24	10.60	0.415	0.220	170	0.6	0.405	. 4	5.1	- 1	- 5	8.60	2.20	34
3339526	0.1	- 1	-,1	0.2	6.9	9.9	44	20	9.10	0.390	0.305	210	0.9	0.650	6	5.5	- 1	- 5	9.30	2.30	40
3339527	-0.1	- 1	- 1	0.2	6.9	10.0	32	28	9.10	0.395	0.380	210	0.6	0.900	8	6.6	- 1	- 5	8.20	2.90	46
3339528	-0.1	- 1	1	0.1	7.4	14.0	32	26	8.85	0.465	0.540	260	0.4	1.240	9	4.9	- 1	- 5	8.00	2.40	80
3339529	-0.1	- 1	1	0.2	5 5	14.0	26	28	8.70	0.730	0.580	310	0.8	1.420	9	6.1	- 1	- 5	8.30	2.90	80
3339530	-0.1	- 1	- 1	-0.1	100	19.0	24	32	8.05	1.260	0.680	340	0.9	1.660	11	4.8	- 1	- 5	5.90	2.80	75
3339531	-0.1	- 1	- 1	0.1	105	31.0	30	40	9.50	1.280	0.910	470	0.9	1.960	1.8	8.0	- 1	- 5	9.10	3.80	130
3339532	-0.1	• 1	- 1	-0.1	65	36.0	34	38	8.55	1.340	0.990	1050	0.6	1.940	18	20.0	- 1	- 5	7.20	2.30	100
3339533	-0.1	- 1	- 1	0.1	49	34.0	20	36	8.55	1.460	1.040	1500	0.5	2.080	19	25.0	- 1	- 5	7.30	1.96	120
3339534	-0.1	- 1	- 1	0.1	135	50.0	26	40	8.65	1.600	1.080	1850	0.5	2.200	24	18.0	- 1	- 5	8.50	2.70	120
3339535	-0.1	4	- 1	0.2	155	48.0	24	42	8.55	1.740	1.140	1350	0.4	2,520	24	9.8	- 1	- 5	8.10	1.92	120
3339536	-0.1	- 1	1	0.1	70	55.0	26	42	8.40	1.540	1.260	1600	0.6	2.700	31	8.4	- 1	- 5	7.00	1.36	150
3339537	-0.1	- 1	1	0.1	42	47.0	22	38	8.05	1.680	1,420	1500	0.8	2.840	30	8.1	1	- 5	7.30	1.44	190
3339538	-0.1	- 1	. 1	-0.1	40	65.0	22	34	8.50	1.780	1.700	2100	0.4	2.200	65	11.0	- 1	- 5	7.30	1.75	200
3339539	-0.1	- 1	- 1	0.1	50	70.0	20	38	7.85	1.580	1.800	2750	0.7	2.380	31	9.9	- 1	- 5	7.10	1.62	150
3339699	-0.1	4	- 1	0.1	49	40.0	28	3.8	8.25	1.420	2.460	1350	0.7	2.400	1.7	12.0	- 1	- 5	6.40	1.28	120
3339700	-0.1	6	- 1	0.2	5.5	44.0	24	38	8.30	1.360	2.600	1350	0.5	2.380	16	10.0	- 1	- 5	7.60	1.24	120
3339701	0.1	- 1	- 1	0.1	50	36.0	22	38	8.80	1.360	2.440	1300	0.5	2.260	15	9.3	- 1	- 5	8.00	1.53	110
3339702	0.1	1	- 1	0.1	55	38.0	22	38	8.35	1.460	2.500	1300	0.5	2.260	19	9.5	1	- 5	7.60	1.30	110
3339703	0.1	6	- 1	0.2	5 5	39.0	24	36	8.55	1.480	2.400	1300	1.2	2.240	21	11.0	<u>- 1</u>	- 5	8.10	1.64	110
3339704	-0.1	12	- 1	-0.1	5 5	38.0	22	34	8.05	1.660	2.060	1150	1.9	2.300	20	11.0	- 1	- 5	6.70	3.30	100
SCHEME	IC3M	IC3M	FA3	IC3M	ІСЗМ	ІСЗМ	ІСЗМ	ІСЗМ	IC3M	IC3M	ІСЗМ	IC3M	IC3M	IC3M	ІСЗМ	ІСЗМ	FA3	FA3	IC3M	ІСЗМ	IC3M
DL	0.1	1	. 1	0.1	0.5	0.2	2	1	0.01	0.001	0.001	. 5	0.2	0.001	2	0.2	1	5	0.02	0.02	2
UNITS	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	%	%	_%	ppm	ppm	%	ppm	ppm	ppb	ppb	ppm	ppm	ppm
LAB:AMDEL																					

CRA EXPLORATION PTY LIMITED

HOLE	AC9	4CW3		CHARLOTTE WEL	L - EL1974	<u> </u>	·											
PROSPEC	T	PINARY DAM	EASTING	594350(AMG)	COMMENCED	8/11/94	DPO	54357	AIRCORE	40.5m	OXIDISED TO	39π	CONTRACTOR		STRATA	·		\exists
AZIMUTH		±	NORTHING	6546000(AMG)	COMPLETED	8/11/94					WATER TABLE	_	DRILLER		JOHN/TI	NY		1
INCLINAT	ION	90°	ZONE	53	GEOLOGIST	WAS							RIG		EXPLOR	ER 200		- 1
TOTAL DE	PTH	40.5m	RL										1					
					GEOLOGICA	L DESCRIPTION	NN								RESULTS	3		
From	To .	Summary				Detail							Sample No	From	То	Int	SI	CPS
0			Orange Bro	wn. Sand, some cemented lumps		<u> </u>							3339540	0	4	4	50	50
3	. 4	Cemented Sand	Orange Bro	wn. Cemented sand, almost silcrete.		<u> </u>							3339541	4	6	2	50	50
4	5	Silcrete	Orange Bro	wn. Silcrete, ferruginous n part, plus	cemented sand.								3339542	6	10	4	20	50
-5	6	Sandy Clay	Light Brown	n. Sandy clay and silcrete.									3339543	_ 10	12	2	150	50
6	10	Sandy Clay	Light Brown	i. Sandy clay.									3339544	12	14	2	500	50
10		Clay	Cream. Clay	<i>(</i>		<u>_</u>							3339545	14	16	2	500	50
11	12	Weathered Dolerite	Red Brown.	Clay and highly weathered dolerite.									3339546	16	18	2	600	50
12			Red Brown	. Highly weathered dolerite, ferruginou	ıs in part.				_				3339547	18	20	2	600	50
17	20	Weathered Dolerite	Orange Bro	wn. Weathered dolerite, ferruginous i	part. Iron stain	ed feldspars.							3339548	20	22	2	2000	50
20	,		}	n. Weathered dolerite, Mn on fracture									3339549	22	24	_ 2	2000	50
39	. 41	Weathered Dolerite	Green. Wk-	Mod weathered dolerite, Mn on fractur	es. Mod magnetil	te,							3339550	24	26	2	1500	50
ECH													3339551	26	28	2	800	50
				<u> </u>									3339552	28	30	2	1500	50
				<u></u>									3339553	30	32	2	2000	50
										···			3339554	32	34	2	2000	50
\longrightarrow				and the second s									3339555	3 4	36	2	2000	50
													3339556	36	38	2	2000	50
				<u> </u>									3339557	38	40	2	3000	50
		ļ ·											3339558	40	40.5	0.5	3000	50
													<u> </u>	ВОН				
				<u> </u>									4					
				<u> </u>		· · · · · · · · · · · · · · · · · · ·]				
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			l										1	1			- 1	- 1

1.4 0.365 0.395

0.84

1.18

0.48

0.47

Mn Мо

75

100 3.3

120 2.8 0.175

1.4

0.35

0.43

Pb Pd Pt

3.4 -1 -5

13 -1 -5

7.6 -1 -5

2.2 0.47

8.6 2.3

9.2 1.24

18

24

13

16

10

Fe

2.3

2.6

9

11

10

SAMPLE

3339540

3339541

3339542

As Au

-0.1

-0.1

Bi Ce Co Cr Cu

-0.1

0.2

0.2

9.2 4.7 370

31 7.4 320

17 3.6 120

3333342	0.1	- 4	- 1	0.2	1.	3.0	120	10	2.0	1.10	0.47	/ 5	1.4	0.43	10	7.6	- 1	1 - 5	9.2	1.24	24
3339543	-0.1	4	- 1	0.2	30	5.1	55	12	7	1.2	0.8	130	1.8	0.67	15	19	- 1	- 5	16	2.5	32
3339544	-0.1	4	- 1	0.1	33	6.5	32	15	12.6	0.225	0.175	110	1.6	0.6	6	22	- 1	- 5	6.1	2.2	38
3339545	0.1	- 1	- 1	-0.1	_ 11	8.2	36	22	12.2	0.25	0.195	190	1.5	0.99	7	7,2	- 1	- 5	5.4	1.95	5.0
3339546	-0.1	- 1	- 1	0.3	6.5	_ 13	34	28	10.8	0.325	0.33	290	0.9	1.48	12	8.5	- 1	- 5	6.7	2.9	70
3339547	-0.1	- 1	- 1	0.2	7.9	18	3.8	24	9.35	0.425	0.475	280	0.8	1.66	16	11	- 1	- 5	6.1	3.2	
3339548	-0.1	6	- 1	0.1	12	25	30	32	12.2	0.84	0.57	400	0.7	1.56	17	14	1	- 5	7.9	4.1	100
3339549	-0.1	- 1	- 1	0.1	65	30	34	32	11.2	1.34	0.75	430	1.2	1.62	13	9.3	- 1	- 5	6.8	3.5	100
3339550	-0.1	. 6	- 1	0,1	70	39	36	3.6	10.4	1.58	0.84	760	2	1.8	18	16	- 1	- 5	7.3	4	110
3339551	-0.1	1.2	- 1	0.1	90	49	26	40	10	1.6	0.9	1700	0.6	1.88	16	4.1	- 1	- 5	6.5	3.1	.110
3339552	0.4	6	- 1	0.1	_ 46	7.5	26	40	9.25	1.6	0.95	2100	0.8	2.12	17	22	- 1	- 5	6.1	2.8	130
3339553	-0.1	4	1	-0.1	40	70	28	42	9.9	1.5	1.24	2700	0.4	2.72	23	18	- 1	- 5	6.2	2	150
3339554	0.8	- 1	- 1	0.2	37	55	24	40	9.4	1.46	1.2	4450	0.7	3.02	17	8.3	- 1	- 5	5.9	2.1	110
3339555	-0.1	- 1	- 1	0.1	3.3	70	24	46	8.7	1.5	1.2	11000	0.8	3.32	13	8.9	- 1	- 5	4.6	2.4	110
3339556	-0.1	- 1	¥ 1.	0.1	38	38	28	40	9.1	1.62	1.14	600	0.5	3.34	14	6.6	- 1	- 5	5.6	1.78	110
3339557	-0.1	4	- 1	0.1	22	44	28	. 32	8.45	1.48	1.38	640	0.9	3.34	15	8.8	- 1	- 5	3	1.14	110
3339558	-0.1	4	1	-0.1	29	38	48	26	8.2	1.62	1.58	600	0.9	3.36	14	7.8	- 1	- 5	4.6	1.2	110
SCHEME	IC3M	IC3M	FA3	IC3M	IC3M	ІСЗМ	ІС3 М	ІСЗМ	ІСЗМ	IC3M	IC3M	IC3M	ІСЗМ	IC3M	ІСЗМ	IC3M	FA3	FA3	ТСЗМ	ІСЗМ	ІС3 М
DL.	0.1	1	1	0.1	0.5	0.2	2	. 1	0.01	0.001	0.001	. 5	0.2	0.001	2	0.2	1	. 5	0.02	0.02	2
UNITS	ppm	ppm	ppb.	ppm	ppm	ppm	ppm	ppm	%	%	%	ppm	ppm	%	ppm	ppm	ppb	ppb	ppm	ppm	. ppm
LAB:AMDEL																					
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CRA EXPLORATION PTY LIMITED

HOLE	AC9	4CW4		CHARLOTTE	WELL - EL1974													
PROSPEC	CT	PINARY DAM	EASTING	594900(AMG)	COMMENCED	9/11/94	DPO	54357	AIRCORE	18m	OXIDISED TO	39m	CONTRACTOR	3	STRATA			
AZIMUTH		•.	NORTHING	6546000(AMG)	COMPLETED	9/11/94					WATER TABLE		DRILLER		JOHN/TI	NY		
NCLINAT	ION	90°	ZONE	53	GEOLOGIST	WAS							RIG		EXPLOR	ER 200		
TOTAL DE	EPTH	18m	RL	140m														
					GEOLOGICAL	DESCRIPTION	N								RESUL	rs		
From	Τó	Summary				Detail				_			Sample No	From	То	Int	SI_	CPS
0		1		vn. Sand with some silcrete.								_	3339559	0	2	2	50	_ 50
1				wn. Silcrete/calcrete.									3339560	2	6	4	20	50
_ 2				n. Cemented sand.	·		_						3339561	6	1.0	4	20	5.0
4				Sandy clay.									3339562	1.0	. 12	2	20	5.0
12	. 18			thered Gawler Range Volcanics	s, finly flow banded (tuff:	aceous?) in	part. Ger	neraly greer	groundmass	with rou	nd pink feldspars,		3339563	12	14	2	40	50
ECH			frquently br	recciated.									3339564	14	16	2	40	
				a set of									3339565	16	18	2	40	5.0
												_		ECH				
				<u> </u>												_		
					<u> </u>													
												0.11						
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SAMPLE	Ag	As	Αú	Bi	Ce	Co	Cr	Cu	Fe	ĸ	Mg	Mn	Мо	Na	Ni	Pb	Pd	Pt	Th	U	Zn
3339559	-0,1	- 1	- 1	-0.1	13	4.7	250	10	1.35	0.4	0.51	90	1.9	0.205	10	3.2	1	- 5	2.4	0.51	20
3339560	-0.1	6	- 1	0.1	17	4.3	140	. 9	1.83	0.87	0.56	85	1.7	0.29	11.	6.2	- 1	- 5	4.9	1.01	20
3339561	0.3	4	1	0.2	20	3.1	95	. 7	2.32	1.06	0.39	65	1.5	0.36	6	7.9	- 1	- 5	12	1.25	18
3339562	0.1	- 1	- 1	0.3	1.8	4.3	50	9	2.96	1.12	0.64	75	0.4	0.63	8	12	- 1	- 5	15	1.54	22
3339563	0.1	- 1	- 1	0.1	85	4.9	42	3	1.98	1.4	0.5	130	1.8	1.82	3	9	- 1	- 5	2 1	2.5	5.5
3339564	-0.1	- 1	- 1	-0.1	75	3.8	36	3	1.54	. 1.44	0.45	95	0.8	2.4	- 2	9.2	- 1	- 5	16	2.2	50
3339565	0.3	- 1	- 1	0.1	80	4.4	28	2	1.35	1.32	0.44	90	0.6	2.24	- 2	14	- 1	- 5	14	2.2	60
SCHEME	IC3M	IC3M	FA3	IC3M	IC3M	ІСЗМ	IC3M	ІСЗМ	IC3M	IC3M	IC3M	ІСЗМ	ІСЗМ	ІСЗМ	IC3M	IC3M	FA3	FA3	IC3M	IC3M	ІСЗМ
DL	0.1	1	_ 1	0.1	0.5	0.2	2	1	0.01	0.001	0.001	5	0.2	0.001	2	0.2	1	5	0.02	0.02	2
UNITS	ppm	ppm	ppb	р́рт	ppm	ppm	ppm	ppm	%	%	%	ppm	ppm	%	ppm	ppm	ppb	ppb	ppm	ppm	ppm
LAB:AMDEL																					

CRA EXPLORATION PTY LIMITED

HOLE	AC94	ICW5		CHARLOTTE	WELL - EL1974												
PROSPEC AZIMUTH INCLINAT		PINARY DAM - 90°	EASTING NORTHING ZONE	593400(AMG) 6546000(AMG) 53	COMMENCED COMPLETED GEOLOGIST	9/11/94 9/11/94 WAS		54357	AIRCORE	53m	OXIDISED TO WATER TABLE	CONTRACTOR DRILLER RIG	•	STRATA JOHN/TI EXPLOR	INY		
TOTAL DE	EPTH	53m	RL	140m								 					
					GEOLOGICA	L DESCRIPTIO	N							RESUL	TS		
From	То	Summary				Detail						 Sample No	From	Τo	Int	SI	CPS
0	3			wn. Sand with some cemented		2.2					<u> </u>	3339566	0	4	4	30	5
3	5			wn. Sand and clay with some c	emented lumps.					and the second control of the second control	er amborinangongan i sebig	3339567	4		3	30	5
. 5	7			vn. Cemented sand.								 3339568	. 7	10	3	20	5
. 7	8		i— v	. Silcrete and sandy clay.								3339569	10	1 4	4	20	5
8	17			. Sandy clay								 3339570	1 4	17	3	20	5
17	19			. Sandy clay, ferruginous in p								 3339571	17	19	2	20	5
19	20			olitic duricrust, pisolites have	goethite skins.							 3339572	19	20	1	600	5
20	23			dy clay, ferruginous in part.								3339573	20	21	1	200	5
23	25			thered Gawler Range Volcanic								3339574	21	22	1	20	5
25	27		1	thered Gawler Range Volcanic						actures.	<u> </u>	3339575	22	25	3	20	5,0
27	30		1	weathered Gawler Range Volc								 3339576	25	27	2	20	5.0
3.0	37			n. Weathered Gawler Range V								 3339577	27	3.0	3	20	50
37	39			thered Gawler Range Volcanic						n fracture	S	 3339578	30	32	2	20	5 (
39	42			n. Weathered flow banded Gav		inding approx	15° to CA. I	<u>Vin</u> on tr	actures.			 3339579	32	34	2	20	5 (
42	4 4		t	cciated Gawler Range Volcanic								 3339580	34	36		20	5 (
44	45			n. Weathered flow banded Gar					ures.			 3339581	36	38	2	20	5 (
4.5	5.3		Brown, Weat	thered flow banded Gawler Rar	ige Volcanics. Banding 9	0° to CA. Mn	on fractures	•				 3339582	38	40	2	20	5 (
ВОН					 	1 1201	·					3339583	40	42	2	20	50
												 3339584	42	44	2	20	50
	— -l				·							 3339585	44	46	2	20	5 0
												 3339586	46	4.8		20	50
						<u> </u>			4 - 4 - 4			 3339587	48	50		20	50
												 3339588	50	53	3	20	5.0
												 	ВОН				
								-									
											<u> </u>						
		<u> </u>								<u> · </u>	<u> </u>	 					
		. ,		<u> </u>	· · · · · · · · · · · · · · · · · · ·				-	·		 					
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339568		0.00																				
339567	SAMPLE	Ag	As	Au	Bi	Ce	Co	Cr	Cu	Fe	K	Mg	Mn	Mo	Na	. Ni	Pb	Pd	Pt	Th	U	Zn
339568	3339566	-0.1	- 1	- 1	-0.1	7.8	2.1	300	. 6	1.06	0.35	0.225	60	2.1	0.094	. 8	3.9	- 1	- 5	1.64	0.22	14
3339570 -0.1 -1 -1 -1 0.2 -15 4.7 55 9 3.8 1.2 0.81 120 1.2 0.67 13 6.9 -1 -5 14 1.92 28 339570 -0.1 -1 -1 0.2 5.8 2 230 8 3.64 0.235 0.385 50 3 0.36 7 4.2 -1 -5 11 1.25 24 3339572 -0.1 8 1 0.2 5.8 2 230 8 3.64 0.235 0.385 50 3 0.36 7 4.2 -1 -5 11 1.25 24 3339573 -0.1 -1 -1 0.2 3.6 1.8 340 7 4.1 0.145 0.355 45 2.1 0.35 5 4.9 -1 -5 5 6.6 0.84 14 3339574 -0.3 -1 1 0.1 0.2 3.6 1.8 340 7 4.1 0.145 0.355 45 2.1 0.35 5 4.9 -1 -5 6.6 0.84 14 3339575 0.1 -1 1 0.2 28 1.9 80 6 1.8 1.8 1.38 0.475 35 1.5 0.275 3 7.1 -1 5 1.5 1.4 2.4 20 3339575 0.1 -1 1 0.2 28 1.9 80 6 1.8 1.8 1.38 0.475 35 1.5 0.275 3 7.1 -1 5 1.5 1.4 2.4 20 339575 0.1 -1 1 0.1 0.2 28 1.9 80 6 1.8 1.38 0.475 35 1.5 0.275 3 7.1 -1 5 1.5 1.8 2.8 4339577 0.1 -1 1 0.1 0.2 28 1.9 80 6 1.8 1.38 0.475 35 1.5 0.275 3 7.1 -1 5 1.5 1.4 2.4 20 339576 -0.1 -1 1 0.2 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	3339567	-0.1	- 1	- 1	0.2	21	6.9	200	11	2.34	0.86	0.48	90	1.8	0.27	13	11	- 1	- 5	8.1	1.88	32
339570 -0.1	3339568	-0.1	6	- 1	0.2	15	3.8	110	8	3	1.06	0.55	85	1.8	0.42	10	9.4	- 1	- 5	9	1.59	28
3399571 0.1	3339569	-0.1	4	- 1	0.2	15	4.7	5 5	9	3.18	1.2	0.81	120	1.2	0.67	13	6.9	- 1	- 5	14	1.92	28
3339572 -0.1 8 1 0.2 6.6 2.9 290 6 10.5 0.145 0.265 65 2.7 0.245 6 8.5 -1 -5 9.7 0.9 13 3339573 -0.1 -1 -1 0.2 3.6 1.8 340 7 4.1 0.145 0.355 45 2.1 0.35 5 4.9 -1 -5 6.6 0.84 14 3339574 0.3 -1 -1 0.1 3.5 2.4 260 6 2.64 0.12 0.4 40 2.3 0.405 6 3 -1 -5 4.8 0.73 14 3339575 0.1 -1 1 0.2 28 1.9 80 6 1.8 1.38 0.475 35 1.5 0.275 3 7.1 -1 -5 1.4 2.4 20 3339576 -0.1 -1 1 0.2 31 1.9 20 4 2.94 1.46 0.59 35 0.9 0.355 -2 5.8 -1 -5 18 2.5 44 3339577 0.1 -1 0.1 10.5 5.1 19 4 5.3 1.64 0.65 65 0.9 0.55 -2 7.9 -1 -5 18 2.8 75 3339578 0.1 -1 -1 0.1 210 5.9 14 -1 3.68 1.16 0.66 75 0.8 0.72 -2 8.5 -1 -5 24 3.5 65 3339579 0.2 -1 -1 0.2 190 7.4 18 3 5.95 1.36 0.61 140 2.1 1.7 2 8.2 -1 -5 22 3.8 55 3339580 0.1 -1 1 0.2 140 5.8 26 3 3.16 1.76 0.62 80 0.7 1.52 -2 7 7 1 -5 22 3.8 55 3339581 0.1 -1 -1 0.1 155 11 30 3 3.06 1.46 0.67 620 0.7 1.52 -2 7 7 1 -5 24 4.3 60 3339583 0.1 -1 -1 0.1 155 11 38 20 4 2.98 1.4 0.65 1500 1.8 1.72 -2 9.7 -1 -5 18 3.9 65 3339584 0.1 -1 -1 0.1 155 11 30 3 3.68 1.56 0.74 3250 1.2 1.34 3 11 -1 5 2.0 5.5 60 3339585 0.1 -1 -1 0.1 10 1 2 30 4 2.98 1.4 0.65 1500 1.9 1.94 3 8.6 -1 -5 18 3.9 65 3339586 0.2 -1 -1 0.1 10 0.1 95 1.5 26 3 3.68 1.56 0.74 3250 1.2 1.34 3 11 -1 5 5 15 3.6 3.6 70 3339587 0.1 -1 -1 0.1 10 12 30 4 3.2 1.4 0.51 1.00 1.5 1.54 3 9.5 -1 -5 18 2.9 65 3339588 0.2 -1 -1 -1 0.1 10 4.8 15 4 3.02 1.34 0.52 1000 1.9 1.94 3 8.6 -1 -5 15 3.3 48 SCHEME 13M FAX 103M FAX 103M IC3M IC3M IC3M IC3M IC3M IC3M IC3M IC	3339570	-0.1	- 1	- 1	0.2	9.1	3.1	100	. 7	2.98	0.81	0.83	110	1.2	0.69	8	6.3	. 1	- 5	12	1.65	20
3339573	3339571	0.1	- 1	- 1	0.2	5.8	2	230	. 8	3.64	0.235	0.385	50	3	0.36	7	4.2	- 1	- 5	11	1.25	24
3339574 0.3 -1 -1 0.1 3.5 2.4 260 6 2.64 0.12 0.4 40 2.3 0.405 6 3 -1 -5 4.8 0.73 14 3339575 0.1 -1 1 0.2 28 1.9 80 6 1.8 1.38 0.475 35 1.5 0.275 3 7.1 -1 -5 14 2.4 20 3339576 -0.1 -1 1 0.2 31 1.9 20 4 2.94 1.46 0.59 35 0.9 0.355 -2 5.8 -1 -5 18 2.5 44 3339577 -0.1 -1 -1 -1 0.1 105 5.1 19 4 5.3 1.64 0.65 65 0.9 0.55 -2 7.9 -1 -5 18 2.8 75 3339578 -0.1 -1 -1 0.1 210 5.9 14 -1 3.68 1.16 0.66 75 0.8 0.72 -2 8.5 -1 -5 24 3.5 65 3339579 0.2 -1 -1 0.2 190 7.4 18 3 5.95 1.36 0.61 140 2.1 1.7 2 8.2 1.7 5 22 3.8 55 3339580 -0.1 -1 1 0.2 140 5.8 26 3 3.16 1.76 0.62 80 0.7 1.52 -2 7 -1 -5 22 3.8 55 3339581 0.1 -1 1 0.1 155 11 30 3 3.06 1.46 0.67 620 0.7 1.6 -2 8.4 -1 -5 24 4.3 60 3339582 0.1 -1 -1 0.1 155 11 30 3 3.06 1.46 0.67 620 0.7 1.6 -2 8.4 -1 -5 24 4.3 60 3339583 -0.1 -1 -1 0.1 90 15 26 3 3.68 1.56 0.74 0.62 500 0.8 1.72 -2 9.7 -1 -5 18 3.9 65 3339586 0.1 -1 -1 0.1 90 15 26 3 3.68 1.56 0.74 0.62 500 0.8 1.72 -2 9.7 -1 -5 18 3.9 65 3339586 0.1 -1 -1 0.1 90 15 26 3 3.68 1.56 0.74 0.65 1500 1.9 1.94 3 8.6 -1 -5 17 3.1 60 3339586 0.2 -1 -1 0.1 0.1 100 4.8 13 3.76 1.28 1.56 1.50 0.8 1.24 -2 1.8 4 3 11 -1 5 15 15 2.9 65 3339587 0.1 -1 -1 0.1 90 8.4 18 3 3.76 1.28 1.56 1.50 0.8 1.24 -2 1.7 1 -5 1.5 15 3.6 60 3339588 0.1 -1 1 0.1 0.1 90 8.4 18 3 3.76 1.28 1.56 1.50 0.8 1.24 -2 1.7 1 -5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.	3339572	-0.1	8	1	0.2	6.6	2.9	290	6	10.5	0.145	0.265	65	2.7	0.245	6	8.5	- 1	- 5	9.7	0.9	13
3339575	3339573	-0.1	- 1	- 1	0.2	3.6	1.8	340	7	4.1	0.145	0.355	45	2.1	0.35	5	4.9	- 1	- 5	6.6	0.84	14
3339576 -0.1 -1 1 0.2 31 1.9 20 4 2.94 1.46 0.59 35 0.9 0.355 -2 5.8 -1 -5 18 2.5 44 3339577 -0.1 -1 -1 -0.1 105 5.1 19 4 5.3 1.64 0.65 65 0.9 0.55 -2 7.9 -1 -5 18 2.8 75 3339578 -0.1 -1 -1 0.1 210 5.9 14 -1 3.68 1.16 0.66 75 0.8 0.72 -2 8.5 -1 -5 24 3.5 65 3339579 0.2 -1 -1 0.2 190 7.4 18 3 5.95 1.36 0.61 140 2.1 1.7 2 8.2 -1 -5 21 4.5 75 3339580 -0.1 -1 1 0.2 140 5.8 26 3 3.16 1.76 0.62 80 0.7 1.52 -2 7 -1 -5 22 3.8 55 3339581 0.1 -1 -1 0.1 155 11 30 3 3.06 1.46 0.67 620 0.7 1.6 -2 8.4 -1 -5 24 4.3 60 3339582 0.1 -1 -1 0.1 155 11 30 3 3.06 1.46 0.67 620 0.7 1.6 -2 8.4 -1 -5 24 4.3 60 3339583 -0.1 -1 -1 0.1 155 38 20 4 2.66 1.74 0.6 2500 0.8 1.72 -2 9.7 -1 -5 18 3.9 65 3339584 -0.1 -1 -0.1 95 10 34 4 2.32 1.34 0.52 1000 1 1.36 -2 18 -1 -5 20 5.5 60 3339585 0.1 -1 -1 0.1 150 12 30 4 2.98 1.4 0.65 1500 1.9 1.94 3 8.6 -1 -5 15 3.6 70 3339586 0.2 -1 1 -0.1 10 12 30 4 3.2 1.4 0.61 1500 1.5 1500 1.5 154 3 9.5 11 -5 15 2.9 65 3339588 -0.1 -1 -1 -0.1 10 12 30 4 3.2 1.4 0.91 1400 1.5 1.54 3 9.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1	3339574	0.3	- 1	- 1	0.1	3.5	2.4	260	6	2.64	0.12	0.4	40	2.3	0.405	6	3	- 1	- 5	4.8	0.73	1.4
3339577	3339575	0.1	- 1	1	0.2	28	1.9	8.0	6	1.8	1.38	0.475	35	1,5	0.275	. 3	7.1	1	- 5	14	2.4	20
3339578	3339576	-0.1	- 1	. 1	0.2	31	. 1.9	20	4	2.94	1.46	0.59	3.5	0.9	0.355	- 2	5.8	- 1	- 5	18	2.5	44
3339579	3339577	-0.1	. • 1	1	-0.1	105	5.1	19	4	5.3	1.64	0.65	65	0.9	0.55	- 2	7.9	1	- 5	18	2.8	75
3339580 -0.1 -1 1 0.2 140 5.8 26 3 3.16 1.76 0.62 80 0.7 1.52 -2 7 -1 -5 22 3.8 55 3339581 0.1 -1 -1 0.1 155 11 30 3 3.06 1.46 0.67 620 0.7 1.6 -2 8.4 -1 -5 24 4.3 60 3339582 0.1 -1 -1 -0.1 115 38 20 4 2.66 1.74 0.6 2500 0.8 1.72 -2 9.7 -1 -5 18 3.9 65 3339583 -0.1 -1 -1 -0.1 95 10 34 4 2.32 1.34 0.52 1000 1 1.36 -2 18 -1 -5 20 5.5 60 3339584 -0.1 -1 -1 -0.1 90 15 26 3 3.68 1.56 0.74 3250 1.2 1.34 3 11 -1 -5 15 3.6 70 3339585 0.1 -1 -1 -0.1 90 8.5 60 4 2.98 1.4 0.65 1500 1.9 1.94 3 8.6 -1 -5 17 3.1 60 3339586 0.2 -1 1 -0.1 110 12 30 4 3.2 1.4 0.91 1400 1.5 1.54 3 9.5 -1 -5 15 15 2.9 65 339587 0.1 -1 -1 -0.1 90 8.4 18 3 3.76 1.28 1.56 1850 0.8 1.24 -2 111 -1 -5 15 15 2.9 65 339588 -0.1 -1 -1 -0.1 100 4.8 15 4 3.02 1.32 1.36 1500 0.5 1.32 -2 17 -1 -5 15 18 2.9 70 339588 -0.1 -1 1 -1 -0.1 100 4.8 15 4 3.02 1.32 1.36 1500 0.5 1.32 -2 17 -1 -5 15 3.3 48 SCHEME IC3M IC3M IC3M IC3M IC3M IC3M IC3M IC3M	3339578	-0.1	- 1	- 1	0.1	210	5.9	14	- 1	3.68	1.16	0.66	7.5	0.8	0.72	- 2	8.5	- 1	- 5	24	3.5	65
3339581 0.1 -1 -1 0.1 155 11 30 3 3.06 1.46 0.67 620 0.7 1.6 -2 8.4 -1 -5 24 4.3 60 339582 0.1 -1 -1 -0.1 115 38 20 4 2.66 1.74 0.6 2500 0.8 1.72 -2 9.7 -1 -5 18 3.9 65 339583 -0.1 -1 -1 -0.1 95 10 34 4 2.32 1.34 0.52 1000 1 1.36 -2 18 -1 -5 20 5.5 60 339584 -0.1 -1 -1 -0.1 90 15 26 3 3.68 1.56 0.74 3250 1.2 1.34 3 11 -1 -5 15 3.6 70 339585 0.1 -1 -1 -0.1 95 9.5 60 4 2.98 1.4 0.65 1500 1.9 1.94 3 8.6 -1 -5 17 3.1 60 339586 0.2 -1 -1 -0.1 110 12 30 4 3.2 1.4 0.91 1400 1.5 1.54 3 9.5 -1 -5 15 2.9 65 339587 0.1 -1 -1 -0.1 90 8.4 18 3 3.76 1.28 1.56 1850 0.8 1.24 -2 11 -1 -5 15 2.9 65 339588 -0.1 -1 1 -0.1 100 4.8 15 4 3.02 1.32 1.36 1500 0.5 1.32 -2 17 -1 -5 15 3.3 48 SCHEME IC3M IC3M IC3M IC3M IC3M IC3M IC3M IC3M	3339579	0.2	- 1	-1	0.2	190	7.4	18	3	5.95	1.36	0.61	140	2.1	. 1.7	2	8.2	- 1	- 5	21	4.5	75
3339582	3339580	-0.1	- 1	_ 1	0.2	140	5.8	26	3	3.16	1.76	0.62	80	0.7	1.52	- 2	7	- 1	- 5	22	3.8	55
3339583	3339581	0.1	- 1	1	0.1	155	11	30	3	3.06	1.46	0.67	620	0.7	1.6	- 2	8.4	- 1	- 5	24	4.3	60
3339583	3339582	0.1	- 1	- 1	-0.1	115	38	20	4	2.66	1.74	0.6	2500	0.8	1.72	- 2	9.7	1	- 5	18	3.9	6.5
3339585	3339583	-0.1	1	- 1	-0.1	95	10	34	4	2.32	1.34	0.52	1000	. 1	1.36	- 2	18	- 1			5.5	60
3339585	3339584	-0.1	- 1	- 1	-0.1	90	15	26	3	3.68	1.56	0.74	3250	1.2	1.34	3	11	- 1	- 5	15	3.6	70
3339587	3339585	0.1	- 1	- 1	-0.1	95	9.5	60	4	2.98	1.4	0.65	1500	1.9	1.94	3	8.6	- 1			3.1	60
3339588 -0.1 -1 -1 -0.1 100 4.8 15 4 3.02 1.32 1.36 1500 0.5 1.32 -2 17 -1 -5 15 3.3 48 SCHEME IC3M IC3M IC3M IC3M IC3M IC3M IC3M IC3M	3339586	0.2	1	- 1	-0.1	110	12	30	4	3.2	1.4	0.91	1400	1.5	1.54	3	9.5	- 1	- 5	15	2.9	65
SCHEME IC3M <	3339587	0.1	- 1	- 1.	-0.1	90	8.4	18	3	3.76	1.28	1.56	1850	0.8	1.24	- 2	11	- 1	- 5	18	2.9	70
DL 0.1 1 1 0.1 0.5 0.2 2 1 0.01 0.001 5 0.2 0.001 2 0.2 1 5 0.02 0.02 2 UNITS ppm ppm ppm ppm ppm ppm ppm ppm ppm pp	3339588	-0.1	- 1	- 1	-0.1	100	4.8	1,5	4	3.02	1.32	1.36	1500	0.5	1.32	- 2	17	- 1	- 5	15	3.3	48
UNITS ppm ppm ppb ppm ppm ppm ppm ppm ppm ppm	SCHEME	ІСЗМ	IC3M	FA3	ІСЗМ	IC3M	IC3M	ІСЗМ	ІСЗМ	ІСЗМ	IC3M	IC3M	IC3M	IC3M	IC3M	IC3M	ІСЗМ	FA3	FA3	IC3M	IC3M	ІСЗМ
	DL	0.1	1	1.	0.1	0.5	0.2	2	1	0.01	0.001	0.001	5	0.2	0.001	2	0.2	1	5	0.02	0.02	2
LAB:AMDEL	UNITS	ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	%	%	%	ppm	ppm	%	ppm	ppm	ppb	ppb	ppm	ppm	ppm
	LAB:AMDEL																					

HOLE	E AC/	DD9	ICW	6			CHARLOTTE WELL - EL1974						
PROSPEC			PASC	OE WELL	EASTIN		, , , , , , , , , , , , , , , , , , , ,	CONTRACTOR	3	STRAT/	•		
INCLINA				000	ZONE	53 53	, ,,,	RIG					
TOTAL D				252m		135m		HIG		EXPLOF	EH 200		
	CORE BL	OCKS.	-	232111	Iur	13311	GEOLOGICAL DESCRIPTION	-		RESUL		-	
From	To	_	%rec	From	То	Summary	Detail	Sample No	From	To	Int	Sı	CPS
1.10111	10	1100	70100	0.00	6.00	 	Orange Brown. Sand with some cemented sand & clay	3339589	0.00	4.00		50	40
		+		6.00	7.00		Orange Brown. Clay with some cemented sand	3339590	4.00	6.00		50	40
				7.00	12.00		Orange Brown, Sandy clay	3339590	6.00	10.00		50	40
			_	12.00		Tent Hill Fm?	Orange Brown, Sandy clay with silicified sandstone (Tent Hill Fm?)	3339591	10.00	12.00		20	40
				13.00		Tent Hill Fm?	White. Partly silcreted sandstone, fine-med grained.	3339592	12.00	14.00		200	40
i i	· · ·			16.00		Tent Hill Fm?	White. Qtz, clay sandstone, a bit soft, weathered kaolinitic	3339594	14.00	18.00	\rightarrow	200	40
	-			18.00		Tent Hill Fm?	Light Brown. Powdered to a sandy clay, damp (water inject thereafter) at 18m.	3339595	18.00	22.00	_	20	40
		1		32.00		Tent Hill Fm?	Light Grey. Powdered to a sandy clay.	3339596	22.00	26.00	_	20	40
				36.00		Tent Hill Fm?	Light Brown. Powdered to a sandy clay.	3339597	26.00	30.00	$\overline{}$	20	40
	_			37.00	_	Tent Hill Fm?	Light Grey. Powdered to a sandy clay.	3339598	30.00	34.00	_	20	40
	_		-	44.00		Tent Hill Fm?	Brown, Powdered to a sandy clay.	3339599	34.00	38.00		20	40
		t		45.00		Tent Hill Fm?	As above, but more sand	3339600	38.00	42.00		20	40
		<u> </u>		46.00		Tent Hill Fm?	Brown. Harder, a few small chips of sandstone, mainly pulverised to sand. Pandurra?	3339601	42.00	45.00		20	40
				51.00		Tent Hill Fm?	Pink Brown, Clayey sandstone, pulverised by hammer.	3339602	45,00	48.00		20	40
				57.00		Tent Hill Fm?	Pink Brown. Sandstone pulverised to mostly sand, some clay.	3339603	48.00	52.00		10	40
				60.00		Tent Hill Fm?	Light Grey. Fine to med clayey sandstone, poor-mod consolidated, cemented bands/horizons	3339604	52.00	56.00	4.00	10	40
				64.00		Tent Hill Fm?	Purple Brown. Fine to coarse, poorly sorted, poorly consolidated sandstone ferruginous cemented horizons, pebble bands	3339605	56.00	60.00	1111 - 1	20	40
							Base of unconformity?	3339606	60.00	64.00	4.00	40	40
				68.00	71.00	Pandurra?	Pink Brown, Clayey sandstone. Fine grained with coarse sand - small gritty pebble bands/horizons	3339607	64.00	68.00		30	40
				71.00		Pandurra	Light Brown, V. fine to coarse sandstone. Cemented sand lenses/horizons. Cemented fine sandstone bands white-light grey are	3339608	68.00	72.00		70	40
							contamination from higher up hole,	3339609	72.00	74.00		10	40
								3339610	74.00	76.00		10	40
							High water flow limiting penetration. Change to diamond coring at 72m	3339611	76.00	78.00		10	40
								3339612	78,00	80.00	2.00	10	40
		I I		72.00	72.20	Pandurra	Pandurra Fm - med-coarse gritty, mod consolidated, bedded, x-bedded, Fe stained beds	3339613	80.00	82.00	2.00	10	40
							Fracture at 72.2m	3339614	82.00	84.00		10	40
72.00	72.40	0.50	125	72,20	73.40	Pandurra	Fine to coarse, graded & cross bedded sandstone, banded (grey, purple, maroon) colouration light tan/orange/red/maroon	3339615	84.00	86.00	2.00	10	40
72.40	73.00	0.65	108	73.40	75.50	Pandurra	Fine to coarse graded sandstone, minor bedding, whispy clay laminations, rare small pebble	3339616	86.00	88.00	2.00	10	40
73.00	75.00	1.75	88				clasts, generally poorly sorted (maroon colour)	3339617	88.00	90.00	2.00	20	40
75.00	75.80	0.70	88	75.50	75.60	Pandurra	Foliated silty mudstone, micaceous bedding planes, finely bedded, (purple brown), mod indurated	3339618	90.00	92.00	2.00	10	40
75.80	78.00	2.10	95	75.60	75.70	Pandurra	Fine-medium, mod sorted, mod-well indurated, rare-minor coarse gritty clasts, bedded (tan, purple, brown)						
78.00	81.00	2.95	98	75.70	77.45	Pandurra	Fine-coarse gritty, matrix supported sandstone, poorly sorted , mod indurated, bedded with minor						
81.00	84.00	2.90	97				irregular fine sandstone and mudstone lenses/horizons. (light grey/brown/orange/purple)						
84.00	87.00	2.85	95	77.45	77.60	Pandurra	Foliated silty mst, interbedded with narrow fine sandstone, poor-mod indurated (brown-orange-purple)						
87.00	90.00	2.90	97	77.60	84.00	Pandurra	Thick, mod-well sorted, graded, med grained-gritty sandstone, mod-well indurated		i				
							Rare interbedded lenses of mst, or gritty peoble conglomerate (maroon/brown)						
			T	84.00	87.00	Pandurra	Interbedded, mod-well sorted, fine to coarse sandstone, siltstone and mudstone, thin beds/lenses			1			
		LI					Minor cross-bedding and grading. Poor-well consolidated (light grey, tan, orange, brown)			1			
				87.00	89.50	Pandurra	Fine to coarse sandstone. Poorly sorted, poorly bedded, mod-well indurated, thin whispy clay/mst						
							bands throughout. (purple brown-light grey)			1			
				89.50	90.85	Pandurra	Fine to coarse sandstone, mod-well sorted massive homogeneous sandstone. Rare mst whisps mod-well						
							indurated (purple brown) minor bedding						

HOLE AC	/DD94	1CW	6	_		CHARLOTTE WELL - EL1974				_		
PROSPECT		PASC	OE WELL	EASTIN	G 608875(AMG)		CONTRACTOR		STRATA	-		
AZIMUTH			-	NORTHI	• •		DRILLER		JOHN /			
NCLINATION			90°	ZONE	53	GEOLOGIST WAS	RIG		EXPLOR	RER 200		
TOTAL DEPTH			252m	RL	135m							
COREBL						GEOLOGICAL DESCRIPTION		,	RESUL			
From To	Rec	%ге с	From	То	Summary	Detail	Sample No	From	To_	Int	SI	CPS
90.00 93.00	0 2.90	97	90.85	90.95	Pandurra	Interpedded fine-med sandstone, mudstone, mod indurated, sheared on bedding planes, whispy clay bands (white/brown/purple)	3339619		94.00		10	4
93.00 96.00	0 2.90	97	90.95	92.80	Pandurra	Fine to medium, poorly bedded sandstone, minor coarse gritty graded zone at 91.2-91.4m	3339620	94.00	96.00	_	10	4
96.00 99.00	3.00	100				Rare thin sillstone/mudstone bands, banded purple/brown/orange/light tan	3339621		98.00	-	10	4
99.00 102.00		98	_		Pandurra	Poor-mod consolidated, finely interbedded clayey sandstone, med grained (light brown)	3339622	+ +	100.00	_	10	4
102.00 105.00	0 2.95	98	92.85	94.30	Pandurra	Mod-well consolidated, fine-med grained well sorted, poor to mod bedded sst	3339623			-	10	4
105.00 108.00	-	98				Rare coarse sandy clasts near 94.1m. Colour banded (purple/brown/red/light tan). Rare clayey whisps.	3339624				10	. 4
	0 3.00	100	94.30	94.50	Pandurra	Poor-mod consolidated, clayey v. fine sandstone, with bedding plane shearing (brecciation)	3339625		106.00	, ,	10	5
111.00 114.00	3.00	100				and thin whispy clayey & gypsiferous bands (purple-brown/red/white)	3339626			_	10	5
	0 3.00		94.50	94.90	Pandurra	Fine well consolidated sst interbedded with poorly-mod consolidated sst moderate thin bedding, minor whispy clay horizons.	3339627				10	5
117.00 120.00	0 3.00	100				Rare coarse sand clasts. Colour banded/mottled (light grey-tan, light brown purple, red)	3339628	110.00	112.00	2.00	10	5
120.00 123.00	3.00	100	94.90	96.75	Pandurra	Fine to small pebble, mod sorted, well consolidated, graded sandstone, minor bedding (purple-brown)	3339629				10	5
			96.75	96.85	Pandurra	Med to coarse poorly sorted sst interbedded with lenses of mudstone/shale. Mod-well consolidated (light grey/orange)	3339630	-			10	. 5
			96.85	96.95	Pandurra	V. fine sandy-silty mudstone-shale well bedded-layered. (orange brown)	3339631	116.00	118.00	2.00	10	5
			96.95	97.20	Pandurra	Fv. coarse, well consoliated, poorly sorted sst porous, minor mst lenses (grey brown)	3339632	118.00	120.00	2.00	10	5
			97.20	98.75	Pandurra	Fmed well consolidated, mod-well sorted sst, moderate bedding. Minor narrow	3339633	120.00	122.00	2.00	10	5
						coarse-v. coarse sandstone horizons, coloured banding (purple grey/maroon/light tan)	3339634	122.00	124.00	2.00	10	5
			98.75	98.80	Fault Pug	Unconsolidated clayey sand - bedding plane fault/or cavity fill (tan-light brown)	3339635	124.00	126.00	2.00	10	5
			98.80	99.30	Pandurra	V. fine to fine silty clayey sandstone. Well consolidated. Well sorted. Minor x-bedding	3339636	126.00	128.00	2.00	10	4
						Laminated, clayey bands toward 99.30m (brown-red-tan)	3339637	128.00	130.00	2.00	10	4
	. []		99.30	105.70	Pandurra	Graded fine to v. coarse interbedded moderately well sorted sandstone, some	i					
						vague bedding and x-bedding. Colour banded (purple brown-minor red/tan/grey)						
			105.70	105.80	Pandurra	Laminated mst/shale (red brown)						
			105.80	106.80	Pandurra	Med-coarse, mod-well sorted, well consolidted sandstone, rare bedding + x-bedding. Minor						
	I					line sandstone-clayey bands (purple, brown)						
			106.80	107.10	Pandurra	Laminated/bedded mudstone/shale, with minor silty sandy bands toward base. (orange brown)					F	
			107.10	111.00	Pandurra	Fine to coarse, mod-well sorted graded, mod-well consolidated sandstone. Vague bedding and x-bedding. Minor fine silty						
					1	sandstone lenses/beds. Also minor coarse gritty lenses/beds. Colour zonation within bedding.						
						(light grey-tan/orange/brown/purple)					1	
			111.00	110.05	Pandurra	Laminated/bedded mudstone/shale (orange/brown)		ŀ		i		
					Pandurra	Med-coarse, poor-well sorted, graded sandstones. Bedding and minor x-bedding with dispersed narrow v. fine sandstone						
						and siltstone horizons, Banded rare coarse gritty sandstone horizons. Colour zonations with bedding (purple brown/orange						
	1					brown/light tan/red)						
			117.50	117,60	Pandurra	Laminated mudstone/shale - micaceous (sericitic) (orange brown)						
<u> </u>					Pandurra	Med-coarse, mod-sorted, graded sandstone, vague bedding and colour zonation						
1						Rare narrow siltstone or gritty sandstone horizons (purple-brown-orange)						
			119.30	120.25	Pandurra	Laminated mod consolidated red brown mudstone						
<u> </u>			120.25		Pandurra	V. fine-med grained, mod sorted sandstone with narrow interbedded red brown mudstone horizons (grey-purple/-red brown)				· · · · · · · · · · · · · · · · · · ·		
	1		120.60		Pandurra	Fine grading to coarse gritty, poor sorted consolidated sandstone. Poor-mod bedding (purple brown). Minor x-bedding and					1	
	1 1		,, 23.,00			clay horizons				- 1		
	1		122 40	123.60	Pandurra	Laminated moderately fissile. Slightly micaceous, silty, mod consolidated				-		
	+ -	-+	122.40	123.00	i unuuna .	red orange brown mudstone		- 1				
	1		122.00	120.20	Pandurra	•				- 1	-	
	ı l		123.60	129.30	randurra	Med-coarse poor to mod sorted, graded sandstone. Poor bedding and		1	. 1	. 1		

HOLE	AC/I	DD94	ICW	6			CHARLOTTE WELL - EL1974						
PROSPECT	Г		PASC	OE WELL	EASTIN	G 608875(AMG)	Traverse 1 (Local) COMMENCED 11/11/94 DPO 54357 PC 0-72m OXIDISED TO 13r	CONTRACTOR	3	STRATA		· · · · · · · · · · · · · · · · · · ·	
AZIMUTH				-	NORTHI	NG 6547750(AMG)	11700 (local) COMPLETED 18/11/94 LAB AMDEL BQ 72-252m WATER TABLE 20r	n DRILLER		JOHN /	TINY		
INCLINAT	ON			90°	ZONE	53	GEOLOGIST WAS	RIG		EXPLOR	ER 200		
TOTAL DE	PTH			252m	RL	135m		1					
C	XORE BLC	OCKS					GEOLOGICAL DESCRIPTION			RESUL	TS		
From	То	Rec	%rec	From	То	Summary	Detail	Sample No	From	То	Int	SI	CPS
	126.00	_	103				x-bedding. Rare siltstone/mudstone band at 127.1m (purple brown)	3339638	130.00	132.00	2.00	10	4
	129.00		100	129.30	131.40	Pandurra	Fine-med, poor-well sorted, graded silty sandstone, consolidated	3339639	132.00	134.00	2.00	10	4
			100				(purple brown)	3339640	134.00	136.00	2.00	10	4
	135.00			131.40		Pandurra	Laminated, slightly micaceous, consolidated red brown mudstone	3339641	136.00	138,00	2.00	10	4
				131.41		Pandurra	Fine-med, mod sorted, consolidated sandstone (purple brown)	3339642				10	5 (5 (
	141.00	\rightarrow		131.70		Pandurra	Muddy siltstone, fissile & laminated, consolidated (purple brown)	3339643			-	10	5
	144.00		_	131.85		Pandurra	Fine-med, mod sorted, poorly bedded, consolidated sandstone (purple brown)	3339644	142.00	144.00	2.00	10	6
	147.00	-	98	133.50	134.50	Pandurra	Interbedded fine silty sandstone and narrow beds of laminated red brown mudstone	3339645	144.00	146.00	2.00	10	6
	150.00		98				Consolidated, mod-well bedded (purple brown)	3339646	146.00	148.00	2.00	10	. 5
		3.05	102			Pandurra	Fine-v. coarse, moderately sorted, graded sandstone, consolidated (purple brown)	3339647	148.00	150.00	2.00	10	4 (
	156.00					Pandurra	Laminated slightly micaceous red brown mudstone/shale	3339648	150.00	152.00	2.00	10	4
156.00	159.00	3,00	100	138.00	138,40	Pandurra	Fine-coarse, poor-mod sorted, graded sandstone (purple brown)	3339649	152.00	154.00	2.00	10	4
159.00	162.00	2.95	98	138.40		Pandurra	Laminated, slightly micaceous, red brown mudstone/shale	3339650	154.00	156.00	2.00	10	4 (
162.00	165.00	3.00	100	138.90	139.00	Pandurra	Sandy siltstone (grading into sst) (grey orange brown)	3339651	156.00	158.00	2.00	10	41
				139.00		Pandurra	Fine-v. coarse, poorly sorted sandstone (purple brown)	3339652	158.00	160.00	2.00	10	4(
				141.30		Pandurra	Fine-v. fine sitty sandstone, well sorted (purple grey brown)	3339653	160.00	162.00	2.00	10	5 (
				141.90	142.50	Pandurra	Laminated, slightly micaceous (red brown) mudstone/shale	3339654	162.00	164.00	2.00	10	50
				142.50	144.50	Pandurra	V. fine silty sandstone with thin interbedded mudstone (grey-brown-red)						
				144.50	144.95	Pandurra	V. fine to coarse, micaceous & muddy banded graded sandstone (purple brown)				1		
_				144.95		Pandurra	Laminated, slightly micaceous, silty banded mudstone/shale (red brown)						
				146.30	150.50	Pandurra	Fine-coarse, poorly sorted, graded sandstone with minor siltstone and						
						<u>_</u>	mudstone bands/lenses (purple brown)						
				150.50	153.00	Pandurra	Interbedded, well sorted very fine sandstone/siltstone/and laminated						
							mudstone (purple brown/red brown) minor banding of colours						
				153.00	154.20	Pandurra	Fine to coarse, poorly sorted, graded sandstone, minor bedding/x-bedding						
							Rare siltstone horizons (purple brown)						
				154.20	154.22	Pandurra	Laminated brown mudstone	l			1.		
				154.22	154.70	Pandurra	V. fine to very coarse graded sandstone, poor-mod sorted. Grading to						
							siltstone in part (purple brown)	1					
	[154.70		Pandurra	Interbanded v. fine sandy siltstone and mudstone, mod-well bedded (grey purple brown)						
				155.00	155.70	Pandurra	V. fine sandy siltstone with minor graded sandy bands (purple brown)		l i			1	
				155.70	158.70	Pandurra	Fine to very coarse, graded, poor-mod sorted sandstone, rare mst lenses				1.		
							Poor bedding (purple brown)						
]	158.70	160.10	Pandurra	V. fine sandstone and siltstone rare mudstone horizons, poorly laminated (purple brown)						
ĺ			.]	160.10	160.50	Pandurra	Med to v. coarse, poorly sorted, sandstone, poor-mod bedding small mudstone						
							lenses (purple brown)			Ì			
		I]	160.50	161.40	Pandurra	Laminated mudstone interbedded with very fine sandy siltstone (red brown/purple brown)						
				161.40	163.00	Pandurra	V. fine silty sandstone interbanded siltstone. Poor-mod bedding (purple brown)					1	
						Pandurra	Fine to coarse, poorly sorted sandstone (purple brown)					1	
				163.70	163.75	Pandurra	Laminated mudstone, slightly micaceous (red brown)				1		
						Pandurra	V. fine to coarse poorly sorted graded sandstone, rare mudstone layers				İ		
							and lenses (purple brown)						

HOLE	AC/D	D94	CW	6			CHARLOTTE WELL - EL1974						
PROSPECT			PASC	OE WELL	EASTIN	G 608875(AMG)	Traverse 1 (Local) COMMENCED 11/11/94 DPO 54357 RC 0-72m OXIDISED TO 13m	CONTRACTOR	7	STRATA			
AZIMUTH				-	NORTH	NG 6547750(AMG)	11700 (local) COMPLETED	DRILLER		JOHN /	ΓINY		
INCLINATIO	N			90°	ZONE	53	GEOLOGIST WAS	RIG		EXPLOR	ER 200		
TOTAL DEP				252m	RL	135m					_		
00	ORE BLO	CKS			•		GEOLOGICAL DESCRIPTION			RESUL"	rs		
From	То	Rec	%rec	From	То	Summary	Detail	Sample No	From	То	Int	SI	CPS
165.00 1	68.00	2.95	98	164.90	164.94	Pandurra	Laminate, slightly micaceous mudstone (red brown)	3339655	164.00	166.00	2.00	. 10	40
	71.00		100	164.94	169.20	Pandurra	Very fine to v. coarse, graded, poor-mod well sorted sandstone vague bedding	3339656	166.00	168.00	2.00	10	40
171.00 1		\rightarrow	98				and x-bedding. Rare mudstone lenses (purple brown)	3339657	168.00	170.00	2.00	1.0	40
174.00 1		$\overline{}$	100	169.20	169.30	Pandurra	Interbedded laminated slightly micaceous mudstone with a central lense	3339658	170.00	172.00	2.00	10	40
177.00 1	80.00	3.00	100				of poorly sorted med-coarse sandstone (red brown)	3339659	172.00	174.00	2.00	10	40
180.00 1	83.00	3.05	102	169.30	171.00	Pandurra	Med-coarse, mod sorted, bedded & x-bedded, homogeneous sandstone (purple brown)	3339660	174.00	176.00	2.00	. 10	40
	86.00		98	171.00	173.80	Pandurra	V. fine-v. coarse, poor-mod sorted, interbedded and graded sandstone mod bedded	3339661	176.00	178,00	2.00	10	40
	89.00		98				and x-bedded, rare mudstone lenses & horizons (purple brown)	3339662	178.00	180.00	2.00	10	40 40 40
	92.00			173.80	173.90	Pandurra	Laminated, slightly micaceous mudstone (red brown)	3339663	180.00	182.00	2.00	10	40
	95.00					Pandurra	Fine-v. coarse, poorly sorted, interbedded and graded sandstone, poor bedding	3339664	182.00	184.00	2.00	10	40
	98.00		98				and x-bedding (purple brown)	3339665	184.00	186.00	2.00	10	40
	01.00	-	98	177.40	177.90	Pandurra	Very fine sandstone and siltstone, well bedded with bands and lenses of	3339666	186.00	188.00	2.00	10	40
	04.00	_	103				mudstone (purple brown & red)	3339667	188.00	190.00	2.00	10	40
-	07.00		100	177.90	183.10	Pandurra	Fine to v. coarse gritty poorly sorted graded and interbedded sandstone	3339668	190.00	192.00	2.00	10	40 40
							Rare siltstone and mudstone lenses/horizons. Moderately well bedded	3339669	192.00	194.00	2.00	10	40
							n parts (brown-brown purple)	3339670	194.00	196.00	2.00	10	
				183.10	183.30	Pandurra	Laminated slightly micaceous mudstone (red brown)	3339671	196.00	198.00	2.00	10	
				183.30	184.50	Pandurra	Interbedded v. coarse gritty poorly sorted sandstone and v. fine-med silty	3339672	198.00	200.00	2.00	10	40
							sandstone. Mod bedding, minor siltstone/mudstone lenses (brown)	3339673	200.00	202.00	2.00	10	40
				184.50	187.30	Pandurra	Interbedded v. coarse gritty sandstone poorly sorted and laminated/	3339674	202.00	204.00	2.00	10	40
							nterbedded "tiger striped" v. fine sandy siltstone and mudstone (red)	3339675	204.00	206.00	2.00	10	40
							(brown red) well bedded. Mudstone lenses				1		
				187.30	195.60	Pandurra	Med-very coarse gritty (almost small pebbly) sandstone. Poorly sorted		İ				
						-	graded bedding, poor bedding/x-bedding. Some med grained						
		Ī					sandstone interbeds. Minor/rare red mudstone lenses (brown)	·					
		\neg	i	195.60	195.90	Pandurra	Fine-coarse, poor-mod sorted, mod bedded sandstone with thin						
							enses/horizons of red siltstone-mudstone interbedded (brown, red)						
				195.90	196.80	Pandurra	Med-v. coarse gritty sandstone, poorly sorted, poorly graded (brown)						
				196.80	197.80	Pandurra	interbanded coarse gritty sandstone siltstone, and red mudstone "tiger stripe"						
	1						Well bedded, poor-well sorted (brown, red, light tan)						
				197.80	197.90	Pandurra	Laminated mudstone (red brown) rare mica (and carboniferous material)						
						Pandurra	Fine to very coarse gritty graded sandstone with moderate bedding				1		
		$\neg \uparrow$					k-bedding, poor-mod sorted, rare mudstone/siltstone/& arkose						
							sandstone beds lenses very thin (brown grey red)				. 1		
		\neg		201,12	201.45	Pandurra	aminated mudstone (red brown) rare micaceous material						i
				201.45		Pandurra	Fine-v. coarse massive graded poorly sorted sandstone rare red						
							mudstone lenses (brown)						
				204.10	204.40	Pandurra	Gritty poorly sorted, v. small pebble conglomerate (graded) (grey brown)						
						Pandurra	Med-coarse, well bedded, graded poor-mod sorted sandstone with						<u> </u>
							rare siltstone and rare thin arkose sandstone horizons, rare mudstone						
							aminations (brown)				· 1		[
				205.15	205.30	Pandurra	Finely interbedded, v. fine sandy siltstone and mudstone ("tiger striped")	1					

HOLE	AC/E	D94	ICW	6			CHARLOTTE WELL - EL1974						
PROSPECT	•		PÁSC	OE WELL	EASTIN	G 608875(AMG)	Traverse 1 (Local) COMMENCED 11/11/94 DPO 54357 PC 0-72m OXIDISED TO 13r	n CONTRACTO	4	STRATA	١		
AZIMUTH				-	NORTHI	NG 6547750(AMG)	11700 (local) COMPLETED 18/11/94 LAB AMDEL BQ 72-252m WATER TABLE 20r	DRILLER		JOHN /	TINY		ł
INCLINATION	ON			90°	ZONE	53	GEOLOGIST WAS	RIG		EXPLOR	ER 200		
TOTAL DE	PTH			252m	RL	135m		1.					
C	ORE BLC	xxxs					GEOLOGICAL DESCRIPTION			RESUL	rs		
From	To.	Rec	%rec	From	To	Summary	Detail	Sample No	From	То	Int	SI	CPS
207.00 2	210.00	2.95	98				(red brown grey)	3339676				10	40
210.00 2	213.00	3.50	117	205.30	206.05	Pandurra	Fine to coarse poorly sorted, massive, poorly bedded sandstone (brown)	3339677	+	-	_	10	
213.00 2	216.00	3.00		206.05		Pandurra	Med to v. coarse gritty, poorly sorted massive sandstone (brown)	3339678	+	_	$\overline{}$	10	40
	219.00	_		206.65	206.80	Pandurra	Interbedded fine-coarse sandstone, siltstone, mudstone, poor-mod bedding	3339679				10	40
219.00 2			100				x-bedding, 1cm mudstone layer at base (brown-red-light grey)	3339680				10	
222.00 2		$\overline{}$			207.80	Pandurra	Fine to coarse, poorly sorted, graded, poor-mod bedded sandstone, narrow	3339681			-	10	
225.00 2			100				bands of coarse gritty sand-small pebbles (brown)	3339682			$\overline{}$	10	
228.00 2				207.80		Pandurra	Laminated, slightly micaceous mudstone (red brown)	3339683				10	
231.00 2				208,10	208.80	Pandurra	Med to v. coarse poorly sorted, graded, poor-mod bedded sandstone, thin	3339684				10	
	237.00		102				arkose horizons (brown, light tan)	3339685				10	50
-	240,00	_				Pandurra	V. fine-med silty sandstone ("tiger striped") mod x-bedding (brown-red brown)	3339686				10	
240.00 2	243.00	3.05				Pandurra	Laminated, slightly silty mudstone, well bedded, (red brown)	3339687	_			10	40
243.00 2	246,00	3.01	100	209.15	209.60	Pandurra	Interbedded v. fine-med poorly sorted sandstone, and sandy siltstone. Good	3339688	•	_	-	10	
							x-bedding ("tiger striped") (red brown-light cream)	3339689		_	_	1.0	40
				209.60	210.20	Pandurra	Interbedded arkose, qtz sandstone and rare siltstone, fine-v. coarse grained	3339690				10	
							poor-mod sorted poor-mod bedding (brown, cream, red)	3339691		-	-	10	40
				210.20	210.40	Pandurra	Interbedded fine-med poor sorted sandstone and sandy siltstone ("tiger stripe"	3339692				10	
							x-bedded) (brown, red) finely interbedded	3339693	240.00	242.00	2.00	10	40
				210.40	210.95	Pandurra	Med to v. coarse, poorly sorted graded bedded sandstone. Arkose	3339694				10	
				_			toward base (brown, cream)	3339695	244.00	246.00	2.00	10	40
				210.95	212.25	Pandurra	Finely interbedded fine to med, sandstone and sandy siltstone, ("tiger stripe")						
							Mod-good bedding/x-bedding. Thin arkose bands toward base						
						<u> </u>	(brown-red)	ļ					
						Pandurra	Laminated mudstone (red brown)	1					
				212.35	226.09	Pandurra	Interbedded med-v. coarse gritty (even small pebble) poorly sorted						
]					graded sandstone, grit conglomerate. Arkose in composition.	<u> </u>					
							Ferruginous quartzose banded. Interbanded with thin laminated						
							red mudstone horizons. Poor to good bedding (red brown/cream)						
				226.09	226.25	Pandurra	Laminated mudstone (red brown) interbedded with thin siltstone	1	1				
							well bedded						
				226.25	227.85	Pandurra	Fine to coarse well bedded mod sorted, arkosic sandstone & grit						
							Rare to minor v. coarse gritty lenses rare interbedded siltstone						
							and mudstone laminations. Bedding well defined by Fe staining (pink/red, cream)						
						Pandurra	Laminated silty mudstone (red brown)	1					
				228.00	228.45	Pandurra	V. finely bedded/x-bedded/interbedded siltstone and fine to medium	1					
							arkose sandstone (pink-light cream grey)						
]			228.45	228.80	Pandurra	Laminated silty mudstone (red brown)	L					
				228.80	231.08	Pandurra	Interbedded very fine to very coarse poor to mod sorted, well bedded						
]					and x-bedded arkosic sandstone. Minor interbedded siltstone and	1					:
				231.08	231.42	Pandurra	mudstone laminations. Bedding well defined by colour (pink, red, cream grey)						
]	231.42	246.70	Pandurra	Laminated mudstone interbedded with fine thin siltstone (red brown grey)	<u> </u>					
							Interbedded, well bedded and x-bedded fine to coarse moderately	3					

HOLE	AC/	DD9	4CW	6				CHARLOTT	E WELL	- EL1974	1										
PROSPEC	मं		PASC	OE WELL	EASTING	608875(AMG)	Traverse 1 (Lo	al) COMMENCED	11/11/94	DPO	54357	RC .	0-72m	OXIDISED TO	13n	n CONTRACTOR	٦	STRATA		-	
AZIMUTH	l				NORTHING	6547750(AMG)	11700 (loc	al) COMPLETED	18/11/94	LAB	AMDEL	BO	72-252m	WATER TABLE	20п	n DRILLER		JOHN /	TINY		
INCLINA	ION			90°	ZONE	53		GEOLOGIST	WAS							RIG		EXPLOR	ER 200		
TOTAL D	EPTH			252m	RL	135m															
	CORE BLO	ocks						GEC	LOGICAL DES	CRIPTION		_						RESUL	TS		
From	Ťó	Rec	%rec	From	То	Summary					etail					Sample No	From	То	Int	SI	CPS
246.00	249.00	3.00	100				sorted sandstone/si	Itstone/and muds	tone. Beds	vary and are						3339696	246.00	248.00	2.00	10	40
249,00	252.00	3.00	100				commonly 5-20cm	thick and grade b	etween each	other		_				3339697	248.00	250.00	2.00	10	40
252.00	ВОН						Bedding is well de	tailed by ferrugir	nous colourat	ion						3339698	250.00	252.00	2.00	10	40
							amongst interbedde	d units. Mudstor	nes are comm	nonly											
							laminated and are				orange	brown)								
	-											_									
							Mst band at 245.5r	n (20cm)								1					
				246.70	247.50		Interbedded lamina	ted mudstone and	d siltstone, w	ell bedded (r	ed brov	vn)									
				247.50	252.00		Interbedded, well b	edded and x-bed	ded, fine to d	coarse moder	ately so	rted									
					ЭН	·	sandstone/siltstone/														
						•	commonly 5-20cm														
		·					is well detailed by														
							interbedded units.			•											
							are slightly micace	_	•					*							
							arkose bands	., .						· · · · · · · · · · · · · · · · · · ·		1.					
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i							No Gawler Range	Volcanics intersec	cted												
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Sample No	From	То	۱ ۸ ۵	A =	Au	Bi	Ce	Co	Cr	Cu	Fe	К	Ma	Mn	Мо	Na	Ni	Pb	Th	U	Zn
3339589	0	4	-0.1	As	AU	-0.1	17	3.3	240	8	1.08	0.295	0.59	80	1.4	0.135	8	5.3	3	0.53	22
3339590	4	6	-0.1	- 1	- 1	0.1	50	9.9	220	10	1.01	0.205	0.39	80	1.7	0.133	13	11	5.6	2.6	16
3339591	6	10	0.8	6	- 1	0.1	24	4.8	130	11	2	0.74	0.51	110	3.5	0.425	10	13	9.4	2.3	30
3339592	10	12	0.8	10	- 1	0.3	17	3.7	160	11	2.24	0.66	0.395	65	2.1	0.423	9	10	8.4	2.1	22
3339593	12	14	0.7	- 1	- 1.	0.3	5.9	4.1	390	3	1.97	0.285	0.333	60	1.1	0.315	11	9.8	5.1	2.7	28
3339594	14	18	2.7	4	- 1	0.3	26	1.8	300	17	1.35	0.283	0.14	120	3.3	0.315	7	11	5.7	1.22	24
3339595	18	22	-0.1	- 1	1	0.1	18	2.7	360	9	0.91	1.28	0.098	100	1.3	0.465	9	16	5.1	0.99	18
3339596	22	26	-0.1	4	1	0.1	20	4.2	270	9	1.01	1.7	0.038	160	3.3	0.365	9	17	5.1	1.28	40
3339597	26	30	-0.1	- 1	- 1	0.2	25	3	320	10	0.94	1,68	0.078	150	1.6	0.225	10	15	9.1	1.56	19
3339597	30	34	0.1	- 1	- 1	0.1	35	3.2	320	6	0.75	2.2	0.08	150	4.2	0.235	13	19	12	1.92	22
3339599	34	38	-0.1	- 1	- 1	0.1	25	2.7	440	6	0.73	1,72	0.08	150	1.3	0.233	6	15	8.3	1.86	18
3339600	38	42	-0.1	- 1	1	-0.1	17	2.6	330	4	0.67	1.72	0.066	120	2.7	0.245	5	15	5.2	0.97	14
3339600	42	45	-0.1	- 1	- 1	-0.1	27	3.1	380	7	0.84	1.9	0.066	130	1.3	0.243	5	14	7.7	1.43	14
3339602			-0.1	- 1		0.1		3.1	320	10	0.92	1.56	0.084	110	2.9	0.485	8	8.6	7.9	1.95	14
3339602	45 48	48 52	-0.1	4	- 1	0.1	28 34	3.9	230	14	0.92	1.8	0.084	150	0.9	0.485	11	12	9.6	3.2	30
3339603	52	56	-0.1	- 1	1	0.1	29	4.8	250	10	0.89	1.82	0.14	160	3.2	0.305	13	12	7,8	2.3	26
3339604	56	60	-0.1	- 1	- 1	0.1	120	3.8	280	11	1.05	1.68	0.084	160	3.5	0.303	14	14	26	3.7	26
3339606	60	64	-0.1	- 1	1	-0.1	15	1.7	260	. 8	0.76	1.54	0.094	70	1.6	0.45	3	5.7	4.5	0.91	9
3339607	64	68	-0.1	- 1	- 1	-0.1	15	1.4	290	6	0.78	1.04	0.105	70	0.9	0.355	6	4.8	5.3	1.13	20
3339608	68	72	-0.1	1	- 1	0.1	20	2.8	350	6	0.87	1.82	0.103	95	2.7	0.333	8	9.2	5.4	1.31	20
3339609	72	74	-0.1	4	- 1	0.1	42	4.6	320	18	0.96	1.5	0.113	800	0.9	0.285	10	9.6	11	2.8	24
3339610	74	76	-0.1	8	- 1	0.2	65	4.6	320	16	2.04	2.04	0.12	1950	2.5	0.41	11	12	15	1.7	26
3339611	76	7.8	-0.1	6	- 1	0.2	50	4.7	340	19	2.28	1.78	0.125	1300	0.8	0.375	13	21	9.7	2.1	32
3339612	78	80	-0.1	4	- 1	0.2	60	7.1	340	12	1.95	2.06	0.120	1150	2.9	0.4	19	16	15	1.85	24
3339613	80	82	0.3	4	- 1	0.2	55	5.7	390	14	2.08	1.9	0.098	1300	1.2	0.34	17	14	11	1.56	24
3339614	82	84	-0.1	4	- 1	0.2	55	5.5	350	14	1.9	2.02	0.098	1600	3	0.39	22	14	12	1.97	24
3339615	84	86	-0.1	6	- 1	0.2	55	6.8	400	16	1.47	1.88	0.092	800	1.2	0.375	16	14	12	2.8	22
3339616	86	88	0.1	- 1	- 1	0.1	47	7.2	380	17	1.64	1.96	0.086	1150	3.2	0.385	18	11	11	1.72	19
3339617	88	90	-0.1	4	- 1	0.1	44	7.5	370	13	1.76	1.82	0.078	1450	1	0.355	13	12	12	1.5	28
3339618	90	92	-0.1	- 1	- 1	0.2	55	7.4	370	11	1.68	2	0.092	1050	3.3	0.405	23	14	13	1.81	22
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3339619	92	94	-0.1	- 1	- 1	0.2	60	7	350	16	1.84	1.64	0.098	780	1.1	0.395	19	_	14	2.1	22
3339620	94	96	-0.1	4	- 1	0.2	65	7	290	16	2.06	1.7	0.12	760	2.2	0.355	15	14	15	2.9	28
3339621	96	98	-0.1	4	- 1	0.2	60	6.1	320	13	1.77	1.66	0.115	580	0.7	0.37	16	14	13	1.87	22
3339622	98	100	1	4	- 1	0.2	55	5.3	250	16	1.56	2.2	0,11	640	2.7	0.34	16	13	15	2.9	28
3339623	100	102	-0.1	- 1	1	0.2	75	6.3	360	17	1.92	1.88	0.11	660	0.9	0.385	18	16	22	3.1	24
3339624	102	104	.0.1	6	- 1	0.3	60	7.6	290	16	1,98	1.78	0.135		2.1	0.335	17	16	16	3.4	32
3339625	104	106	0.2	6	- 1	0.4	85	10	300	24	2.84	1.82	0.135		0.8	0.35	22	22	19	3.1	32
3339626	106	108	-0.1	4	- 1	0.4	90	10	240	26	2.8	1:98	0.19		2.7	0.34	34	20	20	3.6	44
3339627	108	110	-0.1	• 1	- 1	0.3	70	7.4	320	17	2.22	1.7	0,12	560	1.2	0.33	21	14	18	4.6	34
3339628	110	112	-0.1	4	- 1	0.4	85	1.1	270	17	2.16	1.76	0.135	520	3.3	0.34	30	_	25	4.2	36
3339629	112	114	0.2	1	1	0.3	75	8.2	330	13	1.89	1.74	0.096	800	1.1	0.305	29	15	14	1.93	26
3339630	114	116	-0.1	- 1	- 1	0.3	65	6.1	340	14	1.89	1.98	0.088	420	2.8	0.305	19	14	12	1.77	26
3339631	116	118	-0.1	- 1	- 1	0.3	80	5.3	320	13	1.63	1.90	0.008	480	0.5	0.303	12	11	18	1.81	32
3339632			-0.1	-	- 1	0.4	70	10	240	30	2.88	2.66	0.094	-	2.3	0.33	27	16	14	3.6	75
3339632	118	120	0.4	6	- 1	0.4	65	13	240	30	3.1	1.98	0.25	600	1.2	0.33	34	16	15	4.3	50
-	120 122	122	0.4	8	- 1	0.4	125	18	120	55	3.1	1.98	0.17	780	1.5	0.275	35	42	29	8.3	90
3339634																		$\overline{}$		-	34
3339635	124	126	-0.1	8	1	0.3	85	10	260	26	2.46	1.84	0.11	1250	1	0.35	32	18	18	5.7	
3339636	126	128	-0.1	8	- 1	0.3	90	11	250	19	2.5	1.94	0.105	740	2.6	0.34	21	17	18	2.4	32
3339637	128	130	-0.1	6	- 1	0.5	120	9.5	340	22	2.76	1.76	0.1	960	1.2	0.285	10	21	18	10	48
 																					
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Sample No	From	То	_	As	Au			<u></u>	Cr	Cu	Fe	K	_		Mo	Na	Ni		Th	U	Zn
3339638	130	132	-0.1	8	- 1	0.5	105	12	240	24	3.1	2.02	0.16		3	0.28	13	23	27	3.6	60
3339639	132	134	-0.1	6	- 1	0.5	90	11	230	26	3.22	2.18	0.19	_	1	0.29	13	22	24	3.6	50
3339640	134	136	-0.1	12	- 1	0.6	85	12	180	30	3.72	1.96	0.185	860	2.2	0.3	13	22	22	4.6	60
3339641	136	138	-0.1	10	- 1	0.5	90	12	230	30	3.58	1.88	0.16		0.9	0.315	13	22	21	3	48
3339642	138	140	-0.1	10	- 1	0.6	90	14	150	38	3.88	1.78	0.275		2	0.27	16	28	22	3.6	75
3339643	140	142	-0.1	14	- 1	0.4	85	11	210	3.0	3.46	1.84	0.175	700	0.7	0.29	12	20	23	3.9	50
3339644	142	144	-0.1	14	- 1	0.7	110	1.6	95	44	4.36	1.78	0.35	1350	1.4	0.235	18	26	28	5	90
3339645	144	146	-0.1	1.4	- 1	0.8	120	1 7.	100	50	4.56	1.8	0.36	840	0.7	0.215	19	21	29	4.7	100
3339646	146	148	-0.1	12	- 1	0.7	105	13	120	. 36	4.2	2	0.265	720	1.6	0.225	14	23	22	5.3	70
3339647	148	150	-0.1	12	- 1	0.4	60	11	210	28	3.46	1.74	0.145	760	0.7	0.255	13	17	13	3.1	50
3339648	150	152	-0.1	18	- 1	0.7	95	15	140	36	3.92	1.9	0.25	1600	2.1	0.235	18	29	23	5,5	70
3339649	152	154	-0.1	12	- 1	0.4	75	11	160	26	3.08	1.7	0.175	640	0.6	0.26	12	21	22	3	55
3339650	154	156	∙0.1	12	- 1	0.4	85	12	180	26	3.2	1.9	0.175	800	1.8	0.26	12	25	21	3.1	55
3339651	156	158	-0.1	8	- 1	0.3	65	9.2	310	20	2.78	1.56	0.105	1500	0.8	0.265	10	21	13	2.4	36
3339652	1.58	160	-0.1	10	1.	0.5	120	14	190	30	3.6	1.58	0.195	1250	2.2	0.29	16	27	21	3.2	55
3339653	160	162	-0.1	12	• 1	0.5	105	15	200	34	3.76	1.42	0.25	900	0.8	0.265	17	32	29	6.4	65
3339654	162	164	-0.1	10	- 1	0.4	75	1.1	220	26	3.52	1.88	0.17	1500	2.2	0.27	13	26	19	2.7	44
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3339655	164	166		8	- 1		75	11	310	24	2.88	1.46	0.145	1100	0.9	0.305	13	33	22	2.6	36
3339656	166	168	-0,1	12	- 1	0.3	65	13	270	24	3,24	1.52	0.14	1600	2.4	0.335	13	3.5	15	5.1	38
3339657	168	170	-0.1	. 12	- 1	0.5	95	16	200	32	3.84	1.58	0.225	1600	0.7	0.32	17	43	28	5	55
3339658	170	172	-0.1	8	- 1	0.4	85	14	290	24	3.7	1.74	0.14	1100	2.4	0.33	14	38	20	3.2	36
3339659	172	174	-0.1	12	- 1	0.4	90	12	180	28	2.86	1.5	0.195	4250	0.6	0.285	13	30	24	3.8	48
3339660	174	176	-0.1	10	- 1	0.2	55	10	290	20	2.7	1.66	0.12	2100	2.1	0.285	[11]	29	14	2.2	32
3339661	176	178	-0.1	14	- 1	0.4	75	15	280	30	3.66	1.78	0.22	2550	0.8	0.325	17	36	22	4.1	55
3339662	178	180	-0.1	8	- 1	0.2	5,5	9.1	300	16	2.3	1.64	0.12	1450	2.2	0.29	10	26	15	1.89	26
3339663	180	182	-0.1	12	- 1	0.3	70	11	290	19	2.68	1.64	0.13	2300	0.8	0.26	12	34	19	3	36
3339664	182	184	-0.1	8	- 1	0.3	70	12	250	22	2.7	2.1	0.21	2950	2.1	0.3	14	48	18	2.9	46
3339665	184	186	-0.1	10	- 1	0.2	70	10	170	17	1.76	2.16	0.13	3250	0.7	0.28	11	23	20	3.2	34
3339666	186	188	-0.1	14	- 1	0.4	70	12	210	22	2.38	2.14	0.17	7800	2.4	0.295	14	28	. 17	3	32
3339667	188	190	-0.1	8	- 1	0.1	44	9.1	350	11	1.97	1.68	0.098	1400	1	0.335	10	17	10	1.34	20
3339668	190	192	-0.1	10	- 1	0.2	60	9	270	12	1.87	1.86	0.125	5300	2.4	0.335	10	25	12	1.86	22
3339669	192	194	-0.1	6	1	0.2	45	8.4	340	. 11	1.98	1.92	0.1	1750	1	0.305	10	22	9.8	1.44	19
3339670	194	196	-0.1	10	- 1	0.2	70	8.5	280	13		1.96	0.12	2900	2.6	0.295	10	21	13	2.1	22
3339671	196	198	-0.1	10	- 1	0.2	60	9.1	260	14	1.97	1.54	0.14	2400	0.8	0.315	11	25	14	3,1	26
3339672	198	200	-0.1	10	- 1	0.2	65	8.1	250	16	1.91	1.6	0.125	1850	2	0.32	10	22	14	2.3	24
3339673	200	202	-0.1	10	- 1	0.4	85	14	260	24	3.12	1.7	0.255	3900	1	0.305	20	34	18	3.7	48
3339674	202	204	-0.1	1	- 1	0.1	37	6.2	330	11	1.81	1,62	0.088	1700	2.4	0.315	8	17	6.7	0.92	14
3339675	204	206	-0.1	6	- 1	0.2	70	8.2	270	13	1.89	1.8	0.14	3700	0.7	0.295	10	27	16	1.98	26
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3339676	206	208	-0.1	10	- 1	0.3	90	9.4	240	17	2.5	1.7	0.185	-	2.2	0.29	14	29	17	4.2	34
3339677	208	210	-0.1	12	- 1	0.3	80	10	140	20	2.64	2.38	0.165		0.8	0.28	16	47	18	4.6	40
3339678	210	212.35	-0.1	8	-1	0.2	70	6.6	150	15	1.92	1.86	0,16	2000	1.5	0.275	9	21	19	2.2	30
3339679	212.35	214	-0.1	- 1	- 1	-0.1	28	4.6	320	8	1.07	1.76	0.098	400	1	0.26	9	17	8.4	1.3	14
3339680	214	216	-0.1	1	- 1	0.1	38	4.4	240	9	1.09	1.88	0.1	350	2.4	0.3	7	21	11	2.1	15
3339681	216	218	-0.1	- 1	- 1	0.1	49	4.1	230	10	1.04	2.1	0.1	660	0.9	0.28	6	17	8.2	4.3	16
3339682	218	220	-0.1	- 1	- 1	0.1	28	3.9	230	17	1.07	2.04	0.11	240	2.6	0.325	6	22	9	1.43	15
3339683	220	222	-0.1	. 1	- 1	-0.1	23	3.4	290	6	0.85	1.54	0.084	180	0.8	0.26	5	17	7.7	1.5	11
3339684	222	224	-0.1	• 1	- 1	0.1	28	3.6	280	9	0.89	1.6	0.105	180	2	0.31	4	18	11	1.18	15
3339685	224	226	-0.1	1	1	0.2	49	3.7	200	9	. 1	1.74	0.13	240	1.6	0.28	3	21	13	2.3	19
3339686	226	228	-0.1	• 1	- 1	0.2	5.5	4.4	170	11	1,52	1.58	0.18	320	2	0.27	5	25	15	2.1	30
3339687	228	230	-0.1	- 1	- 1	0.3	80	5.7	100	11	1.48	2.22	0.225	500	1.6	0.26	8	27	19	2.7	36
3339688	230	232	-0.1	- 1	- 1	0.2	65	4.7	140	15	1.56	2	0.22	520	1.6	0.265	6	24	16	2.4	36
3339689	232	234	-0.1	- 1	- 1	0.2	5.5	4.3	130	1,1	1.31	2,12	0.185	320	1.7	0.26	5	23	1,5	2.4	32
3339690	234	236	-0.1	- 1	- 1	0.2	5.5	4.6	160	12	1.26	2.2	0.175	340	1.8	0.255	6	24	12	3.1	36
3339691	236	238	-0.1	. 1	1	0.2	50	4.8	120	14	1.52	2.24	0.205	450	1.8	0.27	6	27	16	2.9	32
3339692	238	240	-0.1	4	. 1	0.1	55	3.5	130	. 9	0.85	1.6	0.15	560	1.5	0.285	. 4	27	11	3	24
3339693	240	242	-0.1	- 1	- 1	0.2	65	4.6	130	13	1.34	1.64	0.185	320	1.7	0.265	6	27	15	3	34
3339694	242	244	-0.1	4	- 1	0.3	60	5	110	12	1.64	1.78	0.26	420	1.5	0.265	6	27	16	2.7	42
3339695	244	246	-0.1	. 4	• 1	0.2	90	4.8	95	12	1.45	2.52	0.23	600	1.5	0.25	6	29	23	2.9	40
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Sample No	From	То	Ag	As	Àυ	Bi	S)	8	Or.	2	Fe	K	Mg	Mn	Мо	Na	Ni	Pb	Th	U	Zn
3339696	246	248	-0.1	- 1	- 1	0.2	7.5	4.6	110	13	1.84	2.16	0.28	310	1.3	0.25	7	22	19	3	50
3339697	248	250	-0.1	4	1	0.2	65	3.8	160	11	1.38	1.76	0.135	520	1.8	0.255	5	26	15	2.3	28
3339698	250	252	~0.1	- 1	- 1	0.1	32	2.7	220	10	1.02	2.34	0.105	140	2.3	0.255	5	18	. 11	1.33	16
SCHEME			ІСЗМ	ІСЗМ	AA9	ІС3М	IC3M	ІСЗМ	IC3M	ЮЗМ	IC3M	IC3M	IC3M	ІСЗМ	IC3M	IC3M	ЮЗМ	ЮЗМ	ІСЗМ	ІСЗМ	ІСЗМ
DL .			0.1	1	1	0.1	0.5	0.2	2	1	0.01	0.001	0.001	5	0.2	0.001	2	0.2	0.02	0.02	2
UNITS			ppm	ppm	ppb	ppm	ppm	ppm	ppm	ppm	%	%	%	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm

HOLE	RC94	CW7			CH	IARLOTTI	WELL -	EL	1974														
PROSPEC1		PASCOE WELL		608800(AMG)	Traverse 1(Local)		29/11/94 D	РО	54320 PC		0-119m					CONTR			STRATA				
AZIMUTH			NORTHING	6547875(AMG)	17150(Local)		30/11/94					WATE	ER TABLE		51 m	DRILLE	₹			TREVO	R		
INCLINATIO			ZONE	53		GEOLOGIST	DWW									RG			EXPLOR	ER 200			
TOTAL DE	PTH	119m	PL.	142m		<u> </u>										<u> </u>				_			
				GEOLOGICAL DESCR						,			 			S (ppm)							
From	То	Summary			Detail			SI	CPS Sample No	From	То	Int	Αu	Ag	As	Co	Cr	Cu	Fe %	Mn	Ni	Pb	Zn
0		SAND		Sand, mod. qtz, clay,				70	50 3942620	0	4	4	<0.02	<1	4	3	12	1.4	1.63	65	8		15
1		SAND	t	Sand, mod. qtz, clay,			-	60	50 3942621	4	. 8		<0.02	<1	_	_	9	< 2	1.21	15	4	< 5	2
2		SANDSTONE	Ť :	n. f/med. qtz Sst. abur				30	50 3942622	8	12		<0.02	<1	< 3		120	< 2	0.43	25	4	< 5	< 2
3	_	SANDSTONE	1	h. f/med. qtz Sst. abu				30	50 3942623	12	16		<0.02	< 1	< 3	8	44	< 2	0.35	6,5	8	5	2
4		SANDSTONE		h. f/med. qtz Sst. abu				20	65 3942624	16	20	4	<0.02	< 1	< 3	. 7	44	< 2	0.28	5.5	8	10	2
5		SANDSTONE	1	n. med. qtz Sst, ang-ro		е		20	65 3942625	20	24	.4	<0.02	<1	< 3		24	5	0.59	80	8	15	7
6		SANDSTONE	 	med. qtz Sst, ang-rd o				1.5	65 3942626	24	28	4	< 0.02	< 1	< 3	< 2	85	3	0.44	100	9	5	4
7		SAND		/c qtz Sand, poor sort				15	65 3942627	28	32	4	< 0.02	<u>. <1</u>	4	< 2	60	7	0.52	220	8	10	5
8		SAND	†	/c qtz Sand, poor son				15	55 3942628	32	3.6	4	< 0.02	< 1	+ -	2	75	4	0.40	55	- 7	5	5
9		SAND		/c qtz Sand, poor sort				15	55 3942629	36	40	4	< 0.02	<1	-	4	48	7	0.76	160	6	10	13
10		SAND		/c qtz Sand, poor sort			-	10	55 3942630	40	44	.4.	< 0.02	< 1		3	75	8	1.36	2450		10	13
11		SAND		qtz Sand, mod. sorting				10	50 3942631	44	48	4	<0.02	< 1	+ -	3	70	9	1.13	1650	6	10	11
12		SAND		qtz Sand, mod. sorting				10	50 3942632	48	52	4	<0.02	<1	-	5	50	13	1.88	1650	8	15	19
13		SAND	1	qtz Sand, mod. sorting				10	50 3942633	52	56	4	<0.02	<1	4	5	85	10	1.84	1400	9	15	14
14		SAND/CLAY		qtz Sand, mod. sorting		DI		10	50 3942634	56	60 64	4	<0.02	<1 <1	4	4	75 80	10	1.76	1100	11	15	13
16		SAND/CLAY	1	Sand-powdery clay, min qtz Sand-powdery cla				15 20	50 3942635 50 3942636	60 64	68	4	<0.02 <0.02	<1		3	100	8	1.36	880	7	10	10
17		SAND/CLAY	† · · · ·	qtz Sand-powdery cla	•			40	50 3942637	68	72	4	<0.02	<1	_	3	140	7	1.28	560	10	5	9
18		SAND/CLAY		qtz Sand-powdery cia		<u> </u>		50	55 3942637	72	76	4	<0.02	<u>< 1</u> <1	-	6	18	17	2.52	940	13	30	34
19		SAND/CLAY	1	qtz Sand, min. powde				50	55 3942639	76	80	4	<0.02	<1	6	5	26	17	2.58	880	10	15	30
20		SAND/CLAY		qtz Sand, mod. powd				50	60 3942640	80	84		<0.02	<1	8	6	20	26	2.50	430	9	25	28
21	_	SAND/CLAY		z Sand-powdery clay,				40	85 3942641	84	88	, ,	<0.02	< 1	8	7	28	18	2.82	800	11	20	30
22	_	SAND/CLAY		z Sand-powdery clay,		·		20	90 3942642	88	92	- A	<0.02	×1:		8	13	24	3.66	1000	11	25	40
23		SAND/CLAY		z Sand-powdery clay,				90	90 3942643	92	96		<0.02	<1		9	19	26	3.82	2450	16	35	42
24	_	SAND/CLAY		qtz Sand-powdery cla				60	70 3942644	96	100	4	<0.02	<1	6	7	36	14	2.50	1400	10	25	22
25	-	SAND/CLAY		qtz Sand-powdery cla	•	· · · · · · · · · · · · · · · · · · ·		250	60 3942645	100	104	4	<0.02	<1		7	70	18	2.58	2700	12	40	24
26		SAND/CLAY		z Sand-powdery clay,	-			50	65 3942646	104	108	4	<0.02	<1	6	6	65	11	2.50	700	13	15	17
27	- '	SAND/CLAY		qtz Sand-powdery cla				80	65 3942647	108	112	4	<0.02	<1	10	8	28	22	3.26	1050	13	30	32
28		SAND/CLAY	_	z Sand-powdery clay,				200	65 3942648	112	116	4	<0.02	<1	12	10	28	22	3.62	840	14	35	40
29		SAND/CLAY		Sand-powdery clay, mir				80	80 3942649	116	119	3	<0.02	<1	8	8	36	19	2.92	560	12	20	32
30		SAND/CLAY		Sand-powdery clay, mir	•			00	70	EOH			1										
31		SAND/CLAY		qtz Sand-powdery cla				40	75				- İ								7		
32	-	SAND/CLAY		ed. qtz Sand-powdery				60	70									1					
33		SAND/CLAY		z Sand-powdery clay			12	200	70						† †	$\neg \uparrow$						\neg	
34		SAND/CLAY		med. qtz Sand, mod.	powdery clav. min. F	e, c qtz		50	75										- 1		$\neg \uparrow$		\neg
35		SAND/CLAY		med. qtz Sand, mod.				80	75	- 1													\Box
36	$\overline{}$	SAND/CLAY	-	Sand-powdery clay (S			,,	-+	120	•					\Box	1	1		1		\neg		\neg
37				Sand-powdery clay (110								1					$\neg \uparrow$	\neg
38		SAND		Sand/Grav, mod. sort		Fe		50	70			İ								-			

HOLE R	C94CW7			CH	IARLOTTI	E WELL - E	L19	74									*					
PROSPECT AZIMUTH INCLINATION TOTAL DEPTI	PASCOE WELL 90°	NORTHING ZONE	53 142m	Traverse 1(Local) 17150(Local)	COMMENCED	29/11/94 DPO 30/11/94 DWW		54320 FC		0-119m	1	SED TO		51 m	DRILLE PIG			STRAT/ MARTY EXPLOR	/TREVO	R		
-	r		GEOLOGICAL DESCR			g	1 ~~	S Sample No	From	То	Int	Au	TAg	·	rs (ppm Co) Cr	Τω	Fe %	Mn	Ni	Pb	Zn
	Fo Summary 4 0 SANDSTONE	Či madia a	tz Sst, mod. sorting,	Detail	-	20	_	S Sample No	From	10	int.	Au	Ag	AS	- (4)	Ur	W	F# 76	I IVIII	1/41	FU	211
39						130	_	0		+	+ +		 	 		1	1			-	\vdash	
41			z Sst, poor sorting, m z Sst, mod. sorting, m			80	+	0		<u> </u>			+	-			1					
42			gtz Sst, mod. sorting, in			150		0		1			+	1	 -		1	 				
43	44 FE SANDSTONE		ed. atz Sst. mod. sorting.		IRA EM	60										 -	†		i			\vdash
44			gtz Sst, min. Wh Sst,	<u> </u>		60			1				_	†		<u> </u>		<u> </u>				
45			ed. qtz Sst, mod. sort			60					1		†		****	 						
46			ed. qtz Sst, mod. sort			60		0			1		1 -									
47			c qtz Sst, mod. sorting			60	+-	10			1 1											
48			c qtz Sst, mod. sorting		Total Salar	60	+	10								1	İ					
49			c qtz Sst, mod. sorting			60	+	10														
50			c qtz Sst, mod. sorting			60	+	10														
51			ed/c qtz Sst, mod. so			60	9	0					İ									
52			ed/c qtz Sst, mod. so			60	9	0														
53			ed/c qtz Sst, mod. so		 -	60	9	0					1									
54			ed/c qtz Sst, mod. so		lay, qtz	60	10	0														
5.5	56 FE SANDSTONE	Br/Gy Fe me	ed/c qtz Sst, mod. so	rting, min. clay, qtz		60	10	00														
56	57 FE SANDSTONE	Br/Gy Fe me	ed/c qtz Sst, mod. so	rting, min. clay, qtz		60	10	00														
57			ed/c qtz Sst, mod. so			60	9	0.														L
58			ed/c qtz Sst, mod. so			60	7	0									age the second to one					L
59	60 FE SANDSTONE	Br/Gy Fe me	ed/c qtz Sst, mod. so	rting, min. clay, qtz		80	8 (0							L				ļ.,.,			
60	61 FE SANDSTONE	Br/Gy Fe me	ed/c qtz Sst, mod. so	ting, min. clay, qtz		20	8	0		<u> </u>						<u> </u>						
61	62 FE SANDSTONE	Br/Gy Fe me	ed/c qtz Sst, mod. so	rting, min. clay, qtz		20	8 (0					<u>L</u> _				L	ļ				-
62	63 FE SANDSTONE	Br/Gy Fe me	ed/c qtz Sst, mod. so	ting, min. clay, qtz		20	8	0									L	<u> </u>				
63	64 FE SANDSTONE	Br/Gy Fe me	ed/c qtz Sst, mod. so	rting, min. clay, qtz		20	8	0		-				<u> </u>	<u> </u>							
64	65 FE SANDSTONE	Br/Gy Fe me	ed/c qtz Sst, mod. so	ning, min. clay, qtz			8	0						1			2					لــــا
65			ed/c qtz Sst, mod. so			60	8	0			1											
66	67 FE SANDSTONE	Br/Gy Fe me	ed/c qtz Sst, mod. soi	ting, min. clay, qtz		60	8 (0									ļ	_				
67	68 FE SANDSTONE	Br/Gy Fe me	ed/c qtz Sst, mod. so	ting, min. clay, qtz		60	8 (0							<u> </u>		ļ				ألحم	
68			ed/c qtz Sst, mod. sor			200	8	0					1									
69	70 FE SANDSTONE	Br/Gy Fe me	ed/c qtz Sst, mod. sor	ting, min. Shale, clay	, qtz	80	8	o			<u> </u>											
70	71 FE SST/SHALE	Br/Gy Fe me	ed/c qtz Sst, mod. sor	ting, ab. Shale, min.	clay, qtz	200	8	0			1											
71	72 FE SANDSTONE	Br/Gy Fe me	ed/c qtz Sst, mod. sor	ting, min. Shale, clay	, qtz	200	9	0														
72	73 FE SST/SHALE	Gy. Fe med/	c qtz Sst, mod. sorting	g, Shale, min. Fe, cla	ıy, qtz	1,50	10	0					ļ		ļ		<u> </u>					
73	74 FE SILTSTONE	Br. mica Sit,	min. Fe/Mn on beddir	ng		60	16	0														
74	75 FE SLT/SST	Br. mica Sit,	mod. Fe Sst, min. qtz			80	13	0							L							
75	76 FE SLT/SST	Br. mica Sit,	mod. Fe Sst, min. qtz	:		60	12	0			$oxed{L}$											
76	77 FE SLT/SST	Br. mica Sit,	abund. Fe Sst, min. g	tz		40	12	0							<u> </u>	ļ]		
77	78 FE SST/SHALE	Br. Fe med/d	c qtz Sst, mod. sorting	, Shale, min. qtz	. ,	40	10	5	_	1					l			1				

PROSPECT PASSOC WALL (ASTINIA GOBBOTAMO) Traverse 1 (1,000) COMAR-SCE) 261119-10 DO 34122 PC DO 1190 DO DO DO DO DO DO DO D	HOLE F	RC94CW7			CH	HARLOTT	E WELL	- EL	1974	1									<u>. </u>					
To To Symmaty	AZIMUTH INCLINATION	N 90°	NORTHING ZONE	6547875(AMG) 53	٠, ,	COMPLETED	30/11/94	DPO		54320 R	·······	0-119n			.		DRILLE			MARTY	/TREVO	R		
79 79 FE.STISALE				GEOLOGICAL DESCRI	PTION										R	ESUL1	(ppm)							
79 80 FE SSTISUT Bir For marker gar Sat, most sorting, abund, mine St. min. gr. 20 80 80 81 FE SSTISUT Bir marker st. 81 82 FE SANDSTONE Bir marker st. 81 82 FE SANDSTONE Bir For marker gr. 83 83 84 FE SANDSTONE Bir For marker gr. 83 83 84 FE SANDSTONE Bir For marker gr. 83 83 84 FE SANDSTONE Bir For marker gr. 83 83 84 FE SANDSTONE Bir For marker gr. 83 83 84 FE SANDSTONE Bir For marker gr. 83 83 84 FE SANDSTONE Bir For marker gr. 83 83 84 FE SANDSTONE Bir For marker gr. 83 83 84 FE SANDSTONE Bir For marker gr. 83 83 84 FE SANDSTONE Bir For marker gr. 83 83 84 FE SANDSTONE Bir For marker gr. 83 83 84 FE SANDSTONE Bir For marker gr. 83 83 84 FE SANDSTONE Bir For marker gr. 83 84 84 84 84 84 84 84	From	To Summary			Detail			.SI	CPS :	Sample No	From	То	Int	Au	Ag	As	Co	Cr.	Cu	Fe %	Mn.	Ni	Pb	Zn
80 81 FE SILISTONE 8. mine St. min. Fo St. 20 125 31 32 53 52 53 53 53 54 54 54 54 54	78	79 FE SST/SHALE	Br. Fe med/	c qtz Sst, mod. sorting	, Shale, min. qtz			20	80			İ							<u> </u>					
B B S FE SANSTONE B F. E medic qt; St mod. sorting, min. qt; 40 110 10 10 10 10 10 1	79	80 FE SST/SLT	Br. Fe med/	c qtz Sst, mod. sorting	, abund, mica Sit, n	nin, qtz		20	80															
B2 B3 FLEANISTONE B1 F. Fe made's git St. Mr. and. sorling, min. git git 40 110	80	81 FE SILTSTONE	Br. mica Sit,	min. Fe Sst				20	125													The same of the same of		
80 84 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 80 120 85 86 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. State, tr. qtz 200 130 86 87 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. State, tr. qtz 200 130 87 88 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. Rev. gtz 50 180 87 88 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. Rev. gtz 40 150 88 89 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. Rev. gtz 40 150 88 99 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. Rev. gtz 40 150 89 99 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 70 140 99 99 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 100 99 99 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 100 99 99 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 100 99 99 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 100 99 99 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 100 99 99 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 100 99 99 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 100 99 99 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 150 99 99 REMONSTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 150 99 PR. SANASTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 150 99 PR. SANASTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 150 99 PR. SANASTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 160 99 99 PR. SANASTONE Br. For madic gtz Stst., mod. sorting, min. mica, tr. qtz 200 160 99 99 PR. SANASTONE Br. For madic gtz Stst., mod. sorting, min. mica,	81	82 FE SANDSTONE	Br. Fe med/	c qtz Sst, mod. sorting	g, min. mica Sit, qtz			30	140															
B	82	83 FE SANDSTONE	Br. Fe med/	c qtz Sst, mod. sorting	g, min. qtz			40	110															
B4 85 RE SANDSTONE B1 Fe medic qt 25 kt, mot. sorting, min. Shae, tr. qt 2 200 130	83	84 FE SANDSTONE	Br. Fe med/	c qtz Sst, mod. sorting	g, min. mica, tr. qtz			80	120															
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87 88 F.S. SADISTONE B. F. Fe medic qt 2 Sst, mod. soning, nica, tr. qtz 40 155	85	86 FE SANDSTONE	Br. Fe med/	c qtz Sst, mod. sorting	, min. Shale, tr. qtz			200	130														L1	
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102 103 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, min. mica, tr. qtz 80 120 105 104 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, qtz, tr. mica 200 105 105 105 105 106 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, abund. qtz, tr. mica 250 80 107 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, mod. qtz, tr. mica 200 80 107 TE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, abund. qtz, tr. mica 200 80 107 108 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, mod. qtz, tr. mica 150 90 108 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, min. mica, tr. qtz 50 150 109 110 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, mica, qtz 90 140 111 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, mica, qtz 80 90 111 112 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, mod. Slt, mica, min. chl. 80 120 113 114 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, mica, qtz 60 90 111 115 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, mod. Slt, mica, min. chl. 80 130 113 114 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, mica, qtz 60 90 111 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, mica, qtz 60 90 111 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, min. mica, qtz 60 90 111 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, min. mica, qtz 60 90 111 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, min. mica, qtz 60 90 111 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, min. mica, qtz 60 90 115 116 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, abund. mica Sil, tr. qtz 20 120	100	101 FE SLT/SHALE	Gy/Br Slt/Sh	ale, mod. Fe, min. mic	a	•		200	160	_			T											
102 103 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, min. mica, tr. qtz 80 120 105 104 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, qtz, tr. mica 200 105 105 105 106 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, abund. qtz, tr. mica 250 80 105 106 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, mod. qtz, tr. mica 200 80 107 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, abund. qtz, tr. mica 200 80 107 108 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, mod. qtz, tr. mica 200 80 109 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, min. mica, tr. qtz 50 150 109 110 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, mica, qtz 90 140 111 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, mica, qtz 60 90 111 112 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, mod. Slt, mica, min. chl. 80 130 131 14 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, mica, qtz 60 90 113 114 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, mica, qtz 60 90 111 112 FE SST/SLT Br. Fe med/c qtz Sst, mod. Sorting, mica, qtz 60 90 111 112 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, mica, qtz 60 90 111 112 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, mica, qtz 60 90 111 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, min. mica, qtz 60 90 111 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, min. mica, qtz 60 90 111 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, min. mica, qtz 60 90 111 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. Sorting, qtz, min. mica 20 70 115 116 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, abund. mica Sit, tr. qtz 20 120	101	102 FE SANDSTONE	Br. Fe med/	c qtz Sst, mod. sorting	, mica, gtz			200	160															
103 104 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, qtz, tr. mica 200 105 105 105 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, abund, qtz, tr. mica 250 80 105 106 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, mod. qtz, min. mica 40 100 107 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, abund, qtz, tr. mica 200 80 107 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, mod. qtz, tr. mica 250 80 107 108 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, mod. qtz, tr. mica 150 90 108 109 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, min. mica, tr. qtz 50 150 150 109 110 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, mica, tr. qtz 90 140 111 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, mica, qtz 60 90 111 112 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, mod. Slt, mica, min. chl. 60 120 113 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, mod. Slt, mica, min. chl. 80 130 113 114 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, min. mica, qtz 60 90 114 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, min. mica, qtz 60 90 114 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, qtz, min. mica 20 70 115 116 FE SST/SLT Br. Fe med/c qtz Sst, mod. sorting, abund. mica Slt, tr. qtz 20 12	102							80	120															
104	103							200	105				1 7											
105	104					a		250	80															
106	105							40	100		1													
107 108 FE SANDSTONE Br. Fe med/c qtz Sst, poor sorting, mod. qtz, tr. mica 150 90 108 109 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, min. mica, tr. qtz 50 150 150 150								_			1										•			
108 109 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, min. mica, tr. qtz 50 150	107							150	90	*		1	İ					_						
109 110 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, mica, tr. qtz 90 140 140 150 140 150 150 140 150	108	 							150			<u> </u>			1									
110								-	_		1	1			ŀ									
111 112 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, mod. Slt, mica, min. chl. 60 120 112 113 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, mod. Slt, mica, min. chl. 80 130 113 114 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, min. mica, qtz 60 90 114 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, qtz, min. mica 20 70 115 116 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, abund. mica Slt, tr. qtz 20 120	-												1 1		<u> </u>						_		\neg	\neg
112 113 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, mod. Slt, mica, min. chl. 80 130 113 114 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, mln. mica, qtz 60 90 114 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, qtz, min. mica 20 70 115 116 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, abund. mica Slt, tr. qtz 20 120						n. chl.							1-1		Ť.									
113 114 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, mln. mica, qtz 60 90 114 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, qtz, mln. mica 20 70 115 116 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, abund. mica Sit, tr. qtz 20 120	-							_					1							1 1		-		
114 115 FE SANDSTONE Br. Fe med/c qtz Sst, mod. sorting, qtz, min. mica 20 70 115 116 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, abund. mica Sit, tr. qtz 20 120												ļ	T		†									\exists
115 116 FE SST/SLT Br. Fe med/c qtz Sst, poor sorting, abund. mica Sit, tr. qtz 20 120												<u> </u>		-										
						ntz					+	<u> </u>	1							1		\neg		
	116	• •				. 4			100			 	1 1		1		\vdash		<u> </u>				\rightarrow	

HOLE	RC94	CW7			CH	IARLOTT	E WELL	- EL	_197	4														
PROSPECT	Ī	PASCOE WELL	EASTING	608800(AMG)	Traverse 1(Local)	COMMENCED	29/11/94	DPO		54320 FC		0-119m	OXIDIS	SED TO	•	7·m	CONTR	ACTOR		STRATA	١			
AZIMUTH			NORTHING			ľ			WATE	R TABLE		51 m	DRILLE	R ⁱ		MARTY	/TREVC	λR		1				
INCLINATIO	N	90	ZONE									RG			EXPLOR	ER 200								
TOTAL DE	PTH	1 1 9 n	RL .	142m																				
				GEOLOGICAL DESCR	IPTION							•			RE	SULT	S (ppm)							
From	To	Summary			Detail			S	CPS	Sample No	From	То	Int	Au	Âg	As	Co	Cr	c	Fe %	Mn	Ni_	Pb	Zn
117	118	FE SST/SLT	Br. Fe med	/c qtz Sst, poor sortin	g, abund, mica Slt, ti	r. qtz		20	80														L	
118	119	FE SST/SLT	Br. Fe med	/c qtz Sst, poor sorting	g, abund, mica Sit, ti	r. qtz		20	80														L	
EOH			1		_																			

HOLE RC	94CW8		CHARLOTT	E WELL	- EL	197	4														
PROSPECT	PASCOE WELL	EASTING 607700(AMG)	COMMENCED	30/11/94	DPO		54320 R	<u> </u>	0-92m	OXIDI	SED TO		5m	CONTRA	CTOR	;	STRATA				
AZIMUTH	-	NORTHING 6549700(AMG)	COMPLETED	1/12/94						WATE	R TABLE		33m	DRILLER	l	1	MARTY	TREVO	a		
INCLINATION	90°	ZONE 53	GEOLOGIST	DWW			İ							RG		1	EXPLOR	ER 200			
TOTAL DEPTH	92m	FL 149m																			
	•	GEOLOGICAL DESCRIPTION								2.5.		RI	ESULT	S (ppm)							
From To	Summary	Detail			S	CPS	Sample N	o From	To	Int	Au	Ag	As	Co	Cr	Cu	Fe %	Mn	Ni	Pb	Zn
0	1 SANDSTONE	Ye/Br weath, med/c qtz Sst, poor sorting, min. cla	y, qtz, tr. Fe		20	60	3942650	0	4	4	< 0.02	<1	4	< 2	46	4	1.67	50	5	< 5	4
1	2 SANDSTONE	Ye/Br weath, med/c qtz Sst, poor sorting, min. cla	y, qtz, tr. Fe		20	60	3942651	. 4	8	4	< 0.02	< 1	< 3	< 2	65	3	1.19	35	4	< 5	3
2	3 SANDSTONE	Ye/Br weath, med/c qtz Sst, poor sorting, min. qtz	, tr. Fe		20	60	3942652	8	12	4	<0.02	< 1	<3	< 2	36	2	0.42	10	. 3	<5	< 2
3	4 SANDSTONE	Ye/Br weath, med/c qtz Sst, poor sorting, min. qtz	, tr. Fe		10	60	3942653	12	16	4	< 0.02	< 1	< 3	< 2	65	< 2	0.40	15	4	10	< 2
4	5 SANDSTONE	Ye/Br weath, med/c qtz Sst, poor sorting, min. qtz	, tr. Fe		10	50	3942654	16	, 20	4	<0.02	< 1	< 3	< 2	55	3	0.28	15	4	10	< 2
5	6 SAND	Ye c/vc qtz Sand, well sorted, subrd qtz, min. Sst		_	10	5,0	3942655	20	24	4	<0.02	<1	<3	< 2	75	< 2	0.42	20	6	10	< 2
6	7 SAND	Ye/Br med/c qtz Sand, poor sorting, subrd qtz			15	60	3942656	24	28	4	<0.02	< 1	< 3	< 2	50	3	0.32	15	7	20	< 2
7	8 SAND/SST	Ye/Wh c/vc qtz Sand, well sorted, subrd qtz, mod.	Sst		15	50	3942657	28	32	4	<0.02	< 1	< 3	< 2	80	3	0.41	20	8	10	< 2
8	9 SAND	Ye/Wh c/vc qtz Sand, well sorted, subrd qtz, tr. S	st		20	45	3942658	32	3.6	4	<0.02	<1	<3	< 2	40	< 2	0.18	10	3	5	< 2
9	10 SANDSTONE	Wh/Ye f/med. qtz Sst, mod. sorting, min. qtz, tr. F	е		20	45	3942659	36	40	4	<0.02	< 1	<3	3	95	10	0.42	65	. 5	5	4
10	11 SAND	Rd/Br f/med. qtz Sand, mod. sorting, min. c Sand			40	50	3942660		44	4	< 0.02	< 1	<3		75	5	0.56	70	6	10	10
11	1 2 SAND	Wh. c/vc qtz Sand, poor sorting, subang-subrd qtz	min. clay		200	60	3942661	44	48	4	<0.02	< 1	4	5	75	11	1.72	160	11	5	28
12	13 SAND/CLAY	Wh. c/vc qtz Sand, poor sorting, subang-subrd qtz	ab. clay		20	60	3942662		5.2	-	<0.02	< 1	< 3		130	7	1.57	140	. 8	5	20
13	14 SAND/CLAY	Wh. c/vc qtz Sand, poor sorting, subang-subrd qtz	ab. clay	<u> </u>	20		3942663		56		<0.02	< 1	< 3		120	8	1.81	110	10	10	24
14	15 SAND	Wh. f/med. qtz Sst, mod. sorting, min. c qtz, clay,	tr. Fe		15	45	3942664		60	4	< 0.02	< 1	< 3		55	7	1.70	120	6	10	18
	16 SAND	Wh. f/med. qtz Sst, mod. sorting, min. c qtz, clay	and a second of the second of		20		3942665		64	-	<0.02	< 1	4	6	75	. 7	2.34	210	8	10	28
	17 SAND	Wh. f/med. qtz Sst, mod. sorting, min. clay	*		20		3942666		68		<0.02	< 1	8		46	8	3.72	520	11	20	46
17	18 SAND	Wh. f/med. qtz Sst, mod. sorting, abund. qtz, min.	clay		70	_	3942667		7.2	_	<0.02	< 1	6		5.5	9	3.96	500	26		100
	19 SAND/CLAY	Wh, vf/f qtz Sand-powdery/sticky clay			60		3942668		76		<0.02	< 1	6	8	48	. 8	3.16	360	13	15	40
	20 SAND/CLAY	Wh. med. qtz Sand, well sorted, mod. powdery/stic			60		3942669		80		<0.02	< 1	4	5	110	8	2.98	340	10	5	19
	21 SAND/CLAY	Wh. med. qtz Sand, well sorted, mod. powdery/stic	ky clay		60		3942670		84	_	<0.02	< 1	< 3	6	100	6	2.28	270	10	10	36
	22 SAND/CLAY	Wh. vf qtz Sand-powdery clay, min. c qtz, Fe		<u> </u>	20		3942671	84	88	-	<0.02	< 1	< 3		170	4	1.46	170	6	5	8
	23 SAND/CLAY	Wh. vf qtz Sand-powdery clay, min. c qtz, Fe			20		3942672		92	4	<0.02	< 1	< 3	2	46	2	1.53	190	3	< 5	6
<u> </u>	24 SAND/CLAY	Wh. vf/med. qtz Sand-powdery clay, abund. c/vc q			60	60		EOH												\dashv	
		Wh. vf/med. qtz Sand-powdery clay, abund. c/vc q			20	60							ļ						\longrightarrow	\dashv	
F	26 CLAY	Wh. powdery Clay, mod. competent clay, min. c qt			30	80												}		\rightarrow	[
	27 CLAY	Wh. powdery Clay, mod. competent clay, min. c qt			30	110	 			<u> </u>			<u> </u>						\rightarrow		\dashv
		Wh/Ye vf/med. qtz Sand-powdery clay, ab. c/vc qt			40	100				<u> </u>										\rightarrow	
—		Wh/Lt. Gy vf/med. qtz Sand-powdery clay, min. m			250	70	-			<u> </u>									\rightarrow		
		Wh/Lt. Gy vf/med. qtz Sand-powdery clay, mod. r			20	65							_						\longrightarrow		
		Wh/Lt. Gy vf/med. qtz Sand-powdery clay, mod. r			200	65	+	<u> </u>											\rightarrow		
		Wh. med/c qtz Sand, poor sorting, mod. clay, min.			5	55				-			_	<u> </u>					\rightarrow		
		Wh. c/vc qtz Sand, mod. sorting, subang-rd qtz, m			5	55				\vdash				<u> </u>					\rightarrow	\rightarrow	
·		Wh. f/c qtz Sand, poor sorting, subang-rd qtz, min			10	55														\rightarrow	
H	35 SAND	Wh. med/c qtz Sand, mod. sorting, subang-rd qtz,	min. clay		5	45				\sqcup									\rightarrow		\dashv
	36 SANDSTONE	Wh. med. qtz Sst, well sorted, rd qtz, clean			5	50				_						-			\rightarrow	\perp	
		Wh. c/vc qtz Sand, poor sorting, subrd qtz, min. S			20	50	+												\longrightarrow	$-\downarrow$	
		Wh. f/vf qtz Sand, mod. sorting, min. med/c qtz, t		<u> </u>	30	70				ļ										\rightarrow	ا دریا
38	39 SAND	Wh. f/vf qtz Sand, mod. sorting, min. med/c qtz, t	. clay	,	30	70	_														2

HOLE F	C94	ICW8			CHARLOTT	E WELL -	EL	197	4														
PROSPECT AZIMUTH INCLINATION			NORTHING ZONE	607700(AMG) 6549700(AMG) 53	COMMENCED COMPLETED GEOLOGIST	30/11/94 DI 1/12/94 DWW	PO		54320 FC		0-92m	1	SED TO R TABLE			CONTR DRILLEI FIG				TREVORER 200	DR .		
TOTAL DEP	ГН	92m	PL	149m		.,		1	_, _ .			<u> </u>				<u> </u>							
<u> </u>		T -	1	GEOLOGICAL DESCRIPTION			2:			1		т. т				S (ppm)		1 _	1	T	1		
-	То	Summary		Detail			_		Sample No	From	То	Int	Au,	Ag	As	Co	Cr	Cu	Fe%	Mn_	Ni	Pb	Zn
39		SAND	+	z Sand, mod. sorting, min. med/c	qtz, tr. clay		30	75		 		 						-					
40		SAND	1	Sand, poor sorting, min. vc qtz	tlou		30	75 75			 										<u> </u>	\vdash	-
42		SAND	 	ed. qtz Sand, mod. sorting, min. c qtz Sand, mod. sorting, min. med			60	90								ļ			-	<u> </u>	 		
43		SAND	1	qtz Sand, mod. sorting, min. med. o				100			 							<u> </u>					
44		SAND	1	qtz Sand, mod. sorting, c/vc qtz,			_	100		1	 				_				<u> </u>				$\overline{}$
45		FE SANDSTONE	1	d. gtz Sst, mod. sorting, c/vc qtz,				110		 								 	<u> </u>		+ -	\vdash	
46		FE SANDSTONE	1	d. qtz Sst, mod. sorting, c/vc qtz,			_	105			 								1				
47		SANDSTONE		. qtz Sst, mod. sorting, Fe, tr. qtz			100	90											ļ —				
48		SAND	1	tz Sand, poor sorting, rd qtz, min.			80	85	** * * *	<u> </u>													
49	50	SAND		ed. atz Sand, mod. sorting, rd atz			80	70		1	•	Ħ											
50	51	SAND	1:	ed. qtz Sand, mod. sorting, rd qtz,			200	70															
51	52	SAND/SST	Lt. Br/Wh m	med/c qtz Sand, mod. sorting, mo	d. Sst		60	80															
52	53	SST/SAND	Br. med. qtz	z Sst, mod. sorting, Fe, tr. qtz PAI	NDURRA FM.	2	200	80										Ī		İ			
53	54	SANDSTONE	Br. med. qt	tz Sst, mod. sorting, qtz, min. Fe			150	80															
54		SST/SAND	Br. med. qt.	tz Sst/Sand, mod. sorting, qtz			40	90															
55		SST/SAND	Lt. Br/Ye m	ned. qtz Sst, mod. sorting, Sand, q	tz, min. Fe		90	90								_		<u> </u>				أحب	
56		SST/SAND_	+	ned. qtz Sst/Sand, mod. sorting, q			200	70		 													
57		FE SANDSTONE		d. qtz Sst, mod. sorting, min. Wh. o	4.			110															
58		FE SANDSTONE		d. qtz Sst, mod. sorting, min. Wh. c				110									-						
59		FE SANDSTONE	1	d. qtz Sst, mod. sorting, mica/chl, o			20	70															
60		FE SANDSTONE		d. qtz Sst, mod. sorting, min. mica	· · · · · · · · · · · · · · · · · · ·			110		-	-												
61		FE SANDSTONE		d. qtz Sst, mod. sorting, min. mica	/chi, tr. qtz			130		ļ												\longrightarrow	
62		FE SANDSTONE FE SANDSTONE	,	d. qtz Sst, mod. sorting, tr. qtz	<u> </u>	·		120		<u> </u>		\vdash							-			-	
64		FE SANDSTONE		I. qtz Sst, mod. sorting I. qtz Sst, mod. sorting, min. chl.			-	110				├ ─┤							<u> </u>			-+	
65		FE SILTSTONE		t, min. Shale, abund. Fe	•		_	180	*	 										-		\rightarrow	
66		FE SANDSTONE	 	d. qtz Sst, mod. sorting, min. mica,	tr. otz		_	140		1												-+	
67	_	FE SANDSTONE		f. qtz Sst, mod. sorting, min. mica,				110														-+	
68		FE SANDSTONE		I. qtz Sst, mod. sorting, min. qtz	11, 412		20	90			 	-											
69	_	FE SANDSTONE	1	l. qtz Sst, mod. sorting, clay, min.	atz	<u> </u>	20	80														-	
70		FE SANDSTONE	†	I. qtz Sst, mod. sorting, mod. qtz	1'7		60	90							-							\neg	
71		FE SANDSTONE		I. qtz Sst, mod. sorting, min. qtz			_	100										-				\dashv	
72	73	FE SANDSTONE	†	I. qtz Sst, mod. sorting, min. qtz	1 1			100															
73	74	FE SANDSTONE		I. qtz Sst, mod. sorting, min. mica,	tr. atz		_	100					ŀ										
74	75	FE SANDSTONE		l. qtz Sst, mod. sorting, min. Wh. S			40	90							1								
75	76	SANDSTONE		. qtz Sst, mod. sorting, qtz, min. F			_	100	- · · · ·				1										
76	77	FE SANDSTONE	i	l. qtz Sst, mod. sorting, min. mica,			90	90															
77	78	FE SANDSTONE	Br. Fe med.	I. qtz Sst/Wh. Sst, mod. sorting, m	in. qtz		40	90															

HOLE R	C94CW8		CI	HARLOTTI	E WELL	- EL	1974															
PROSPECT AZIMUTH	PASCOE WELL	EASTING NORTHING	607700(AMG) 6549700(AMG)	COMMENCED	30/11/94 1/12/94			54320	FC:	0-92n		SED TO	•		CONTR	ACTOR R		STRAT/		·R		
INCLINATION	1 90°	ZONE	53	GEOLOGIST	DWW	1								001	FIG			EXPLOP				
TOTAL DEPT	ΓH 92m	PL.	149m		<i></i>						1				L							
			GEOLOGICAL DESCRIPTION						,		· · ·		R	SULT	S (ppm)							
From	To Summary		Detail			S	CPS S	Sample	No Fron	1 To	Int	Au	Ag	As	Co	Cr	Cu	Fe %	Mn	Ni	Pb	Zn
78	79 FE SANDSTONE	Br. Fe med.	qtz Sst, mod. sorting, abund. qtz			50	70														\sqcup	
79	8 0 FE SANDSTONE	Br. Fe med.	qtz Sst, mod. sorting, min. qtz			8.0	70	_														
80	8 1 FE SANDSTONE	Br. Fe med.	qtz Sst, mod. sorting, qtz			50	70														لـــا	
81	8 2 FE SANDSTONE	Br. Fe med.	qtz Sst/Wh. Sst, mod. sorting, min. chl, t	r. qtz		30	70														i. 1	
82			qtz Sst/Wh, Sst, mod. sorting, chl, min. o			30	70															
83	84 SAND	Br/Wh med/	c qtz Sand, mod. sorting, subrd qtz, min.	Fe		40	70															
84	85 SAND	Br/Wh med/	c qtz Sand, mod, sorting, subrd qtz, mod.	Fe		40	60															
85	86 SAND	Br/Wh med/	c qtz Sand, mod. sorting, subrd qtz, mod.	Fe		40	60															
86			c qtz Sand, mod. sorting, subrd qtz, mod.			40	60				1			•								
87			c qtz Sand, mod. sorting, subrd qtz, clear			20	60															
88			c qtz Sand, mod. sorting, subrd qtz, clear			40	60															
89	_		atz Sand, mod. sorting, subrd qtz, clean			40	 			1		·····										\neg
90			tz Sand, mod. sorting, subrd qtz, clean, n	nin. Fe		10	60				i i											
91			tz Sand, mod. sorting, subrd qtz, clean, n			10		-														
EOH			the learner, mean beauting, does a diet dioditt in				30															

HOLE	RC94CW9			СН	IARLOTTE	WELL - EI	_197	4				<u> </u>	<u> </u>									
PROSPECT AZIMUTH		WELL EASTING	G 6546100(AMG)	Traverse 1(Local) 15200(Local)	COMPLETED	1/12/94 DPO 2/12/94		54320 FC		0-90m		ISED TO ER TABLE			CONTRA				/TREVO	R		
INCLINATIO		90° ZONE	53		GEOLOGIST	DWW									FIG			EXPLOR	ER 200			
TOTAL DEP	'IH	90m PL	137m	NOTON							ļ			50111.7								
From	To Summar	. 1	GEOLOGICAL DESCR	Detail		s	1 000	Sample No	From	·	1 1 4		Aa	As	S (ppm)	Cr	<u> </u>	F- 01	Mn	Ni I	Pb	
0	1 SAND		vc qtz Sand, poor sortin		<u></u>	60		3942673	From	To	Int 4	Au <0.02	Ag < 1	AS	3	50	Cu 8	Fe %	- Mn 60	NI 7	PD.	Zn 13
1	2 SAND		vc qtz Sand, poor sortin			60		3942673	4	8	4	<0.02	<1	6	 +	44	- 8	2.24	75	10	- 5	20
2	3 SAND		ve qtz Sand, poor sorting		En	70	·	3942674 3942675	8	12	_	<0.02	<1	< 3		44	10	2.60	60	11	10	20
3	4 SAND/CLAY		n. med. qtz Sand/Clay, p		. 1 6	60	+	3942676	12	16	-	<0.02	<1	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	2	36	7	2.44	35	10	- 5	12
4	5 SAND/CLAY		n. med. qtz Sand/Clay, p			60		3942677	16		+ -	<0.02	<1	< 3	3	80	3	1,48	30	11	5	5
5	6 SAND/CLAY		n. med. qtz Sand/Clay, p			40	-	3942678	20	24	_	<0.02	<1	4	3	80	4	0.59	460	17	10	4
6	7 SAND/CLAY		n, med. qtz Sand/Clay, p		min. Fe	40	\rightarrow	3942679	24	28	_	<0.02		4	<2	120	5	0.53	460	12	10	4
7	8 SAND/CLAY		n. med. qtz Sand/Clay, p			40		3942680	28	32		<0.02		6	2	65	10	1.33	660	8	10	10
8	9 SAND/CLAY		n. med. qtz Sand/Clay, p		Fe	20		3942681	32	3.6		<0.02	<1	6	4	75	18	1.08	140	11	5	12
9	10 SAND/CLAY		n. med. qtz Sand, poor s			20	+	3942682	36	40		<0.02	<1	10	5	19	14	2.06	580	10	10	24
10	11 SAND/CLAY		n. med. qtz Sand, poor s			40	55	3942683	40	44	4	<0.02	<1	6	4	80	11	1.75	700	14	10	15
11	12 SAND/CLAY	Br. weat	n. med. qtz Sand/Clay, p	oor sorting, mod. qtz,	min. Fe	60	55	3942684	44	48	4	<0.02	< 1	4	.4	40	10	1.13	180	11	< 5	15
12	13 SAND/CLAY	Br. med.	qtz Sand, mod. sorting,	Clay, Fe, min. qtz		.80	60	3942685	48	52	4	<0.02	< 1	4	3	60	13	1.34	200	11	5	14
13	14 SAND/CLAY	Br. med.	qtz Sand, mod. sorting,	Clay, Fe, min. qtz		70	60	3942686	52	56	4	< 0.02	<1	8	4	3 2	9	2.26	480	10	10	17
14	15 SAND/CLAY	Br. med.	qtz Sand/Clay, poor sor	ting, mod. Fe, min. qt	<u> </u>	50	50	3942687	56	. 60	4	<0.02	< 1	8	5	40	15	2.40	410	12	10	26
1.5	16 SAND/CLAY		qtz Sand, mod. sorting,			50	5.5	3942688	60	_ 64	4	<0.02	< 1	14	8	9	24	3.58	360	12	20	5 5
16	17 CLAY/SAND	Lt. Br/Wi	Clay/ I/med. Sand, poo	or sorting, min. qtz, F	θ	20	60	3942689	64	68	4	<0.02	<1	12	6	19	19	3.66	940	7	15	40
17	18 SAND		/ f/med. Sand, poor sort			60	50	3942690	68	72	4	< 0.02	< 1	8	6	13	18	2.92	460	. 9	15	44
18	19 SAND		d. Sand, mod. sorting, n			50		3942691	72	76	_	< 0.02	_ < 1	12	9	24	22	3.72	760	11	15	42
19	20 SAND		nd, mod. sorting, min. p			2,0	-	3942692	76	80		<0.02	< 1	18	5	50	14	3.60	660	_ 6	10	26
20	21 SAND/CLAY		ed/c Sand, poor sorting			30	 	3942693	80	84		<0.02	<1	14	3	100	5	1.53	170	5	5	8
21	22 SAND/CLAY		vc Sand, poor sorting, r		. qtz	20		3942694	84	88		<0.02	<1	6	3	9	6	1.79	260	4	5	26
22	23 SAND/CLAY		y vf/f Sand-powdery cla			200		3942695	88	90	2	<0.02	<1	<3	4	30	5	2.38	290	3	10	38
23	24 SAND/CLAY		y vf/f Sand, mod. powde			60	t t		EOH			-								— ∔	\rightarrow	
24	25 SAND/CLAY 26 SAND/CLAY		y f/med. Sand, mod. pov			60	-															
26	27 SAND/CLAY		y vi/i Sand, mod. powd		Įtz	200	70		+							-+					\rightarrow	
27	28 SAND		y t/med. Sand, min. pov vi Sand, min. clay, med/			200	70 60		-												\rightarrow	\dashv
28	29 SAND		Sand, min. clay, med/c o			100	90		1		\vdash	-								+	+	-
29	30 SAND/CLAY		vi/i Sand, mod. powder		mod atz	80	100						-							\dashv	\rightarrow	\dashv
30	31 SAND/CLAY		and, mod. powdery clay			200	100		 	-					+	+		-		+	+	-
31	32 SAND/CLAY		Sand, mod. powdery clay			80	100		1						- +		-			\rightarrow	-+	\dashv
32	33 SAND/CLAY		vt/f Sand, mod. powder			80	100		+ +		\vdash					+	 			+	+	-
33	34 SAND/CLAY		vi/i Sand, mod. powder			60	80		1 1		\vdash					-				\rightarrow	+	-
34	35 SAND/CLAY		vf/f Sand, mod. powder		mou, qiz	250	80		1				- 1		:		-+		- +	\rightarrow	\rightarrow	-
35	36 FE SANDSTONE		med. Sst, mod. sorting,		URRA FM	200	100	·	1						- 1				- +	\rightarrow	+	\dashv
36	37 FE SANDSTONE		med. Sst, mod. sorting			200	110			-		+				-		\rightarrow	+	-+	-+	\dashv
37	38 FE SANDSTONE		med. Sst, mod. sorting,			100	120				\vdash	1			+	-+	1	1	+	\dashv	\dashv	\dashv
38	39 FE SANDSTONE		ale/mica Sit, mod, Fe, m			60	120					1		$-\dagger$						\dashv	\dashv	

HOLE	RC94	1CW9			CH	ARLOTTE	WELL -	EL1	974															
PROSPECT AZIMUTH INCLINATION TOTAL DE	ON			609475(AMG) 5546100(AMG) 53 137m	Traverse 1(Local) 15200(Local)		1/12/94 D 2/12/94 DWW	OPO		64320 FC		0-90m	4	SED TO R TABLE			CONTR DRILLE PIG		·	STRAT/ MARTY EXPLOR	/TREVC	OR		
			G	SEOLOGICAL DESCRIP	PTION										RE	SULT	S (ppm)							
From	Τo	Summary		2 0 00 0 20 0	Detail			SI (OPS S	ample No	From	То	Int	Au	Ag	As	Co	Cr	Cú	Fe %	Mn	Ni	Pb	Zn
39	40	FE SANDSTONE	Br. Fe med. Ss	st, mod. sorting, min	. shale/Sit, tr. qtz			200	90															
40	. 41	FE SANDSTONE	Br. Fe med. Ss	st, mod. sorting, min	, qtz				80								endonamento de la camada y					1		
41	4 2	FE SANDSTONE	Br. Fe med. Ss	st, mod. sorting, min	. qtz			250	70											<u> </u>		1		
42	43	FE SHALE/SLT	Br. Shale/mica	SIt, mod. Fe, min. S	st, min. mica Sit	4		200	130		· ·									1				ļ
43		FE SANDSTONE	Br. Fe med. Ss	st, mod. sorting, min	. qtz				90														ļ.,	
44		FE SANDSTONE	+	st, mod. sorting, abu				250	90			Ĭ								ļ	<u> </u>			
45		FE SANDSTONE		st, mod. sorting, min.				250	70													<u> </u>		
46		FE SANDSTONE		st, mod. sorting, qtz,			arratement or the barrane bearing and the second	300	80								anar		ļ <u> </u>	ļ	ļ·	<u> </u>		
47		SANDSTONE		. Sst. mod. sorting,				_	80		-	<u> </u>	\vdash							 		-		
48		SANDSTONE	 	. Sst, mod. sorting,					70							-			-			<u> </u>		
49		SANDSTONE		. Sst, mod. sorting,					90		 		├ —							}			-	
50		FE SANDSTONE		st, mod. sorting, min					120		-			· · · · · · · · · · · · · · · · · · ·						<u> </u>				
51		FE SANDSTONE		st, mod. sorting, min					100		-											-		
52		FE SANDSTONE	1	st, mod. sorting, min.					110		+									ļ	· -		-	
53		FE SANDSTONE		st, mod. sorting, tr. o			·		100		-		-									-		
54		FE SILTSTONE		od sorting, mica/chi		According to the Association of States of Stat			130										-			-	-	
55		FE SILTSTONE	+	od, sorting, mica/chi					180		1		1							 	-		_	
56		FE SANDSTONE	1	st, mod. sorting, min.					130									~				-		
57 58		FE SANDSTONE FE SANDSTONE	+	st, mod. sorting, mic				-	140		<u> </u>									 			<u> </u>	
59		FE SANDSTONE		st, mod. sorting, mic					90		<u> </u>		++								<u> </u>	1		H
60		FE SILTSTONE	Br mica Sit, mod	st, mod. sorting, clay	, min. qtz			_	120				\vdash							<u> </u>	-			
61		FE SILTSTONE	Br mica Sit, mod					_	130				\vdash											-
62		FE SILTSTONE	Br mica Sit, mod						120				╁			-				-				
63		FE SST/SLT		st, mod. sorting, mice	Sit min att		-	-	140															
64		FE SANDSTONE		st, mod. sorting, mic.		• •	-		100		+		-											
65		FE SANDSTONE	1	t, mod. sorting, min.				-	100															
66		FE SANDSTONE	7	st, mod. sorting, min.					150															
67		FE SST/SLT	-	st, mod. sorting, mice			-		160															
68		FE SANDSTONE		st, mod. sorting, min.		2 2			150		1				-									
69		FE SANDSTONE	† · · · · · · · · · · · · · · · · · · ·	st, mod. sorting, tr. o			_	_	135				+ +											
70		FE SANDSTONE		st, mod. sorting, qtz,		<u></u>			105														-	
71		FE SANDSTONE		st, mod. sorting, qiz,					75	-	 													
72		FE SANDSTONE	† 	t, mod. sorting, min.		-	•		100		†	-	† †											
73		FE SANDSTONE		st, mod. sorting, min.					80	· · · · · · · · · · · · · · · · · · ·				1							· · · · ·			
74		FE SANDSTONE		it, mod. sorting, qtz,					80				1 1											
75		FE SANDSTONE	*	st, mod. sorting, min.					100							•								
76		FE SANDSTONE	†	t, mod. sorting, min.					120															
77		FE SANDSTONE		st, mod. sorting, tr. o					80						-		-							

HOLE F	RC94CW9			CH	IARLOTTE	WELL	- EL	.197	4															
PROSPECT	PASCOE WELL	EASTING	609475(AMG)	Traverse 1(Local)	COMMENCED	1/12/94	DPO		54320	PC		0-90m	OXIDIS	SED TO		5m	CONTR	ACTOR	_	STRATA	A			
AZIMUTH	-	NORTHING	6546100(AMG)	15200(Local)	COMPLETED	2/12/94							WATE	R TABLE	•	59 m	DRILLE	R		MARTY	TREVO)R		
INCLINATIO	N 90°	ZONE	53		GEOLOGIST	DWW											RIG			EXPLOF	RER 200			
TOTAL DEP	TH 90m	RL.	137m						_													<u> </u>		
			GEOLOGICAL DESCR	RIPTION	<u> </u>										RE	ESULT	S (ppm)	<u> </u>		,			<u> </u>	
From	To Summary			Detail			SI	CPS	Sample	No F	rom	То	Int	Àυ	Ag	As	Со	Cr	Cu	Fe %	Mn	Ni	Pb	Zn
78	79 FE SANDSTONE	Br. Fe med.	Sst, mod. sorting, m	od. qtz			20	60															igsquare	
79	80 FE SANDSTONE	Br. Fe med.	Sst, mod. sorting, py	rite aggreg, min. qtz			20	60											L					
80	81 FE SST/SAND	Br. Fe med.	Sst/Sand, mod. sort	ing, qtz, tr. pyrite agg	reg.		40	65																
81	82 FE SAND/SST	Br/Wh c qtz	Sand/Sst, mod. sort	ng, subrd qtz, min. F	ө		20	60													L		لحنا	
82	83 FE SAND/SST	Br/Wh med/	c qtz Sand/Sst, mod	sorting, subrd qtz, F	е		20	60																<u>-</u>
83	84 FE SAND/SST	Br/Wh med/	c qtz Sand/Sst, mod	. sorting, subrd qtz, F	е		20	60									<u> </u>				ļ	<u> </u>	L	L
84	85 FE SAND/SST	Br/Wh med/	c qtz Sand/Sst, mod	. sorting, subrd qtz, F	е		20	70													<u> </u>	ļ		
85	86 FE SST/SAND	Br/Wh med.	qtz Sst/Sand, mod.	sorting, min. chl.			20	130	<u> </u>								Lagrange of the Control				<u> </u>	ļ'		ا تاسبام
86	87 FE SST/SAND	Br/Wh med.	qtz Sst/Sand, mod.	sorting, min. chl.			20	140													<u> </u>	<u> </u>		
87	88 FE SST/SAND	Br/Wh med.	qtz Sst/Sand, mod.	sorting, chl.			20	140	<u> </u>												<u> </u>	<u> </u>		
88	89 FE SST/SAND	Br/Wh med.	qtz Sst/Sand, mod.	sorting, chl.			4.0	130							1							<u> </u>		
89	90 FE SST/SAND	Br/Wh med.	qtz Sst/Sand, mod.	sorting, min. chl.			80	130	,											_	<u> </u>	<u> </u>		
ECH								1			i		i 1		1				ſ	1	1	1 ,	1 1	, 1

HOLE R	C94CW10		CH	IARLOTTE	WELL	- EL	197	74												-		
PROSPECT	PASCOE WELL	3/12/94								STRATA												
AZIMUTH	•	NORTHING 6549600(AMG)	3/12/94						WATE	ER TABLE		63m	DRILLEF	3		MARTY/TREVOR						
INCLINATION		ZONE 53		DWW										FIG			EXPLO	RER 200				
TOTAL DEPTH 81m RL 149m																						
		GEOLOGICAL DESCR						ļ							S (ppm)						· - · ·	
From	To Summary		Detail			SI		Sample N		То	Int	Au	Ag	As	Co	Cr	Cu	Fe %	Mn	Ni	Pb	Zn
0	1 SAND	Br/Wh qtz Sand, calcrete?, weath				40		3942696		. 4	.4	< 0.02	< 1	< 3	2	42	5	1.14	. 25	5	< 5	. 5
1	2 SAND	Br/Wh qtz Sand, calcrete?, weath				20		3942697		8	4	< 0.02	< 1		< 2	90	< 2	0.56	15	4	< 5	< 2
2	3 SANDSTONE	Ye. weath. med/c qtz Sst, poor so		, min. Fe		20		3942698		12	4	<0.02	< 1		< 2	36	< 2	0.26	10	4		< 2
3	4 SANDSTONE	Ye. vc qtz Sst, well sorted, subrd	*			5		3942699		16	4	<0.02	<1	<3	< 2	46	< 2	0.34	1 5	4	15	< 2
4	5 SANDSTONE	Ye. vc qtz Sst, well sorted, subrd		<u> </u>		5		3942700		20	4	<0.02	< 1	< 3	< 2	26	< 2	0.38	10	4	5	< 2
5	6 SANDSTONE	Wh. vc qtz Sst, well sorted, subrd				5		3942701	_	24	4	<0.02	< 1	< 3	< 2	50	4	0.46	20	7		2
6	7 SANDSTONE	Wh. vc qtz Sst, well sorted, subrd				5		3942702		28	4	<0.02	< 1	4	< 2	3 <u>0</u> 32		0.43	35	7	20	4
7	8 SANDSTONE	Wh. vc qtz Sst, well sorted, subrd				15		3942703		32	4	<0.02	<1	6	< 2	32	16	0.39	40 75	10 5		5 3
8	9 SANDSTONE/CLAY	Wh. vc qtz Sst-powdery Clay, mo				15		3942704		3.6	4	<0.02	< 1	< 3	2	75	4	0.32		9	10	6
9		Wh. vc qtz Sst-powdery Clay, mo			·	40		3942705		40	4	<0.02	< 1	4	3	90	6 5	1.05	130	9	_	17
10	11 CLAY/SANDSTONE	Wh. powdery Clay-vc qtz Sst, mo				60		3942706		4.4	4	<0.02	<1	4	5	4 4 6 5		0.50	440	11	5	17
11	1 2 SANDSTONE	Wh. c/vc qtz Sst, weak consol. (s			·	60		3942707		48 52	4	<0.02	< 1	4	4		12	1.48	980	11	5	13
12	13 SANDSTONE	Wh. c/vc qtz Sst, weak consol. (s		_	· · · · · · · · · · · · · · · · · · ·	60		3942708			4	<0.02	<1		4	46		2.02	1000	12	_	
13	14 SANDSTONE	Wh, c/vc qtz Sst, weak consol. (c		_	· · · · - · · · · · · · ·	60		3942709		56	4	<0.02	<1	6	5	60	12	2.48	680	12	15	16
14	1 5 SANDSTONE	Wh. c/vc qtz Sst, weak consol. (c				60	_	3942710		60	4	<0.02	<1	6	4	70	14	2.04		10	-	13
15	16 SANDSTONE/CLAY	Wh. c/vc qtz Sst-powdery Clay, w		rting		40		3942711		64	4	<0.02	<1	6	3	150	8	1.42	330 880	8	15	26
16	17 SAND	Br/Or med. Sand, well sorted, clea				5		3942712		68 72	4	<0.02 <0.02	<1 <1	6		4 4 6 5	17	2.24	780	9		16
17	18 SAND	Br/Or med. Sand, well sorted, clea			·			3942713		72	4	1,512,5	-	<3	4	42	10	1.74	600	8	10	15
18	1 9 SANDSTONE 20 SANDSTONE	Wh. med/c qtz Sst, weak consol,				40		3942714	- +	81	- 4	<0.02 <0.02	<1 <1	< 3 4	5	55	17	2.56	1100	8		
19	20 SANDSTONE 21 SAND	Wh. med/c qtz Sst, weak consol,		sand/clay		10	50	1	FOH	81	- 5	<0.02	< 1	4	. 5	55	1 7	2.56	1100		15	_20
<u> </u>		Br/Or med. Sand, well sorted, clea	•			50	50	,	ECH	-											-+	
21	22 SAND/SST 23 SAND/SST	Wh. I/med qtz Sand/Sst, weak co Wh. I/med qtz Sand/Sst, weak co				50	50				-	N								=	\rightarrow	
22				and aloue		80	50			-								-	- 1		\rightarrow	
24		Wh. med qtz Sst, weak consol, po Wh. vf/f Sand, well sorted, min. S		anu, ciay		80	70				_	1								-	-+	
24		Wh. vi/f Sand, well sorted, min. S				80	70		1		\vdash										\rightarrow	-1
26		Br. f/med Sand, poor sorting, min.				80	70				-											\rightarrow
27		Br. I/med Sand, poor sorting, min.				40	80	+			-										\rightarrow	-
28		Lt. Gy. f/med Sand, mod. sorting, min				40	70	+		- A A.										\rightarrow		
29		Lt. Gy. n/med Sand, mod. soning, Lt. Gy. med/c Sand, mod. sorting,				40	70	 											-	\rightarrow	-	
30		Lt. Gy. med/c Sand, mod. sorting,				40	60	 								-				-	-	
31		Lt. Gy. med/c Sand, poor sorting,				40	80	}	1											-+	\rightarrow	
32	33 SAND/CLAY	Lt. Gy. med/f Sand, mod. sorting,		* * *		40	70	+					_								-+	
33		Wh. med, Sand, well sorted, rd qtz				5	50															
34		Wh. med. Sand, well sorted, rd qtz	·			5	50				-		_					-	-	\rightarrow	-+	
35		Wh. med/f Sand, mod. sorting, mi				200	80	 							- 1					-+	$\rightarrow +$	
36		Wh. med/f Sand, mod. sorting, mil				150	70												-		-+	
37		Wh/Ye med/c Sand, mod. sorting, mil				150	70	-	+ -				-	\vdash	-				-	-+		
38		Wh/Ye f/med Sand, mod. sorting,				200	70	ļ-·	_			 	\dashv							\dashv	\rightarrow	
[38]	a a l a wind	vviii re iritied Sand, mod. soning,	ппп. скау			200	/ U	Щ				<u>_</u>			1	1						

HOLE	RC94	4CW10		CH	IARLOTTE	WELL	- EL	1974	<u> </u>														
PROSPEC AZIMUTH INCLINATI TOTAL DE	ON	PASCOE WELL 90° 81 m	NORTHING 6549600(AMG) 18925(Local) COMPLETED 3/12/9 ZONE 53 GEOLOGIST DW				DPO	54320 FC			0-81m	10				CONTR DRILLEI FIG			STRATA MARTY / TREVOR EXPLORER 200				
	···										R	ESUL	rs (ppm)										
From	To	Summary		Detail			S	OPS S	Sample No	From	То	Int	Au	Ag	As	Co	Cr.	Cu	Fe %	Min	Ni	Pb	Zn
39	40	SAND	Lt. Br/Wh f/med Sand, mod. sortii	ng, min. c sand			60	70								Ī.,							
40	41	SAND	Lt. Gy/Wh t/med Sand, mod. sorti	ing, min. c sand			120	75															
41	42	SAND	Lt. Gy. f/med Sand, mod. sorting,	min. Sst, c sand			90	75															
42	43	SAND	Lt. Gy. f/med Sand, mod. sorting,	min. Sst, c sand			80	70															
43	44	SAND	Lt. Gy. f/med Sand, mod. sorting,	min. Sst, c sand			80	70															
44	45	SAND	Ye/Br f/med Sand, poor sorting, n	nin. c sand			80	80		<u> </u>	<u> </u>			<u> </u>									
4.5	46	SAND	Lt. Br/Wh f Sand, mod. sorting, m	nin. Sst. med/c sand			60	90]				L .									
4.6	4.7	SANDSTONE	Br Fe med. qtz Sst/Wh Sst, mod.	sorting, min. qtz		e	100	80		<u> </u>					<u> </u>								
4.7	48	SANDSTONE	Wh. med. qtz Sst, mod. sorting, r	min. qtz			200	70													<u> </u>		
48		SAND	Wh. f/med qtz Sand, mod. sorting	, min. Sst, c sand			200	70		ļ	ļ										<u> </u>	\sqcup	\vdash
49		SAND	Wh. f/med qtz Sand, mod. sorting			_	200	70		_		ļ				ļ			<u> </u>			\vdash	
50		SAND	Wh. f/vf qtz Sand, mod. sorting, i				200	80										├					<u> </u>
51		SAND	Lt. Br/Wh med/f qtz Sand, mod. s				70	80				1		<u> </u>		ļ						\vdash	
52		SAND	Lt. Br. med/f qtz Sand, mod. sorti				200	95		1	ļ —	\vdash		ļ						_		\vdash	
5.3		SAND	Lt. Br. med/f qtz Sand, mod. sorti				200	95		 		1		<u> </u>				ļ				$\vdash \vdash$	$\vdash \vdash \vdash$
54		FE SST/SAND	Lt. Br. Fe med. qtz Sst, mod. sortir				200	80			<u> </u>											\vdash	├
5.5		FE SST/SAND	Lt. Br. Fe med. qtz Sst, mod. sort		nod. qtz		200	80		! —		-	· · · · · · · · · · · · · · · · · · ·									\vdash	\vdash
56		FE SANDSTONE	Lt. Br. Fe med. qtz Sst, mod. son		 		200	80								ļ		 		ļ	-	\vdash	H
57		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting		<u></u>			110			-					-		-					<u> </u>
58		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting	•			200	90			 							 			-	\vdash	<u> </u>
59		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting				200	80		-	ļ		نستان الد		<u> </u>								\vdash
60		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting				60	80							-			-		-			\vdash
61		FE SANDSTONE FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting				50	70 60		1	<u> </u>			<u> </u>	-							$\vdash \vdash \vdash$	\vdash
62			Br. Fe med. qtz Sst, mod. sorting				40	65						-								1	
63		FE SANDSTONE FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting				30	80									-	-					
65		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting, Br. Fe med. qtz Sst, mod. sorting				70	95		 				-									-
66		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting		tr. ota			140		1	-	\vdash			-								\Box
67		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting					115		<u> </u>					\vdash		-	-	-			\Box	-
68		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting		, 11 <u>, q</u> 12	-		105		1									-				
69		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting				80	80		1												\Box	Г
70		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting				40	80		1		\vdash			-	-						\Box	\Box
71		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting				60	95		1	i i	\vdash										\vdash	Г
71		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting	· · · · · · · · · · · · · · · · · · ·			10	80		1		\vdash			 							\dashv	
73		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting				10	75		l		+ +	<u> </u>							· -			
74		FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting				40	75		-			-	-					-			\rightarrow	$\vdash\vdash\vdash$
75	_	FE SANDSTONE	Br. Fe med. qtz Sst, mod. sorting				70	70		 	-	1	· · ·	-				 		-		-	\Box
76		FE SST/SLT	Br. Fe med. qtz Sst/mica Slt/Shal	· • • • • • • • • • • • • • • • • • • •		·	20	80			<u> </u>		-		-							-	$\overline{}$
77		FE SAND	Br. Fe med. qtz Sst/mica Sit/Shai		ĮLZ .		30	65		-	-										\vdash		\vdash
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HOLE	RC94	ICW10			CH	IARLOTTE	E WELL .	· EL	1974															
PROSPEC	т	PASCOE WELL	PASCOE WELL EASTING 608275(AMG) Traverse 1(Local) COMMENCED 3				3/12/94	DPO	54	54320 FC 0-81m OXIDISED TO 3m CONT				CONTR	CONTRACTOR STRATA									
AZIMUTH		-	NORTHING	IG 6549600(AMG) 18925(Local) COMPLETED			3/12/94						WATER TABLE 63 n			63m	n DRILLER			MARTY / TREVOR				1
INCLINATI	ON	90°	ZONE	53 GEOLOGIST			DWW			-							FIG:			EXPLORER 200				
TOTAL DE	PTH	81 m	PL .	149m																				
	GEOLOGICAL DESCRIPTION									RESULTS (ppm)														
From	То	Summary			Detail			SI	CPS Sa	nple No	From	To	Int	Au	Ag	As	Co	Cr	Cu	Fe %	Mn_	Ni	Pb	Zn
78	79	FE SANDSTONE	Br. Fe med.	. qtz Sst, mod. sorting	, qtz			40	80				1										L	
79	80	FE SLT/SST	Br. Fe Slt/S	st, mod. sorting, min.	clay			60	95															
80	81	FE SILTSTONE	Br. Fe Sit, m	nin. Fe Sst				40	70														L1	
ECH				Control of the Contro															<u></u> ,			لـــا		Ĺ

APPENDIX VIII

Mineralogical Report No. 6764 by Purvis, A.C., Pontifex and Associates P/L

Pontifex & Associates Pty. Ltd. 100169

TELEPHONE (08) 332 6744 FAX (08) 332 5062 26 KENSINGTON ROAD, ROSE PARK SOUTH AUSTRALIA 5067 A.C.N. 007 521 084 P.O. BOX 91, KENT TOWN SOUTH AUSTRALIA 5071

MINERALOGICAL REPORT NO. 6764 by A.C. Purvis, PhD

December 21, 1994

TO:

CRA Exploration Pty Ltd 31 Osmond Terrace NORWOOD SA 5067

Attention:

Warwick Stewart Dave Jackson

COPY TO:

Snr. Administration Officer CRA Exploration Pty Ltd 31 Osmond Terrace NORWOOD SA 5067

Information Officer

CRA Exploration Pty Ltd

PO Box 3709

MANUKA ACT 2603

YOUR REFERENCE:

DPO No. P54358

MATERIAL & IDENTIFICATION:

2 Rock samples

1156565 and 1156566

WORK REQUESTED:

Polished thin section preparation, petrographic

descriptions, with comments and photomicrographs,

as specified.

SAMPLES & SECTIONS:

Returned to you with this report.

achuna

PONTIFEX & ASSOCIATES PTY. LTD.

1156565

Basalt with a coarse framework of plagioclase, pyroxene(s) and skeletal opaque oxides and a mesostasis of plagioclase microlites in chlorite - k felspar-altered possible glass, with clay-quartz-carbonate-(chalcopyrite)-filled possible vesicles and trace pyrite.

Field Note: Altered dolerite.

This is quite an unusual rock, with an apparently cage-like framework of coarse plagioclase laths to 3 mm long, commonly containing patches of sericite and carbonate, encapsulating large areas of quenched mesostasis. The plagioclase-rich framework also contains some (~7%) granular to prismatic clinopyroxene to 2 mm grainsize, commonly altered to clays and partly skeletal opaque oxide crystals to 2 mm long. Some largely clay-altered possible orthopyroxene is also present (<1%).

The mesostasis has cores to 3 mm diameter which may be vesicles and contain quartz, chloritic clays, carbonate and sulphides in various proportions. The mesostasis proper is dominated by plagioclase microlites, many of which are curved and/or hollow, reflecting rapid quenching. Interstitial chloritic clays are common, together with less abundant carbonate, sphene and dendritic fine opaque oxide crystals. Some of the mesostasis also contains diffuse patches of alkali felspar.

One of the vesicles has a grain of chalcopyrite about 0.15 mm in size and there is rare pyrite in the host rock.

This sample appears to have commenced to cool slowly, forming the framework and then been quenched. It may be classified as a basalt with a bimodal grainsize.

1156566

Similar "bimodal" basalt to that in 1156565, with a green area rich in chlorite and a brown area rich in alkali felspar, with chloritised ferromagnesian minerals and quartz-chlorite-carbonate-filled vesicles throughout. Pyrite more abundant in the brown zone than in the green zone. Zoned quartz-carbonate vein separating the zones, with trace pyrite.

Field Note: Altered dolerite in contact with strong alteration band/vein

This is essentially a similar rock to that in the previous sample, but shows a green variant on one side of a quartz-carbonate vein and a brown variant on the other side. The basic rock is texturally similar to that in the previous sample but has a more abundant framework component, and less abundant mesostasis + vesicles. The vesicles, which are up to 4 mm in diameter, have been filled by various proportions of chlorite, carbonate and quartz.

The framework has plagioclase laths from 1 to 4 mm long, rarely to 8 mm long, and totally chloritised ferromagnesian grains but with smaller skeletal opaque oxides to 0.1 mm grainsize. The framework is coarser than in the previous sample but the mesostasis is finer-grained, with networks of generally planar plagioclase microlites to 0.5 mm in diameter. In the green facies, interstitial chlorite is rather more abundant than alkali felspar but in the brown zone most of the material between the plagioclase microlites is alkali felspar.

The brown zone has more abundant, if rather irregularly distributed pyrite than the green zone, with some areas having up to 7% pyrite as cubes about 0.1 mm in size. Pyrite in the green zone is rare (1%) and fine grained, except in small areas adjacent to the median vein, where there are a few grains to 0.1 mm in size.

The veins between these two zones vary in mineralogy both across and along the vein but are essentially composed of quartz and carbonate. There is a trace of pyrite in the vein.

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SELECTED PHOTOMICROGRAPHS

TO ACCOMPANY

REPORT 6764

FOR

C.R.A. EXPLORATION ADELAIDE, S.A.

21/12/94

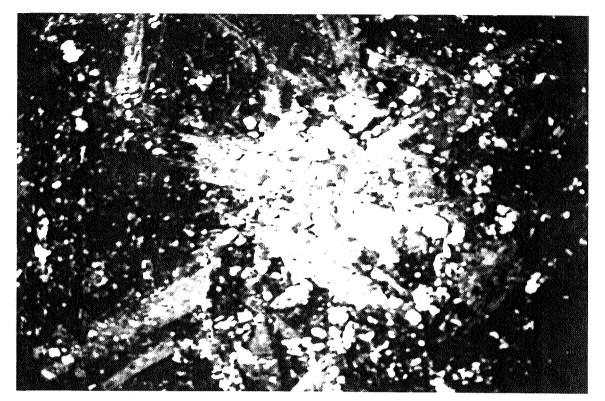


Fig 1 1156565 Scale: 10mm represents 0.32mm

Xnic, basalt, showing unusual cage-like framework of coarse plagioclase laths with patches of sericite and carbonate; with quenched mesostasis in between.

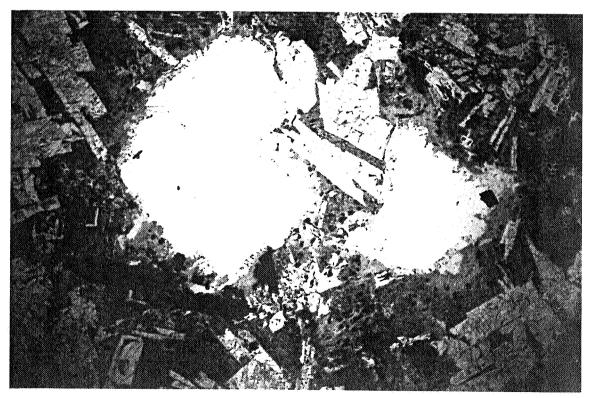


Fig 2 1156565 Scale: 10mm represents 0.32mm

Ordinary light, two "cores" within mesostasis, probably vesicles occupied by quartz + rare carbonate. Some coarser plagioclase laths and opaque oxides also in mesostasis.

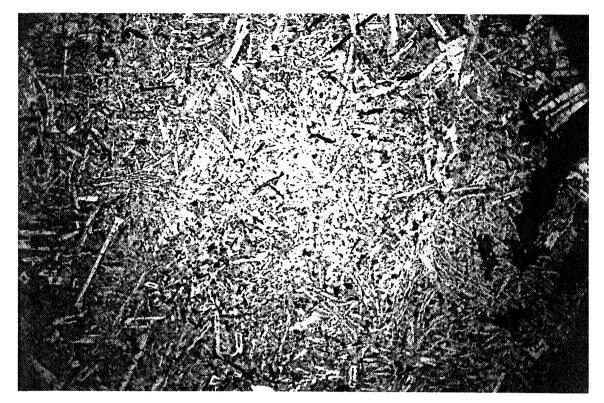


Fig 3 Scale: 10mm represents 0.32mm Ordinary light, mesostasis only, dominated by randomly interlocking plagioclase microlites, some curved and hollow characteristic of rapid quenching.



Fig 4 1156565 Scale: 10mm represents 0.32mm Xnicols equivalent of Fig 3, showing dispersed fine carbonate and sericite.



Fig 5 1156566 Scale: 10mm represents 0.32mm

Ordinary light; similar "bimodal" basalt to 1156565, showing framework coarse plagioclase crystals, enclosing mesostasis here dominated by an area of ultrafine plagioclase microlites, with greenish extremely fine chlorite interstitial (with scattered fine granular opaque oxides).

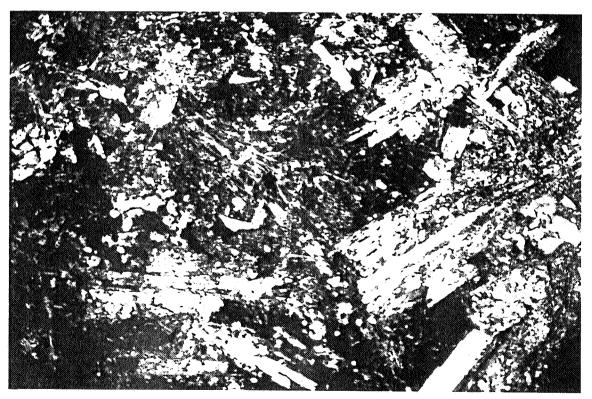


Fig 6 Scale: 10mm represents 0.32mm Xnicols equivalent of Fig 5, showing moderate fine sericitic alteration in coarser plagioclase.



Fig 7 1156566 Scale: 10mm represents 0.32mm

Ordinary light, basically the same textural relationships s in Figs 5 and 6 (same sample), but more brownish material in mesostasis is extremely fine k-spar clouded with iron oxide dust.

END

DEDON

SECOND AND FINAL REPORT FOR EXPLORATION LICENCE 1974 CHARLOTTE WELL, SOUTH AUSTRALIA THE PERIOD ENDING 7TH MAY, 1996

Gairdner SH5315, South Australia

AUTHOR:

S.P. NEWBERY

COPIES TO:

MESA

ET&I BOX HILL CRAE ADELAIDE

DATE:

JUNE, 1996

SUBMITTED BY:

ACCEPTED BY:

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Mines & Energy SA R96/01500





CRA EXPLORATION PTY LIMITED A.C.N. 000 057 125

SUBJECT:

ANNUAL REPORT FOR CHARLOTTE WELL EL 1974,

SOUTH AUSTRALIA, FOR THE PERIOD ENDED 31ST JULY, 1995

AUTHOR:

M.G. BARLOW & W.A. STEWART

DATE:

26TH SEPTEMBER, 1995

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CRAE REPORT NO.: 21098

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3.	CONCLUSIONS AND RECOMMENDATIONS	1
4.	INVESTIGATIONS	1
LOC	CATION	2
KEY	WORDS	2

LIST OF PLANS

Plan No. Title

<u>Scale</u>

SAa 6255

Charlotte Well EL 1974 - S.A. Location plan

1:250 000

1. SUMMARY

EL 1974 was acquired on the 1st August 1994 as part of a programme to evaluate the areas potential for base metal mineralisation.

Exploration during that time has focused upon two main prospect areas namely Pascoe Dam and Pinery Dam. All work pertaining to these prospect areas is contained within previous reports.

A partial relinquishment of the tenement was made on the 11th July 1995.

No additional exploration activities have been completed since that time and the decision has been made to relinquish the remainder of the tenement.

2. INTRODUCTION

EL 1974 was granted on the 1st August 1994 over an area of approximately 2046 square kilometres. The EL location and boundaries are presented in plan SAa 6255.

A partial relinquishment of the tenement to an area of 234 square kilometres was effected on the 11th July 1995.

All previously completed exploration activities are documented in CRAE report 21098.

This report summarises the work completed during the second and final year of tenure.

3. CONCLUSIONS AND RECOMMENDATIONS

On the basis of the results of the initial programmes it was concluded that no additional follow-up work was justified.

The tenement was recommended for relinquishment.

4. INVESTIGATIONS

No exploration activities were completed during the reporting period.

S.P. NEWBERY

SPN/dt Reports#Charlotte Well#1974#ARPT#05/96

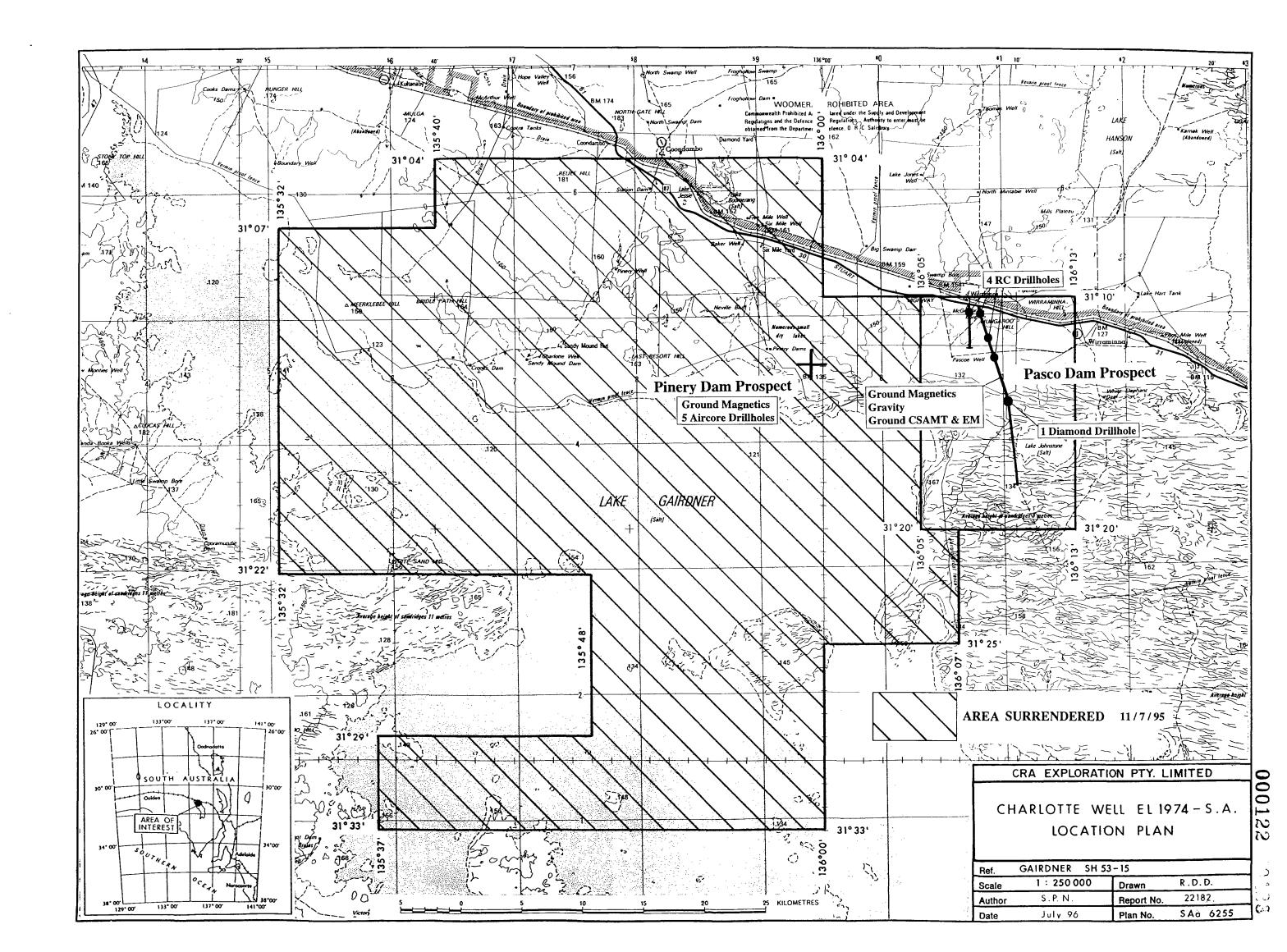
LOCATION

Gairdner

SH53-15 1:250 000 sheet

KEYWORDS

Base Metals, Pinery Dam, Pascoe Dam, Charlotte Well.



END