

SOUTH AUSTRALIA
DEPARTMENT OF MINES AND ENERGY



OPEN FILE ENVELOPE NO. 2674

PEL 5 AND PEL 6, TOOLACHEE BLOCK

EROMANGA AND COOPER BASINS

KIDMAN 1

TEST REPORTS

Submitted by

Delhi International Oil Corporation and Santos Ltd

1989

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SCANNED

ENVELOPE 2674

TENEMENT: PEL 5 and PEL 6, Toolachee Block; Eromanga and Cooper Basins

TENEMENT HOLDER: Delhi International Oil Corporation (operator), Santos Ltd and Vamgas Ltd

CONTENTS OF VOLUME ONE

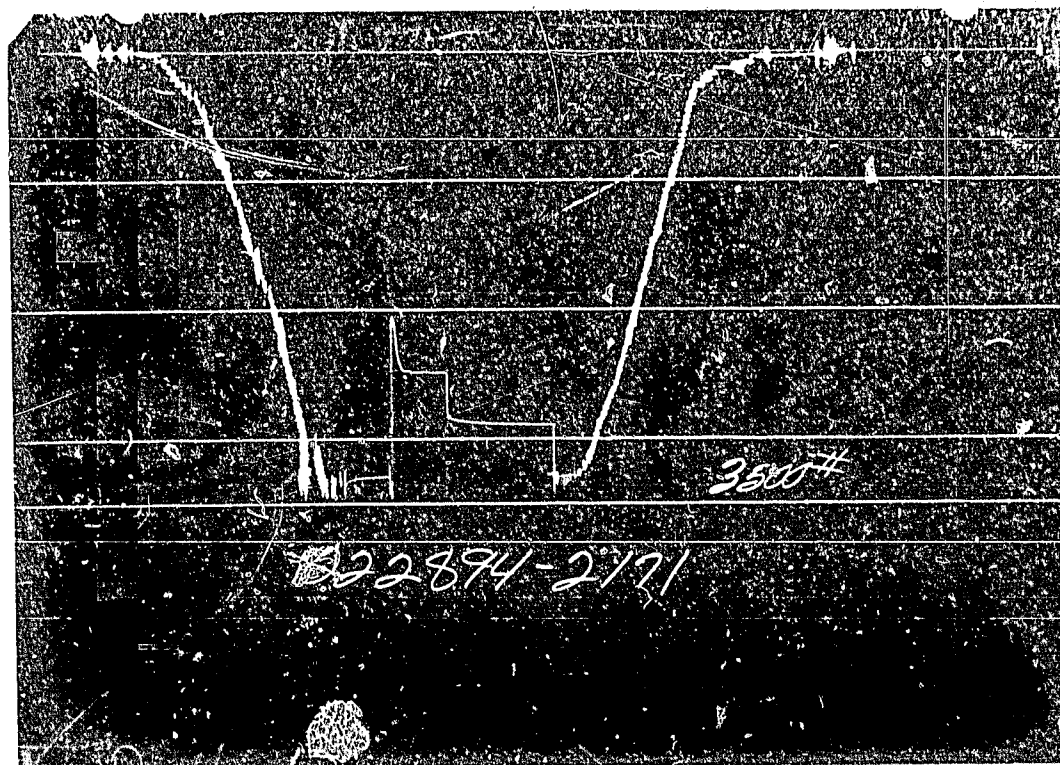
REPORTS:	Halliburton Services, 1977. Formation testing service report - (open hole) DST 2 (2 October 1977).	SADME NO. 2674 R 1 Pgs 3-7
	Halliburton Services, 1977. Formation testing service report - (open hole) DST 2 (10 April 1977).	2674 R 2 Pgs 8-12
	Halliburton Services, 1977. Formation testing service report - (open hole) DST 3 (10 July 1977).	2674 R 3 Pgs 13-17
	Halliburton Services, 1977. Formation testing service report - (open hole) DST 4A (12 October 1977).	2674 R 4 Pgs 18-22
	Pfitzer, L.W., 1977. Well velocity survey report. (Velocity Data Pty Ltd, October 1977).	2674 R 5 Pgs 23-35A
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REPORTS:	Challenger Geological Services, 1977. Core photographs (coloured), cores 1-3.	2674 R 6 Pgs 36-42
	Coment Computer Enterprises Ltd, 1983. Log analysis report.	2674 R 7 Pgs 43-89
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	Computerized log interpretation printouts: run 1 - 7/12/82. run 2 - 19/01/83.	2674-3 2674-4

CONTENTS OF VOLUME TWO

REPORT:	Paspaliaris, T.G., 1984. Reservoir engineering interpretation and results of the pre-production modified isochronal test of the Toolachee Formation gas reservoir perforated intervals 6606-6634 feet and 6673-6692 feet, conducted over the period 15-20 May 1984 (Santos Ltd Reservoir Engineering Department report no. RE: 207/84, dated 6 December 1984).	2674 R 8 Pgs 90-108
APPENDIX A:	Well test summary sheets - field and deliverability calculations.	Pgs 109-124

REPORTS:	Larkin, R., 1986. Results of reservoir pressure buildup and flowing plus static pressure gradient surveys of the Toolachee producing zone conducted over the period 13-19 December 1986 (Expertest Pty Ltd).	SADME NO. 2674 R 9 Pgs 125-143
	Saunders, M., 1987. Results of reservoir pressure buildup and static pressure gradient surveys of the Toolachee producing zone conducted over the period 12-16 May 1987 (Expertest Pty Ltd).	2674 R 10 Pgs 144-161
	Halliburton Services 1988. Formation testing service report - (cased hole) DST 1 (11 January 1988).	2674 R 11 Pgs 162-172
	Smith, A., 1988. Results of 96 hour reservoir pressure buildup and static pressure gradient surveys of the Toolachee producing zone conducted over the period 27 July - 1 August 1988 (Expertest Ltd).	2674 R 12 Pgs 173-187
	Smith, A., 1989. Results of reservoir pressure buildup and static pressure gradient surveys of the Toolachee producing zone conducted over the period 8-14 September 1989 (Expertest Ltd).	2674 R 13 Pgs 188-199

END OF CONTENTS



Each Horizontal Line Equal to 1000 p.s.i.

000 x

FLUID SAMPLE DATA				Date	Ticket Number	
Sampler Pressure _____ P.S.I.G. at Surface Recovery: Cu. Ft. Gas _____ cc. Oil _____ cc. Water _____ cc. Mud _____ Tot. Liquid cc. _____ Gravity _____ ° API @ _____ °F. Gas/Oil Ratio _____ cu. ft./bbl. RESISTIVITY CHLORIDE CONTENT				Kind of Job Tester Drilling Contractor Formation Tested Elevation Net Productive Interval All Depths Measured From Total Depth Main Hole/Casing Size Drill Collar Length Drill Pipe Length Packer Depth(s) Depth Tester Valve	10-2-77 022894 OPEN HOLE TEST W. H. LOVELL O D & E DRILLING COMPANY #6 TH EQUIPMENT & HOLE DATA S Toolachee 227' 29.6' Kelly Bushing 6622' 8 1/2" 437.47' I.D. 2.375" 6127.05' I.D. 3.826" 6578' 6522.25'	
Mud Weight 9.7 vis 43 sec TYPE AMOUNT Cushman _____ Ft. Depth Back Pres. Valve _____ Surface Choke 1/2" Bottom Choke .75"				Mud Weight _____ vis _____ sec TYPE AMOUNT Cushman _____ Ft. Depth Back Pres. Valve _____ Surface Choke _____ Bottom Choke _____		
Recovered 232 Feet of condensate. Recovered 29 Feet of water. Recovered _____ Feet of _____ Recovered _____ Feet of _____ Recovered _____ Feet of _____ Recovered _____ Feet of _____ Remarks See Production Test Data Sheet . . .				Recovered _____ Feet of _____ Recovered _____ Feet of _____ Recovered _____ Feet of _____ Recovered _____ Feet of _____ Remarks See Production Test Data Sheet . . .		
TEMPERATURE Gauge No. 2170 Gauge No. 2171 Gauge No. _____ TIME Depth: 6564.25 Ft. Depth: 6619 Ft. Depth: _____ Hour Clock Est. _____ °F. Blanked Off NO Blanked Off YES Blanked Off _____ Hour Clock Actual 238 °F. Pressures Pressures Pressures Field Office Field Office Field Office Initial Hydrostatic 3425 3261 3444 3286 Flow - Initial 2079 1920 2201 2061 Final 2582 2430 2627 2489 Closed in 3020 2877 3035 2887 Second Period Flow Initial _____ Final _____ Closed in _____ Third Period Flow Initial _____ Final _____ Closed in _____ Final Hydrostatic 3425 3259 3444 3281				Tool Opened 1036 A.M. Opened _____ A.M. Bypass 1421 P.M. Reported Minutes Computed Minutes _____ 75 75 150 150		

FORM 151-R2—PRINTED IN U.S.A.

FORMATION TEST DATA

LIFE SIZE 102548 BM 9/78

KIDMAN		65781 - 66221		DELHI INTERNATIONAL OIL CORPORATION	
Lease Name	Well No. 1	Test No. 1	Leased Interval	Lease Owner/Company Name	
Field				State	SOUTH AUSTRALIA

DELHI INTERNATIONAL OIL CORPORATION

0005

Casing perf.		Bot. om choke		Gas		Surf. temp.		Ticket No.	
		.75"				113 °F		022894	
Gas gravity		Oil gravity		GOR					
Spec. gravity		Chlorides		ppm		Res.		@ °F	
INDICATE TYPE AND SIZE OF GAS MEASURING DEVICE USED									
Date	a.m.	Choke	Surface	Gas	Liquid	Remarks			
Time	p.m.	Size	Pressure	Rate	Rate				
			psi	MCF	BPD				
0330						Started to pick up tools.			
0930						Tools on bottom.			
						Made up surface equipment.			
1035						Set weight on tools.			
1036		1/2				Hydrospring opened with a good blow.			
1037		"				Gas to surface.			
1040		"	700	3,838		Cleaned up rathole mud.			
1045		"	1000	5,448		"			
1050		"	1800	9,742		"			
1055		"	1800	9,742		"			
1100		"	"	"		"			
1105		"	"	"		"			
1110		"	"	"		"			
1115		"	"	"		"			
1120		"	"	"		"			
1125		"	"	"		"			
1130		"	"	"		"			
1135		"	"	"		"			
1140		"	"	"		"			
1145		"	"	"		"			
1150		"	"	"		"			
1151		"	"	"		Closed tool.			
1421						Opened bypass and unseated tools.			
						Closed tester valve.			
1845						Tools out of hole.			

Gauge No. 2170					Depth 6564.25		Clock No. 6719			24 hour		Ticket No. 022894			
First Flow Period			First Closed In Pressure			Second Flow Period		Second Closed In Pressure			Third Flow Period		Third Closed In Pressure		
	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.
0	.0000	1920	.0000		2430										
1	.0514*	2396	.0342		2836										
2	.0925	2430	.0685		2847										
3	.1336	2424	.1028		2854										
4	.1748	2425	.1370		2859										
5	.2153	2427	.1713		2862										
6	.2570	2430	.2056		2865										
7			.2398		2867										
8			.2741		2869										
9			.3083		2872										
10			.3426		2872										
11			.3769		2873										
12			.4111		2873										
13			.4454		2875										
14			.4796		2875										
15			.5140		2877										

Gauge No. 2171					Depth 6619		Clock No. 8083			24 hour	
	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	
0	.0000	2061	.0000		2489						
1	.0512*	2459	.0339		2849						
2	.0921	2485	.0677		2859						
3	.1331	2482	.1016		2866						
4	.1740	2482	.1354		2871						
5	.2150	2484	.1693		2874						
6	.2560	2489	.2032		2877						
7			.2370		2879						
8			.2709		2881						
9			.3047		2882						
10			.3386		2884						
11			.3725		2884						
12			.4063		2886						
13			.4402		2886						
14			.4740		2887						
15			.5080		2887						

Reading Interval 12 10

REMARKS: * - first interval is equal to 15 minutes.

SPECIAL PRESSURE DATA

TICKET NO. 022894

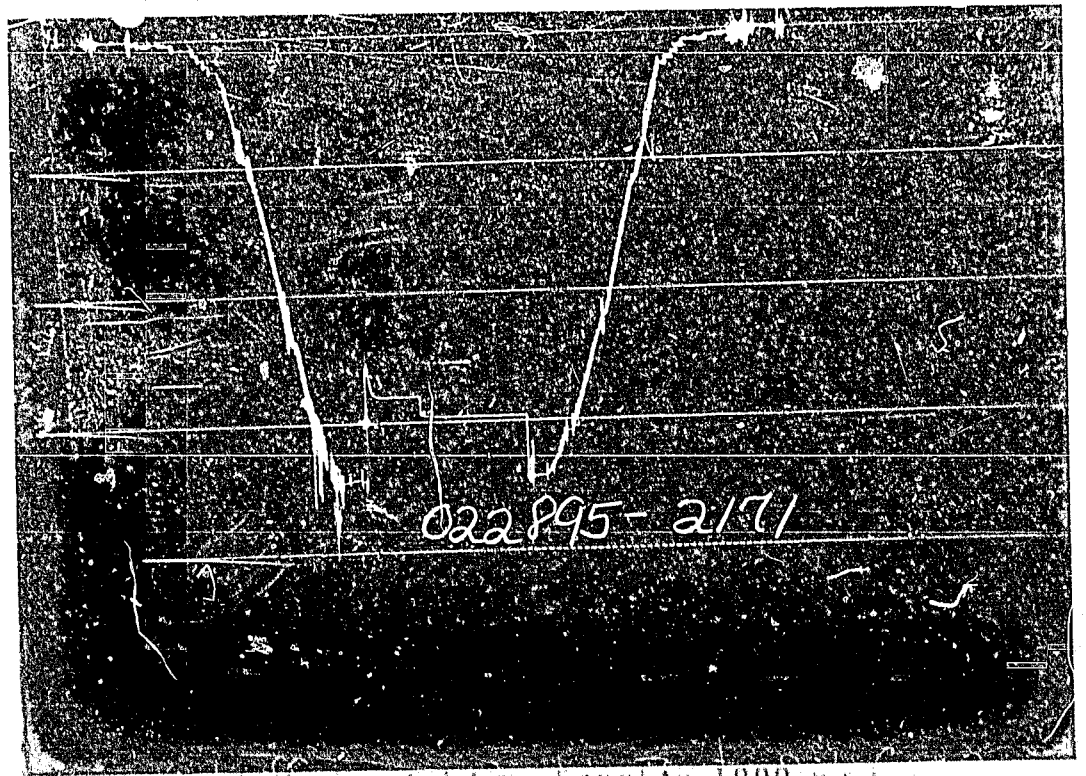
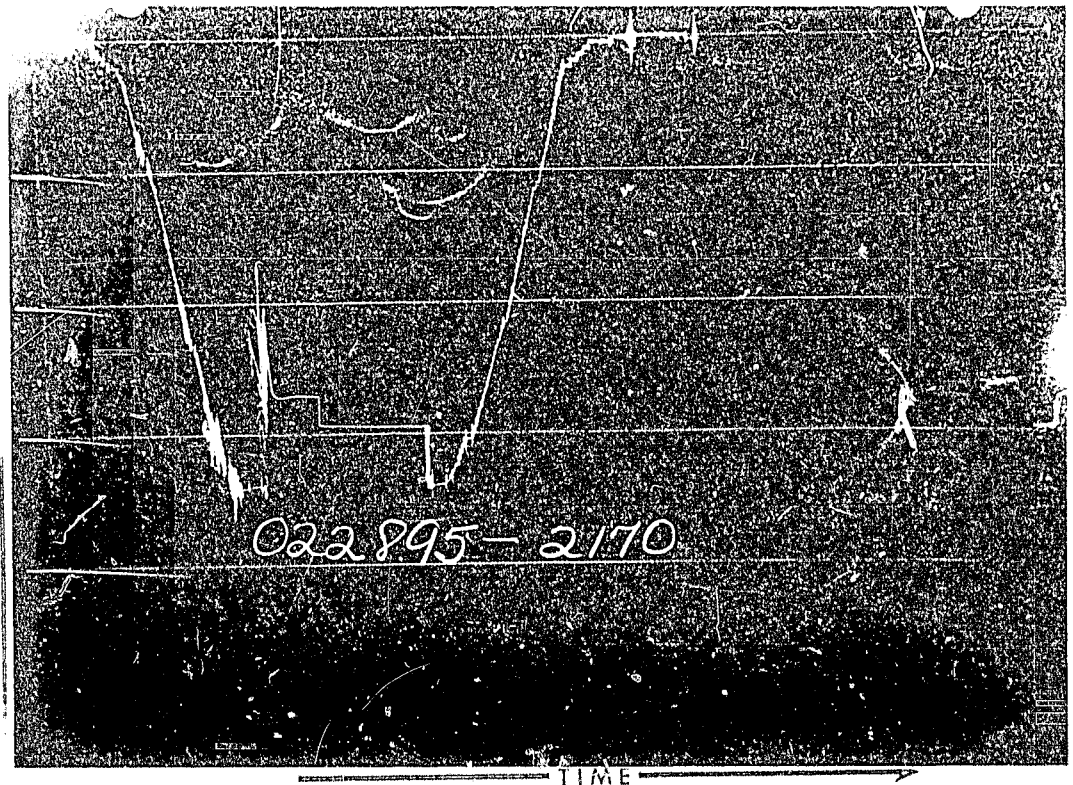
0007

	O. D.	I. D.	LENGTH	DEPTH
Drill Pipe or Tubing				
Reversing Sub	6"	3"	1'	
Water Cushion Valve				
Drill Pipe	4 1/2"	3.826"	6127.05'	
Drill Collars	6.50"	2.375"	437.47'	
Handling Sub & Choke Assembly	5.87"	2.58"	2.65'	
Dual CIP Valve	5"	.87"	4'	
XXXXXX-XXXXXX X OVER	5.75"	2.50"	.65'	
Hydro-Spring Tester	5"	.75"	5'	6522.25'
X OVER	5.75"	2.75"	.75'	
Multiple CIP Sampler				
Extension Joint				
AP Running Case	5"	2.25"	4.10'	6564.25'
Hydraulic Jar	5"	1"	3.25'	
VR Safety Joint	5"	1"	2.35'	
Pressure Equalizing Crossover				
Packer Assembly	7.75"	1.75"	6.15'	6578'
Distributor				
Packer Assembly				
Flush Joint Anchor	5"	2.37"	39'	
Pressure Equalizing Tube				
Blanked-Off B.T. Running Case				
Drill Collars				
Anchor Pipe Safety Joint				
Packer Assembly				
Distributor				
Packer Assembly				
Anchor Pipe Safety Joint				
Side Wall Anchor				
Drill Collars				
Flush Joint Anchor				
Blanked-Off B.T. Running Case	5"	2.44"	4'	6619'
Total Depth				6622'

FORM 107-R1-PRINTED IN U.S.A.

EQUIPMENT DATA

LITTLE'S PATENT 752



Each Horizontal Line Equal To 1000 psi.

0010

Casing perf. _____		Bottom choke .75"		Gas Surf. temp. 114 °F		Ticket No. 022895	
Gas gravity _____		Oil gravity _____		GOR _____			
Spec. gravity _____		Chlorides _____		ppm Res. _____		@ _____ °F	
INDICATE TYPE AND SIZE OF GAS MEASURING DEVICE USED _____							
Date 4-10-77 Time a.m. p.m.	Choke Size	Surface Pressure psi	Gas Rate MCF	Liquid Rate BPD	Remarks		
0030					Started to make up tools.		
0630					Tools on bottom.		
					Made up surface equipment.		
0713					Set weight on tools.		
0714	1/2				Opened tool with a good blow.		
0714	"				Gas to surface.		
0715	"	400	2,228				
0720	"	1350	7,327				
0725	"	1975	10,682		Cleaning up		
0730	"	2050	11,084		Rat hole mud.		
0735	"	"	"				
0740	"	"	"				
0745	"	"	"				
0750	"	"	"				
0755	"	"	"				
0800	"	"	"				
0805	"	"	"				
0810	"	"	"				
0815	"	"	"				
0820	"	"	"				
0825	"	"	"				
0830	"	"	"				
1100					Opened bypass. Closed tool.		
1107					Pulled packers loose.		
1530					Tools out of the hole.		

Gauge No. 2170				Depth 5695		Clock No. 6719			24 hour		Ticket No. 022895				
First Flow Period			First Closed In Pressure			Second Flow Period		Second Closed In Pressure			Third Flow Period		Third Closed In Pressure		
	Time Defl. ".000"	PSIG Temp. Corr.	Time Defl. ".000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. ".000"	PSIG Temp. Corr.	Time Defl. ".000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. ".000"	PSIG Temp. Corr.	Time Defl. ".000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.
0	.0000	2252-0	.0000		2715										
1	.0371*	2688	.0102		2935										
2	.0808	2725	.0204	-	2937										
3	.1246	2714	.0307	-	2939										
4	.1684	2710	.0409	-	2939										
5	.2123	2712	.0511		2940										
6	.2560	2715	.0613		2940										
7			.0715		2940										
8			.0818		2942										
9			.0920		2942										
10			.1022		2943										
11			.1840		2945										
12			.2657		2947										
13			.3475		2948										
14			.4292		2948										
15			.5110		2950										

Gauge No. 2171				Depth 6771		Clock No. 8083			24 hour						
	Time Defl. ".000"	PSIG Temp. Corr.	Time Defl. ".000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. ".000"	PSIG Temp. Corr.	Time Defl. ".000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. ".000"	PSIG Temp. Corr.	Time Defl. ".000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.
0	.0000	2542	.0000		2806										
1	.0369*	2788	.0101		2953										
2	.0805	2809	.0203		2956										
3	.1241	2804	.0304		2959										
4	.1677	2804	.0406		2961										
5	.2113	2804	.0507		2961										
6	.2550	2806	.0608		2962										
7			.0710		2962										
8			.0811		2962										
9			.0913		2962										
10			.1014		2964										
11			.1825		2966										
12			.2636		2966										
13			.3443		2966										
14			.4259		2967										
15			.5070		2967										

Reading Interval 13 ** Minutes

REMARKS: * INTERVAL = 11 MINUTES ** FIRST TEN INTERVALS = 3 MINUTES EACH; LAST FIVE INTERVALS = 24 MINUTES EACH

Q = QUESTIONABLE

TICKET NO. 022895

0012

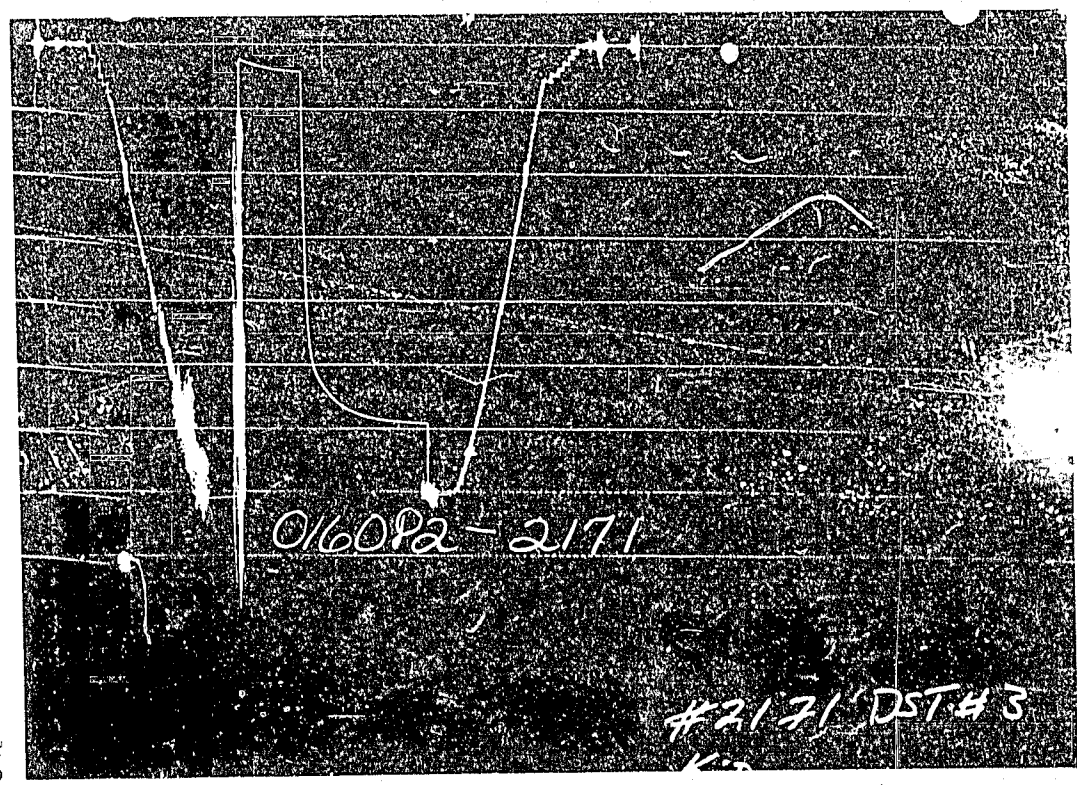
	O. D.	I. D.	LENGTH	DEPTH
Drill Pipe or Tubing				
Reversing Sub	6"	3"	1'	
Water Cushion Valve				
Drill Pipe	4.50"	3.826"	6275'	
Drill Collars	6.50"	2.3750"	408.40'	
Handling Sub & Choke Assembly	5.75"	2.50"	.65' X OVER	
Dual CIP Valve	5.75"	2.75"	.75' X OVER	
Dual CIP Sampler	5.87"	2.58"	2.65' HANDLING SUB & CHOKE	
Hydro-Spring Tester	5.00"	.75"	5'	6693.45'
	5"	.87"	4' DUAL CIP VALVE	
Multiple CIP Sampler				
Extension Joint				
AP Running Case	5"	2.25"	4.10'	6695.45
Hydraulic Jar	5"	1"	3.25'	
VR Safety Joint	5"	1"	2.35'	
Pressure Equilizing Crossover				
Packer Assembly	7.75"	1.75"	6.15'	6709.20
Distributor				
Packer Assembly				
Flush Joint Anchor				
Pressure Equilizing Tube				
Blanked-Off B.T. Running Case				
Drill Collars	5"	1.50"	4'	
Anchor Pipe Safety Joint				
Packer Assembly				
Distributor				
Packer Assembly				
Anchor Pipe Safety Joint				
Side Wall Anchor	5.75"	2.75"	.75' X OVER	
Drill Collars	6.50"	2.375"	29.07	
	5.75"	2"	.70' X OVER	
Flush Joint Anchor	5.00"	2.37"	25'	
Blanked-Off B.T. Running Case	5"	2.44"	4'	6771'
Total Depth				6774'

FORM 107-R-1-PRINTED IN U.S.A.

EQUIPMENT DATA

LITTLE'S PATENT 7-12-74

8



Each Horizontal Line Equal to 1000 psi

[illegible]

0015

[illegible]

Gauge No. 2171					Depth 5960		Clock No. 6789			24 hour		Ticket No. 016082			
First Flow Period			First Closed In Pressure			Second Flow Period		Second Closed In Pressure			Third Flow Period		Third Closed In Pressure		
	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.
0	.0000	119	.0000		215										
1	.0507	149	.0473*		2405										
2	.1013	170	.0878		2631										
3	.1520	186	.1284		2729										
4	.2026	200	.1689		2799										
5	.2533	208	.2095		2848										
6	.3040	215	.2500		2881										
7			.2905		2905										
8			.3311		2922										
9			.3716		2935										
10			.4122		2944										
11			.4527		2951										
12			.4932		2956										
13			.5338		2959										
14			.5743		2962										
15			.6150		2964										

Gauge No. 2170					Depth 7071		Clock No. 8083			24 hour		
	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.
0	.0000	170	.0000		255							
1	.0507	193	.0475*		2466							
2	.1013	212	.0881		2659							
3	.1520	230	.1288		2758							
4	.2026	243	.1695		2828							
5	.2533	248	.2102		2873							
6	.3040	255	.2509		2907							
7			.2915		2933							
8			.3322		2953							
9			.3729		2972							
10			.4136		2982							
11			.4543		2989							
12			.4949		2994							
13			.5356		2997							
14			.5763		3000							
15			.6170		3003							

Reading Interval 15 12 Minutes

REMARKS: * 14 MINUTES

TICKET NO. 016082

0017

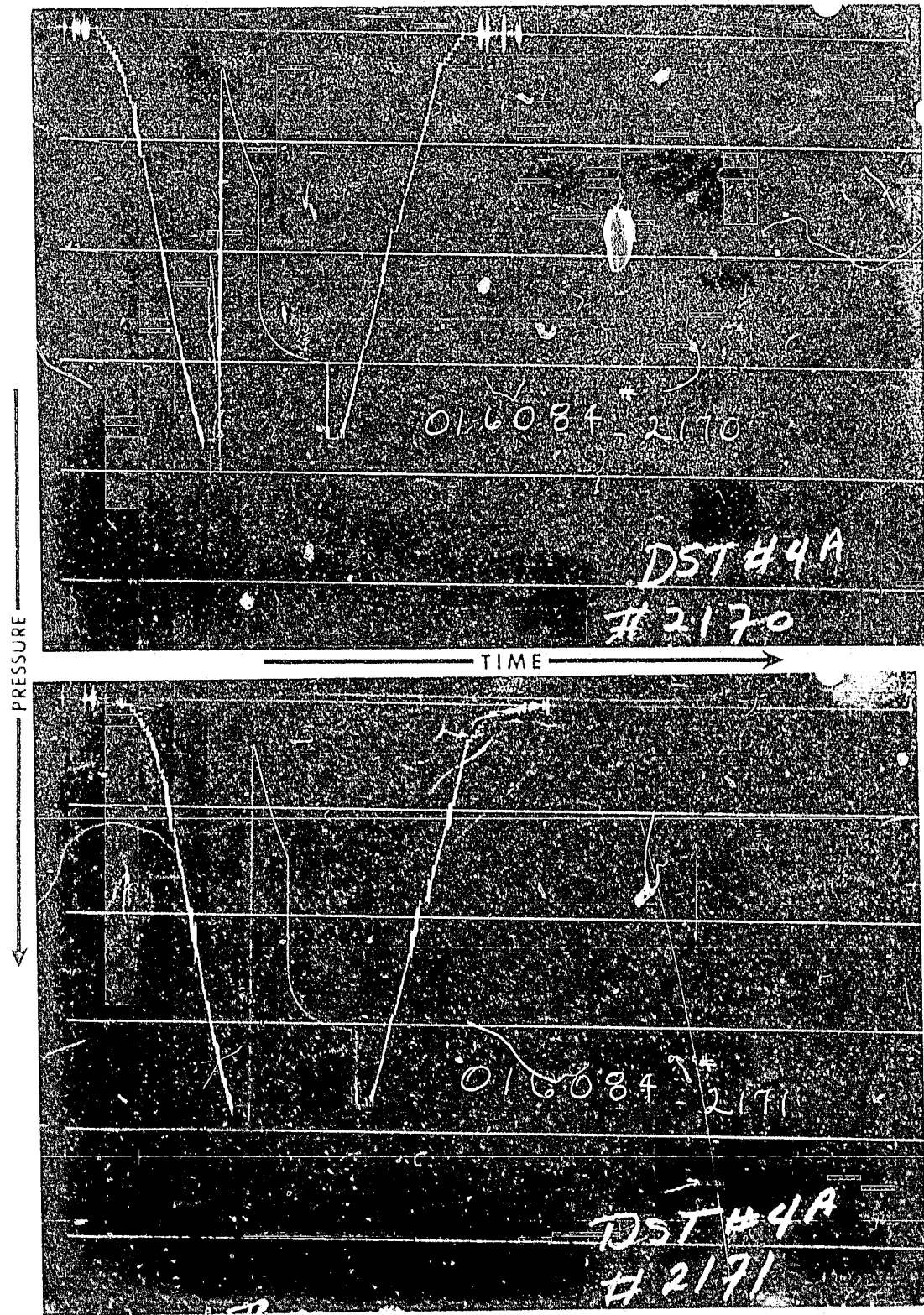
	O. D.	I. D.	LENGTH	DEPTH
Drill Pipe or Tubing				
Reversing Sub	6"		1'	
Water Cushion Valve				
Drill Pipe	4.50"	3.826"	6377'	
Drill Collars		2 13/16"	570'	
Handling Sub & Choke Assembly				
Dual CIP Valve	5"	.87"	4'	
Dual CIP Sampler				
Hydro-Spring Tester	5"	.87"	5'	6955'
Multiple CIP Sampler				
Extension Joint				
AP Running Case	5"		4.10'	6960'
Hydraulic Jar	5"	.75"	3.33'	
VR Safety Joint	5"	.75"	2.50'	
Pressure Equalizing Crossover				
Packer Assembly	7.75"		6'	6974'
Distributor				
Packer Assembly				
Flush Joint Anchor				
Pressure Equalizing Tube				
Blanked-Off B.T. Running Case				
Drill Collars				
Anchor Pipe Safety Joint	5"		4'	
Packer Assembly				
Distributor				
Packer Assembly				
Anchor Pipe Safety Joint				
Side Wall Anchor Flush Jt. Anchor	5"		30'	
Drill Collars	6.25"		58.75'	
Flush Joint Anchor				
Blanked-Off B.T. Running Case	5"		4'	7071'
Total Depth				7075'

FORM 187-R1-PRINTED IN U.S.A.

EQUIPMENT DATA

LITTLE'S PATENT TOOL

8



Each Horizontal Line Equal to 1000 p.s.i.

0020

[illegible]

FORM 102-R1--PRINTED IN U.S.A.

PRODUCTION TEST DATA

LITTLE'S 96672 SM 8/74

Gauge No.		2170		Depth		7252'		Clock No.		6719		24 hour		015084	
First Flow Period			First Closed In Pressure			Second Flow Period		Second Closed In Pressure			Third Flow Period		Third Closed In Pressure		
	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.
0	.000	392	.000		1404										
1	.0373	549*	.0269		2623										
2	.0713	775	.0537		2724										
3	.1052	968	.0806		2786										
4	.1391	1130	.1075		2833										
5	.1731	1274	.1343		2870										
6	.2070	1404	.1612		2898										
7			.1881		2919										
8			.2149		2938										
9			.2418		2953										
10			.2687		2964										
11			.2955		2976										
12			.3224		2985										
13			.3493		2992										
14			.3761		2998										
15			.4030		3005										

Gauge No.		2171		Depth		7353'		Clock No.		8053		24 hour	
0	.000	470	.000		1464								
1	.0373	626*	.0269		2683								
2	.0713	844	.0539		2781								
3	.1052	1026	.0808		2846								
4	.1391	1187	.1077		2892								
5	.1731	1332	.1347		2930								
6	.2070	1464	.1616		2958								
7			.1885		2979								
8			.2155		2997								
9			.2424		3010								
10			.2693		3023								
11			.2963		3033								
12			.3232		3041								
13			.3501		3051								
14			.3771		3057								
15			.4040		3064								

Reading Interval TO 8

REMARKS: * INTERVAL = 11 MINUTES.

SPECIAL PRESSURE DATA

TICKET NO. 016084

0022

	O. D.	I. D.	LENGTH	DEPTH
Drill Pipe or Tubing	6"		1.00'	
Reversing Sub				
Water Cushion Valve				
Drill Pipe	4 1/2"	3.826"	6569'	
Drill Collars		2 13/16"	570'	
Handling Sub & Choke Assembly	5"	.87"	4.00'	
Dual CIP Valve				
Dual CIP Sampler	5"	.87"	5.00'	7247'
Hydro-Spring Tester				
Multiple CIP Sampler				
Extension Joint				
AP Running Case	5"		4.10'	7252'
Hydraulic Jar	5"	.75"	3.33'	
VR Safety Joint	5"	.75"	2.50'	
Pressure Equalizing Crossover				
Packer Assembly	7.75"		6.00'	7266'
Distributor				
Packer Assembly				
Flush Joint Anchor				
Pressure Equalizing Tube				
Blanked-Off B.T. Running Case				
Drill Collars	5"		4.00'	
Anchor Pipe Safety Joint				
Packer Assembly				
Distributor				
Packer Assembly				
Anchor Pipe Safety Joint				
FLUSH JOINT ANCHOR				
Side Wall Anchor	5"		30.00'	
Drill Collars	6.25"	2 13/16"	58.75'	
Flush Joint Anchor				
Blanked-Off B.T. Running Case	5"		4.00'	7363'
Total Depth				7367'

FORM 137-R-1-PRINTED IN U.S.A.

EQUIPMENT DATA

LITTLE'S 016084 7367' 8/4

WELL VELOCITY SURVEY

KIDMAN NO. 1

P.E.L. 5 & 6

South Australia

for

DELHI INTERNATIONAL OIL CORPORATION

by

VELOCITY DATA PTY. LTD.

Brisbane, Australia

October, 1977

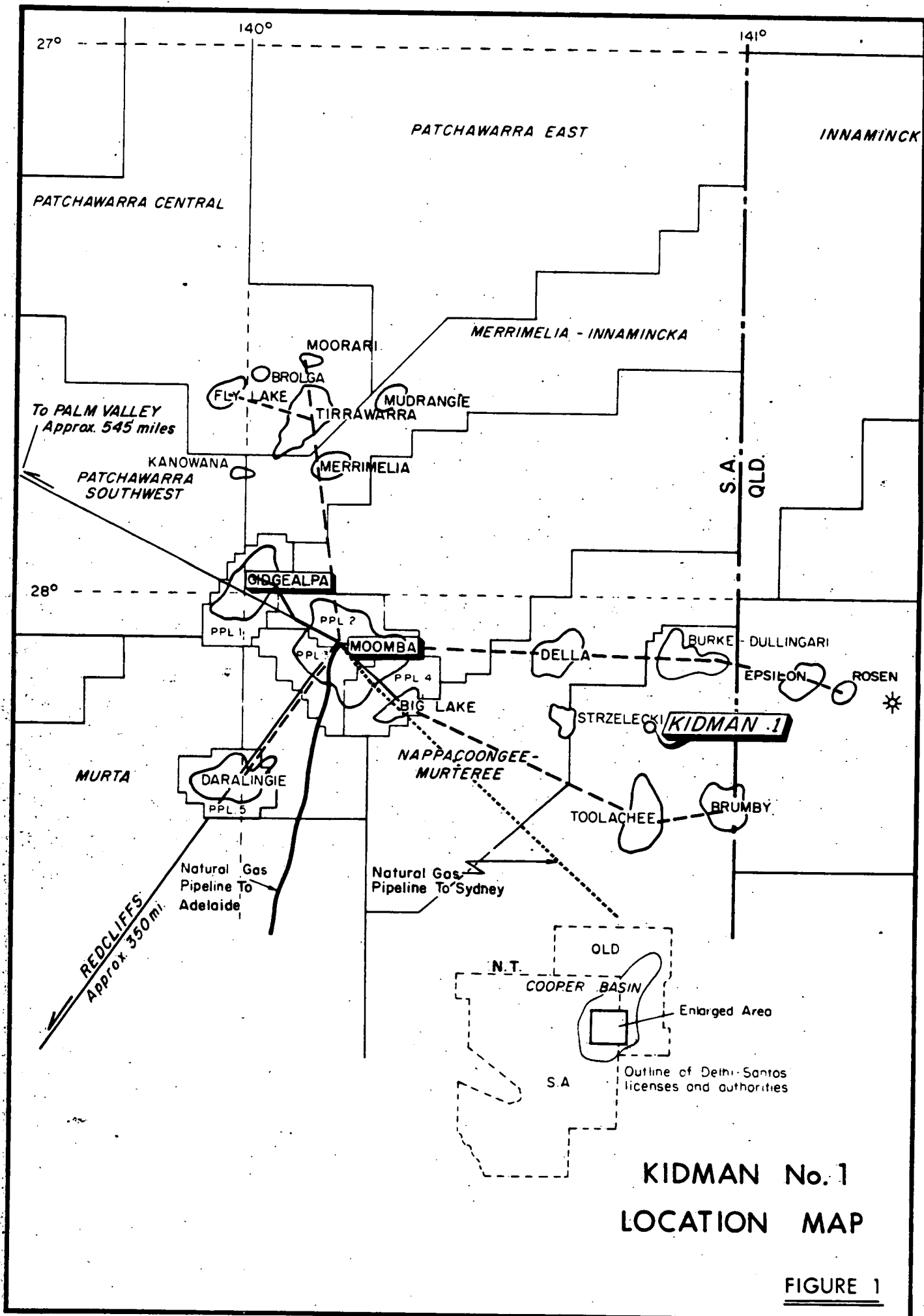
SCANNED

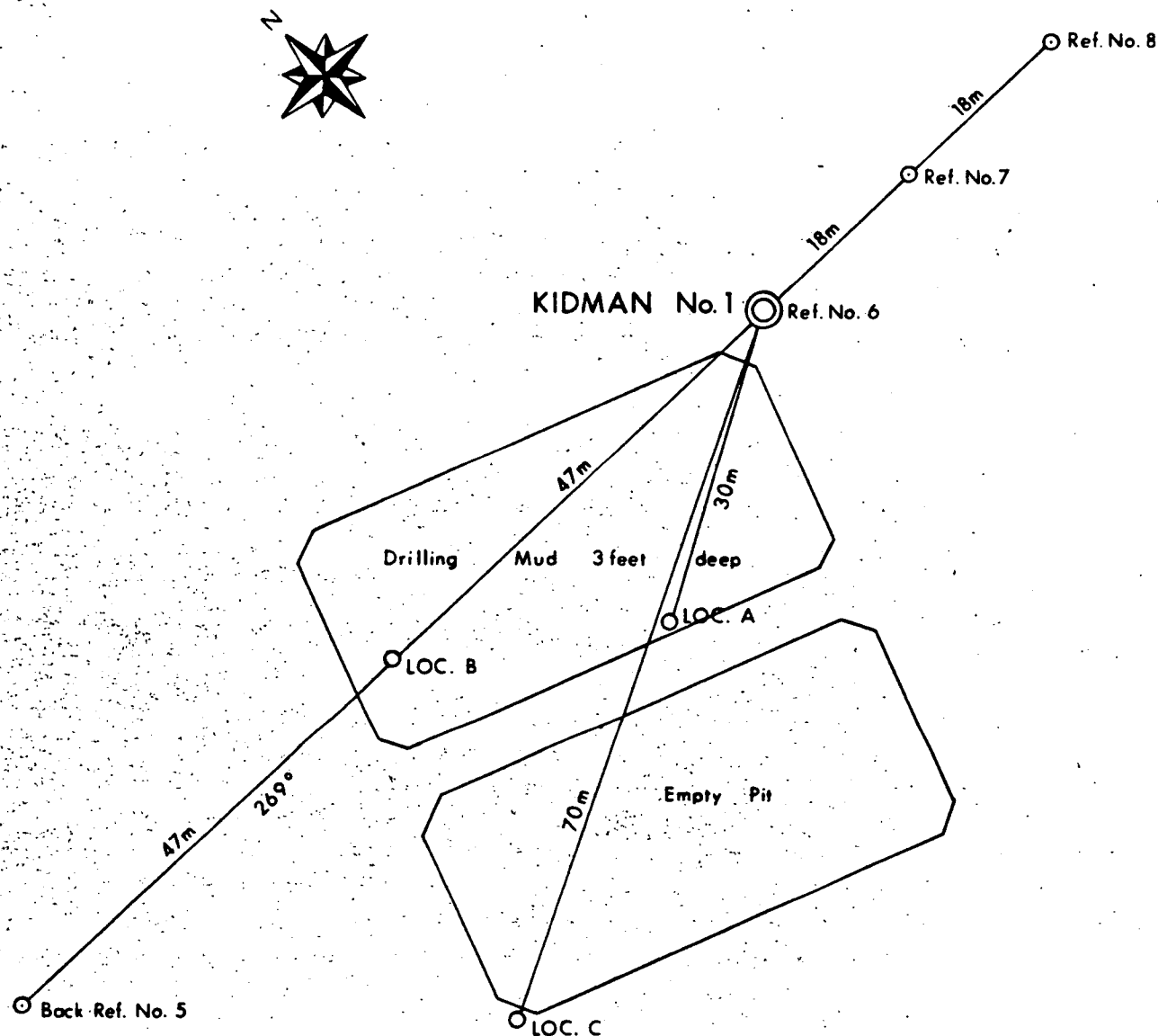
INDEX

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GENERAL COMMENTS	1
EQUIPMENT	2
RECORDING	2
COMPUTATIONS	3
COMPUTATION SHEETS	

Figures:

Figure 1	Location map
Figure 2	Shot location sketch
Figure 3	Time-depth curve and velocity functions
Pocket 1	Time-depth, average velocities and interval velocity curves
	Sample records





KIDMAN No. 1
SHOT LOCATION SKETCH

Scale: 1" = 16m

SUMMARY

Velocity Data Pty. Ltd. conducted a velocity survey for Delhi International Oil Corporation in the Kidman No. 1 well, P.E.L.5 and 6, South Australia. The date of the survey was October 17, 1977.

Twenty-two shots were taken at 17 levels in the well. Record quality was fair and the results considered to be reliable. Dynamite was the energy source with 2½ pounds being fired at a depth of 5 ft in the mud pit.

The survey has been used to calibrate the sonic logs. A calculated velocity functions of $V = 5920 + .822$ to the Transition Beds and a constant velocity of $V = 12800'$ /sec. below, fit the time-depth curve closely.

The well was surveyed to a depth of 7583 ft below K.B.

GENERAL

Velocity Data Pty. Ltd. of Brisbane, Australia, conducted a velocity survey for Delhi International Oil Corporation on October 17, 1977.

Two men and the equipment travelled from Brisbane by air charter.

Name of Well	:	Kidman No. 1
Location	:	P.E.L. 5 & 6, South Australia
Co-ordinates	:	Lat. $28^{\circ} 14' 23''$ S. Long. $140^{\circ} 49' 27''$ E.
Date of Survey	:	October 17, 1977
Elevation of K.B.	:	241' ASL.
Logging	:	Schlumberger
Weather	:	Overcast, light wind
Duration of Survey	:	Three hours twenty minutes
Total Depth of Well	:	7732 ft below K.B.
Casing Depth	:	1267 ft below K.B.
Operator	:	W. J. Larsen

EQUIPMENT

Energy Source : Dynamite
Recording Instruments : S.I.E. RS-4A
Downhole Geophone : Geospace WLS-1000 wall-lock geophone
Reference Phones : Hall Sears HSI

RECORDING

Charge size : 2½ lbs
Depth of shots : 5 ft
Shot offset : 154 ft
Reference sensor offset : Refer Figure 2

Downhole sensor:

6 HSI 4.5 Hz - 215 ohm high temperature detectors in series-parallel

Frequency response 8 - 300 Hz within 3 db

Preamplifier - 48 db fixed gain

Frequency response 5 - 200 Hz within 3 db.

Record Traces:

- 1 Well geophone - high gain
- 2 Well geophone)
) medium gains
- 3 Well geophone)
- 4 Well geophone - low gain
- 5 Reference phone (Back) 322 ft offset
- 6 Well head reference phone
- 7 Forward reference phone 59' offset
- 8 Forward reference phone 118' offset
- 9 Time break
- 10 100 Hz timing standard

Records were produced photographically. Quality was fair.

COMPUTING

Record times were corrected to a mean sea level datum. Three shots were taken at datum at varying offset distances. Two of these shots have been averaged to give a time, shot to datum, of .049 seconds. The long offset shot indicated a discrepancy of .005 seconds and has not been used. Elsewhere times have been averaged where more than one shot was taken at a level, an exception being shot 8, at total depth, because of its doubtful quality.

The sonic log intervals indicate that shot 21 at the 2600 ft level is possibly in error. Since some difficulty was experienced in locking the down-hole tool at this level, this shot has not been used in the calculations.

Sonic logs were calibrated using the check-shot depth at 1275 ft as datum - this being the start of the sonic log.

Discrepancies between sonic interval times and check-shot times were generally small, and, over some short check-shot intervals, below the limit of accuracy in picking record times.

The largest discrepancy - over the 3307-3800 ft interval was .006 seconds.

Sonic times were adjusted to check-shot times using two methods.

Where check-shot interval times were longer than equivalent sonic times, errors were assumed to be instrumental and adjusted using a linear correction -

$$\frac{(t_L - t_R)_2 - (t_L - t_R)_1}{Z_2 - Z_1} = \text{corrections in } \mu \text{ secs/ft}$$

Where check-shots indicated higher interval velocities, it was assumed that sonic errors occurred from caving or mud cake and a differential correction was applied -

$$\frac{t_{R_2} - t_{R_1}}{t_{L_2} - t_{L_1}} \quad \begin{array}{l} \text{where } t_L = \text{sonic log time} \\ t_R = \text{record time} \\ \text{and } Z_2 - Z_1 = \text{depth interval} \end{array}$$

Calibration points on the sonic logs were selected where changes in velocity were noted on the log in addition to the check-shot levels.

A velocity function of $V = 5920 + .82Z$ was calculated using the Miller method. Except for the 2600 check-shot, this results in a good fit down to the Transition. Below the Transition a constant velocity of 12800 ft/sec. is best suited. (Refer Figure 3.) Time-depth, velocity curves and reproductions of sample records at each level are furnished with this report.

Respectfully submitted,



L. W. PFITZNER

Computation Sheet

0030

Check Shot

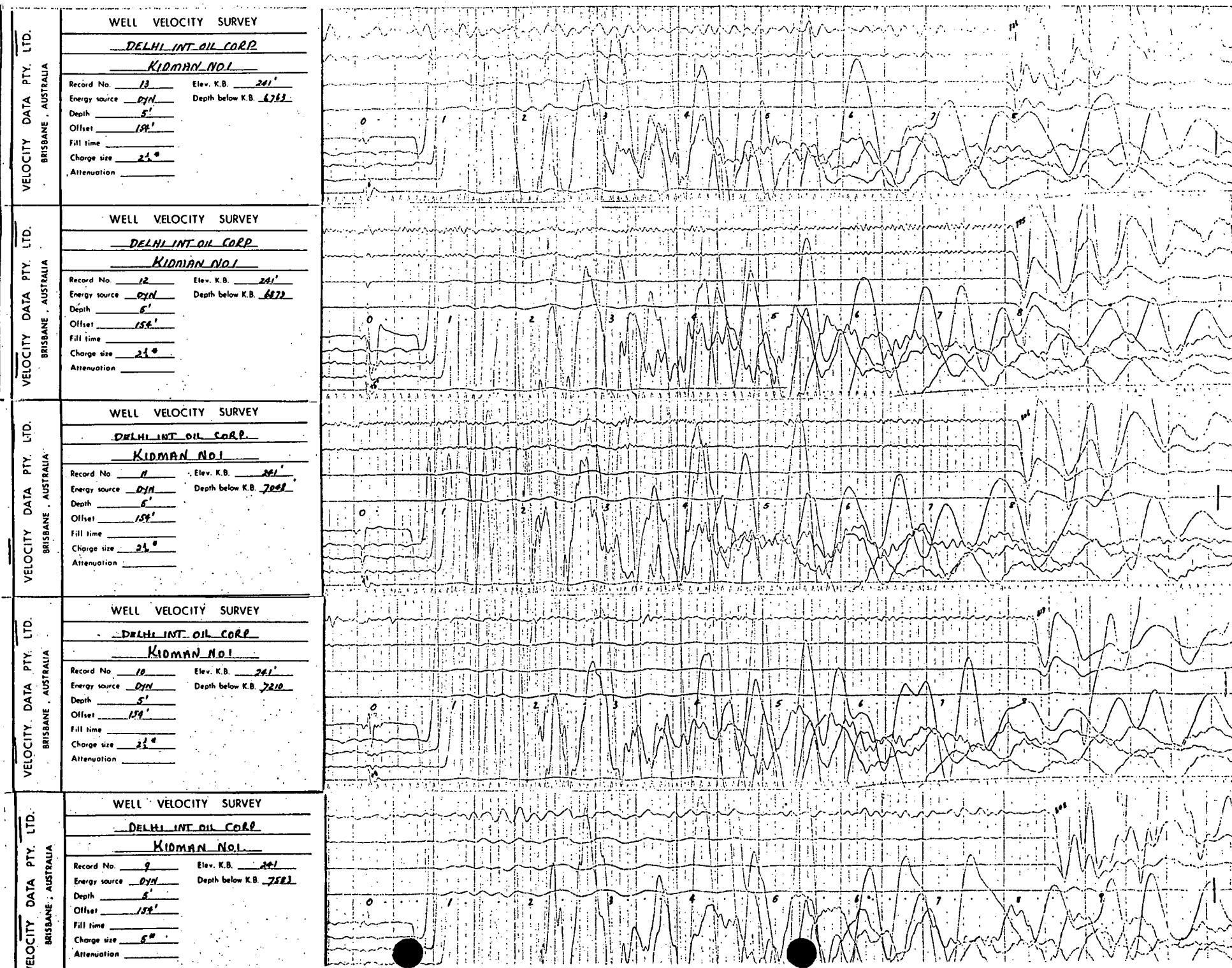
	Record No.	ZKB	Ds	O/S	Z	t	T	T av.
WELL - Delhi International Oil Corporation Kidman No. 1	1	241'	4'	98'	0	.053	(.048 ¹) 0	(.048 ⁸)
	2	241'	5'	154'	0	.059	(.048 ⁹) 0	
	3	241'	5'	230'	0	.061 ⁺	(.043 ³) 0	
	4	1275'	5'	154'	1034	.212	.161 ⁶	
Date - October 17, 1977	22	1900'	5'	154'	1659	.302	.252 ²	
	21	2600'	5'	154'	2359	.381	.331 ⁵	
EKB 241' A.S.L.	5	3307'	5'	154'	3066	.475	.425 ⁷	
EG 227' A.S.L.	20	3800'	5'	154'	3559	.536	.486 ⁸	
Ed Sea Level	6	4340'	5'	154'	4099	.598	.548 ⁸	.548
	19	4340'	5'	154'	4099	.597	.547 ⁸	
	18	5538'	5'	154'	5297	.691	.641 ⁹	
	17	5678'	5'	154'	5437	.702	.652 ⁹	
	16	5933'	5'	154'	5692	.722	.672 ⁹	
	7	6367'	5'	154'	6126	.751	.702	.701 ⁵
	15	6367'	5'	154'	6126	.750	.701	
EKB Elevation Kelly Bushing	14	6720'	5'	154'	6479	.782	.733	
EG Elevation of Ground	13	6763'	5'	154'	6522	.786	.737	
Ed Elevation of Datum	12	6879'	5'	154'	6638	.795	.746	
Ds Depth of Shot	11	7048'	5'	154'	6807	.806	.757	
O/S Shot Offset	10	7210'	5'	154'	6969	.819 ⁹	.770	
ZKB Geophone depth below Kelly Bushing (ft)	8	7583'	5'	154'	7342	.849 ⁹	?	
Zs Geophone depth below shot	9	7583'	5'	154'	7342	.848	.799	
Z Geophone depth below Datum (ft)								
t Record time (secs)								
T Corrected time from Datum								

[illegible]

Sonic Calibration

0032

	1	2	3	4	5	6	7	8
WELL - Delhi International Oil Corporation	4340	4099	379'		(548 ³)		7476	
Kidman No. 1		270	025 ⁶		025 ⁵			10588
Date - October 17, 1977	4610	4369	404 ⁷		573 ⁸		7614	
Column 1		480	039 ²		039 ⁰	(093 ⁴) 094 ¹		12308
Depth below KB (ft)	5090	4849	443 ⁹		612 ⁸		7913	
Column 2		448	029 ³		029 ¹			15395
Depth below Datum (ft)	5538	5297	473 ²		(641 ⁹)		8252	
Interval Distance		140	011 ⁴		011	(011) 011 ⁴		12727
Column 3	5678	5437	484 ⁶		(652 ⁹)		8327	
Sonic Calibration Time		255	019 ⁶		020	(020) 019 ⁶		12750
Sonic Interval Time	5933	5692	504 ²		(672 ⁹)		8459	
Column 4		434	030 ³		028 ⁶	(028 ⁶) 030 ³		15175
Sonic Time (secs)	6367	6126	534 ⁵		(701 ⁵)		8733	
Column 5		353	029 ⁴		031 ⁵	(031 ⁵) 029 ⁴		11206
Well Velocity Time ()	6720	6479	563 ⁹		(733)		8839	
Corrected Sonic Interval Times		43	003 ⁴		004	(004) 003 ⁴		10750
Corrected Sonic Times	6763	6522	567 ³		(737)		8849	
Column 6		116	009 ³		009	(009) 009 ³		12889
Sonic Interval Time between Checkpoints	6879	6638	576 ⁶		(746)		8898	
Geophone interval time between Checkpoints ()		169	011 ⁵		011	(011) 011 ⁵		15364
Column 7	7048	6807	588 ⁶		(757)		8992	
Average Velocities (ft/sec.)		162	011 ⁵		013	(013) 011 ⁵		12462
Column 8	7210	6969	599 ⁶		(770)		9050	
Interval Velocities (ft/sec)		373	027 ¹		029	(029) 027 ¹		12862
	7583	7342	626 ⁷		(799)		9189	



VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.

KIDMAN NO.1.

Record No. 5 Elev. K.B. 241'

Energy source DYN Depth below K.B. 3307'

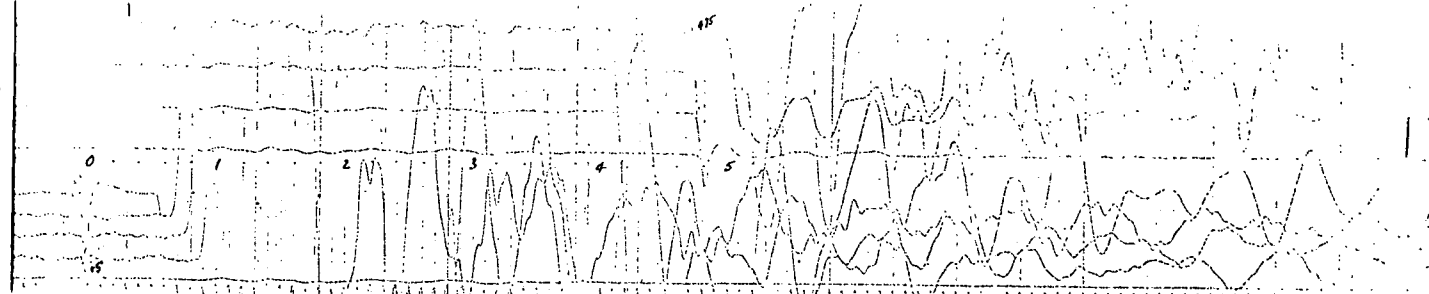
Depth 5'

Offset 154'

Fill time _____

Charge size 2 1/2"

Attenuation _____



VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INTERNAT. OIL

KIDMAN NO.1

Record No. 20 Elev. K.B. 241'

Energy source DYN Depth below K.B. 3300'

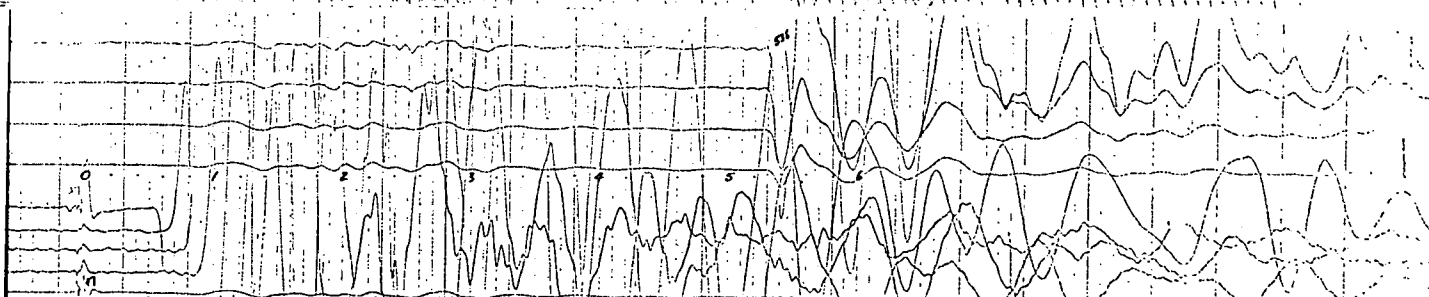
Depth 5'

Offset 154'

Fill time _____

Charge size 2 1/2"

Attenuation _____



VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.

KIDMAN NO.1

Record No. 6 Elev. K.B. 241'

Energy source DYN Depth below K.B. 3340'

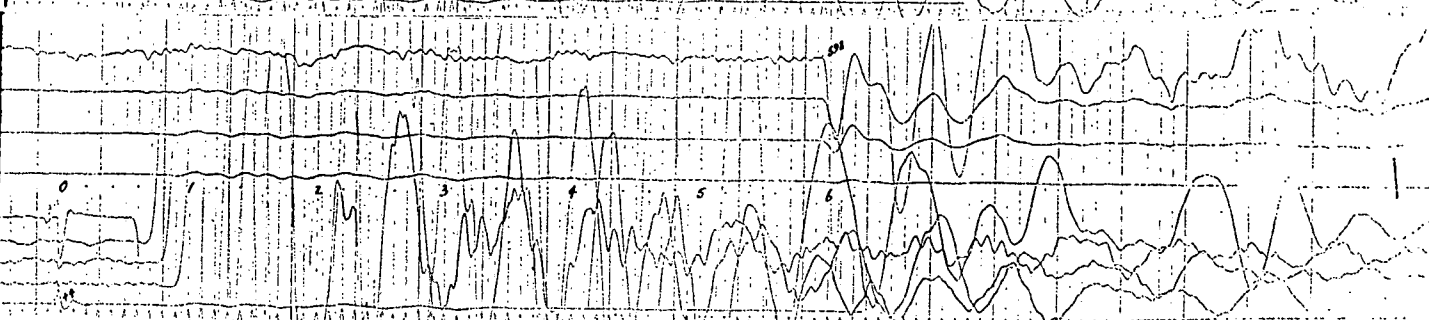
Depth 5'

Offset 154'

Fill time _____

Charge size 2 1/2"

Attenuation _____



VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.

KIDMAN NO.1.

Record No. 12 Elev. K.B. 241'

Energy source DYN Depth below K.B. 3340'

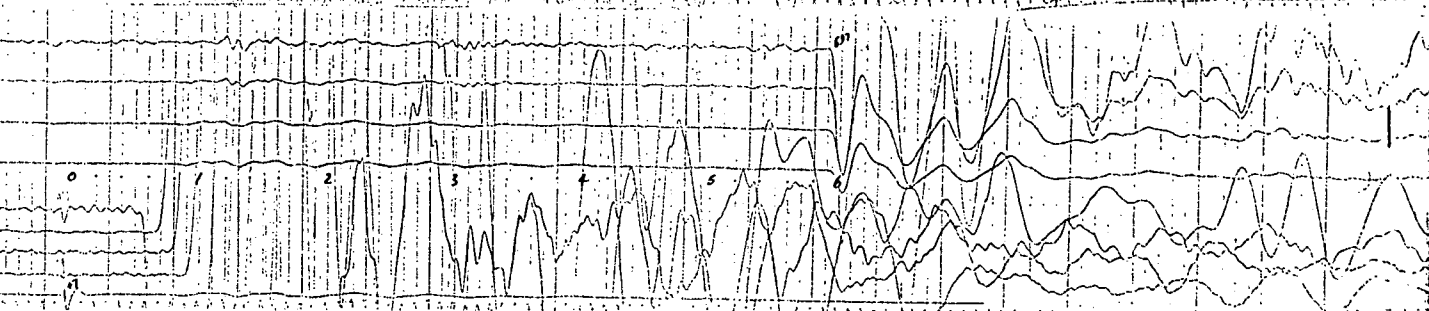
Depth 5'

Offset 154'

Fill time _____

Charge size 2 1/2"

Attenuation _____



VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.

KIDMAN NO.1.

Record No. 18 Elev. K.B. 241'

Energy source DYN Depth below K.B. 3338'

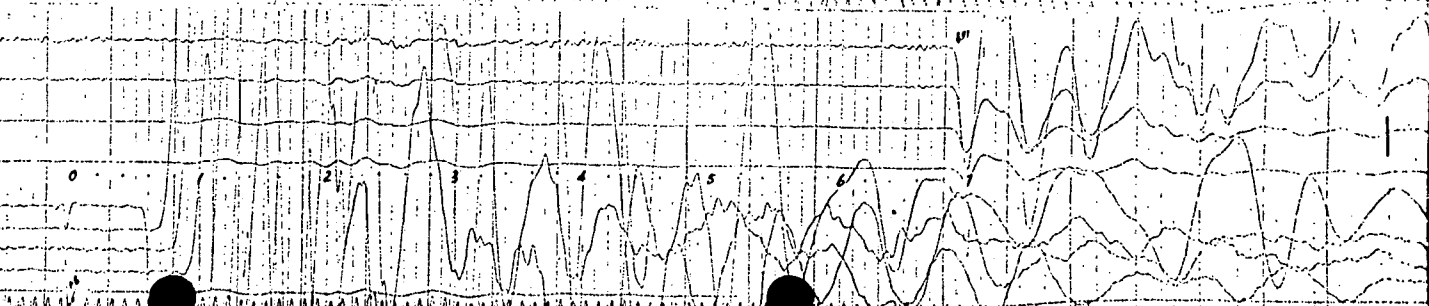
Depth 5'

Offset 154'

Fill time _____

Charge size 2 1/2"

Attenuation _____



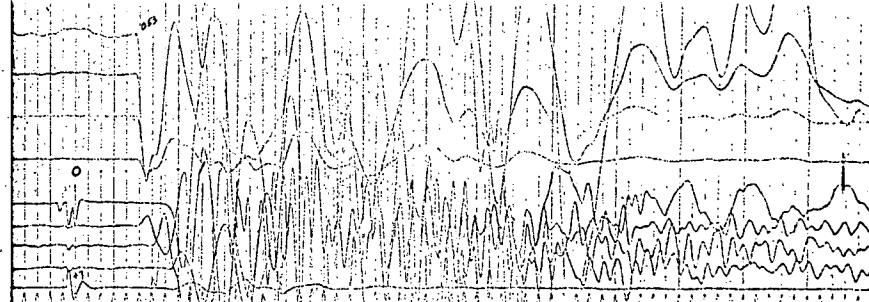
0035

VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.KIDMAN #1

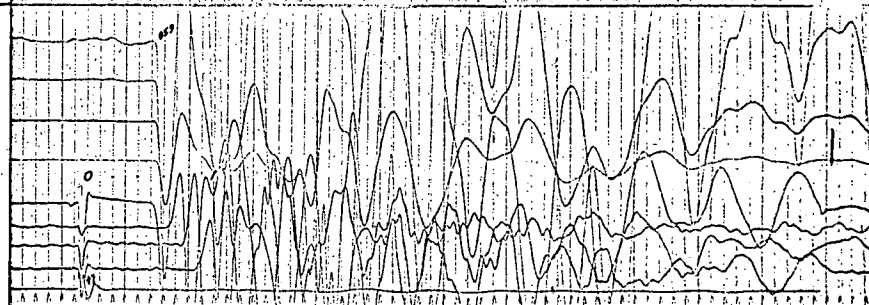
Record No. 1 Elev. K.B. 241'
 Energy source DYN. Depth below K.B. 241'
 Depth 4'
 Offset 98'
 Fill time _____
 Charge size 1"
 Attenuation _____

VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.KIDMAN #1

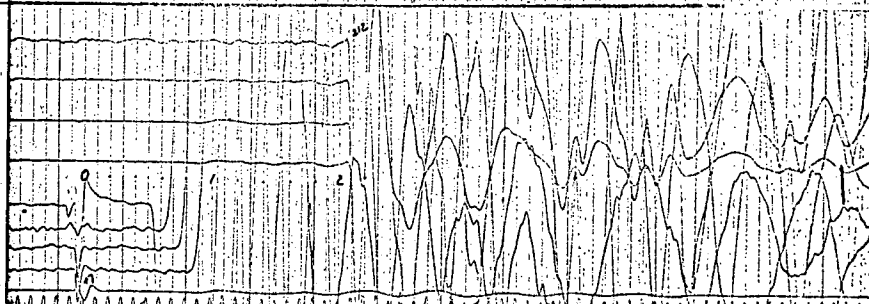
Record No. 2 Elev. K.B. 241'
 Energy source DYN. Depth below K.B. 241'
 Depth 5'
 Offset 154'
 Fill time _____
 Charge size 1"
 Attenuation _____

VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.KIDMAN NO1

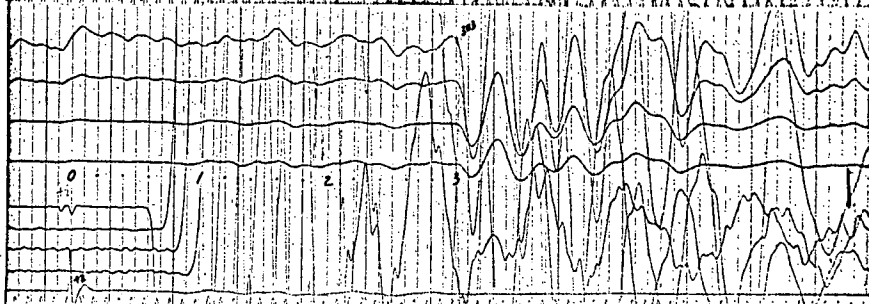
Record No. 4 Elev. K.B. 241'
 Energy source DYN. Depth below K.B. 1275'
 Depth 5'
 Offset 154'
 Fill time _____
 Charge size 2 1/2"
 Attenuation _____

VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.KIDMAN NO1

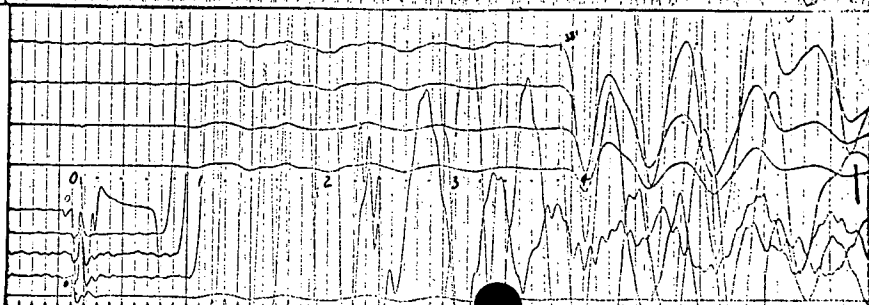
Record No. 22 Elev. K.B. 241'
 Energy source DYN. Depth below K.B. 1200'
 Depth 5'
 Offset 154'
 Fill time _____
 Charge size 2 1/2"
 Attenuation _____

VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.KIDMAN NO1

Record No. 21 Elev. K.B. 241'
 Energy source DYN. Depth below K.B. 2500'
 Depth 5'
 Offset 145'
 Fill time _____
 Charge size 2 1/2"
 Attenuation _____



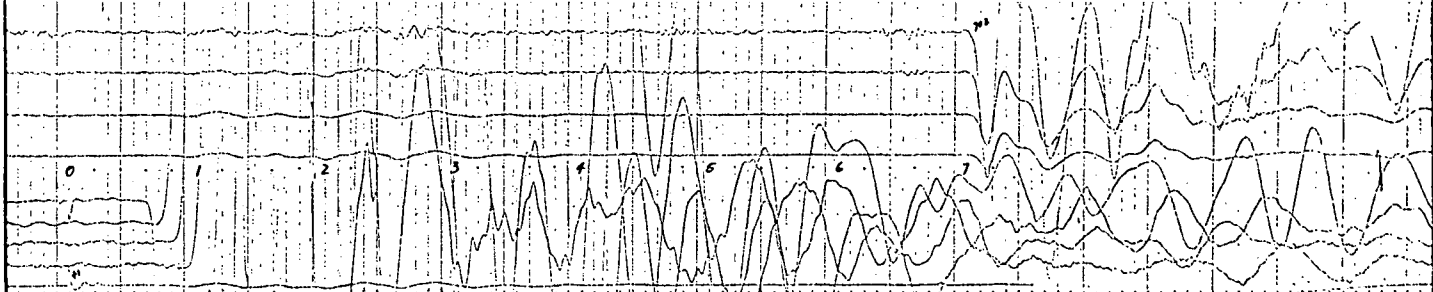
VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.

KIDMAN NO. 1.

Record No. 17 Elev. K.B. 241
Energy source DYN Depth below K.B. 5378
Depth 5'
Offset 154'
Fill time
Charge size 2 1/2"
Attenuation

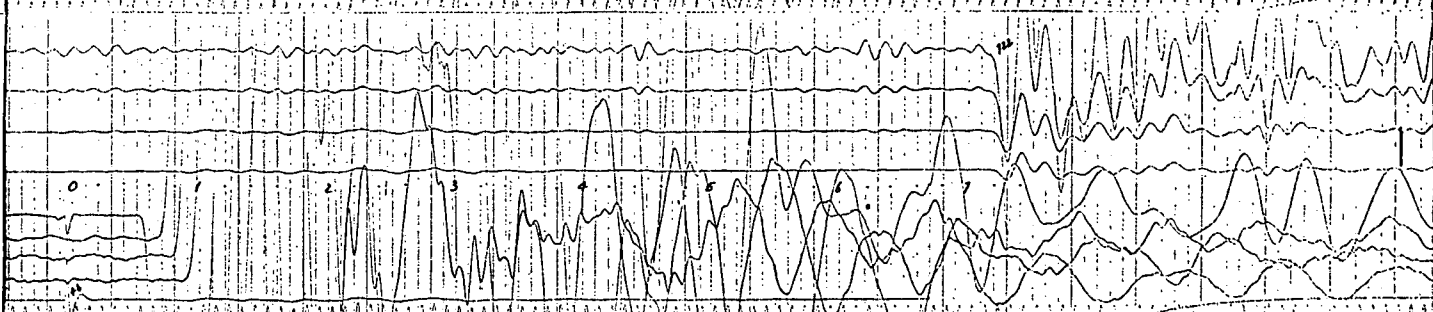
VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.

KIDMAN NO. 1.

Record No. 16 Elev. K.B. 241
Energy source DYN Depth below K.B. 5378
Depth 6'
Offset 154'
Fill time
Charge size 2 1/2"
Attenuation

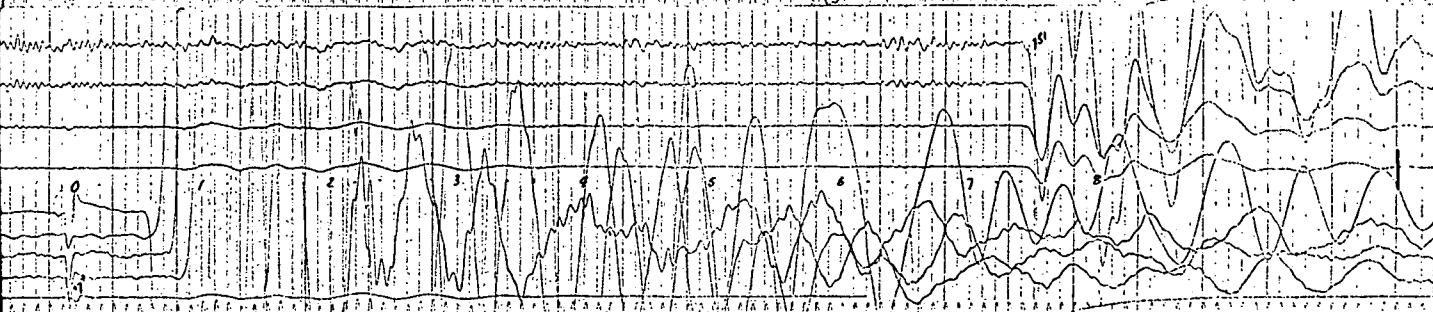
VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.

KIDMAN NO. 1.

Record No. 15 Elev. K.B. 241
Energy source DYN Depth below K.B. 5367
Depth 5'
Offset 154'
Fill time
Charge size 2 1/2"
Attenuation

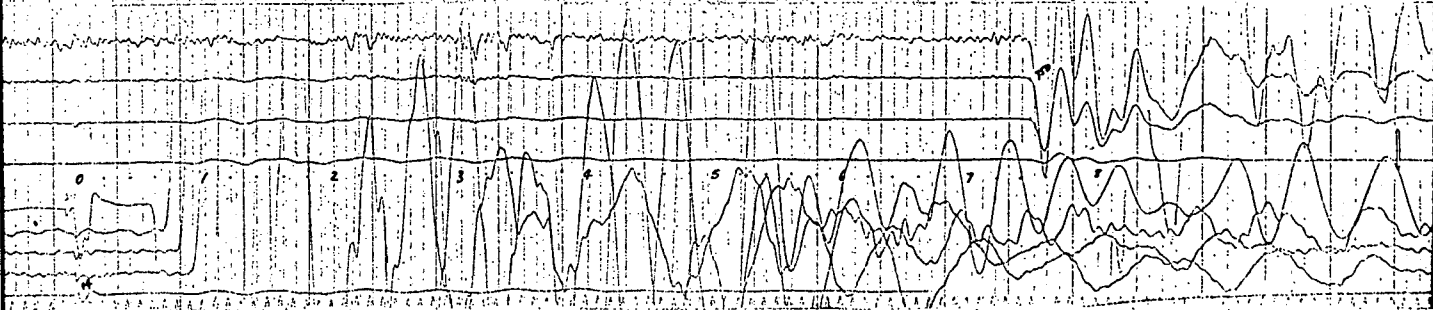
VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.

KIDMAN NO. 1.

Record No. 7 Elev. K.B. 241
Energy source DYN Depth below K.B. 5367
Depth 5'
Offset 154'
Fill time
Charge size 2 1/2"
Attenuation

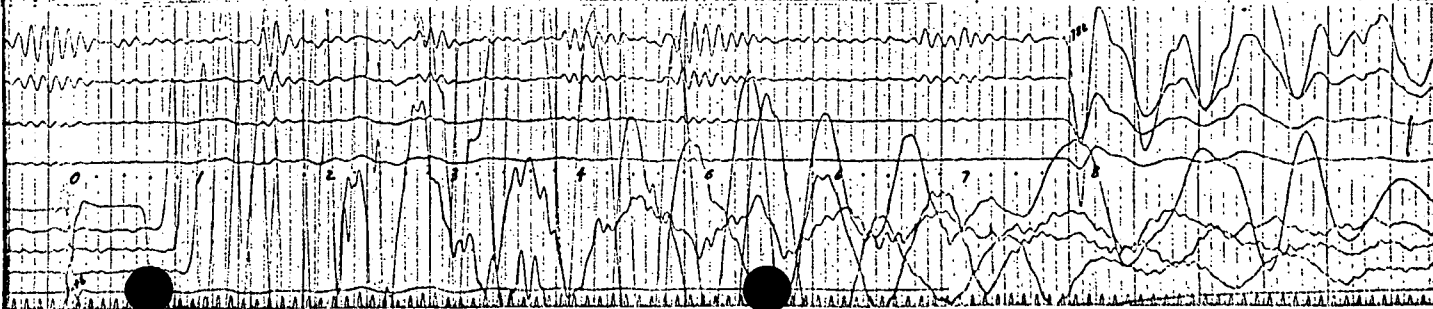
VELOCITY DATA PTY. LTD.
BRISBANE, AUSTRALIA

WELL VELOCITY SURVEY

DELHI INT. OIL CORP.

KIDMAN NO. 1.

Record No. 14 Elev. K.B. 241
Energy source DYN Depth below K.B. 5320
Depth 5'
Offset 154'
Fill time
Charge size 2 1/2"
Attenuation



2674-1

SEISMIC SECTION
LINE 75-JBV
SP 165 KIDMAN LOCATION

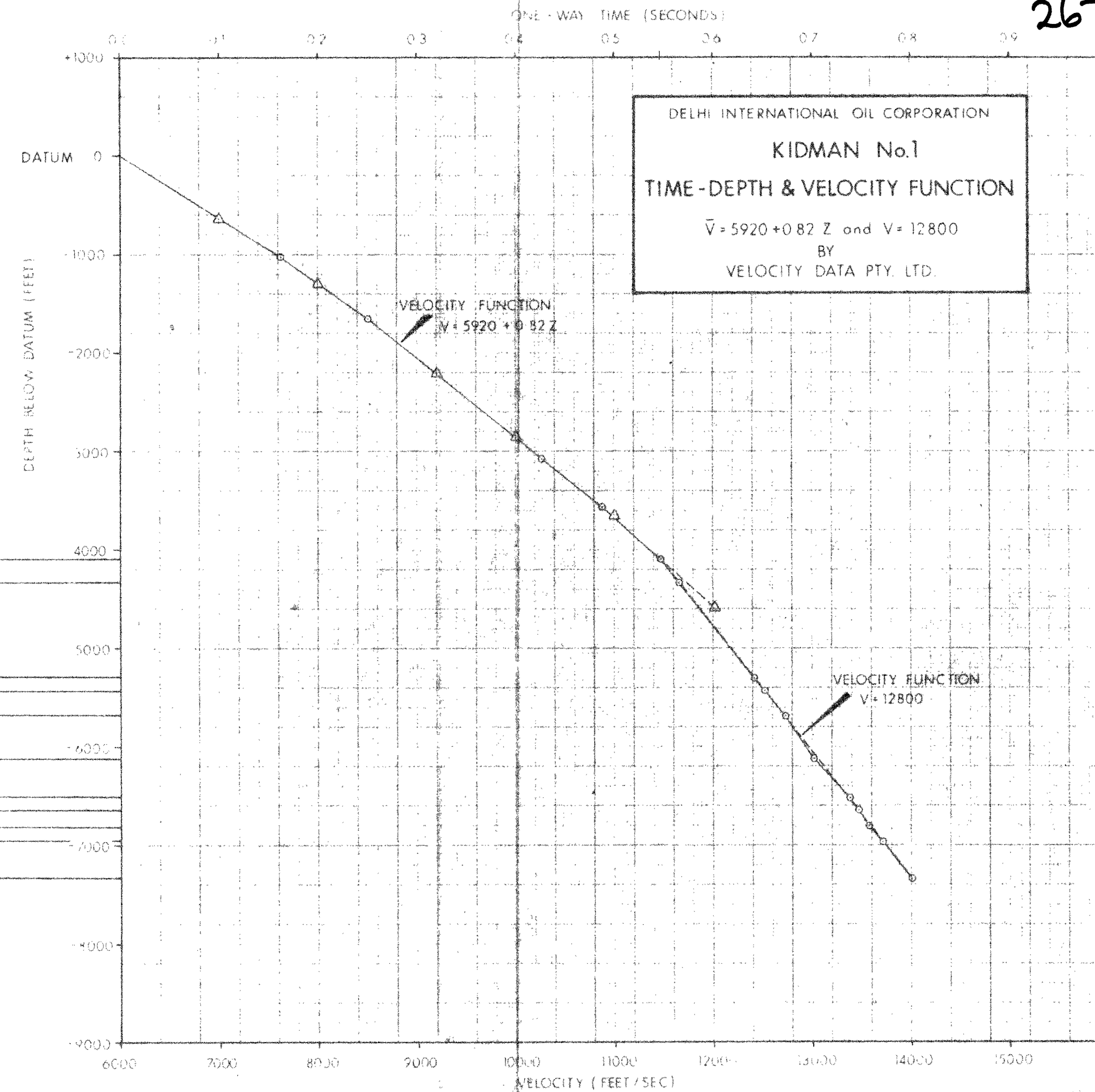
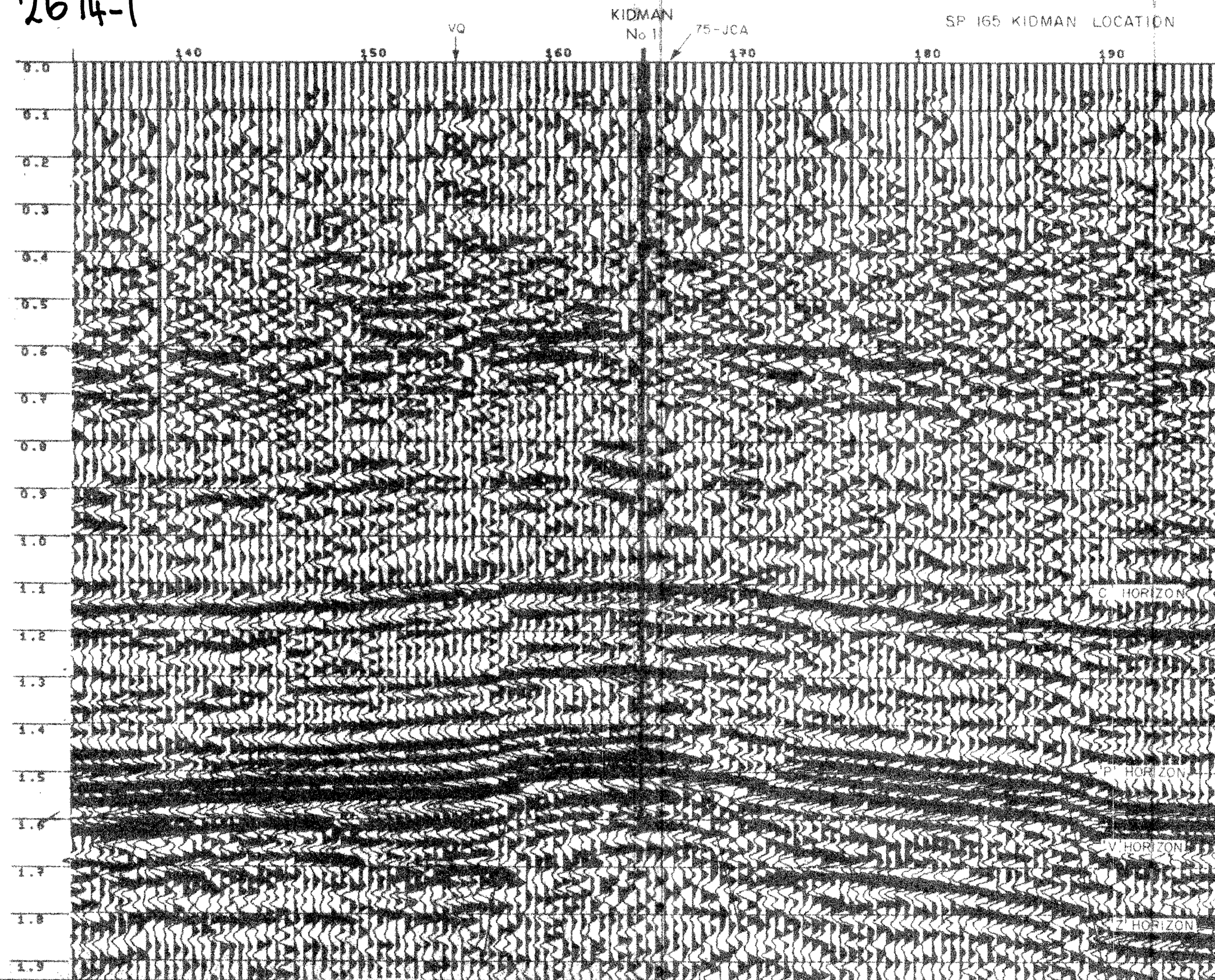
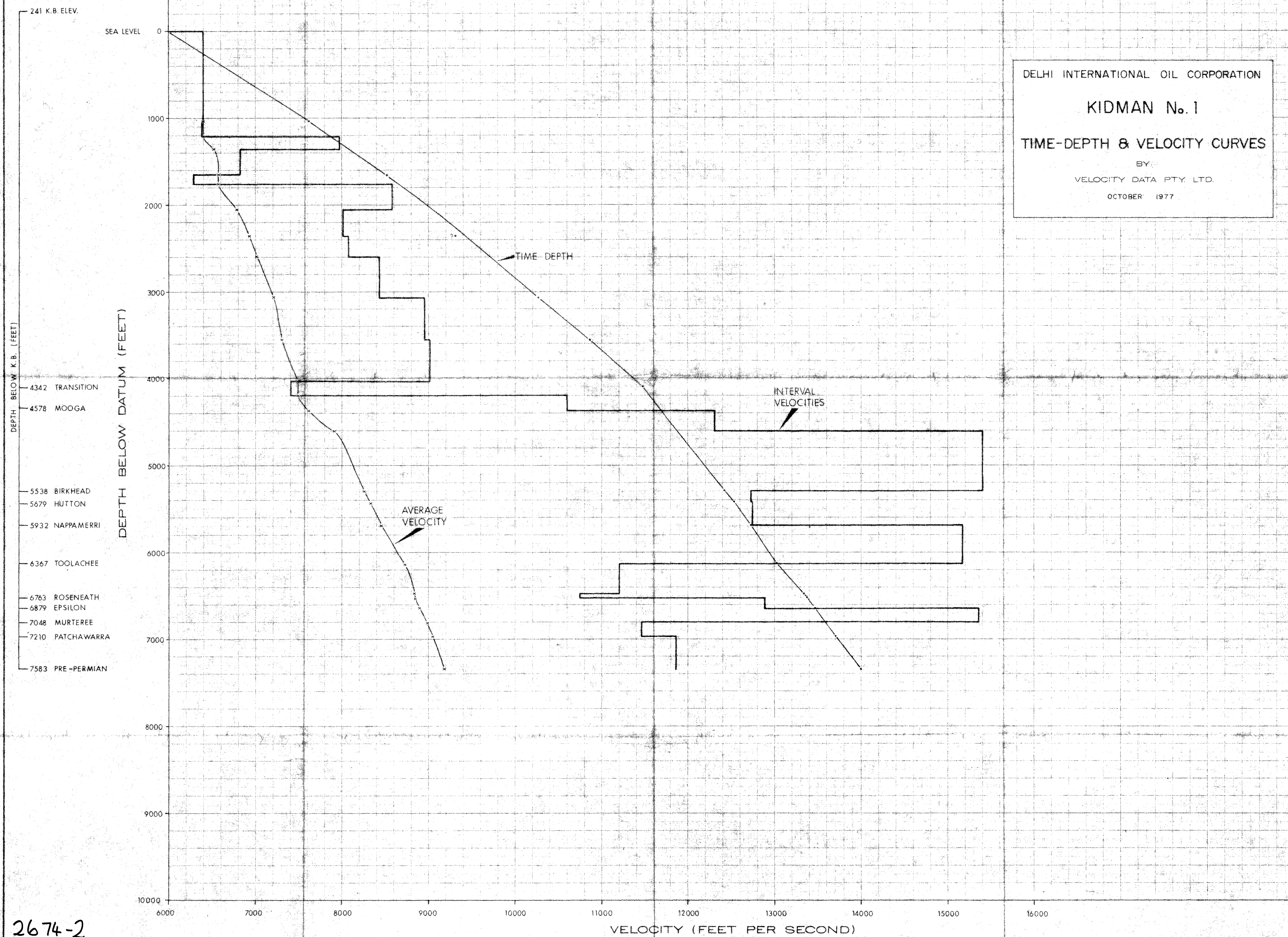


FIGURE 3

2674-2



2674-2

43

Coment

Computer
Enterprises Ltd.

1020-444 5th Ave. S.W.,
Calgary, Alberta,
T2P 2T8
Bus. 261-5012

17/01/83

LOG ANALYSIS REPORT
FOR

KIDMAN #1
28-14-23S/140-49-27E

Env. 2674

Coment Ltd.

LOG ANALYSIS Parameters

General Log Analysis program (CARBAN)

Explanation of the parameter names and their values.

A - Formation Factor Coefficient

M - Formation Factor Cementation Exponent

N - Saturation exponent in formation factor equation.

R_w - Formation water resistivity at formation temperature (TEMP)

TEMP - Formation temperature at Top of analysis interval. This value and R_w are corrected for depth using the formation temperature gradient (GRAD).

GRAD - The geothermal gradient in degrees per 100 feet (Imperial) or degrees per meter (S.I.)

GMAX - The Maximum Gamma ray. The gamma ray reading at the point where all of the rock is considered to be shale.

GMIN - The Minimum Gamma ray. This value is biased upwards from the 'minimum' to include all 'clean' carbonate rocks. That is all points below this value are considered clean.

R_{sh} - The resistivity of the shales, using the deep resistivity log.

Corr C Q I - Log Correction codes: (1 = used, 2 = not used)

C - Caliper correction. Bore hole effects on the density and gamma-ray logs are corrected.

Q - Gas corrections. This allows for correction of gas effect on the neutron and density logs.

I - Invasion correction applied to the Deep resistivity.

PTYP - Porosity type used in the analysis:

1=Acoustic log

2=Neutron log

3=Density log

4=Neutron/density cross-plot

5=Acoustic/neutron cross-plot

6=M*N Porosity

7=Core porosity

MAT - Matrix value used in single log porosity calculation.

FLD - Fluid value used in single log porosity calculation. (Ptyp 1 to 3)

RhoS - Shale density.

PhiS - Neutron Shale porosity

DTSH - Acoustic transit time of Shale

LOG ANALYSIS Parameters

LS

Sandstone Analysis Program (SANDAN)

Explanation of the parameter names and their values.

A - Formation Factor Coefficient

M - Formation Factor Cementation Exponent

N - Saturation exponent in formation factor equation.

R_w - Formation water resistivity at formation temperature (TEMP)

TEMP - Formation temperature at Top of analysis interval. This value and R_w are corrected for depth using the formation temperature gradient (GRAD).

GRAD - The geothermal gradient in degrees/ 100 feet (Imperial) or degrees/ metre (S. I.)

GMAX - The Maximum Gamma Ray. The gamma ray reading at the point where the lithology changes from grain supported to mud supported rock (The shale boundary)

GMIN - The Minimum Gamma Ray. The lowest gamma ray in a clean sand section. May also be projected from cross-plots.

R_{sh} - The resistivity of the shales, using the deep resistivity log.

Corr C C I - Log Correction codes: (1 = used, 2 = not used)

C - Caliper correction. Bore hole effects on the density and gamma-ray logs are corrected.

G - Gas correction. Corrections applied to the neutron and density logs for gas effects and rough hole effects.

1=Prime log is Neutron

2=Prime log is density

3=No gas corrections.

I - Invasion Corrections applied to the Deep resistivity.

RhoG - Grain Density

RhoS - Shale Density (derived from the cross-plots)

PhiS - Neutron shale porosity (derived from the cross-plots)

PhiC - Neutron clay porosity (usually 24 but may be changed)

Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

Page 1

Zone Name = TK-3

Top = 6357.00 Base = 6540.50 Date = 07/12/82

Caliper Cutoff = ***** Permeability Cutoff = 0.00
Gross Shale Cutoff = 50.00 Shale Cutoff = 30.00

Porosity*Sw cutoff = 0.0 Porosity cutoff = 10.0 Saturation cutoff = 50.0

Gross Thickness = 21.00 Sand Thickness = 9.50 Sand > por. Cutoff = 6.50

Average Porosity = 13.89 Average water saturation = 18.85 Net thickness = 2.50

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Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

Page 2

Zone Name = TK-2

Top = 6541.00 Base = 6718.50 Date = 07/12/82

Caliper Cutoff = ***** Permeability Cutoff = 0.00
Gross Shale Cutoff = 50.00 Shale Cutoff = 30.00

Porosity*Sw cutoff = 0.0 Porosity cutoff = 10.0 Saturation cutoff = 50.0
Gross Thickness = 110.00 Sand Thickness = 79.50 Sand > por. Cutoff = 76.00
Average Porosity = 15.17 Average water saturation = 26.08 Net thickness = 66.00

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Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

Page 3

Zone Name = TK-1

Top = 6719.00 Base = 6762.00 Date = 07/12/82

Caliper Cutoff = ***** Permeability Cutoff = 0.00
Gross Shale Cutoff = 50.00 Shale Cutoff = 30.00

Porosity*Sw. cutoff = 0.0 Porosity cutoff = 10.0 Saturation cutoff = 50.0

Gross Thickness = 31.50 Sand Thickness = 27.50 Sand > por. Cutoff = 24.00

Average Porosity = 17.64 Average water saturation = 22.17 Net thickness = 22.50

Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

Page 4

Zone Name = EPSILON

Top = 6914.00 Base = 7048.00 Date = 07/12/82

Caliper Cutoff = ***** Permeability Cutoff = 0.00
Gross Shale Cutoff = 50.00 Shale Cutoff = 30.00

Porosity*Sw cutoff = 0.0 Porosity cutoff = 10.0 Saturation cutoff = 50.0

Gross Thickness = 42.00 Sand Thickness = 29.00 Sand > por. Cutoff = 28.50

Average Porosity = 12.47 Average water saturation = 42.59 Net thickness = 26.50

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Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

Page No 1

Porosity cutoff = 10.0 Saturation cutoff = 50.0 Caliper cutoff = bit size +***** Shale Cutoff = 30.0
Permeability cutoff = 0.000
TOP BASE A M N RW TEMP GRAD GMAX GMIN RSH COR C G I RHOG RHOS PHIS PHIC
6340.00 6770.00 1.00 2.00 2.00 0.260 223.0 2.250 144.00 32.00 50.00 2 2 2 2.650 2.660 15.0 24
Porosity derived from Neutron/Density Cross-Plot
6900.00 7250.00 1.00 2.00 2.00 0.180 235.0 2.250 140.00 48.00 56.00 2 2 2 2.650 2.760 14.0 24
Porosity derived from Neutron/Density Cross-Plot

Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

Page No 2

DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6340.00	100.00	47.67	0.01	9.08	0.00	100.00	0.00			
6340.50	96.71	45.49	0.38	8.93	3.65	37.03	134.98			
6341.00	100.00	48.01	0.01	7.41	0.00	100.00	0.00			
6341.50	95.57	44.96	0.00	7.19	1.97	67.81	133.63			
6342.00	81.20	38.20	0.03	8.55	4.12	68.00	280.22			
6342.50	74.77	35.17	0.29	10.02	5.94	56.92	338.16			
6343.00	67.41	31.71	1.14	11.37	7.69	51.64	397.28			
6343.50	97.46	45.85	0.13	8.13	2.81	39.04	109.80			
6344.00	100.00	50.29	0.01	7.49	0.00	100.00	0.00			
6344.50	100.00	54.89	0.01	7.12	0.00	100.00	0.00			
6345.00	100.00	53.25	0.01	7.43	0.00	100.00	0.00			
6345.50	100.00	50.76	0.01	7.71	0.00	100.00	0.00			
6346.00	100.00	53.23	0.01	7.28	0.00	100.00	0.00			
6346.50	100.00	52.01	0.01	7.78	0.00	100.00	0.00			
6347.00	94.79	44.59	0.01	7.44	2.27	63.42	143.69			
6347.50	88.55	41.66	0.00	7.10	2.26	78.36	177.38			
6348.00	74.13	34.87	0.03	8.33	4.28	68.14	291.54			
6348.50	85.99	40.45	0.00	6.97	2.27	79.19	179.93			
6349.00	96.89	45.58	0.00	6.58	1.29	68.97	88.98			
6349.50	99.49	46.80	0.11	7.30	1.87	26.27	49.01			
6350.00	85.02	39.99	0.02	8.02	3.38	64.52	218.18			
6350.50	100.00	48.49	0.01	5.97	0.00	100.00	0.00			
6351.00	100.00	52.54	0.01	5.27	0.00	100.00	0.00			
6351.50	99.13	46.63	0.00	6.49	1.08	53.29	57.35			
6352.00	97.85	46.03	0.01	7.18	1.84	51.50	94.82			
6352.50	100.00	53.36	0.01	5.96	0.00	100.00	0.00			
6353.00	100.00	56.40	0.01	5.64	0.00	100.00	0.00			
6353.50	100.00	51.85	0.01	7.41	0.00	100.00	0.00			
6354.00	100.00	50.74	0.01	8.36	0.00	100.00	0.00			
6354.50	100.00	51.47	0.01	8.66	0.00	100.00	0.00			
6355.00	100.00	55.69	0.01	7.59	0.00	100.00	0.00			
6355.50	100.00	55.12	0.01	7.46	0.00	100.00	0.00			
6356.00	100.00	52.75	0.01	7.72	0.00	100.00	0.00			
6356.50	100.00	60.15	0.01	6.06	0.00	100.00	0.00			
6357.00	100.00	63.97	0.01	5.62	0.00	100.00	0.00			
6357.50	100.00	67.75	0.01	5.11	0.00	100.00	0.00			
6358.00	100.00	68.78	0.01	4.77	0.00	100.00	0.00			
6358.50	100.00	65.49	0.01	4.59	0.00	100.00	0.00			
6359.00	100.00	62.01	0.01	5.54	0.00	100.00	0.00			
6359.50	100.00	60.01	0.01	6.76	0.00	100.00	0.00			
6360.00	100.00	60.29	0.01	7.29	0.00	100.00	0.00			
6360.50	100.00	70.16	0.01	5.18	0.00	100.00	0.00			
6361.00	100.00	72.55	0.01	4.92	0.00	100.00	0.00			
6361.50	100.00	69.10	0.01	5.81	0.00	100.00	0.00			
6362.00	100.00	68.47	0.01	6.04	0.00	100.00	0.00			
6362.50	100.00	70.19	0.01	5.89	0.00	100.00	0.00			
6363.00	100.00	74.66	0.01	5.43	0.00	100.00	0.00			
6363.50	100.00	68.79	0.01	7.80	0.00	100.00	0.00			
6364.00	100.00	64.80	0.01	9.73	0.00	100.00	0.00			
6364.50	100.00	62.42	0.01	11.43	0.00	100.00	0.00			

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Well name = KIDMAN #1

Location = 28-14-235/140-49-27E

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6365.00	100.00	62.11	0.01	12.69	0.00	100.00	0.00			
6365.50	100.00	62.60	0.01	13.90	0.00	100.00	0.00			
6366.00	100.00	62.95	0.01	15.34	0.00	100.00	0.00			
6366.50	100.00	56.84	0.01	18.58	0.00	100.00	0.00			
6367.00	100.00	53.18	0.01	21.77	0.00	100.00	0.00			
6367.50	71.98	33.86	0.60	9.04	5.11	44.22	226.17			
6368.00	62.30	29.31	1.73	10.28	6.88	43.43	298.86			
6368.50	61.10	28.74	56.57	19.22	15.89	22.79	362.10			
6369.00	75.68	35.60	11.64	14.45	10.32	27.68	285.64			
6369.50	93.74	44.10	4.92	10.78	5.66	25.75	145.74			
6370.00	89.34	42.03	3.75	10.77	5.89	29.98	176.56			
6370.50	75.72	35.62	13.06	12.59	8.46	29.58	250.24			
6371.00	72.32	34.02	14.62	14.75	10.80	24.49	264.48			
6371.50	98.33	46.26	56.30	18.35	12.98	5.59	72.50			
6372.00	96.84	45.56	115.74	20.72	15.44	6.42	99.16			
6372.50	100.00	50.00	0.01	22.00	0.00	100.00	0.00			
6373.00	100.00	52.50	0.01	23.82	0.00	100.00	0.00			
6373.50	91.39	42.99	1085.04	27.59	22.60	5.97	134.92			
6374.00	82.31	38.72	1898.51	29.27	24.77	7.37	182.55			
6374.50	67.15	31.59	3.87	9.66	6.00	30.28	181.52			
6375.00	66.98	31.51	3.90	9.68	6.03	30.38	183.15			
6375.50	67.65	31.83	2.27	9.60	5.90	35.27	208.24			
6376.00	71.22	33.50	0.64	9.14	5.25	44.49	233.72			
6376.50	74.38	34.99	0.26	8.74	4.68	49.94	233.55			
6377.00	100.00	47.34	0.01	10.31	0.00	100.00	0.00			
6377.50	100.00	47.82	0.01	10.38	0.00	100.00	0.00			
6378.00	100.00	47.76	0.01	10.37	0.00	100.00	0.00			
6378.50	71.15	33.47	0.20	9.15	5.27	56.85	299.40			
6379.00	69.95	32.91	0.86	9.30	5.48	42.78	234.62			
6379.50	83.58	39.32	941.89	27.11	22.54	7.65	172.45			
6380.00	72.29	34.01	757.05	25.91	21.96	8.23	180.71			
6380.50	73.32	34.49	3341.87	30.23	26.22	5.93	155.62			
6381.00	45.70	21.50	16.82	12.41	9.91	13.42	133.02			
6381.50	33.38	15.70	31.86	13.98	12.16	13.46	163.67			
6382.00	23.87	11.23	46.24	15.20	13.90	16.13	224.12	0.07	0.06	0.50
6382.50	21.32	10.03	45.36	15.53	14.36	19.25	276.44	0.14	0.12	1.00
6383.00	21.34	10.04	36.47	15.52	14.36	23.85	342.41	0.21	0.17	1.50
6383.50	53.49	25.17	70.35	19.99	17.07	24.25	413.96			
6384.00	69.73	32.80	18.89	16.86	13.05	31.54	411.68			
6384.50	98.85	46.50	28.92	12.13	6.74	13.37	90.10			
6385.00	100.00	47.36	0.01	11.03	0.00	100.00	0.00			
6385.50	98.77	46.46	9.18	10.70	5.31	17.02	90.32			
6386.00	90.31	42.48	4.15	11.58	6.65	33.16	220.54			
6386.50	89.35	42.03	5.46	11.77	6.89	31.53	217.31			
6387.00	89.83	42.26	6.05	11.73	6.82	30.11	205.41			
6387.50	100.00	50.40	0.01	10.71	0.00	100.00	0.00			
6388.00	78.84	37.09	9.34	12.86	8.55	33.46	286.10			
6388.50	85.99	40.45	5.79	11.84	7.15	32.20	230.12			
6389.00	86.11	40.51	3.37	11.22	6.52	34.60	225.49			
6389.50	87.09	40.97	1.28	10.24	5.49	38.76	212.74			

Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6390.00	70.27	33.06	0.21	9.26	5.43	57.06	309.65			
6390.50	73.02	34.35	0.13	8.91	4.93	58.93	290.26			
6391.00	100.00	47.33	0.01	10.31	0.00	100.00	0.00			
6391.50	100.00	47.95	0.01	10.39	0.00	100.00	0.00			
6392.00	100.00	47.59	0.01	10.35	0.00	100.00	0.00			
6392.50	79.47	37.38	0.63	10.03	5.69	47.30	268.98			
6393.00	79.12	37.22	0.78	10.30	5.98	46.83	280.20			
6393.50	76.81	36.13	0.13	9.10	4.91	58.30	286.32			
6394.00	77.88	36.64	0.07	8.68	4.43	61.61	272.77			
6394.50	52.09	24.51	3.53	12.46	9.62	47.68	458.67			
6395.00	69.34	32.62	1.51	11.02	7.23	46.60	337.15			
6395.50	77.76	36.58	1.23	10.52	6.27	43.80	274.78			
6396.00	63.73	29.98	0.58	10.14	6.66	53.77	358.25			
6396.50	59.96	28.21	0.53	10.22	6.95	56.21	390.60			
6397.00	65.61	30.87	0.23	9.54	5.96	59.68	355.83			
6397.50	56.50	26.58	1.10	11.13	8.04	53.61	431.12			
6398.00	60.02	28.24	5.90	12.81	9.53	42.03	400.71			
6398.50	74.47	35.03	6.42	12.31	8.24	36.08	297.44			
6399.00	77.94	36.67	8.60	12.36	8.11	32.46	263.09			
6399.50	71.52	33.65	0.37	9.10	5.20	49.75	258.64			
6400.00	67.08	31.56	0.64	9.67	6.01	49.09	294.93			
6400.50	64.19	30.19	0.30	9.36	5.85	56.16	328.68			
6401.00	50.86	23.93	0.49	10.20	7.42	59.13	438.74			
6401.50	41.53	19.54	3.68	12.73	10.46	50.16	524.61			
6402.00	30.59	14.39	0.28	10.03	8.36	69.33	579.47			
6402.50	43.24	20.34	0.07	8.89	6.53	75.08	490.10			
6403.00	51.56	24.25	0.04	8.48	5.66	75.20	425.64			
6403.50	53.78	25.30	0.07	8.69	5.75	70.13	403.52			
6404.00	54.76	25.76	0.09	8.71	5.72	67.36	385.00			
6404.50	52.49	24.69	0.26	9.34	6.47	61.04	395.17			
6405.00	43.59	20.51	1.18	10.72	8.34	54.14	451.41			
6405.50	29.49	13.87	3.37	12.07	10.46	51.07	534.07			
6406.00	31.92	15.01	1.38	11.36	9.61	57.44	552.28			
6406.50	36.24	17.05	0.42	10.65	8.67	66.36	575.49			
6407.00	37.12	17.46	0.23	10.48	8.45	71.46	604.01			
6407.50	33.06	15.55	0.21	10.57	8.77	73.86	647.64			
6408.00	27.43	12.90	0.24	10.75	9.25	74.21	686.31			
6408.50	17.85	8.39	0.51	11.56	10.58	71.17	752.99			
6409.00	11.37	5.35	0.99	12.37	11.74	67.89	797.38			
6409.50	14.53	6.83	0.70	11.96	11.16	69.67	777.78			
6410.00	16.46	7.75	0.70	11.98	11.08	69.54	770.55			
6410.50	15.59	7.33	0.42	11.59	10.74	73.62	790.41			
6411.00	10.52	4.95	0.39	11.62	11.05	75.42	833.31			
6411.50	8.03	3.78	0.18	10.66	10.22	80.93	827.37			
6412.00	7.47	3.51	0.03	8.97	8.56	94.25	807.17			
6412.50	8.06	3.79	0.02	8.48	8.04	97.41	782.78			
6413.00	12.19	5.73	0.01	8.43	7.77	97.76	759.44			
6413.50	13.45	6.33	0.05	9.46	8.73	88.58	773.19			
6414.00	20.95	9.86	0.14	10.19	9.05	79.34	718.14			
6414.50	53.61	25.22	0.01	7.87	4.94	91.57	452.74			

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Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6415.00	70.61	33.22	0.01	7.55	3.70	76.01	280.86			
6415.50	60.79	28.60	0.31	9.30	5.98	56.39	337.50			
6416.00	73.17	34.42	0.03	8.03	4.04	66.45	268.27			
6416.50	53.22	25.03	0.38	9.95	7.04	60.02	422.49			
6417.00	47.41	22.30	2.83	12.19	9.60	49.93	479.34			
6417.50	47.58	22.38	2.55	12.17	9.57	50.88	486.75			
6418.00	42.71	20.09	3.79	12.79	10.46	49.86	521.35			
6418.50	42.67	20.07	5.00	12.79	10.46	46.99	491.73			
6419.00	44.47	20.92	6.56	12.56	10.14	43.05	436.38			
6419.50	52.63	24.76	3.56	11.52	8.65	43.89	379.45			
6420.00	64.09	30.15	1.13	10.05	6.55	46.23	303.05			
6420.50	87.73	41.27	69.38	19.70	14.91	13.56	202.25			
6421.00	87.21	41.02	88.23	20.41	15.64	12.94	202.51			
6421.50	90.49	42.57	79.89	19.98	15.04	11.44	172.07			
6422.00	90.12	42.39	65.72	19.49	14.57	12.69	184.88			
6422.50	83.39	39.23	89.31	20.57	16.01	14.71	235.59			
6423.00	82.37	38.75	160.52	22.18	17.69	12.70	224.63			
6423.50	85.84	40.38	265.71	23.62	18.93	10.36	196.21			
6424.00	71.74	33.75	266.88	23.57	19.66	13.60	267.37			
6424.50	66.45	31.26	1.95	9.75	6.12	38.15	233.69			
6425.00	58.92	27.72	4.81	10.72	7.50	35.79	268.42			
6425.50	64.18	30.19	484.83	25.18	21.68	13.28	287.77			
6426.00	56.62	26.64	799.51	26.85	23.76	14.48	343.96			
6426.50	42.68	20.08	10.23	12.79	10.46	39.54	413.69			
6427.00	48.42	22.78	2.99	12.06	9.41	48.65	458.02			
6427.50	100.00	48.12	0.01	9.77	0.00	100.00	0.00			
6428.00	91.35	42.97	0.55	9.54	4.55	40.90	186.04			
6428.50	94.57	44.49	0.10	8.10	2.94	43.47	127.80			
6429.00	100.00	47.87	0.01	6.05	0.00	100.00	0.00			
6429.50	82.93	39.01	0.00	7.10	2.57	78.63	202.05			
6430.00	61.73	29.04	0.11	9.22	5.85	66.06	386.34			
6430.50	78.42	36.89	0.01	7.60	3.32	77.57	257.22			
6431.00	69.17	32.54	0.10	9.19	5.41	65.10	352.23			
6431.50	73.64	34.64	0.04	8.59	4.57	67.43	307.94			
6432.00	80.09	37.68	0.10	8.90	4.53	58.70	265.88			
6432.50	60.36	28.39	3.07	12.20	8.91	46.48	414.04			
6433.00	72.68	34.19	1.55	11.07	7.10	45.71	324.72			
6433.50	82.99	39.04	0.82	10.08	5.55	43.73	242.79			
6434.00	72.89	34.29	0.82	10.58	6.60	49.74	328.48			
6434.50	57.64	27.12	0.44	10.75	7.61	61.26	466.01			
6435.00	48.95	23.03	0.12	10.18	7.51	73.95	555.44			
6435.50	52.49	24.69	0.02	9.09	6.22	87.59	545.16			
6436.00	72.07	33.91	0.01	8.47	4.54	89.28	405.25			
6436.50	82.15	38.65	0.02	8.71	4.23	73.21	309.40			
6437.00	89.61	42.16	0.52	9.81	4.92	44.26	217.58			
6437.50	100.00	47.77	0.01	10.14	0.00	100.00	0.00			
6438.00	100.00	58.06	0.01	9.33	0.00	100.00	0.00			
6438.50	100.00	63.23	0.01	9.40	0.00	100.00	0.00			
6439.00	100.00	63.10	0.01	10.49	0.00	100.00	0.00			
6439.50	100.00	67.82	0.01	10.16	0.00	100.00	0.00			

Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6440.00	100.00	63.40	0.01	12.19	0.00	100.00	0.00			
6440.50	100.00	58.95	0.01	14.27	0.00	100.00	0.00			
6441.00	100.00	55.21	0.01	15.91	0.00	100.00	0.00			
6441.50	100.00	57.57	0.01	15.67	0.00	100.00	0.00			
6442.00	100.00	52.38	0.01	17.35	0.00	100.00	0.00			
6442.50	100.00	49.84	0.01	18.30	0.00	100.00	0.00			
6443.00	100.00	51.14	0.01	18.22	0.00	100.00	0.00			
6443.50	100.00	53.65	0.01	17.68	0.00	100.00	0.00			
6444.00	100.00	57.49	0.01	16.61	0.00	100.00	0.00			
6444.50	100.00	59.93	0.01	15.37	0.00	100.00	0.00			
6445.00	100.00	59.06	0.01	15.43	0.00	100.00	0.00			
6445.50	100.00	62.76	0.01	14.55	0.00	100.00	0.00			
6446.00	100.00	64.58	0.01	14.49	0.00	100.00	0.00			
6446.50	100.00	59.24	0.01	15.68	0.00	100.00	0.00			
6447.00	100.00	57.75	0.01	16.39	0.00	100.00	0.00			
6447.50	100.00	55.26	0.01	17.53	0.00	100.00	0.00			
6448.00	100.00	49.17	0.01	17.32	0.00	100.00	0.00			
6448.50	100.00	50.76	0.01	15.25	0.00	100.00	0.00			
6449.00	100.00	56.04	0.01	13.75	0.00	100.00	0.00			
6449.50	100.00	56.76	0.01	12.39	0.00	100.00	0.00			
6450.00	100.00	51.91	0.01	11.70	0.00	100.00	0.00			
6450.50	98.70	46.43	17.14	11.09	5.71	13.04	74.40			
6451.00	91.01	42.82	4.44	10.95	5.98	28.73	171.73			
6451.50	73.49	34.57	11.66	12.87	8.86	32.37	286.79			
6452.00	70.66	33.24	11.79	12.80	8.94	32.57	291.11			
6452.50	64.75	30.46	1.45	10.37	6.84	45.09	308.35			
6453.00	68.45	32.20	0.03	7.83	4.09	68.21	278.95			
6453.50	77.34	36.38	0.00	5.67	1.45	100.00	144.65			
6454.00	64.82	30.50	0.00	6.82	3.28	100.00	328.03			
6454.50	59.19	27.84	0.00	7.65	4.42	92.31	408.18			
6455.00	63.35	29.80	0.02	8.54	5.09	77.87	395.98			
6455.50	47.51	22.35	0.99	11.45	8.86	58.10	514.58			
6456.00	44.62	20.99	2.08	12.18	9.74	53.65	522.49			
6456.50	51.11	24.04	1.36	11.45	8.66	53.97	467.56			
6457.00	52.47	24.68	0.85	10.80	7.94	55.83	443.12			
6457.50	51.69	24.31	0.70	10.48	7.66	56.61	433.63			
6458.00	56.41	26.54	0.65	10.35	7.27	55.57	403.85			
6458.50	64.70	30.44	0.36	9.77	6.24	56.44	351.98			
6459.00	65.19	30.67	0.52	10.09	6.53	54.10	353.09			
6459.50	72.03	33.89	0.46	9.85	5.92	52.05	307.97			
6460.00	77.72	36.56	0.45	9.67	5.43	49.11	266.51			
6460.50	72.58	34.15	0.78	10.06	6.10	47.57	290.23			
6461.00	78.26	36.81	0.42	9.47	5.20	48.39	251.60			
6461.50	79.27	37.29	0.67	9.86	5.53	45.63	252.25			
6462.00	87.21	41.03	0.22	8.87	4.10	46.94	192.63			
6462.50	90.61	42.62	0.06	8.03	3.08	49.79	153.35			
6463.00	86.02	40.47	0.55	9.37	4.68	41.93	196.11			
6463.50	84.83	39.90	1.20	10.03	5.40	38.82	209.69			
6464.00	92.19	43.37	1.09	9.60	4.57	34.02	155.43			
6464.50	95.50	44.92	1.05	9.28	4.07	30.29	123.15			

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Well name = KIDMAN #1

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6465.00	90.06	42.37	0.75	9.57	4.65	38.50	179.19			
6465.50	80.20	37.73	1.25	10.47	6.10	42.63	259.88			
6466.00	75.14	35.35	1.44	10.81	6.71	44.49	298.33			
6466.50	77.73	36.57	0.78	10.19	5.94	46.63	277.17			
6467.00	85.29	40.12	0.73	9.82	5.17	42.41	219.07			
6467.50	93.03	43.76	1.33	9.72	4.64	32.51	150.85			
6468.00	95.28	44.82	3.09	10.11	4.91	25.65	125.89			
6468.50	98.33	46.26	9.52	10.48	5.11	15.32	78.31			
6469.00	100.00	49.34	0.01	11.10	0.00	100.00	0.00			
6469.50	100.00	55.02	0.01	11.09	0.00	100.00	0.00			
6470.00	100.00	53.72	0.01	11.85	0.00	100.00	0.00			
6470.50	100.00	54.57	0.01	11.33	0.00	100.00	0.00			
6471.00	98.91	46.53	56.06	12.68	7.28	9.19	66.93			
6471.50	94.65	44.52	24.86	12.71	7.54	18.90	142.53			
6472.00	100.00	48.32	0.01	11.89	0.00	100.00	0.00			
6472.50	100.00	52.37	0.01	12.28	0.00	100.00	0.00			
6473.00	100.00	53.82	0.01	13.06	0.00	100.00	0.00			
6473.50	100.00	57.21	0.01	12.47	0.00	100.00	0.00			
6474.00	100.00	64.01	0.01	10.15	0.00	100.00	0.00			
6474.50	100.00	57.78	0.01	10.77	0.00	100.00	0.00			
6475.00	100.00	58.47	0.01	9.50	0.00	100.00	0.00			
6475.50	100.00	56.14	0.01	8.92	0.00	100.00	0.00			
6476.00	100.00	48.46	0.01	9.00	0.00	100.00	0.00			
6476.50	100.00	48.41	0.01	7.66	0.00	100.00	0.00			
6477.00	95.36	44.86	0.17	8.21	3.00	38.60	115.94			
6477.50	88.17	41.48	0.11	8.36	3.55	49.14	174.41			
6478.00	82.04	38.59	0.14	8.65	4.17	52.40	218.59			
6478.50	77.66	36.53	0.20	9.00	4.76	52.86	251.49			
6479.00	81.16	38.18	0.34	9.31	4.88	48.28	235.42			
6479.50	84.20	39.61	0.49	9.47	4.88	44.66	217.82			
6480.00	80.85	38.03	0.91	10.05	5.63	43.17	243.05			
6480.50	85.67	40.30	0.60	9.54	4.87	42.44	206.51			
6481.00	95.03	44.70	0.59	8.94	3.76	33.59	126.15			
6481.50	79.44	37.37	1.51	10.53	6.19	41.19	254.96			
6482.00	81.32	38.26	0.86	9.97	5.53	43.13	238.47			
6482.50	87.88	41.34	0.32	9.03	4.23	44.12	186.73			
6483.00	81.40	38.29	0.72	9.84	5.40	44.12	238.10			
6483.50	84.13	39.58	0.54	9.53	4.93	44.04	217.25			
6484.00	89.33	42.02	0.58	9.37	4.49	39.98	179.64			
6484.50	99.26	46.69	16.65	10.70	5.29	10.67	56.42			
6485.00	97.52	45.88	30.71	12.37	7.05	14.31	100.85			
6485.50	91.29	42.95	17.45	12.70	7.71	23.36	180.20			
6486.00	95.87	45.10	13.59	11.67	6.43	19.62	126.17			
6486.50	94.05	44.24	8.12	11.34	6.20	23.73	147.13			
6487.00	97.53	45.88	6.56	10.41	5.08	19.02	96.66			
6487.50	92.07	43.31	4.16	10.79	5.77	28.17	162.47			
6488.00	96.71	45.49	11.32	11.19	5.91	18.59	109.86			
6488.50	100.00	49.76	0.01	10.85	0.00	100.00	0.00			
6489.00	100.00	57.74	0.01	9.42	0.00	100.00	0.00			
6489.50	100.00	58.61	0.01	8.22	0.00	100.00	0.00			

Well name = KIDMAN #1

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6490.00	100.00	62.51	0.01	7.23	0.00	100.00	0.00			
6490.50	100.00	63.25	0.01	7.53	0.00	100.00	0.00			
6491.00	95.98	45.15	18.50	12.02	6.78	18.26	123.84			
6491.50	93.93	44.19	12.03	11.85	6.72	22.42	150.67			
6492.00	89.44	42.07	17.69	12.95	8.07	24.77	199.85			
6492.50	90.43	42.54	10.25	13.97	9.03	21.66	195.59			
6493.00	90.89	42.76	13.68	14.87	9.90	19.68	194.88			
6493.50	97.76	45.99	15.28	14.64	9.31	10.92	101.62			
6494.00	100.00	48.90	0.01	13.95	0.00	100.00	0.00			
6494.50	100.00	51.50	0.01	13.16	0.00	100.00	0.00			
6495.00	100.00	54.44	0.01	12.28	0.00	100.00	0.00			
6495.50	100.00	55.99	0.01	11.88	0.00	100.00	0.00			
6496.00	100.00	56.90	0.01	12.10	0.00	100.00	0.00			
6496.50	100.00	52.11	0.01	14.10	0.00	100.00	0.00			
6497.00	100.00	56.23	0.01	14.30	0.00	100.00	0.00			
6497.50	100.00	61.60	0.01	15.48	0.00	100.00	0.00			
6498.00	100.00	57.56	0.01	16.38	0.00	100.00	0.00			
6498.50	100.00	51.90	0.01	17.30	0.00	100.00	0.00			
6499.00	84.34	39.68	96.25	20.80	16.20	14.27	231.13			
6499.50	74.22	34.92	0.41	8.76	4.71	45.15	212.43			
6500.00	69.30	32.60	1321.66	28.37	24.58	11.13	273.62			
6500.50	88.20	41.49	3387.89	30.81	25.99	4.93	128.08			
6501.00	57.44	27.02	50.61	10.90	7.77	12.51	97.15			
6501.50	51.12	24.05	16.03	11.71	8.92	5.47	48.78			
6502.00	C O A L		C O A L		C O A L		C O A L			
6502.50	C O A L		C O A L		C O A L		C O A L			
6503.00	C O A L		C O A L		C O A L		C O A L			
6503.50	C O A L		C O A L		C O A L		C O A L			
6504.00	C O A L		C O A L		C O A L		C O A L			
6504.50	C O A L		C O A L		C O A L		C O A L			
6505.00	C O A L		C O A L		C O A L		C O A L			
6505.50	C O A L		C O A L		C O A L		C O A L			
6506.00	C O A L		C O A L		C O A L		C O A L			
6506.50	C O A L		C O A L		C O A L		C O A L			
6507.00	C O A L		C O A L		C O A L		C O A L			
6507.50	C O A L		C O A L		C O A L		C O A L			
6508.00	42.31	19.90	11.88	12.84	10.53	28.55	300.64			
6508.50	61.17	28.78	77.64	19.77	16.43	19.46	319.68			
6509.00	82.37	38.75	21.99	16.53	12.03	21.93	263.88			
6509.50	86.51	40.70	16.09	15.70	10.98	23.05	253.00			
6510.00	86.93	40.90	15.82	15.51	10.76	22.01	236.86			
6510.50	88.80	41.77	23.94	16.54	11.69	17.44	203.99			
6511.00	93.60	44.03	25.46	16.24	11.13	11.59	129.04			
6511.50	99.26	46.69	19.75	14.93	9.51	4.69	44.58			
6512.00	100.00	49.52	0.01	13.61	0.00	100.00	0.00			
6512.50	100.00	52.89	0.01	11.88	0.00	100.00	0.00			
6513.00	100.00	55.19	0.01	10.78	0.00	100.00	0.00			
6513.50	100.00	56.14	0.01	10.06	0.00	100.00	0.00			
6514.00	100.00	48.09	0.01	11.74	0.00	100.00	0.00			
6514.50	96.02	45.17	20.19	11.86	6.62	16.51	109.27			

Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6515.00	98.10	46.15	20.25	11.26	5.90	12.48	73.66			
6515.50	100.00	48.54	0.01	10.28	0.00	100.00	0.00			
6516.00	100.00	50.35	0.01	9.47	0.00	100.00	0.00			
6516.50	100.00	51.13	0.01	8.61	0.00	100.00	0.00			
6517.00	99.89	46.99	4.87	8.60	3.14	5.38	16.89			
6517.50	71.47	33.62	6.07	10.79	6.89	30.40	209.35			
6518.00	77.50	36.46	1.24	9.01	4.78	34.22	163.63			
6518.50	100.00	47.13	0.01	5.97	0.00	100.00	0.00			
6519.00	54.80	25.78	10.81	11.43	8.44	31.48	265.75			
6519.50	63.21	29.74	6.18	10.67	7.22	31.86	229.99			
6520.00	89.08	41.91	0.44	8.16	3.30	32.17	106.11			
6520.50	77.28	36.36	2.39	9.66	5.44	31.88	173.41			
6521.00	65.64	30.88	7.14	11.08	7.50	31.66	237.30			
6521.50	61.80	29.07	12.31	11.89	8.52	30.45	259.42			
6522.00	61.58	28.97	21.31	12.67	9.30	27.80	258.62			
6522.50	70.82	33.32	24.53	12.78	8.91	24.84	221.38			
6523.00	77.25	36.34	12.12	13.80	9.58	20.82	199.50			
6523.50	77.81	36.60	23.85	15.90	11.65	17.22	200.56			
6524.00	73.68	34.66	66.72	18.93	14.91	14.35	214.02			
6524.50	70.87	33.34	3.20	9.19	5.32	28.08	149.30			
6525.00	63.58	29.91	17.70	10.12	6.65	18.02	119.81			
6525.50	35.33	16.62	30.01	13.73	11.80	12.39	146.23			
6526.00	28.97	13.63	47.05	14.55	12.96	9.69	125.66	0.28	0.23	2.00
6526.50	C O A L		C O A L		C O A L		C O A L			
6527.00	C O A L		C O A L		C O A L		C O A L			
6527.50	C O A L		C O A L		C O A L		C O A L			
6528.00	C O A L		C O A L		C O A L		C O A L			
6528.50	C O A L		C O A L		C O A L		C O A L			
6529.00	C O A L		C O A L		C O A L		C O A L			
6529.50	C O A L		C O A L		C O A L		C O A L			
6530.00	C O A L		C O A L		C O A L		C O A L			
6530.50	C O A L		C O A L		C O A L		C O A L			
6531.00	C O A L		C O A L		C O A L		C O A L			
6531.50	C O A L		C O A L		C O A L		C O A L			
6532.00	C O A L		C O A L		C O A L		C O A L			
6532.50	C O A L		C O A L		C O A L		C O A L			
6533.00	C O A L		C O A L		C O A L		C O A L			
6533.50	C O A L		C O A L		C O A L		C O A L			
6534.00	C O A L		C O A L		C O A L		C O A L			
6534.50	C O A L		C O A L		C O A L		C O A L			
6535.00	C O A L		C O A L		C O A L		C O A L			
6535.50	C O A L		C O A L		C O A L		C O A L			
6536.00	C O A L		C O A L		C O A L		C O A L			
6536.50	C O A L		C O A L		C O A L		C O A L			
6537.00	C O A L		C O A L		C O A L		C O A L			
6537.50	C O A L		C O A L		C O A L		C O A L			
6538.00	C O A L		C O A L		C O A L		C O A L			
6538.50	C O A L		C O A L		C O A L		C O A L			
6539.00	C O A L		C O A L		C O A L		C O A L			
6539.50	C O A L		C O A L		C O A L		C O A L			

Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H 0.35	Cum Hc*H 0.28	Cum H 2.50
6540.00	24.07	11.33	31.11	15.17	13.86	24.58	340.52			
6540.50	32.79	15.42	18.75	14.06	12.27	27.36	335.69			
6541.00	39.97	18.80	12.17	13.14	10.96	30.65	335.85			
6541.50	51.56	24.26	3.41	10.53	7.71	40.34	311.05			
6542.00	74.79	35.18	1.91	9.87	5.79	36.40	210.62			
6542.50	60.44	28.43	1.03	9.09	5.79	42.88	248.44			
6543.00	52.57	24.73	1.89	9.78	6.91	42.71	295.27			
6543.50	63.02	29.65	0.24	8.19	4.75	51.27	243.43			
6544.00	58.95	27.73	0.09	7.76	4.54	59.88	271.70			
6544.50	48.43	22.78	0.13	8.23	5.59	63.43	354.48			
6545.00	38.02	17.89	0.27	9.03	6.95	63.17	439.31			
6545.50	30.46	14.33	2.83	11.60	9.94	51.12	507.88			
6546.00	29.94	14.08	5.44	12.54	10.91	47.57	518.82	0.40	0.31	3.00
6546.50	30.17	14.19	6.61	12.76	11.11	46.18	513.32			
6547.00	34.33	16.15	2.71	11.44	9.56	50.22	480.26			
6547.50	42.06	19.79	2.09	10.99	8.69	49.60	431.02			
6548.00	45.83	21.56	1.86	10.64	8.14	48.54	395.21			
6548.50	39.85	18.75	7.53	12.33	10.16	41.69	423.38			
6549.00	49.24	23.16	8.03	12.24	9.55	38.88	371.30			
6549.50	46.72	21.98	10.84	12.63	10.08	37.63	379.30			
6550.00	25.10	11.81	15.26	14.57	13.20	37.23	491.47	0.47	0.35	3.50
6550.50	14.30	6.72	12.47	14.44	13.66	43.84	598.86	0.54	0.39	4.00
6551.00	9.52	4.48	7.64	13.69	13.17	50.59	666.40			
6551.50	11.20	5.27	5.54	13.40	12.79	52.91	676.57			
6552.00	11.70	5.50	4.40	13.30	12.66	54.98	696.13			
6552.50	1.22	0.58	10.52	15.18	15.11	52.65	795.47			
6553.00	6.18	2.91	1.67	13.00	12.67	65.10	824.57			
6553.50	0.00	0.00	4.92	14.97	14.97	59.62	892.27			
6554.00	0.00	0.00	6.87	15.79	15.79	58.01	915.72			
6554.50	0.00	0.00	10.58	15.93	15.93	54.97	875.47			
6555.00	0.00	0.00	5.82	14.51	14.51	56.81	824.55			
6555.50	0.04	0.02	3.12	13.15	13.15	59.87	787.26			
6556.00	2.60	1.22	1.50	12.34	12.20	64.91	792.00			
6556.50	9.21	4.33	0.44	11.16	10.66	72.90	776.91			
6557.00	0.38	0.18	1.20	12.56	12.54	68.17	854.47			
6557.50	4.61	2.17	1.13	12.32	12.07	67.46	814.32			
6558.00	16.85	7.93	0.71	11.57	10.65	67.98	723.83			
6558.50	16.89	7.95	1.06	11.89	10.96	64.74	709.82			
6559.00	16.04	7.54	1.30	11.70	10.82	62.17	672.79			
6559.50	14.26	6.71	2.34	11.76	10.98	56.58	621.13			
6560.00	23.81	11.20	1.60	10.74	9.44	55.24	521.22			
6560.50	40.57	19.08	1.13	9.85	7.63	51.47	392.73			
6561.00	50.13	23.58	1.58	9.95	7.22	46.04	332.22			
6561.50	29.31	13.79	10.59	13.21	11.61	38.22	443.92	0.59	0.43	4.50
6562.00	28.86	13.58	10.63	12.75	11.18	41.44	463.10	0.65	0.46	5.00
6562.50	28.98	13.63	14.33	14.55	12.96	37.56	486.95	0.71	0.50	5.50
6563.00	28.94	13.61	13.98	14.55	12.97	38.17	495.14	0.78	0.54	6.00
6563.50	25.33	11.92	32.87	16.76	15.37	30.94	475.65	0.86	0.59	6.50
6564.00	48.55	22.84	26.84	16.23	13.58	26.36	358.05			
6564.50	56.24	26.45	43.25	17.71	14.64	21.80	319.19			

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Well name = KIDMAN #1

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6565.00	39.63	18.65	48.47	17.99	15.83	25.46	402.97			
6565.50	20.35	9.57	19.23	15.65	14.54	38.18	555.07	0.93	0.64	7.00
6566.00	8.07	3.80	25.75	17.22	16.78	41.14	690.36	1.01	0.69	7.50
6566.50	3.57	1.68	28.14	17.80	17.60	42.36	745.48	1.10	0.74	8.00
6567.00	1.94	0.91	35.96	18.00	17.90	39.16	700.87	1.19	0.79	8.50
6567.50	2.73	1.28	45.95	17.90	17.75	34.46	611.86	1.28	0.85	9.00
6568.00	C O A L		C O A L		C O A L		C O A L			
6568.50	C O A L		C O A L		C O A L		C O A L			
6569.00	C O A L		C O A L		C O A L		C O A L			
6569.50	C O A L		C O A L		C O A L		C O A L			
6570.00	17.22	8.10	74.64	16.05	15.11	13.23	199.87	1.35	0.92	9.50
6570.50	23.39	11.00	19.39	15.26	13.98	35.55	497.10	1.42	0.96	10.00
6571.00	40.79	19.19	12.59	13.03	10.81	38.50	416.05			
6571.50	42.09	19.80	11.52	12.87	10.57	38.65	408.57			
6572.00	44.79	21.07	3.64	11.20	8.76	44.08	385.91			
6572.50	53.48	25.16	1.17	9.90	6.98	48.06	335.57			
6573.00	64.04	30.13	0.17	8.37	4.87	55.63	271.13			
6573.50	72.41	34.06	0.01	7.11	3.16	65.92	208.14			
6574.00	76.80	36.13	0.00	6.30	2.10	77.25	162.60			
6574.50	38.67	18.19	1.56	10.86	8.75	52.89	462.80			
6575.00	41.59	19.56	3.40	12.10	9.83	48.85	480.41			
6575.50	44.76	21.06	5.52	12.53	10.08	44.68	450.48			
6576.00	46.10	21.68	5.58	12.36	9.84	43.71	430.08			
6576.50	27.84	13.09	8.43	13.07	11.55	44.98	519.47	1.48	0.99	10.50
6577.00	22.57	10.62	9.52	13.46	12.22	45.70	558.73	1.54	1.03	11.00
6577.50	19.61	9.22	1.20	11.32	10.25	61.16	626.86			
6578.00	17.51	8.24	1.13	11.30	10.34	62.05	641.92			
6578.50	18.75	8.82	0.77	10.90	9.88	64.42	636.37			
6579.00	23.64	11.12	0.10	8.98	7.69	77.02	592.28			
6579.50	44.19	20.79	0.13	8.17	5.76	64.29	370.12			
6580.00	64.56	30.37	0.12	7.54	4.02	52.20	209.75			
6580.50	69.50	32.69	0.87	8.70	4.91	38.84	190.57			
6581.00	51.68	24.31	14.11	11.64	8.82	30.23	266.64			
6581.50	59.02	27.77	13.41	13.50	10.27	23.18	238.15			
6582.00	69.67	32.77	12.95	13.51	9.71	19.77	191.84			
6582.50	68.74	32.34	20.23	14.74	10.98	16.77	184.19			
6583.00	100.00	51.66	0.01	20.87	0.00	100.00	0.00			
6583.50	100.00	47.69	0.01	23.99	0.00	100.00	0.00			
6584.00	60.64	28.53	27.13	10.50	7.18	16.28	116.94			
6584.50	42.25	19.88	20.50	12.85	10.54	12.89	135.81			
6585.00	C O A L		C O A L		C O A L		C O A L			
6585.50	C O A L		C O A L		C O A L		C O A L			
6586.00	C O A L		C O A L		C O A L		C O A L			
6586.50	C O A L		C O A L		C O A L		C O A L			
6587.00	C O A L		C O A L		C O A L		C O A L			
6587.50	C O A L		C O A L		C O A L		C O A L			
6588.00	C O A L		C O A L		C O A L		C O A L			
6588.50	C O A L		C O A L		C O A L		C O A L			
6589.00	49.27	23.18	4647.06	29.71	27.02	5.00	134.99			
6589.50	59.20	27.85	8.70	10.68	7.45	29.37	218.73			

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6590.00	100.00	47.31	0.01	10.31	0.00	100.00	0.00			
6590.50	97.47	45.86	32.66	11.92	6.60	11.40	75.25			
6591.00	96.58	45.43	19.08	11.35	6.08	14.14	85.97			
6591.50	68.55	32.25	18.70	15.19	11.45	22.24	254.59			
6592.00	75.08	35.32	21.50	15.69	11.59	19.51	226.02			
6592.50	94.04	44.24	28.83	16.51	11.38	10.18	115.82			
6593.00	100.00	54.26	0.01	19.73	0.00	100.00	0.00			
6593.50	97.45	45.84	288.89	23.18	17.86	3.54	63.29			
6594.00	77.35	36.39	1010.29	26.89	22.67	7.22	163.60			
6594.50	74.61	35.10	1543.16	28.01	23.93	6.75	161.45			
6595.00	59.80	28.13	537.33	24.41	21.14	9.61	203.21			
6595.50	68.23	32.10	140.20	20.83	17.11	12.17	208.23			
6596.00	61.45	28.91	121.44	20.32	16.96	14.00	237.45			
6596.50	52.65	24.77	17.93	11.52	8.64	27.03	233.63			
6597.00	47.16	22.18	10.92	12.22	9.65	24.65	237.74			
6597.50	38.20	17.97	18.04	13.37	11.28	22.05	248.70			
6598.00	35.78	16.83	21.92	13.68	11.72	19.92	233.51			
6598.50	35.85	16.86	23.52	13.67	11.71	18.02	210.96			
6599.00	35.96	16.91	24.51	13.65	11.69	16.80	196.42			
6599.50	30.44	14.32	31.75	14.36	12.70	17.20	218.39			
6600.00	24.29	11.43	42.42	15.15	13.82	17.56	242.63	1.61	1.08	11.50
6600.50	17.89	8.42	61.65	15.96	14.99	16.40	245.70	1.69	1.15	12.00
6601.00	11.52	5.42	95.88	16.78	16.15	14.11	227.86	1.77	1.21	12.50
6601.50	7.13	3.35	143.69	17.34	16.95	10.91	184.96	1.85	1.29	13.00
6602.00	C O A L		C O A L	C O A L	C O A L	C O A L	C O A L	C O A L		
6602.50	C O A L		C O A L	C O A L	C O A L	C O A L	C O A L	C O A L		
6603.00	C O A L		C O A L	C O A L	C O A L	C O A L	C O A L	C O A L		
6603.50	C O A L		C O A L	C O A L	C O A L	C O A L	C O A L	C O A L		
6604.00	C O A L		C O A L	C O A L	C O A L	C O A L	C O A L	C O A L		
6604.50	C O A L		C O A L	C O A L	C O A L	C O A L	C O A L	C O A L		
6605.00	C O A L		C O A L	C O A L	C O A L	C O A L	C O A L	C O A L		
6605.50	42.58	20.03	15.75	12.81	10.48	20.03	209.95			
6606.00	47.11	22.16	13.46	12.23	9.65	18.15	175.23			
6606.50	42.51	20.00	18.27	12.81	10.49	15.83	166.06			
6607.00	37.01	17.41	24.49	13.52	11.50	15.43	177.35			
6607.50	31.13	14.65	30.30	14.27	12.57	17.50	220.01			
6608.00	25.54	12.02	36.50	14.99	13.59	19.53	265.49	1.92	1.34	13.50
6608.50	21.23	9.99	37.04	15.54	14.38	23.62	339.65	1.99	1.40	14.00
6609.00	18.77	8.83	32.83	15.85	14.83	28.42	421.31	2.07	1.45	14.50
6609.50	17.45	8.21	31.08	16.02	15.07	30.67	462.09	2.14	1.50	15.00
6610.00	16.54	7.78	30.64	16.14	15.23	31.70	482.90	2.22	1.56	15.50
6610.50	15.81	7.44	32.48	16.23	15.37	31.15	478.67	2.30	1.61	16.00
6611.00	15.64	7.36	26.78	15.52	14.67	31.87	467.57	2.37	1.66	16.50
6611.50	15.81	7.44	13.90	13.39	12.53	36.13	452.61	2.43	1.70	17.00
6612.00	15.99	7.52	12.64	12.01	11.14	39.51	440.18	2.49	1.73	17.50
6612.50	13.07	6.15	10.23	12.45	11.74	39.79	467.16	2.55	1.77	18.00
6613.00	11.58	5.45	11.47	12.22	11.59	41.89	485.34	2.60	1.80	18.50
6613.50	12.18	5.73	12.00	13.03	12.36	38.89	480.71	2.67	1.84	19.00
6614.00	13.00	6.11	15.75	13.80	13.09	35.99	471.34	2.73	1.88	19.50
6614.50	14.05	6.61	11.32	12.64	11.87	37.87	449.62	2.79	1.92	20.00

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Well name = KIDMAN #1

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6615.00	14.87	6.99	10.80	12.29	11.48	36.99	424.63	2.85	1.96	20.50
6615.50	15.12	7.11	10.50	12.12	11.30	36.72	414.77	2.90	1.99	21.00
6616.00	13.70	6.44	11.79	11.53	10.78	39.10	421.47	2.96	2.02	21.50
6616.50	9.41	4.43	12.47	12.69	12.17	37.00	450.42	3.02	2.06	22.00
6617.00	6.09	2.86	14.55	13.17	12.84	36.61	470.06	3.08	2.10	22.50
6617.50	3.44	1.62	11.94	12.57	12.38	39.13	484.65	3.15	2.14	23.00
6618.00	1.84	0.87	14.27	12.97	12.87	37.20	478.65	3.21	2.18	23.50
6618.50	0.40	0.19	12.84	12.52	12.50	37.90	473.74	3.27	2.22	24.00
6619.00	0.96	0.45	28.71	14.89	14.83	31.19	462.59	3.35	2.27	24.50
6619.50	2.44	1.15	28.99	14.85	14.71	30.44	447.88	3.42	2.32	25.00
6620.00	3.66	1.72	28.31	14.73	14.53	30.07	437.03	3.49	2.37	25.50
6620.50	3.78	1.78	21.88	13.88	13.68	31.42	429.72	3.56	2.42	26.00
6621.00	1.73	0.81	31.11	14.81	14.72	28.99	426.60	3.63	2.47	26.50
6621.50	0.72	0.34	51.37	16.20	16.16	25.89	418.31	3.72	2.53	27.00
6622.00	2.86	1.35	38.61	15.15	15.00	25.94	389.02	3.79	2.59	27.50
6622.50	6.02	2.83	20.65	13.02	12.69	27.49	348.87	3.85	2.63	28.00
6623.00	7.90	3.72	39.89	14.89	14.46	22.52	325.66	3.93	2.69	28.50
6623.50	9.11	4.29	36.01	14.54	14.04	22.41	314.72	4.00	2.74	29.00
6624.00	6.75	3.18	20.62	12.94	12.57	26.80	336.82	4.06	2.79	29.50
6624.50	3.99	1.88	72.63	17.00	16.78	22.37	375.46	4.14	2.86	30.00
6625.00	1.85	0.87	98.24	18.02	17.92	22.16	396.96	4.23	2.92	30.50
6625.50	0.05	0.02	105.51	18.25	18.24	22.37	408.01	4.32	3.00	31.00
6626.00	0.00	0.00	120.63	18.57	18.57	21.56	400.43	4.42	3.07	31.50
6626.50	0.00	0.00	127.32	18.69	18.69	21.15	395.28	4.51	3.14	32.00
6627.00	0.00	0.00	122.86	18.72	18.72	21.87	409.39	4.60	3.22	32.50
6627.50	0.00	0.00	118.50	18.72	18.72	22.45	420.15	4.70	3.29	33.00
6628.00	0.00	0.00	110.84	18.58	18.58	22.98	427.07	4.79	3.36	33.50
6628.50	0.41	0.19	100.73	18.20	18.18	22.86	415.55	4.88	3.43	34.00
6629.00	2.49	1.17	103.50	17.93	17.80	20.76	369.43	4.97	3.50	34.50
6629.50	5.58	2.63	81.20	17.00	16.69	19.93	332.64	5.05	3.57	35.00
6630.00	8.99	4.23	39.19	14.66	14.17	21.29	301.64	5.12	3.62	35.50
6630.50	11.39	5.36	28.66	13.65	13.02	21.68	282.31	5.19	3.67	36.00
6631.00	9.81	4.62	88.40	17.00	16.46	17.23	283.65	5.27	3.74	36.50
6631.50	5.33	2.51	96.79	17.57	17.28	19.55	337.85	5.36	3.81	37.00
6632.00	3.00	1.41	98.23	17.87	17.71	21.24	376.02	5.45	3.88	37.50
6632.50	4.98	2.34	84.71	17.62	17.34	22.19	384.84	5.53	3.95	38.00
6633.00	9.38	4.41	65.33	17.05	16.54	23.18	383.39	5.62	4.01	38.50
6633.50	14.53	6.84	56.81	16.39	15.60	21.28	331.91	5.69	4.07	39.00
6634.00	21.09	9.92	47.41	15.55	14.40	18.55	267.18	5.77	4.13	39.50
6634.50	36.09	16.98	25.33	13.64	11.67	15.78	184.05			
6635.00	39.43	18.55	22.17	13.21	11.06	14.79	163.55			
6635.50	40.78	19.18	20.33	13.04	10.81	15.28	165.14			
6636.00	37.81	17.79	23.71	13.42	11.35	15.21	172.70			
6636.50	26.65	12.54	47.65	14.84	13.39	12.26	164.12	5.83	4.19	40.00
6637.00	C O A L		C O A L		C O A L		C O A L			
6637.50	C O A L		C O A L		C O A L		C O A L			
6638.00	C O A L		C O A L		C O A L		C O A L			
6638.50	C O A L		C O A L		C O A L		C O A L			
6639.00	47.87	22.52	11.77	12.13	9.51	21.21	201.77			
6639.50	51.31	24.14	10.43	11.69	8.89	19.79	175.90			

Well name = KIDMAN #1

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6640.00	53.22	25.03	11.74	11.44	8.54	12.31	105.12			
6640.50	54.49	25.63	12.40	11.28	8.31	7.87	65.34			
6641.00	55.42	26.07	12.05	11.16	8.14	7.02	57.12			
6641.50	51.49	24.22	14.69	11.67	8.85	7.73	68.47			
6642.00	48.38	22.76	16.04	12.06	9.42	10.47	98.64			
6642.50	54.42	25.60	10.16	11.29	8.32	15.29	127.19			
6643.00	59.45	27.97	22.05	10.65	7.40	19.48	144.15			
6643.50	61.62	28.99	47.81	17.04	13.67	14.01	191.51			
6644.00	56.95	26.79	17.46	10.97	7.86	23.99	188.52			
6644.50	53.50	25.17	21.43	11.41	8.49	24.54	208.30			
6645.00	45.90	21.59	11.69	12.38	9.88	24.32	240.18			
6645.50	38.67	18.19	16.32	13.31	11.19	24.15	270.37			
6646.00	39.20	18.44	25.74	14.76	12.62	21.78	274.91			
6646.50	40.12	18.87	15.25	13.12	10.93	24.22	264.74			
6647.00	41.31	19.43	14.71	12.97	10.71	23.71	253.96			
6647.50	40.65	19.12	15.78	13.05	10.83	22.58	244.60			
6648.00	39.20	18.44	16.85	13.24	11.10	22.62	251.01			
6648.50	37.92	17.84	17.42	13.40	11.33	23.32	264.29			
6649.00	36.71	17.27	17.72	13.56	11.55	24.35	281.35			
6649.50	34.83	16.38	18.51	13.80	11.90	25.42	302.44			
6650.00	34.84	16.39	16.97	13.80	11.89	27.63	328.58			
6650.50	37.03	17.42	13.99	13.52	11.49	30.22	347.41			
6651.00	39.07	18.38	11.83	13.25	11.12	32.46	361.01			
6651.50	81.08	38.14	27.22	16.50	12.07	16.79	202.64			
6652.00	98.45	46.31	31.53	16.45	11.08	5.30	58.73			
6652.50	86.49	40.69	51.67	18.23	13.50	11.20	151.22			
6653.00	61.96	29.15	81.15	19.52	16.13	17.17	276.97			
6653.50	54.70	25.73	5.60	11.25	8.27	37.61	311.00			
6654.00	50.13	23.58	3.36	11.84	9.10	46.28	421.26			
6654.50	64.78	30.47	49.15	19.27	15.73	24.74	389.24			
6655.00	79.95	37.61	106.19	21.16	16.80	15.57	261.64			
6655.50	62.93	29.60	2.51	10.20	6.77	39.00	263.86			
6656.00	64.41	30.30	3.10	10.01	6.50	35.39	229.89			
6656.50	61.17	28.78	6.25	10.43	7.09	31.11	220.46			
6657.00	48.30	22.72	25.67	12.07	9.44	26.36	248.75			
6657.50	45.34	21.33	11.63	12.45	9.98	25.24	251.82			
6658.00	45.54	21.42	11.80	12.43	9.94	24.51	243.64			
6658.50	65.47	30.80	150.47	20.83	17.26	11.67	201.34			
6659.00	100.00	47.67	0.01	21.87	0.00	100.00	0.00			
6659.50	100.00	49.43	0.01	22.67	0.00	100.00	0.00			
6660.00	100.00	52.04	0.01	22.94	0.00	100.00	0.00			
6660.50	100.00	48.42	0.01	21.22	0.00	100.00	0.00			
6661.00	91.70	43.14	42.91	17.38	12.38	7.66	94.85			
6661.50	91.52	43.05	15.95	14.47	9.47	11.10	105.14			
6662.00	78.35	36.86	15.70	14.51	10.23	18.21	186.33			
6662.50	69.03	32.48	25.94	16.07	12.30	19.54	240.40			
6663.00	63.51	29.88	47.05	17.65	14.18	17.46	247.59			
6663.50	79.86	37.57	54.11	18.18	13.81	12.17	168.19			
6664.00	100.00	48.09	0.01	18.27	0.00	100.00	0.00			
6664.50	100.00	48.01	0.01	17.90	0.00	100.00	0.00			

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6665.00	85.08	40.02	105.58	20.01	15.36	7.79	119.62			
6665.50	92.05	43.30	90.49	19.61	14.58	6.07	88.47			
6666.00	97.07	45.66	91.36	19.58	14.28	3.89	55.49			
6666.50	93.61	44.04	126.23	20.61	15.50	5.10	79.10			
6667.00	100.00	52.28	0.01	18.85	0.00	100.00	0.00			
6667.50	100.00	52.83	0.01	17.66	0.00	100.00	0.00			
6668.00	100.00	53.75	0.01	17.65	0.00	100.00	0.00			
6668.50	100.00	49.04	0.01	19.68	0.00	100.00	0.00			
6669.00	100.00	53.71	0.01	18.59	0.00	100.00	0.00			
6669.50	100.00	57.55	0.01	17.09	0.00	100.00	0.00			
6670.00	100.00	58.29	0.01	15.82	0.00	100.00	0.00			
6670.50	100.00	49.89	0.01	14.72	0.00	100.00	0.00			
6671.00	79.81	37.54	17.12	14.34	9.98	13.50	134.77			
6671.50	83.11	39.10	31.69	11.97	7.43	15.83	117.65			
6672.00	88.74	41.75	9.86	10.03	5.18	15.46	80.13			
6672.50	78.33	36.85	10.54	10.09	5.81	18.76	109.04			
6673.00	51.84	24.39	11.81	12.15	9.31	19.41	180.78			
6673.50	18.03	8.48	36.11	14.69	13.71	20.45	280.34	5.90	4.25	40.50
6674.00	5.90	2.77	68.30	16.72	16.40	21.70	355.95	5.98	4.31	41.00
6674.50	0.97	0.45	92.27	17.78	17.73	22.41	397.37	6.07	4.38	41.50
6675.00	0.00	0.00	89.55	17.96	17.96	23.93	429.75	6.16	4.45	42.00
6675.50	0.00	0.00	55.28	16.76	16.76	27.22	456.24	6.25	4.51	42.50
6676.00	0.00	0.00	65.29	17.24	17.24	26.32	453.80	6.33	4.57	43.00
6676.50	0.00	0.00	114.25	18.77	18.77	23.24	436.20	6.43	4.64	43.50
6677.00	0.00	0.00	121.52	18.76	18.76	22.20	416.35	6.52	4.72	44.00
6677.50	0.00	0.00	127.45	18.72	18.72	21.29	398.62	6.61	4.79	44.50
6678.00	0.00	0.00	93.20	17.62	17.62	21.77	383.71	6.70	4.86	45.00
6678.50	0.00	0.00	67.27	16.49	16.49	22.40	369.37	6.78	4.92	45.50
6679.00	0.00	0.00	96.42	17.45	17.45	20.40	355.93	6.87	4.99	46.00
6679.50	0.00	0.00	115.98	17.93	17.93	19.42	348.27	6.96	5.06	46.50
6680.00	0.00	0.00	90.89	17.08	17.08	19.71	336.66	7.05	5.13	47.00
6680.50	0.00	0.00	88.81	16.87	16.87	19.14	322.84	7.13	5.20	47.50
6681.00	0.00	0.00	91.29	16.85	16.85	18.54	312.35	7.21	5.27	48.00
6681.50	6.78	3.19	56.31	15.48	15.11	18.90	285.67	7.29	5.33	48.50
6682.00	0.66	0.31	66.67	15.83	15.79	19.17	302.73	7.37	5.39	49.00
6682.50	0.92	0.43	89.08	16.80	16.75	18.51	309.99	7.45	5.46	49.50
6683.00	0.00	0.00	130.66	18.07	18.07	18.04	326.12	7.54	5.54	50.00
6683.50	0.00	0.00	151.97	18.53	18.53	17.60	326.17	7.64	5.61	50.50
6684.00	0.00	0.00	152.85	18.50	18.50	17.37	321.47	7.73	5.69	51.00
6684.50	0.00	0.00	151.59	18.47	18.47	17.35	320.36	7.82	5.77	51.50
6685.00	0.00	0.00	150.73	18.47	18.47	17.46	322.42	7.91	5.84	52.00
6685.50	0.00	0.00	78.56	16.60	16.60	20.10	333.80	8.00	5.91	52.50
6686.00	0.00	0.00	59.88	15.86	15.86	21.55	341.71	8.08	5.97	53.00
6686.50	0.00	0.00	51.77	15.46	15.46	22.38	345.90	8.15	6.03	53.50
6687.00	0.00	0.00	67.65	16.31	16.31	21.47	350.28	8.23	6.10	54.00
6687.50	0.00	0.00	71.88	16.55	16.55	21.45	354.97	8.32	6.16	54.50
6688.00	0.00	0.00	94.17	17.41	17.41	20.62	359.00	8.40	6.23	55.00
6688.50	0.00	0.00	119.58	18.11	18.11	19.68	356.45	8.49	6.30	55.50
6689.00	0.00	0.00	141.15	18.44	18.44	18.39	339.04	8.59	6.38	56.00
6689.50	0.15	0.07	138.44	18.23	18.22	17.76	323.60	8.68	6.45	56.50

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6690.00	0.00	0.00	98.54	17.20	17.20	18.88	324.80	8.76	6.52	57.00
6690.50	0.00	0.00	61.20	15.86	15.86	21.15	335.53	8.84	6.58	57.50
6691.00	7.40	3.48	30.34	14.61	14.20	26.96	382.94	8.91	6.64	58.00
6691.50	13.82	6.50	19.01	13.55	12.80	30.05	384.56	8.98	6.68	58.50
6692.00	19.95	9.38	15.96	12.85	11.76	28.39	333.89	9.04	6.72	59.00
6692.50	26.74	12.58	13.84	12.31	10.85	26.41	286.67	9.09	6.76	59.50
6693.00	26.47	12.45	10.99	11.39	9.95	26.76	266.26			
6693.50	22.74	10.70	19.97	13.38	12.14	25.03	303.89	9.15	6.81	60.00
6694.00	16.53	7.77	26.39	14.76	13.85	28.18	390.47	9.22	6.86	60.50
6694.50	13.87	6.53	11.33	12.44	11.68	36.85	430.52	9.28	6.90	61.00
6695.00	35.59	16.74	6.55	10.44	8.50	36.94	313.93			
6695.50	54.14	25.47	16.85	10.84	7.88	24.47	192.84			
6696.00	57.64	27.11	13.75	12.70	9.55	16.58	158.43			
6696.50	53.91	25.36	20.84	13.67	10.72	13.90	149.06			
6697.00	50.72	23.86	19.05	13.19	10.42	14.00	145.90			
6697.50	57.62	27.11	40.21	11.07	7.93	15.61	123.76			
6698.00	55.68	26.19	15.87	9.81	6.77	19.80	134.09			
6698.50	53.51	25.17	17.73	10.15	7.23	20.93	151.32			
6699.00	39.17	18.42	19.65	10.69	8.55	25.70	219.78			
6699.50	27.83	13.09	5.62	9.76	8.24	37.46	308.64			
6700.00	31.61	14.87	3.11	9.54	7.82	41.80	326.72			
6700.50	28.79	13.54	3.63	10.28	8.71	43.93	382.59			
6701.00	23.25	10.94	3.39	10.54	9.27	46.82	434.06			
6701.50	12.53	5.89	6.57	11.64	10.95	45.73	500.85	9.33	6.93	61.50
6702.00	7.99	3.76	10.25	12.49	12.05	41.31	498.00	9.40	6.96	62.00
6702.50	11.78	5.54	12.99	12.81	12.17	35.92	437.00	9.46	7.00	62.50
6703.00	18.20	8.56	13.41	12.71	11.71	32.61	381.92	9.51	7.04	63.00
6703.50	18.83	8.86	14.80	12.81	11.79	30.50	359.44	9.57	7.08	63.50
6704.00	15.37	7.24	26.75	14.70	13.86	27.89	386.51	9.64	7.13	64.00
6704.50	11.40	5.36	26.30	14.66	14.04	29.19	409.68	9.71	7.18	64.50
6705.00	9.19	4.32	17.87	13.51	13.01	32.63	424.43	9.78	7.22	65.00
6705.50	7.50	3.53	23.57	14.27	13.86	30.72	425.86	9.85	7.27	65.50
6706.00	9.38	4.41	60.79	17.05	16.54	24.51	405.41	9.93	7.33	66.00
6706.50	11.27	5.30	60.42	16.81	16.20	23.02	372.80	10.01	7.40	66.50
6707.00	9.66	4.54	70.76	17.02	16.49	21.48	354.15	10.09	7.46	67.00
6707.50	4.10	1.93	100.26	17.73	17.50	19.98	349.71	10.18	7.53	67.50
6708.00	4.27	2.01	108.27	17.71	17.47	18.49	323.14	10.27	7.60	68.00
6708.50	C O A L		C O A L		C O A L		C O A L			
6709.00	C O A L		C O A L		C O A L		C O A L			
6709.50	C O A L		C O A L		C O A L		C O A L			
6710.00	C O A L		C O A L		C O A L		C O A L			
6710.50	C O A L		C O A L		C O A L		C O A L			
6711.00	C O A L		C O A L		C O A L		C O A L			
6711.50	C O A L		C O A L		C O A L		C O A L			
6712.00	C O A L		C O A L		C O A L		C O A L			
6712.50	C O A L		C O A L		C O A L		C O A L			
6713.00	C O A L		C O A L		C O A L		C O A L			
6713.50	C O A L		C O A L		C O A L		C O A L			
6714.00	C O A L		C O A L		C O A L		C O A L			
6714.50	C O A L		C O A L		C O A L		C O A L			

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6715.00	0.00	0.00	212.14	18.57	18.57	12.29	228.28	10.36	7.68	68.50
6715.50	C O A L		C O A L		C O A L		C O A L			
6716.00	C O A L		C O A L		C O A L		C O A L			
6716.50	C O A L		C O A L		C O A L		C O A L			
6717.00	C O A L		C O A L		C O A L		C O A L			
6717.50	44.35	20.86	16.98	12.58	10.16	15.25	154.89			
6718.00	51.89	24.41	10.76	11.61	8.78	17.76	155.92			
6718.50	59.03	27.77	4.72	10.70	7.48	35.90	268.47			
6719.00	67.89	31.94	1.34	9.57	5.86	40.51	237.42			
6719.50	100.00	47.76	0.01	10.37	0.00	100.00	0.00			
6720.00	100.00	47.46	0.01	10.33	0.00	100.00	0.00			
6720.50	72.98	34.33	0.47	8.92	4.93	45.40	223.91			
6721.00	70.99	33.40	0.63	9.17	5.30	44.82	237.31			
6721.50	69.88	32.87	0.73	9.31	5.50	44.56	244.97			
6722.00	68.83	32.38	0.84	9.45	5.69	44.31	252.15			
6722.50	67.77	31.88	0.96	9.58	5.88	44.07	259.25			
6723.00	65.69	30.90	1.27	9.85	6.26	43.38	271.69			
6723.50	63.41	29.83	1.70	10.14	6.68	42.60	284.51			
6724.00	61.13	28.76	2.49	10.43	7.10	40.73	288.99			
6724.50	60.09	28.27	3.11	10.57	7.29	39.33	286.53			
6725.00	59.97	28.21	10.72	12.10	8.82	33.11	292.13			
6725.50	67.54	31.77	5.69	11.07	7.39	33.52	247.59			
6726.00	70.20	33.02	3.19	10.29	6.46	34.85	225.03			
6726.50	67.19	31.61	3.63	10.37	6.70	34.81	233.32			
6727.00	65.78	30.95	3.53	10.30	6.71	35.13	235.55			
6727.50	64.38	30.28	2.68	10.22	6.71	38.01	255.02			
6728.00	75.05	35.31	0.45	8.64	4.55	43.12	196.05			
6728.50	74.99	35.28	0.05	7.28	3.19	53.17	169.63			
6729.00	69.66	32.77	0.11	7.62	3.81	51.89	197.90			
6729.50	67.53	31.77	0.55	8.69	5.00	44.18	220.82			
6730.00	63.03	29.65	1.44	9.75	6.31	42.37	267.33			
6730.50	45.76	21.53	3.32	11.28	8.78	45.13	396.19			
6731.00	38.04	17.89	4.33	12.12	10.05	47.07	472.85			
6731.50	34.53	16.24	4.16	12.44	10.56	49.22	519.55			
6732.00	30.61	14.40	7.26	13.52	11.84	47.43	561.76			
6732.50	27.61	12.99	8.94	13.92	12.41	46.89	581.91	10.42	7.72	69.00
6733.00	28.62	13.46	11.31	14.53	12.96	43.13	559.15	10.49	7.75	69.50
6733.50	30.40	14.30	11.47	14.36	12.70	41.62	528.71			
6734.00	31.77	14.94	11.55	14.19	12.45	40.27	501.52			
6734.50	32.18	15.14	12.11	14.14	12.38	38.76	479.84			
6735.00	28.23	13.28	15.75	14.64	13.10	36.02	471.81	10.55	7.60	70.00
6735.50	10.32	4.85	38.70	16.93	16.37	32.10	525.50	10.64	7.85	70.50
6736.00	2.63	1.24	61.51	17.92	17.77	29.54	525.03	10.72	7.91	71.00
6736.50	0.00	0.00	65.47	17.73	17.73	28.32	502.14	10.81	7.98	71.50
6737.00	0.00	0.00	92.47	18.47	18.47	25.49	470.80	10.91	8.05	72.00
6737.50	0.00	0.00	70.68	17.36	17.36	25.44	441.74	10.99	8.11	72.50
6738.00	0.00	0.00	71.16	17.01	17.01	23.76	403.99	11.08	8.18	73.00
6738.50	0.01	0.01	80.33	17.22	17.22	22.55	388.18	11.16	8.24	73.50
6739.00	1.24	0.58	72.44	16.85	16.78	22.42	376.29	11.25	8.31	74.00
6739.50	1.93	0.91	87.71	17.38	17.27	21.25	367.07	11.33	8.38	74.50

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6740.00	2.55	1.20	105.50	17.93	17.79	20.37	362.40	11.42	8.45	75.00
6740.50	2.83	1.35	104.51	17.88	17.73	20.27	359.30	11.51	8.52	75.50
6741.00	2.76	1.30	105.28	17.90	17.75	20.24	359.22	11.60	8.59	76.00
6741.50	2.03	0.98	109.12	17.99	17.87	20.18	360.74	11.69	8.66	76.50
6742.00	1.09	0.51	115.09	18.11	18.05	20.09	362.63	11.78	8.73	77.00
6742.50	0.78	0.37	117.94	18.15	18.11	19.93	360.92	11.87	8.80	77.50
6743.00	3.25	1.53	105.61	17.84	17.66	19.78	349.34	11.96	8.87	78.00
6743.50	5.65	2.66	94.25	17.53	17.22	19.75	340.18	12.04	8.94	78.50
6744.00	2.40	1.13	111.13	17.95	17.81	19.61	349.40	12.13	9.01	79.00
6744.50	0.00	0.00	131.58	18.45	18.45	19.59	361.32	12.23	9.09	79.50
6745.00	0.00	0.00	136.25	18.56	18.56	19.49	361.72	12.32	9.16	80.00
6745.50	0.00	0.00	140.10	18.63	18.63	19.36	360.76	12.41	9.24	80.50
6746.00	0.00	0.00	145.83	18.69	18.69	18.94	353.94	12.50	9.31	81.00
6746.50	0.00	0.00	152.62	18.74	18.74	18.44	345.50	12.60	9.39	81.50
6747.00	0.00	0.00	160.83	18.82	18.82	17.91	337.06	12.69	9.47	82.00
6747.50	0.00	0.00	169.25	18.89	18.89	17.42	329.03	12.79	9.55	82.50
6748.00	0.00	0.00	170.42	18.94	18.94	17.54	332.26	12.88	9.62	83.00
6748.50	0.00	0.00	167.49	18.97	18.97	17.92	339.82	12.98	9.70	83.50
6749.00	0.00	0.00	113.43	17.85	17.85	19.40	346.30	13.07	9.77	84.00
6749.50	0.00	0.00	108.29	17.61	17.61	19.11	336.47	13.15	9.85	84.50
6750.00	0.00	0.00	151.30	18.50	18.50	17.53	324.28	13.25	9.92	85.00
6750.50	0.00	0.00	153.96	18.44	18.44	16.98	313.09	13.34	10.00	85.50
6751.00	0.00	0.00	167.78	18.45	18.45	15.58	287.47	13.43	10.08	86.00
6751.50	0.00	0.00	187.43	18.47	18.47	13.85	255.81	13.52	10.16	86.50
6752.00	0.00	0.00	200.70	18.54	18.54	13.06	242.22	13.62	10.24	87.00
6752.50	0.00	0.00	220.73	18.81	18.81	12.78	240.39	13.71	10.32	87.50
6753.00	0.00	0.00	241.01	19.20	19.14	12.90	246.99	13.81	10.40	88.00
6753.50	0.00	0.00	221.35	19.46	19.34	15.11	292.29	13.90	10.48	88.50
6754.00	0.00	0.00	150.29	19.54	19.40	21.44	415.75	14.00	10.56	89.00
6754.50	0.00	0.00	92.89	19.17	19.12	27.95	534.37	14.10	10.63	89.50
6755.00	0.00	0.00	47.72	17.46	17.46	32.69	570.81	14.18	10.69	90.00
6755.50	0.00	0.00	22.60	15.51	15.51	38.90	603.53	14.26	10.73	90.50
6756.00	0.00	0.00	11.25	13.82	13.82	46.78	646.58	14.33	10.77	91.00
6756.50	0.00	0.00	1.62	11.40	11.40	61.74	703.72			
6757.00	0.00	0.00	0.14	9.22	9.22	79.80	735.78			
6757.50	0.00	0.00	0.01	7.61	7.61	98.51	749.26			
6758.00	3.84	1.81	0.01	7.06	6.85	100.00	684.54			
6758.50	0.45	0.21	0.02	8.19	8.17	93.75	765.84			
6759.00	1.47	0.69	0.13	9.52	9.44	81.47	769.24			
6759.50	2.52	1.19	0.32	10.46	10.32	75.13	775.67			
6760.00	4.57	2.15	0.25	10.42	10.17	77.01	783.29			
6760.50	8.13	3.82	0.11	9.83	9.39	82.62	775.47			
6761.00	21.90	10.30	0.08	9.61	8.41	82.91	697.36			
6761.50	43.83	20.64	0.02	8.49	6.09	83.96	511.50			
6762.00	80.06	37.66	0.00	6.79	2.42	88.07	213.18			
6762.50	100.00	61.07	0.01	8.30	0.00	100.00	0.00			
6763.00	100.00	56.55	0.01	9.64	0.00	100.00	0.00			
6763.50	99.53	46.82	37.47	11.51	6.08	7.10	43.19			
6764.00	100.00	48.80	0.01	11.26	0.00	100.00	0.00			
6764.50	100.00	49.35	0.01	10.59	0.00	100.00	0.00			

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Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

Page No 19

DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6765.00	100.00	49.56	0.01	9.79	0.00	100.00	0.00			
6765.50	100.00	51.20	0.01	8.51	0.00	100.00	0.00			
6766.00	100.00	51.68	0.01	7.75	0.00	100.00	0.00			
6766.50	98.84	46.50	3.32	9.19	3.79	15.87	60.14			
6767.00	100.00	49.24	0.01	10.16	0.00	100.00	0.00			
6767.50	100.00	53.08	0.01	10.84	0.00	100.00	0.00			
6768.00	100.00	58.56	0.01	10.64	0.00	100.00	0.00			
6768.50	100.00	63.48	0.01	10.08	0.00	100.00	0.00			
6769.00	100.00	69.55	0.01	9.09	0.00	100.00	0.00			
6769.50	100.00	69.55	0.01	8.61	0.00	100.00	0.00			

Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

Page No 1

Porosity cutoff = 10.0 Saturation cutoff = 50.0 Caliper cutoff = bit size +***** Shale Cutoff = 30.0
Permeability cutoff = 0.000
TOP BASE A M N RW TEMP GRAD GMAX GMIN RSH COR C G I RHOG RHOS PHIS PHIC
6340.00 6770.00 1.00 2.00 2.00 0.260 223.0 2.250 144.00 32.00 50.00 2 2 2 2.650 2.660 15.0 24
Porosity derived from Neutron/Density Cross-Plot
6900.00 7250.00 1.00 2.00 2.00 0.180 235.0 2.250 140.00 48.00 56.00 2 2 2 2.650 2.760 14.0 24
Porosity derived from Neutron/Density Cross-Plot

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Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

Page No 2

DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6900.00	88.27	53.91	11.69	9.89	9.20	18.75	172.47			
6900.50	80.28	49.02	16.32	11.27	10.64	20.24	215.38			
6901.00	100.00	67.87	0.01	7.86	0.00	100.00	0.00			
6901.50	84.12	51.37	14.12	10.65	9.99	19.40	193.73			
6902.00	88.56	54.07	11.11	9.68	8.98	18.51	166.32			
6902.50	95.74	58.46	39.65	8.27	7.52	13.92	104.65			
6903.00	99.16	60.55	51.64	7.50	6.72	7.23	48.53			
6903.50	100.00	69.23	0.01	5.25	0.00	100.00	0.00			
6904.00	100.00	76.20	0.01	4.01	0.00	100.00	0.00			
6904.50	100.00	74.89	0.01	4.50	0.00	100.00	0.00			
6905.00	100.00	61.69	0.01	7.34	0.00	100.00	0.00			
6905.50	92.43	56.44	21.68	8.19	7.47	19.96	148.98			
6906.00	87.27	53.30	10.18	9.60	8.92	20.88	186.14			
6906.50	87.14	53.21	11.80	9.97	9.28	19.19	178.13			
6907.00	86.11	52.58	11.58	9.84	9.16	18.73	171.57			
6907.50	84.31	51.48	14.79	10.58	9.92	17.40	172.52			
6908.00	80.42	49.11	18.04	11.39	10.75	18.21	195.84			
6908.50	86.94	53.08	13.38	10.26	9.58	17.65	169.01			
6909.00	88.71	54.17	14.88	10.52	9.82	16.43	161.40			
6909.50	94.47	57.68	15.80	10.29	9.55	12.12	115.72			
6910.00	93.41	57.04	14.28	10.07	9.33	13.39	124.94			
6910.50	100.00	67.82	0.01	7.86	0.00	100.00	0.00			
6911.00	100.00	66.08	0.01	7.63	0.00	100.00	0.00			
6911.50	100.00	65.91	0.01	7.61	0.00	100.00	0.00			
6912.00	100.00	63.87	0.01	7.34	0.00	100.00	0.00			
6912.50	74.50	45.49	0.66	4.99	4.41	37.96	167.33			
6913.00	71.69	43.77	1.29	5.46	4.89	34.64	169.52			
6913.50	74.55	45.52	1.05	4.99	4.40	33.05	145.36			
6914.00	100.00	62.68	0.01	7.19	0.00	100.00	0.00			
6914.50	100.00	61.61	0.01	7.05	0.00	100.00	0.00			
6915.00	44.40	27.11	8.92	9.96	9.61	38.00	365.12			
6915.50	42.05	25.67	10.22	11.15	10.82	34.73	375.93			
6916.00	50.54	30.86	14.37	11.83	11.43	29.11	332.70			
6916.50	51.51	31.45	17.91	12.42	12.01	26.97	323.94			
6917.00	58.02	35.43	14.60	11.54	11.09	26.49	293.67			
6917.50	73.37	44.80	15.14	8.81	8.23	27.10	223.07			
6918.00	79.81	48.73	6.40	7.25	6.62	28.47	188.46			
6918.50	84.79	51.77	3.49	6.19	5.52	28.46	157.09			
6919.00	88.38	53.97	12.61	7.29	6.60	21.30	140.55			
6919.50	85.55	52.24	28.73	8.67	8.00	19.42	155.35			
6920.00	82.18	50.18	12.01	9.90	9.25	18.35	169.80			
6920.50	79.23	48.38	16.35	10.92	10.29	17.47	179.82			
6921.00	100.00	66.23	0.01	7.65	0.00	100.00	0.00			
6921.50	100.00	70.73	0.01	8.23	0.00	100.00	0.00			
6922.00	85.29	52.08	13.93	10.27	9.60	16.58	159.17			
6922.50	100.00	67.57	0.01	7.82	0.00	100.00	0.00			
6923.00	100.00	65.15	0.01	7.51	0.00	100.00	0.00			
6923.50	83.31	50.87	10.40	7.16	6.50	22.78	148.10			
6924.00	86.90	53.06	4.56	5.87	5.18	23.47	121.65			
6924.50	84.73	51.74	7.93	6.50	5.83	21.82	127.24			

Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6925.00	67.23	41.05	10.16	9.46	8.93	21.06	188.02			
6925.50	72.49	44.26	38.09	9.24	8.67	19.31	167.47			
6926.00	76.33	46.64	14.56	10.37	9.77	16.68	162.93			
6926.50	83.18	50.79	11.43	9.50	8.85	16.28	144.02			
6927.00	88.60	54.10	30.94	8.25	7.55	16.63	125.53			
6927.50	93.30	56.97	34.21	8.03	7.29	14.38	104.85			
6928.00	98.95	60.42	64.99	7.83	7.05	6.55	46.18			
6928.50	94.71	57.83	43.05	8.32	7.58	13.33	101.01			
6929.00	85.71	52.33	10.06	9.34	8.66	19.00	164.61			
6929.50	100.00	69.77	0.01	8.11	0.00	100.00	0.00			
6930.00	100.00	74.13	0.01	8.68	0.00	100.00	0.00			
6930.50	97.48	59.52	13.01	9.31	8.54	8.69	74.23			
6931.00	100.00	63.46	0.01	8.87	0.00	100.00	0.00			
6931.50	100.00	71.87	0.01	6.86	0.00	100.00	0.00			
6932.00	100.00	70.93	0.01	5.46	0.00	100.00	0.00			
6932.50	100.00	68.43	0.01	5.33	0.00	100.00	0.00			
6933.00	100.00	78.97	0.01	4.62	0.00	100.00	0.00			
6933.50	100.00	63.43	0.01	8.16	0.00	100.00	0.00			
6934.00	91.86	56.09	12.41	9.50	8.78	12.76	111.97			
6934.50	88.50	54.04	13.14	9.83	9.13	14.25	130.15			
6935.00	93.32	56.99	12.35	9.40	8.66	11.78	102.00			
6935.50	100.00	62.98	0.01	8.90	0.00	100.00	0.00			
6936.00	100.00	67.24	0.01	8.54	0.00	100.00	0.00			
6936.50	100.00	69.77	0.01	7.64	0.00	100.00	0.00			
6937.00	92.44	56.44	16.00	10.28	9.55	11.77	112.41			
6937.50	93.94	57.36	13.38	9.67	8.93	11.69	104.36			
6938.00	89.68	54.76	13.47	9.99	9.28	14.82	137.50			
6938.50	88.11	53.80	10.88	9.44	8.75	17.04	149.03			
6939.00	100.00	71.52	0.01	8.34	0.00	100.00	0.00			
6939.50	100.00	71.30	0.01	8.31	0.00	100.00	0.00			
6940.00	100.00	71.19	0.01	8.29	0.00	100.00	0.00			
6940.50	100.00	71.36	0.01	8.32	0.00	100.00	0.00			
6941.00	100.00	70.89	0.01	8.26	0.00	100.00	0.00			
6941.50	100.00	68.67	0.01	7.97	0.00	100.00	0.00			
6942.00	100.00	66.23	0.01	7.65	0.00	100.00	0.00			
6942.50	100.00	62.15	0.01	7.12	0.00	100.00	0.00			
6943.00	71.14	43.44	0.78	5.55	4.99	40.54	202.23			
6943.50	75.17	45.90	1.63	6.00	5.41	35.68	193.08			
6944.00	78.21	47.75	1.91	5.92	5.31	33.39	177.16			
6944.50	73.13	44.65	4.51	6.99	6.41	31.01	198.81			
6945.00	70.14	42.83	3.99	6.95	6.40	32.21	206.03			
6945.50	60.64	37.03	3.57	7.28	6.80	35.50	241.50			
6946.00	58.30	35.60	8.93	8.57	8.12	32.10	260.54			
6946.50	70.35	42.96	12.38	8.49	7.94	27.92	221.53			
6947.00	74.48	45.48	10.22	9.78	9.19	23.13	212.61			
6947.50	85.01	51.91	11.67	9.81	9.14	18.29	167.22			
6948.00	87.59	53.48	24.23	11.94	11.25	13.84	155.62			
6948.50	88.45	54.01	72.31	15.22	14.52	10.40	151.07			
6949.00	100.00	77.64	0.01	9.13	0.00	100.00	0.00			
6949.50	100.00	83.73	0.01	9.92	0.00	100.00	0.00			

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Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6950.00	100.00	83.65	0.01	9.91	0.00	100.00	0.00			
6950.50	100.00	78.51	0.01	9.24	0.00	100.00	0.00			
6951.00	100.00	73.06	0.01	8.54	0.00	100.00	0.00			
6951.50	100.00	68.03	0.01	7.88	0.00	100.00	0.00			
6952.00	100.00	64.94	0.01	7.48	0.00	100.00	0.00			
6952.50	100.00	61.21	0.01	7.00	0.00	100.00	0.00			
6953.00	74.23	45.33	32.38	9.25	8.66	20.95	181.51			
6953.50	76.27	46.59	12.75	10.13	9.53	18.76	178.68			
6954.00	79.27	48.40	15.68	10.68	10.06	16.81	169.04			
6954.50	100.00	66.31	0.01	7.66	0.00	100.00	0.00			
6955.00	100.00	70.79	0.01	8.24	0.00	100.00	0.00			
6955.50	100.00	69.36	0.01	8.06	0.00	100.00	0.00			
6956.00	100.00	68.30	0.01	7.92	0.00	100.00	0.00			
6956.50	100.00	70.06	0.01	8.15	0.00	100.00	0.00			
6957.00	100.00	71.84	0.01	8.38	0.00	100.00	0.00			
6957.50	100.00	72.74	0.01	8.49	0.00	100.00	0.00			
6958.00	100.00	61.65	0.01	6.68	0.00	100.00	0.00			
6958.50	98.94	60.41	12.38	5.29	4.51	8.25	37.22			
6959.00	95.95	58.59	1.32	4.00	3.24	20.05	65.01			
6959.50	100.00	64.55	0.01	7.43	0.00	100.00	0.00			
6960.00	99.64	60.84	53.95	6.95	6.17	3.80	23.42			
6960.50	62.23	38.00	5.60	7.02	6.53	29.38	191.79			
6961.00	51.97	31.73	17.06	8.71	8.30	26.15	217.09			
6961.50	66.91	40.86	18.24	11.14	10.61	16.80	178.29			
6962.00	71.42	43.61	17.14	10.83	10.27	15.87	162.95			
6962.50	77.85	47.54	16.89	10.70	10.09	14.80	149.27			
6963.00	79.07	48.29	19.89	11.22	10.60	14.22	150.72			
6963.50	81.04	49.49	20.02	11.18	10.54	13.59	143.24			
6964.00	100.00	61.65	0.01	7.06	0.00	100.00	0.00			
6964.50	74.25	45.34	1.77	5.04	4.45	28.04	124.80			
6965.00	78.54	47.96	31.36	12.48	11.87	11.72	139.04			
6965.50	77.59	47.38	72.60	15.03	14.42	9.66	139.36			
6966.00	78.62	48.01	117.02	16.43	15.81	8.45	133.69			
6966.50	73.62	44.95	2.77	5.14	4.56	24.22	110.43			
6967.00	74.19	45.30	2.38	5.04	4.46	25.04	111.71			
6967.50	71.00	43.36	2.89	5.57	5.01	27.06	135.63			
6968.00	67.76	41.37	3.20	6.11	5.57	29.69	165.45			
6968.50	59.63	36.41	6.35	7.45	6.98	30.39	212.09			
6969.00	58.65	35.81	12.05	8.52	8.06	28.75	231.79			
6969.50	62.02	37.87	16.95	8.98	8.49	27.01	229.36			
6970.00	56.59	34.55	18.06	11.50	11.05	20.41	225.65			
6970.50	67.10	40.97	37.42	13.39	12.86	14.40	185.25			
6971.00	79.65	48.64	45.09	13.62	12.99	10.87	141.26			
6971.50	71.16	43.45	111.05	16.45	15.89	9.90	157.36			
6972.00	67.60	41.28	6.86	6.13	5.60	21.91	122.70			
6972.50	70.98	43.34	4.77	5.57	5.02	21.87	109.70			
6973.00	73.12	44.65	2.81	5.22	4.65	24.71	114.80			
6973.50	66.56	40.65	4.98	6.30	5.78	26.36	152.32			
6974.00	62.22	37.99	6.99	7.02	6.53	27.08	176.82			
6974.50	59.33	36.23	8.75	7.50	7.03	27.30	191.91			

Well name = KIDMAN #1

Location = 28-14-235/140-49-27E

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
6975.00	57.87	35.34	9.79	7.74	7.28	27.36	199.25			
6975.50	56.63	34.58	11.46	7.94	7.50	26.73	200.41			
6976.00	62.78	38.33	6.54	6.93	6.43	27.25	175.31			
6976.50	65.38	39.92	5.15	6.50	5.98	27.23	162.95			
6977.00	58.75	35.87	16.54	7.59	7.13	21.17	150.92			
6977.50	42.39	25.88	15.70	10.29	9.96	15.93	158.63			
6978.00	35.65	21.77	21.88	11.40	11.12	15.65	174.07			
6978.50	49.22	30.06	17.59	10.81	10.42	16.34	170.28			
6979.00	51.88	31.68	28.07	9.00	8.59	22.15	190.26			
6979.50	56.98	34.80	22.62	9.19	8.74	25.01	218.67			
6980.00	54.80	33.46	13.17	10.71	10.28	23.75	244.16			
6980.50	58.82	35.91	6.24	7.58	7.12	31.26	222.51			
6981.00	67.94	41.49	3.07	6.08	5.54	29.93	165.84			
6981.50	99.81	60.95	62.76	6.96	6.18	2.29	14.14			
6982.00	100.00	65.92	0.01	7.61	0.00	100.00	0.00			
6982.50	100.00	70.89	0.01	8.25	0.00	100.00	0.00			
6983.00	100.00	75.64	0.01	8.87	0.00	100.00	0.00			
6983.50	100.00	76.05	0.01	8.93	0.00	100.00	0.00			
6984.00	100.00	76.08	0.01	8.93	0.00	100.00	0.00			
6984.50	100.00	75.68	0.01	8.88	0.00	100.00	0.00			
6985.00	100.00	73.53	0.01	8.60	0.00	100.00	0.00			
6985.50	100.00	70.15	0.01	8.16	0.00	100.00	0.00			
6986.00	100.00	65.33	0.01	7.53	0.00	100.00	0.00			
6986.50	74.06	45.22	0.75	5.07	4.48	37.24	166.93			
6987.00	67.07	40.95	2.03	6.22	5.69	35.17	200.20			
6987.50	60.15	36.73	4.49	7.36	6.89	33.54	231.02			
6988.00	53.27	32.53	8.81	8.50	8.08	32.08	259.10			
6988.50	45.78	27.96	16.60	9.73	9.37	30.65	287.23			
6989.00	35.11	21.44	6.83	8.85	8.57	36.81	315.56			
6989.50	32.21	19.67	9.46	9.62	9.37	36.50	341.85			
6990.00	30.32	18.51	12.85	10.35	10.12	35.98	363.99			
6990.50	25.35	15.48	14.58	12.39	12.19	33.20	404.89	14.39	10.81	91.50
6991.00	25.01	15.27	16.95	13.16	12.96	33.61	435.60	14.45	10.86	92.00
6991.50	24.34	14.86	12.18	12.44	12.25	37.95	464.93	14.52	10.89	92.50
6992.00	41.04	25.06	7.80	10.34	10.02	40.86	409.47			
6992.50	56.94	34.77	9.39	9.87	9.42	36.77	346.48			
6993.00	55.82	34.09	11.80	10.16	9.72	35.48	344.82			
6993.50	50.66	30.94	12.48	11.62	11.22	31.61	354.80			
6994.00	51.46	31.42	7.93	8.79	8.39	34.50	289.41			
6994.50	55.77	34.06	9.97	8.08	7.64	28.87	220.65			
6995.00	56.26	34.35	11.85	8.00	7.56	26.68	201.72			
6995.50	48.53	29.63	16.52	9.28	8.90	28.89	256.96			
6996.00	24.58	15.01	19.08	13.23	13.04	31.24	407.16	14.58	10.94	93.00
6996.50	10.98	6.70	10.13	12.57	12.48	43.60	544.05	14.64	10.97	93.50
6997.00	11.43	6.98	10.48	13.17	13.08	45.42	594.24	14.71	11.01	94.00
6997.50	13.08	7.99	11.71	13.70	13.59	44.98	611.39	14.78	11.05	94.50
6998.00	19.65	12.00	12.25	13.59	13.44	43.32	582.12	14.84	11.08	95.00
6998.50	22.51	13.75	11.18	13.08	12.90	43.10	555.98	14.91	11.12	95.50
6999.00	15.12	9.23	13.72	13.84	13.72	41.96	575.66	14.98	11.16	96.00
6999.50	20.05	12.25	7.81	11.90	11.74	46.37	544.64	15.04	11.19	96.50

Well name = KIDMAN #1

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
7000.00	26.42	16.13	4.97	10.84	10.63	47.60	505.90	15.09	11.22	97.00
7000.50	34.79	21.24	10.06	11.13	10.86	41.00	445.19			
7001.00	31.77	19.40	13.44	12.44	12.19	35.19	429.03			
7001.50	27.44	16.76	15.69	12.76	12.54	33.26	417.13	15.15	11.26	97.50
7002.00	30.14	18.41	14.28	12.31	12.07	33.05	399.00			
7002.50	9.87	6.03	10.08	12.00	11.92	41.09	489.96	15.21	11.30	98.00
7003.00	19.23	11.74	4.74	10.59	10.44	47.48	495.74	15.26	11.32	98.50
7003.50	35.36	21.59	1.72	9.08	8.81	52.11	458.92			
7004.00	39.35	24.03	4.62	10.03	9.72	45.25	439.69			
7004.50	41.15	25.13	8.37	10.44	10.12	40.46	409.35			
7005.00	35.96	21.96	10.87	11.65	11.36	36.17	411.02			
7005.50	34.69	21.18	10.11	10.52	10.24	38.92	398.61			
7006.00	28.84	17.61	6.51	10.21	9.98	42.61	425.49			
7006.50	19.19	11.72	8.20	11.28	11.12	43.97	489.17	15.32	11.36	99.00
7007.00	9.14	5.58	9.51	12.39	12.32	45.98	566.31	15.38	11.39	99.50
7007.50	7.25	4.43	6.52	12.23	12.17	49.50	602.60	15.44	11.42	100.00
7008.00	8.67	5.29	4.55	11.80	11.73	51.95	609.59			
7008.50	9.82	6.00	4.25	11.62	11.55	52.11	601.71			
7009.00	9.29	5.67	5.06	11.87	11.79	51.03	601.83			
7009.50	3.72	2.27	9.06	12.95	12.92	48.13	621.77	15.51	11.45	100.50
7010.00	1.78	1.09	11.00	13.53	13.51	46.05	622.35	15.57	11.49	101.00
7010.50	5.53	3.38	10.58	13.20	13.15	45.49	598.27	15.64	11.53	101.50
7011.00	11.07	6.76	10.41	12.57	12.48	45.51	568.09	15.70	11.56	102.00
7011.50	16.15	9.86	8.76	12.00	11.87	45.55	540.73	15.76	11.59	102.50
7012.00	17.21	10.51	9.38	11.99	11.86	44.80	531.24	15.82	11.62	103.00
7012.50	11.41	6.97	9.93	12.26	12.17	45.10	548.82	15.88	11.66	103.50
7013.00	10.33	6.31	17.42	14.14	14.05	38.19	536.75	15.95	11.70	104.00
7013.50	8.64	5.27	20.94	14.57	14.50	36.23	525.23	16.02	11.75	104.50
7014.00	0.95	0.58	14.52	13.60	13.59	40.15	545.72	16.09	11.79	105.00
7014.50	4.54	2.77	12.49	12.99	12.96	40.76	528.05	16.16	11.83	105.50
7015.00	9.32	5.69	11.70	12.51	12.44	44.16	549.31	16.22	11.86	106.00
7015.50	13.00	7.94	7.08	12.03	11.93	47.94	572.03	16.28	11.89	106.50
7016.00	16.23	9.91	4.95	11.66	11.53	50.49	582.27			
7016.50	15.08	9.21	6.31	11.98	11.86	48.93	580.19	16.34	11.92	107.00
7017.00	15.69	9.58	10.71	12.75	12.63	42.92	542.01	16.40	11.96	107.50
7017.50	18.83	11.50	9.58	11.53	11.38	43.14	490.94	16.46	11.99	108.00
7018.00	15.88	9.70	12.24	11.86	11.74	41.66	488.98	16.52	12.03	108.50
7018.50	9.02	5.51	11.41	12.75	12.68	41.61	527.48	16.58	12.06	109.00
7019.00	2.06	1.26	10.47	12.81	12.79	44.19	565.29	16.64	12.10	109.50
7019.50	0.00	0.00	11.23	12.79	12.79	45.55	582.48	16.71	12.13	110.00
7020.00	0.00	0.00	9.40	12.45	12.45	46.47	578.43	16.77	12.17	110.50
7020.50	0.00	0.00	11.03	12.97	12.97	43.75	567.56	16.84	12.20	111.00
7021.00	0.76	0.46	10.07	12.23	12.22	45.11	551.30	16.90	12.24	111.50
7021.50	3.69	2.25	9.03	11.80	11.77	44.93	528.78	16.96	12.27	112.00
7022.00	6.75	4.12	7.89	11.42	11.36	45.11	512.53	17.01	12.30	112.50
7022.50	12.82	7.83	8.09	11.17	11.07	43.94	486.43	17.07	12.33	113.00
7023.00	20.56	12.56	8.21	10.92	10.76	42.80	460.38	17.12	12.36	113.50
7023.50	23.69	14.46	11.20	12.23	12.04	39.01	469.82	17.18	12.40	114.00
7024.00	28.07	17.14	13.09	12.65	12.43	37.12	461.51	17.24	12.44	114.50
7024.50	31.15	19.02	11.29	12.14	11.90	38.08	453.07			

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
7025.00	31.45	19.21	10.48	12.09	11.85	39.71	470.49			
7025.50	29.02	17.72	10.89	12.50	12.27	40.83	500.88	17.30	12.47	115.00
7026.00	25.38	15.50	11.98	13.10	12.90	41.47	534.79	17.37	12.51	115.50
7026.50	21.74	13.27	11.76	13.28	13.11	42.85	561.94	17.43	12.55	116.00
7027.00	18.45	11.27	11.77	13.36	13.21	43.28	571.88	17.50	12.59	116.50
7027.50	19.27	11.77	14.80	13.80	13.65	39.97	545.51	17.57	12.63	117.00
7028.00	29.37	17.93	14.57	12.95	12.72	35.98	457.71	17.63	12.67	117.50
7028.50	34.68	21.17	12.28	11.93	11.66	34.58	403.05			
7029.00	49.97	30.52	10.00	9.21	8.82	33.82	298.31			
7029.50	61.46	37.53	4.45	7.14	6.66	32.47	216.23			
7030.00	86.54	52.84	26.56	11.92	11.23	11.26	126.50			
7030.50	94.59	57.76	47.30	13.23	12.48	6.07	75.76			
7031.00	100.00	85.25	0.01	10.12	0.00	100.00	0.00			
7031.50	100.00	88.72	0.01	11.28	0.00	100.00	0.00			
7032.00	100.00	87.81	0.01	12.19	0.00	100.00	0.00			
7032.50	100.00	86.51	0.01	13.49	0.00	100.00	0.00			
7033.00	100.00	84.88	0.01	15.12	0.00	100.00	0.00			
7033.50	100.00	83.75	0.01	16.25	0.00	100.00	0.00			
7034.00	100.00	82.36	0.01	17.64	0.00	100.00	0.00			
7034.50	100.00	82.62	0.01	17.38	0.00	100.00	0.00			
7035.00	100.00	83.28	0.01	16.72	0.00	100.00	0.00			
7035.50	100.00	84.74	0.01	15.26	0.00	100.00	0.00			
7036.00	100.00	85.97	0.01	14.03	0.00	100.00	0.00			
7036.50	100.00	87.32	0.01	12.68	0.00	100.00	0.00			
7037.00	100.00	72.86	0.01	8.51	0.00	100.00	0.00			
7037.50	100.00	63.88	0.01	7.34	0.00	100.00	0.00			
7038.00	72.73	44.41	0.32	5.29	4.71	47.80	225.31			
7038.50	68.16	41.62	1.19	6.04	5.50	39.54	217.56			
7039.00	64.12	39.16	2.62	6.71	6.20	35.51	220.20			
7039.50	67.30	41.09	10.27	9.76	9.23	23.27	214.69			
7040.00	58.45	35.69	10.28	10.15	9.69	26.88	260.38			
7040.50	57.15	34.90	6.52	8.67	8.22	35.81	294.29			
7041.00	46.71	28.52	4.30	9.10	8.73	42.24	368.62			
7041.50	41.38	25.27	3.55	9.48	9.15	45.91	420.12			
7042.00	49.11	29.99	2.61	8.70	8.31	45.73	380.08			
7042.50	66.73	40.75	5.72	7.84	7.31	33.11	242.17			
7043.00	78.24	47.78	8.28	7.17	6.56	25.46	166.95			
7043.50	71.30	43.53	20.59	8.60	8.04	23.06	185.31			
7044.00	67.06	40.95	21.04	8.98	8.45	24.60	207.97			
7044.50	78.53	47.95	4.56	6.62	6.00	28.60	171.69			
7045.00	73.25	44.73	4.49	7.06	6.48	31.41	203.52			
7045.50	76.22	46.54	3.35	6.75	6.15	32.67	200.98			
7046.00	81.61	49.83	2.85	6.33	5.69	31.59	179.59			
7046.50	78.82	48.13	7.71	7.62	7.00	28.48	199.31			
7047.00	75.55	46.13	22.98	9.10	8.50	23.87	202.92			
7047.50	77.53	47.34	31.92	9.25	8.64	21.03	181.79			
7048.00	83.57	51.03	29.93	8.62	7.96	18.85	150.10			
7048.50	85.53	52.22	12.75	9.82	9.15	15.44	141.31			
7049.00	94.49	57.70	11.77	9.14	8.39	10.69	89.72			
7049.50	100.00	61.18	0.01	7.57	0.00	100.00	0.00			

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
7050.00	100.00	61.10	0.01	7.06	0.00	100.00	0.00			
7050.50	98.64	60.23	71.65	8.07	7.29	6.68	48.72			
7051.00	89.97	54.94	12.56	9.68	8.97	14.23	127.60			
7051.50	100.00	62.48	0.01	7.78	0.00	100.00	0.00			
7052.00	100.00	64.09	0.01	7.25	0.00	100.00	0.00			
7052.50	99.29	60.63	81.75	8.07	7.29	5.31	38.74			
7053.00	100.00	77.88	0.01	9.16	0.00	100.00	0.00			
7053.50	100.00	79.96	0.01	9.43	0.00	100.00	0.00			
7054.00	100.00	80.28	0.01	9.48	0.00	100.00	0.00			
7054.50	100.00	80.07	0.01	9.45	0.00	100.00	0.00			
7055.00	95.91	58.57	49.58	8.36	7.61	12.00	91.26			
7055.50	99.33	60.65	10.62	8.35	7.57	5.09	38.50			
7056.00	94.95	57.98	14.29	9.85	9.10	11.13	101.30			
7056.50	95.77	58.48	17.68	10.43	9.68	9.78	94.70			
7057.00	100.00	63.19	0.01	9.56	0.00	100.00	0.00			
7057.50	100.00	66.07	0.01	8.66	0.00	100.00	0.00			
7058.00	100.00	69.12	0.01	7.40	0.00	100.00	0.00			
7058.50	100.00	72.25	0.01	6.52	0.00	100.00	0.00			
7059.00	100.00	74.68	0.01	6.62	0.00	100.00	0.00			
7059.50	100.00	65.85	0.01	8.48	0.00	100.00	0.00			
7060.00	100.00	64.61	0.01	8.41	0.00	100.00	0.00			
7060.50	100.00	65.61	0.01	8.16	0.00	100.00	0.00			
7061.00	100.00	65.27	0.01	8.34	0.00	100.00	0.00			
7061.50	100.00	64.08	0.01	7.92	0.00	100.00	0.00			
7062.00	97.90	59.78	10.53	8.57	7.80	8.26	64.47			
7062.50	97.03	59.25	12.30	9.16	8.39	9.12	76.52			
7063.00	99.95	61.03	14.63	9.05	8.27	1.32	10.94			
7063.50	99.95	61.03	16.10	9.34	8.55	1.22	10.45			
7064.00	100.00	64.67	0.01	8.53	0.00	100.00	0.00			
7064.50	100.00	70.85	0.01	6.53	0.00	100.00	0.00			
7065.00	100.00	74.10	0.01	5.60	0.00	100.00	0.00			
7065.50	95.78	58.49	12.68	9.36	8.61	10.31	88.78			
7066.00	100.00	74.58	0.01	8.73	0.00	100.00	0.00			
7066.50	100.00	77.87	0.01	9.16	0.00	100.00	0.00			
7067.00	100.00	78.91	0.01	9.30	0.00	100.00	0.00			
7067.50	92.61	56.55	40.02	8.32	7.59	14.16	107.51			
7068.00	93.35	57.00	10.12	8.80	8.07	12.76	102.93			
7068.50	89.90	54.90	11.23	9.31	8.61	14.58	125.50			
7069.00	87.97	53.71	14.26	10.15	9.46	14.59	138.07			
7069.50	96.08	58.67	12.22	9.20	8.44	9.89	83.48			
7070.00	95.82	58.51	12.21	9.25	8.49	10.44	88.66			
7070.50	84.83	51.80	17.11	10.96	10.29	16.14	166.17			
7071.00	83.49	50.98	17.80	11.16	10.51	16.69	175.32			
7071.50	90.62	55.34	14.43	10.18	9.47	14.30	135.42			
7072.00	100.00	63.42	0.01	7.98	0.00	100.00	0.00			
7072.50	100.00	73.91	0.01	6.11	0.00	100.00	0.00			
7073.00	100.00	80.04	0.01	4.68	0.00	100.00	0.00			
7073.50	100.00	82.93	0.01	3.35	0.00	100.00	0.00			
7074.00	100.00	81.06	0.01	3.60	0.00	100.00	0.00			
7074.50	100.00	73.44	0.01	5.50	0.00	100.00	0.00			

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
7075.00	100.00	63.40	0.01	8.45	0.00	100.00	0.00			
7075.50	100.00	69.22	0.01	7.21	0.00	100.00	0.00			
7076.00	100.00	71.87	0.01	6.73	0.00	100.00	0.00			
7076.50	100.00	63.85	0.01	8.47	0.00	100.00	0.00			
7077.00	100.00	62.18	0.01	8.73	0.00	100.00	0.00			
7077.50	100.00	63.21	0.01	8.99	0.00	100.00	0.00			
7078.00	100.00	67.14	0.01	8.39	0.00	100.00	0.00			
7078.50	100.00	71.53	0.01	7.87	0.00	100.00	0.00			
7079.00	100.00	74.53	0.01	7.67	0.00	100.00	0.00			
7079.50	100.00	73.74	0.01	7.07	0.00	100.00	0.00			
7080.00	100.00	75.63	0.01	6.03	0.00	100.00	0.00			
7080.50	100.00	88.53	0.01	3.05	0.00	100.00	0.00			
7081.00	100.00	86.67	0.01	3.31	0.00	100.00	0.00			
7081.50	100.00	74.28	0.01	5.65	0.00	100.00	0.00			
7082.00	100.00	66.55	0.01	7.25	0.00	100.00	0.00			
7082.50	100.00	67.29	0.01	7.04	0.00	100.00	0.00			
7083.00	100.00	67.86	0.01	6.96	0.00	100.00	0.00			
7083.50	100.00	65.56	0.01	7.51	0.00	100.00	0.00			
7084.00	100.00	62.04	0.01	8.34	0.00	100.00	0.00			
7084.50	95.15	58.10	12.43	9.56	8.81	13.00	114.45			
7085.00	96.35	58.84	12.18	9.36	8.60	11.65	100.19			
7085.50	96.17	58.72	11.85	9.29	8.54	11.96	102.06			
7086.00	100.00	63.56	0.01	7.90	0.00	100.00	0.00			
7086.50	98.61	60.21	11.38	8.78	8.00	7.65	61.19			
7087.00	100.00	62.30	0.01	8.56	0.00	100.00	0.00			
7087.50	100.00	64.40	0.01	8.42	0.00	100.00	0.00			
7088.00	100.00	64.90	0.01	8.69	0.00	100.00	0.00			
7088.50	100.00	67.47	0.01	8.31	0.00	100.00	0.00			
7089.00	100.00	64.28	0.01	8.48	0.00	100.00	0.00			
7089.50	100.00	65.69	0.01	7.52	0.00	100.00	0.00			
7090.00	100.00	72.42	0.01	5.89	0.00	100.00	0.00			
7090.50	100.00	76.42	0.01	4.79	0.00	100.00	0.00			
7091.00	100.00	76.84	0.01	4.75	0.00	100.00	0.00			
7091.50	100.00	67.02	0.01	8.00	0.00	100.00	0.00			
7092.00	100.00	66.31	0.01	8.50	0.00	100.00	0.00			
7092.50	100.00	66.38	0.01	8.62	0.00	100.00	0.00			
7093.00	100.00	67.17	0.01	7.53	0.00	100.00	0.00			
7093.50	100.00	68.16	0.01	7.22	0.00	100.00	0.00			
7094.00	100.00	70.03	0.01	6.82	0.00	100.00	0.00			
7094.50	100.00	63.91	0.01	8.28	0.00	100.00	0.00			
7095.00	100.00	66.62	0.01	7.71	0.00	100.00	0.00			
7095.50	100.00	69.53	0.01	6.23	0.00	100.00	0.00			
7096.00	100.00	71.92	0.01	5.57	0.00	100.00	0.00			
7096.50	100.00	72.02	0.01	5.31	0.00	100.00	0.00			
7097.00	100.00	64.14	0.01	7.34	0.00	100.00	0.00			
7097.50	100.00	62.80	0.01	7.79	0.00	100.00	0.00			
7098.00	100.00	63.57	0.01	8.13	0.00	100.00	0.00			
7098.50	100.00	66.94	0.01	8.11	0.00	100.00	0.00			
7099.00	100.00	72.08	0.01	6.98	0.00	100.00	0.00			
7099.50	100.00	70.80	0.01	7.30	0.00	100.00	0.00			

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Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
7100.00	100.00	70.51	0.01	7.24	0.00	100.00	0.00			
7100.50	100.00	70.81	0.01	6.85	0.00	100.00	0.00			
7101.00	100.00	71.22	0.01	6.38	0.00	100.00	0.00			
7101.50	100.00	69.51	0.01	6.47	0.00	100.00	0.00			
7102.00	100.00	62.13	0.01	8.15	0.00	100.00	0.00			
7102.50	100.00	66.90	0.01	7.69	0.00	100.00	0.00			
7103.00	100.00	64.71	0.01	8.08	0.00	100.00	0.00			
7103.50	100.00	69.57	0.01	7.55	0.00	100.00	0.00			
7104.00	100.00	77.95	0.01	4.13	0.00	100.00	0.00			
7104.50	100.00	83.71	0.01	2.71	0.00	100.00	0.00			
7105.00	100.00	92.37	0.01	0.94	0.00	100.00	0.00			
7105.50	100.00	82.30	0.01	4.21	0.00	100.00	0.00			
7106.00	100.00	67.55	0.01	8.50	0.00	100.00	0.00			
7106.50	100.00	70.21	0.01	7.96	0.00	100.00	0.00			
7107.00	100.00	73.69	0.01	6.66	0.00	100.00	0.00			
7107.50	100.00	76.36	0.01	5.46	0.00	100.00	0.00			
7108.00	100.00	82.72	0.01	4.42	0.00	100.00	0.00			
7108.50	100.00	80.66	0.01	5.56	0.00	100.00	0.00			
7109.00	100.00	72.11	0.01	7.43	0.00	100.00	0.00			
7109.50	100.00	64.57	0.01	8.91	0.00	100.00	0.00			
7110.00	100.00	63.30	0.01	8.72	0.00	100.00	0.00			
7110.50	100.00	66.95	0.01	8.33	0.00	100.00	0.00			
7111.00	100.00	70.71	0.01	7.86	0.00	100.00	0.00			
7111.50	100.00	75.27	0.01	5.93	0.00	100.00	0.00			
7112.00	100.00	71.86	0.01	6.05	0.00	100.00	0.00			
7112.50	100.00	63.68	0.01	7.54	0.00	100.00	0.00			
7113.00	99.77	60.92	13.38	8.93	8.14	3.15	25.65			
7113.50	100.00	64.35	0.01	8.73	0.00	100.00	0.00			
7114.00	100.00	68.78	0.01	8.08	0.00	100.00	0.00			
7114.50	100.00	73.80	0.01	7.02	0.00	100.00	0.00			
7115.00	100.00	80.20	0.01	5.53	0.00	100.00	0.00			
7115.50	100.00	80.83	0.01	5.47	0.00	100.00	0.00			
7116.00	100.00	81.70	0.01	5.32	0.00	100.00	0.00			
7116.50	100.00	79.86	0.01	4.98	0.00	100.00	0.00			
7117.00	100.00	73.90	0.01	5.18	0.00	100.00	0.00			
7117.50	100.00	79.66	0.01	4.02	0.00	100.00	0.00			
7118.00	100.00	82.18	0.01	3.58	0.00	100.00	0.00			
7118.50	100.00	65.69	0.01	8.30	0.00	100.00	0.00			
7119.00	100.00	69.20	0.01	8.60	0.00	100.00	0.00			
7119.50	100.00	73.43	0.01	7.91	0.00	100.00	0.00			
7120.00	100.00	77.30	0.01	6.65	0.00	100.00	0.00			
7120.50	100.00	77.24	0.01	5.94	0.00	100.00	0.00			
7121.00	100.00	78.67	0.01	5.25	0.00	100.00	0.00			
7121.50	100.00	75.35	0.01	6.87	0.00	100.00	0.00			
7122.00	100.00	69.48	0.01	9.15	0.00	100.00	0.00			
7122.50	100.00	69.63	0.01	8.20	0.00	100.00	0.00			
7123.00	100.00	73.25	0.01	7.52	0.00	100.00	0.00			
7123.50	100.00	76.06	0.01	7.07	0.00	100.00	0.00			
7124.00	100.00	70.58	0.01	7.64	0.00	100.00	0.00			
7124.50	100.00	64.99	0.01	8.37	0.00	100.00	0.00			

Well name = KIDMAN #1

Location = 28-14-235/140-49-27E

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
7125.00	100.00	66.06	0.01	7.63	0.00	100.00	0.00			
7125.50	100.00	73.74	0.01	7.73	0.00	100.00	0.00			
7126.00	100.00	70.83	0.01	8.84	0.00	100.00	0.00			
7126.50	100.00	62.71	0.01	10.35	0.00	100.00	0.00			
7127.00	97.10	59.29	20.29	10.81	10.04	8.89	89.34			
7127.50	100.00	67.17	0.01	8.94	0.00	100.00	0.00			
7128.00	100.00	71.00	0.01	8.19	0.00	100.00	0.00			
7128.50	100.00	70.59	0.01	7.47	0.00	100.00	0.00			
7129.00	100.00	67.45	0.01	7.43	0.00	100.00	0.00			
7129.50	100.00	70.92	0.01	6.76	0.00	100.00	0.00			
7130.00	100.00	68.67	0.01	7.36	0.00	100.00	0.00			
7130.50	100.00	69.09	0.01	7.34	0.00	100.00	0.00			
7131.00	100.00	73.86	0.01	6.87	0.00	100.00	0.00			
7131.50	100.00	74.28	0.01	6.03	0.00	100.00	0.00			
7132.00	100.00	79.87	0.01	5.79	0.00	100.00	0.00			
7132.50	100.00	82.27	0.01	5.99	0.00	100.00	0.00			
7133.00	100.00	81.34	0.01	5.65	0.00	100.00	0.00			
7133.50	100.00	76.75	0.01	6.39	0.00	100.00	0.00			
7134.00	100.00	78.91	0.01	6.29	0.00	100.00	0.00			
7134.50	100.00	62.56	0.01	10.35	0.00	100.00	0.00			
7135.00	100.00	61.72	0.01	10.02	0.00	100.00	0.00			
7135.50	100.00	64.89	0.01	8.70	0.00	100.00	0.00			
7136.00	100.00	68.38	0.01	7.88	0.00	100.00	0.00			
7136.50	100.00	70.60	0.01	7.45	0.00	100.00	0.00			
7137.00	97.97	59.82	16.67	10.04	9.27	7.75	71.88			
7137.50	97.49	59.53	14.31	9.65	8.88	8.90	79.00			
7138.00	100.00	62.85	0.01	9.08	0.00	100.00	0.00			
7138.50	100.00	64.36	0.01	8.89	0.00	100.00	0.00			
7139.00	99.82	60.95	20.75	10.22	9.44	2.31	21.82			
7139.50	100.00	62.95	0.01	10.20	0.00	100.00	0.00			
7140.00	100.00	67.19	0.01	9.50	0.00	100.00	0.00			
7140.50	100.00	68.78	0.01	8.57	0.00	100.00	0.00			
7141.00	100.00	68.75	0.01	7.77	0.00	100.00	0.00			
7141.50	100.00	66.41	0.01	8.43	0.00	100.00	0.00			
7142.00	100.00	70.44	0.01	7.08	0.00	100.00	0.00			
7142.50	100.00	71.99	0.01	6.26	0.00	100.00	0.00			
7143.00	100.00	65.70	0.01	7.62	0.00	100.00	0.00			
7143.50	96.70	59.05	11.48	9.05	8.28	10.45	86.55			
7144.00	90.25	55.11	12.14	9.74	9.03	15.94	143.95			
7144.50	100.00	64.04	0.01	7.80	0.00	100.00	0.00			
7145.00	100.00	68.73	0.01	7.02	0.00	100.00	0.00			
7145.50	100.00	73.53	0.01	7.06	0.00	100.00	0.00			
7146.00	100.00	70.56	0.01	8.08	0.00	100.00	0.00			
7146.50	100.00	71.13	0.01	7.80	0.00	100.00	0.00			
7147.00	100.00	73.37	0.01	7.49	0.00	100.00	0.00			
7147.50	100.00	70.40	0.01	8.56	0.00	100.00	0.00			
7148.00	100.00	67.77	0.01	9.29	0.00	100.00	0.00			
7148.50	100.00	68.96	0.01	8.93	0.00	100.00	0.00			
7149.00	100.00	70.31	0.01	8.10	0.00	100.00	0.00			
7149.50	100.00	72.28	0.01	7.10	0.00	100.00	0.00			

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Well name = KIDMAN #1

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
7150.00	100.00	75.91	0.01	6.26	0.00	100.00	0.00			
7150.50	100.00	78.60	0.01	5.55	0.00	100.00	0.00			
7151.00	100.00	69.90	0.01	7.36	0.00	100.00	0.00			
7151.50	100.00	63.08	0.01	8.76	0.00	100.00	0.00			
7152.00	100.00	64.16	0.01	8.19	0.00	100.00	0.00			
7152.50	100.00	63.07	0.01	8.19	0.00	100.00	0.00			
7153.00	100.00	64.90	0.01	7.56	0.00	100.00	0.00			
7153.50	100.00	70.05	0.01	7.34	0.00	100.00	0.00			
7154.00	100.00	69.19	0.01	8.13	0.00	100.00	0.00			
7154.50	100.00	64.86	0.01	8.86	0.00	100.00	0.00			
7155.00	100.00	61.37	0.01	9.35	0.00	100.00	0.00			
7155.50	100.00	63.18	0.01	8.50	0.00	100.00	0.00			
7156.00	100.00	65.12	0.01	7.73	0.00	100.00	0.00			
7156.50	100.00	71.74	0.01	5.97	0.00	100.00	0.00			
7157.00	100.00	67.29	0.01	7.53	0.00	100.00	0.00			
7157.50	100.00	65.53	0.01	8.46	0.00	100.00	0.00			
7158.00	100.00	71.05	0.01	8.26	0.00	100.00	0.00			
7158.50	100.00	76.24	0.01	7.43	0.00	100.00	0.00			
7159.00	100.00	75.05	0.01	7.76	0.00	100.00	0.00			
7159.50	100.00	71.46	0.01	7.95	0.00	100.00	0.00			
7160.00	100.00	74.37	0.01	7.04	0.00	100.00	0.00			
7160.50	100.00	73.38	0.01	7.57	0.00	100.00	0.00			
7161.00	100.00	71.22	0.01	8.24	0.00	100.00	0.00			
7161.50	100.00	65.71	0.01	9.04	0.00	100.00	0.00			
7162.00	100.00	64.65	0.01	9.64	0.00	100.00	0.00			
7162.50	100.00	70.88	0.01	8.47	0.00	100.00	0.00			
7163.00	100.00	71.03	0.01	8.28	0.00	100.00	0.00			
7163.50	100.00	68.52	0.01	8.30	0.00	100.00	0.00			
7164.00	100.00	68.94	0.01	8.46	0.00	100.00	0.00			
7164.50	100.00	70.26	0.01	8.32	0.00	100.00	0.00			
7165.00	100.00	61.21	0.01	9.44	0.00	100.00	0.00			
7165.50	92.98	56.78	14.15	10.05	9.31	13.53	125.99			
7166.00	96.99	59.22	16.12	10.06	9.30	9.08	84.45			
7166.50	100.00	63.12	0.01	9.82	0.00	100.00	0.00			
7167.00	100.00	67.36	0.01	9.31	0.00	100.00	0.00			
7167.50	100.00	65.30	0.01	9.50	0.00	100.00	0.00			
7168.00	100.00	62.79	0.01	9.71	0.00	100.00	0.00			
7168.50	97.49	59.53	16.57	10.08	9.32	8.38	78.03			
7169.00	92.87	56.71	16.12	10.47	9.74	13.21	128.64			
7169.50	98.52	60.16	15.82	9.78	9.00	6.78	61.01			
7170.00	100.00	64.58	0.01	9.20	0.00	100.00	0.00			
7170.50	100.00	70.38	0.01	8.24	0.00	100.00	0.00			
7171.00	100.00	73.81	0.01	7.82	0.00	100.00	0.00			
7171.50	100.00	73.24	0.01	8.17	0.00	100.00	0.00			
7172.00	100.00	67.53	0.01	9.18	0.00	100.00	0.00			
7172.50	100.00	63.33	0.01	9.86	0.00	100.00	0.00			
7173.00	100.00	68.66	0.01	8.64	0.00	100.00	0.00			
7173.50	100.00	72.89	0.01	7.89	0.00	100.00	0.00			
7174.00	100.00	72.41	0.01	8.30	0.00	100.00	0.00			
7174.50	100.00	72.69	0.01	8.16	0.00	100.00	0.00			

Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

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DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
7175.00	100.00	69.28	0.01	9.00	0.00	100.00	0.00			
7175.50	100.00	64.90	0.01	10.07	0.00	100.00	0.00			
7176.00	100.00	62.80	0.01	11.38	0.00	100.00	0.00			
7176.50	100.00	63.75	0.01	11.32	0.00	100.00	0.00			
7177.00	100.00	73.44	0.01	8.16	0.00	100.00	0.00			
7177.50	100.00	80.79	0.01	6.07	0.00	100.00	0.00			
7178.00	100.00	85.93	0.01	5.48	0.00	100.00	0.00			
7178.50	100.00	81.93	0.01	6.63	0.00	100.00	0.00			
7179.00	100.00	71.40	0.01	8.77	0.00	100.00	0.00			
7179.50	100.00	64.40	0.01	10.32	0.00	100.00	0.00			
7180.00	100.00	71.12	0.01	9.09	0.00	100.00	0.00			
7180.50	100.00	76.57	0.01	8.85	0.00	100.00	0.00			
7181.00	100.00	79.98	0.01	7.90	0.00	100.00	0.00			
7181.50	100.00	78.23	0.01	7.66	0.00	100.00	0.00			
7182.00	100.00	79.09	0.01	6.86	0.00	100.00	0.00			
7182.50	100.00	79.55	0.01	5.60	0.00	100.00	0.00			
7183.00	100.00	70.78	0.01	6.91	0.00	100.00	0.00			
7183.50	100.00	72.11	0.01	7.32	0.00	100.00	0.00			
7184.00	100.00	71.26	0.01	8.11	0.00	100.00	0.00			
7184.50	100.00	72.29	0.01	7.71	0.00	100.00	0.00			
7185.00	100.00	76.55	0.01	6.32	0.00	100.00	0.00			
7185.50	100.00	75.91	0.01	6.13	0.00	100.00	0.00			
7186.00	100.00	81.62	0.01	5.44	0.00	100.00	0.00			
7186.50	100.00	83.18	0.01	5.12	0.00	100.00	0.00			
7187.00	100.00	70.92	0.01	7.59	0.00	100.00	0.00			
7187.50	100.00	64.30	0.01	8.70	0.00	100.00	0.00			
7188.00	100.00	62.56	0.01	9.13	0.00	100.00	0.00			
7188.50	95.34	58.22	17.03	10.32	9.57	9.92	94.93			
7189.00	92.71	56.61	17.17	10.52	9.79	11.73	114.87			
7189.50	98.01	59.85	16.43	9.92	9.15	6.99	63.92			
7190.00	100.00	65.46	0.01	8.75	0.00	100.00	0.00			
7190.50	100.00	66.25	0.01	8.05	0.00	100.00	0.00			
7191.00	100.00	68.11	0.01	7.35	0.00	100.00	0.00			
7191.50	100.00	71.51	0.01	6.66	0.00	100.00	0.00			
7192.00	100.00	68.12	0.01	8.06	0.00	100.00	0.00			
7192.50	100.00	68.62	0.01	7.90	0.00	100.00	0.00			
7193.00	100.00	65.71	0.01	7.99	0.00	100.00	0.00			
7193.50	100.00	72.99	0.01	5.50	0.00	100.00	0.00			
7194.00	100.00	81.97	0.01	5.21	0.00	100.00	0.00			
7194.50	100.00	80.80	0.01	6.32	0.00	100.00	0.00			
7195.00	100.00	74.88	0.01	7.42	0.00	100.00	0.00			
7195.50	100.00	71.27	0.01	7.29	0.00	100.00	0.00			
7196.00	100.00	66.20	0.01	7.81	0.00	100.00	0.00			
7196.50	93.95	57.37	14.39	9.83	9.09	10.80	98.17			
7197.00	93.12	56.86	20.66	10.98	10.25	10.20	104.52			
7197.50	91.57	55.92	23.40	11.46	10.74	10.76	115.58			
7198.00	88.30	53.92	18.97	10.98	10.29	13.02	133.87			
7198.50	89.32	54.54	14.69	10.14	9.44	13.45	126.91			
7199.00	98.02	59.85	10.69	8.54	7.77	7.27	56.44			
7199.50	100.00	61.39	0.01	8.63	0.00	100.00	0.00			

Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

Page No 14

DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
7200.00	97.73	59.68	13.14	9.20	8.43	7.14	60.18			
7200.50	100.00	61.16	0.01	8.87	0.00	100.00	0.00			
7201.00	100.00	62.66	0.01	8.65	0.00	100.00	0.00			
7201.50	100.00	67.84	0.01	7.51	0.00	100.00	0.00			
7202.00	100.00	71.68	0.01	6.48	0.00	100.00	0.00			
7202.50	100.00	73.12	0.01	5.69	0.00	100.00	0.00			
7203.00	100.00	64.18	0.01	7.61	0.00	100.00	0.00			
7203.50	86.57	52.86	14.22	10.03	9.34	13.65	127.52			
7204.00	78.93	48.20	16.27	10.68	10.06	15.68	157.75			
7204.50	100.00	64.15	0.01	7.38	0.00	100.00	0.00			
7205.00	80.26	49.01	24.28	11.87	11.24	13.70	153.95			
7205.50	79.04	48.26	25.28	12.02	11.40	13.86	158.01			
7206.00	81.58	49.82	16.53	10.63	9.99	14.60	145.84			
7206.50	83.81	51.18	11.84	9.52	8.86	15.22	134.92			
7207.00	80.75	49.31	13.22	9.96	9.32	15.80	147.33			
7207.50	82.65	50.47	14.09	10.11	9.46	15.03	142.22			
7208.00	84.94	51.87	10.24	9.06	8.40	15.76	132.32			
7208.50	88.35	53.95	27.29	7.87	7.17	16.16	115.89			
7209.00	82.54	50.40	21.00	7.90	7.25	19.26	139.58			
7209.50	72.82	44.47	1.39	5.27	4.70	32.46	152.45			
7210.00	70.98	43.34	1.86	5.57	5.02	31.68	158.87			
7210.50	60.79	37.12	6.10	7.26	6.78	29.79	201.84			
7211.00	67.29	41.09	2.14	6.03	5.50	33.45	184.01			
7211.50	53.83	32.87	9.81	8.40	7.98	30.54	243.67			
7212.00	53.04	32.39	9.92	8.53	8.12	31.01	251.73			
7212.50	47.74	29.15	14.59	9.41	9.03	30.71	277.41			
7213.00	42.37	25.87	20.10	10.29	9.96	30.78	306.61			
7213.50	38.73	23.65	11.14	10.89	10.59	30.78	325.97			
7214.00	44.18	26.98	13.67	11.42	11.08	28.23	312.73			
7214.50	52.45	32.03	11.74	10.67	10.25	26.97	276.55			
7215.00	57.12	34.88	17.37	9.22	8.77	27.87	244.47			
7215.50	56.63	34.58	8.70	8.06	7.62	30.17	229.85			
7216.00	51.37	31.37	13.21	8.81	8.41	29.25	245.82			
7216.50	50.73	30.98	9.92	8.91	8.51	32.68	278.30			
7217.00	48.77	29.78	2.32	7.57	7.19	41.91	301.24			
7217.50	52.37	31.99	0.73	6.57	6.16	48.54	299.08			
7218.00	58.95	36.00	0.56	6.21	5.75	48.86	280.79			
7218.50	61.29	37.43	1.35	6.76	6.28	42.86	269.20			
7219.00	66.98	40.90	2.11	6.74	6.22	37.86	235.34			
7219.50	57.82	35.31	10.82	8.90	8.44	31.48	265.80			
7220.00	59.01	36.03	17.86	9.30	8.84	27.84	245.97			
7220.50	56.26	34.35	11.29	10.21	9.77	24.57	240.00			
7221.00	47.12	28.77	14.78	11.15	10.78	24.02	258.88			
7221.50	43.60	26.62	10.33	10.09	9.75	27.17	264.87			
7222.00	43.06	26.30	10.31	10.18	9.84	27.92	274.79			
7222.50	45.90	28.03	12.00	8.96	8.60	31.04	266.94			
7223.00	46.50	28.39	6.90	8.22	7.85	33.64	264.18			
7223.50	44.80	27.36	21.10	9.89	9.54	28.78	274.57			
7224.00	43.28	26.43	10.41	10.14	9.80	27.34	268.04			
7224.50	39.53	24.14	12.58	10.76	10.45	26.34	275.28			

Well name = KIDMAN #1

Location = 28-14-23S/140-49-27E

Page No 15

DEPTH	V Shale	V clay	Perm.	PhiZ	PhiE	Sw	PhiE*Sw	Cum Phi*H	Cum Hc*H	Cum H
7225.00	33.29	20.33	15.59	11.79	11.53	27.57	317.89			
7225.50	27.75	16.95	19.53	12.70	12.49	27.65	345.21	17.70	12.71	118.00
7226.00	24.16	14.75	23.15	13.30	13.11	27.13	355.59	17.76	12.76	118.50
7226.50	24.77	15.13	23.95	13.20	13.00	25.74	334.69	17.83	12.81	119.00
7227.00	41.32	25.23	10.40	10.07	9.74	26.92	262.31			
7227.50	48.66	29.71	12.68	8.50	8.12	28.45	230.88			
7228.00	49.55	30.26	16.15	9.11	8.72	28.44	248.11			
7228.50	55.58	33.94	22.83	9.68	9.24	26.85	248.08			
7229.00	57.74	35.26	13.24	10.69	10.23	23.26	238.06			
7229.50	54.18	33.08	20.25	11.90	11.47	20.29	232.77			
7230.00	49.74	30.37	22.16	9.08	8.69	25.00	217.15			
7230.50	51.82	31.64	19.34	8.74	8.33	24.95	207.74			
7231.00	47.29	28.88	25.67	9.28	8.91	24.34	216.75			
7231.50	61.29	37.43	27.32	8.60	8.12	20.47	166.15			
7232.00	69.88	42.67	34.71	8.48	7.93	17.15	135.94			
7232.50	74.18	45.30	42.79	8.51	7.93	14.96	118.63			
7233.00	70.63	43.13	42.81	8.52	7.96	15.10	120.19			
7233.50	69.98	42.73	41.95	8.76	8.21	16.40	134.74			
7234.00	69.60	42.50	12.21	9.68	9.13	16.67	152.22			
7234.50	60.47	36.93	25.24	12.15	11.67	15.92	185.89			
7235.00	59.98	36.63	12.73	7.39	6.92	22.84	157.93			
7235.50	62.11	37.93	12.08	7.04	6.55	21.48	140.64			
7236.00	59.22	36.16	17.88	7.51	7.05	19.95	140.63			
7236.50	52.90	32.30	32.72	8.56	8.14	18.68	152.10			
7237.00	45.04	27.50	12.85	7.57	7.21	24.21	174.64			
7237.50	49.83	30.43	8.98	7.15	6.76	25.67	173.52			
7238.00	45.38	27.71	28.09	8.90	8.54	21.96	187.64			
7238.50	52.69	32.17	12.26	9.70	9.29	17.97	166.87			
7239.00	68.14	41.61	19.03	10.85	10.32	13.20	136.18			
7239.50	62.68	38.28	34.47	12.84	12.35	12.83	158.42			
7240.00	61.62	37.63	82.18	15.58	15.10	11.21	169.30			
7240.50	69.43	42.40	263.04	18.93	18.38	7.85	144.36			
7241.00	68.02	41.53	565.04	21.12	20.59	6.42	132.09			
7241.50	53.26	32.52	1583.49	24.07	23.65	5.29	125.12			
7242.00	53.91	32.92	10.32	8.39	7.97	10.93	87.05			
7242.50	57.43	35.07	42.59	7.81	7.36	12.42	91.37			
7243.00	58.31	35.60	34.39	7.66	7.21	13.91	100.27			
7243.50	55.00	33.58	40.26	8.21	7.78	14.94	116.18			
7244.00	54.78	33.45	35.81	8.25	7.82	16.32	127.57			
7244.50	55.54	33.92	25.75	8.12	7.68	19.17	147.25			
7245.00	53.53	32.69	27.36	8.45	8.03	20.08	161.27			
7245.50	53.37	32.59	12.17	9.75	9.33	18.59	173.56			
7246.00	60.94	37.21	15.86	10.67	10.19	17.53	178.54			
7246.50	68.79	42.00	18.79	10.96	10.42	14.41	150.11			
7247.00	63.61	39.84	30.92	12.47	11.97	12.83	153.52			
7247.50	55.46	33.86	26.77	8.13	7.70	18.83	144.92			
7248.00	51.85	31.66	39.16	8.73	8.32	17.58	146.30			
7248.50	49.00	29.92	40.35	8.76	8.38	17.51	146.68			
7249.00	42.51	25.96	21.94	11.60	11.27	16.67	187.89			
7249.50	39.04	23.84	46.15	14.09	13.79	15.50	213.61			

KIDMAN #1

28-14-23S/140-49-27E

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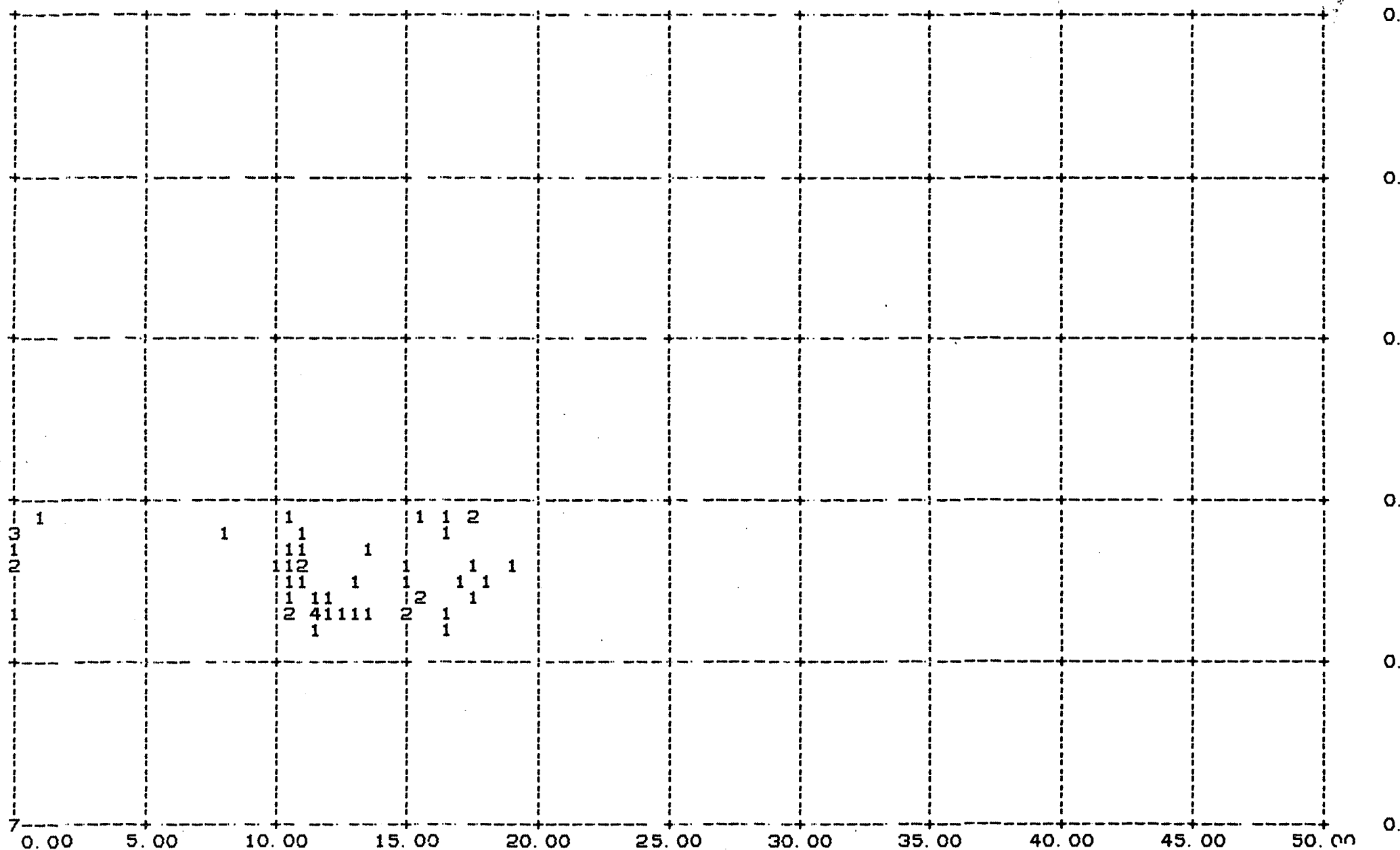
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17/01/83

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Z Axis =

Y Axis = LOG POROSITY (TOTAL)



CORE POROSITY

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KIDMAN #1

28-14-23S/140-49-27E

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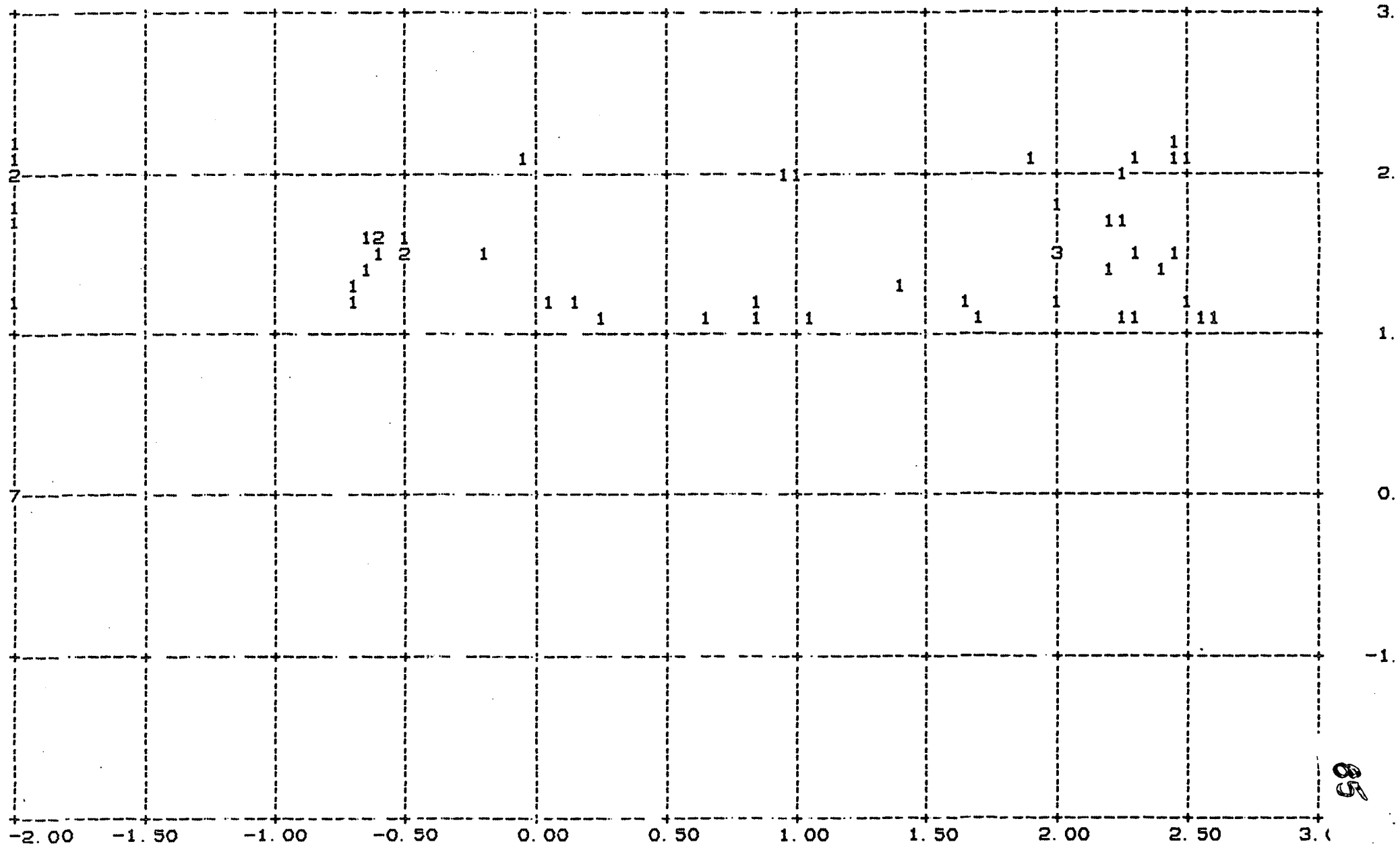
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17/01/83

FREQUENCY CUTOFF = 0 CALIPER CUTOFF = 1000.0

Z Axis =

Y Axis = LOG PERMEABILITY



CORE PERMEABILITY

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28-14-235/140-49-27E

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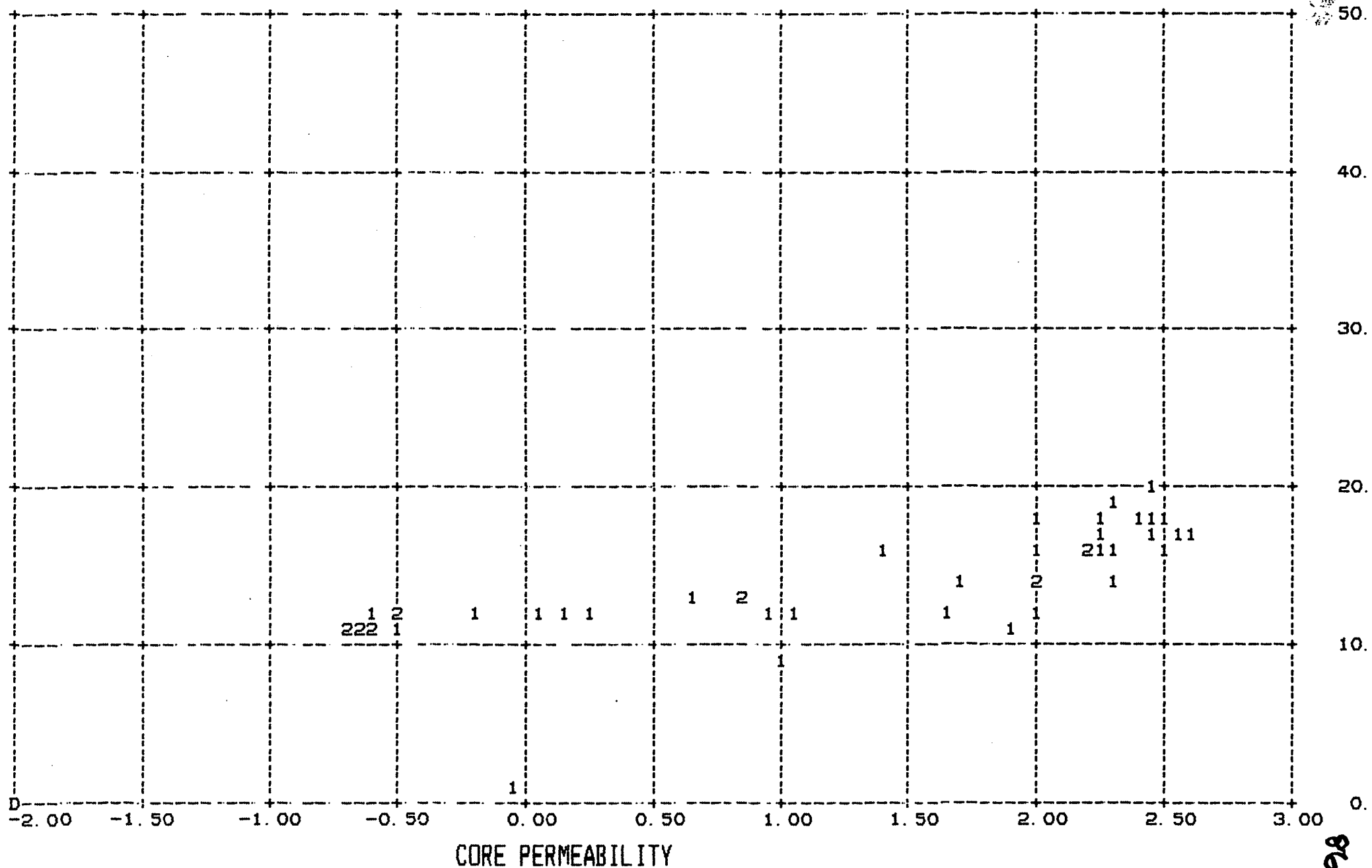
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17/01/83

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28-14-23S/140-49-27E

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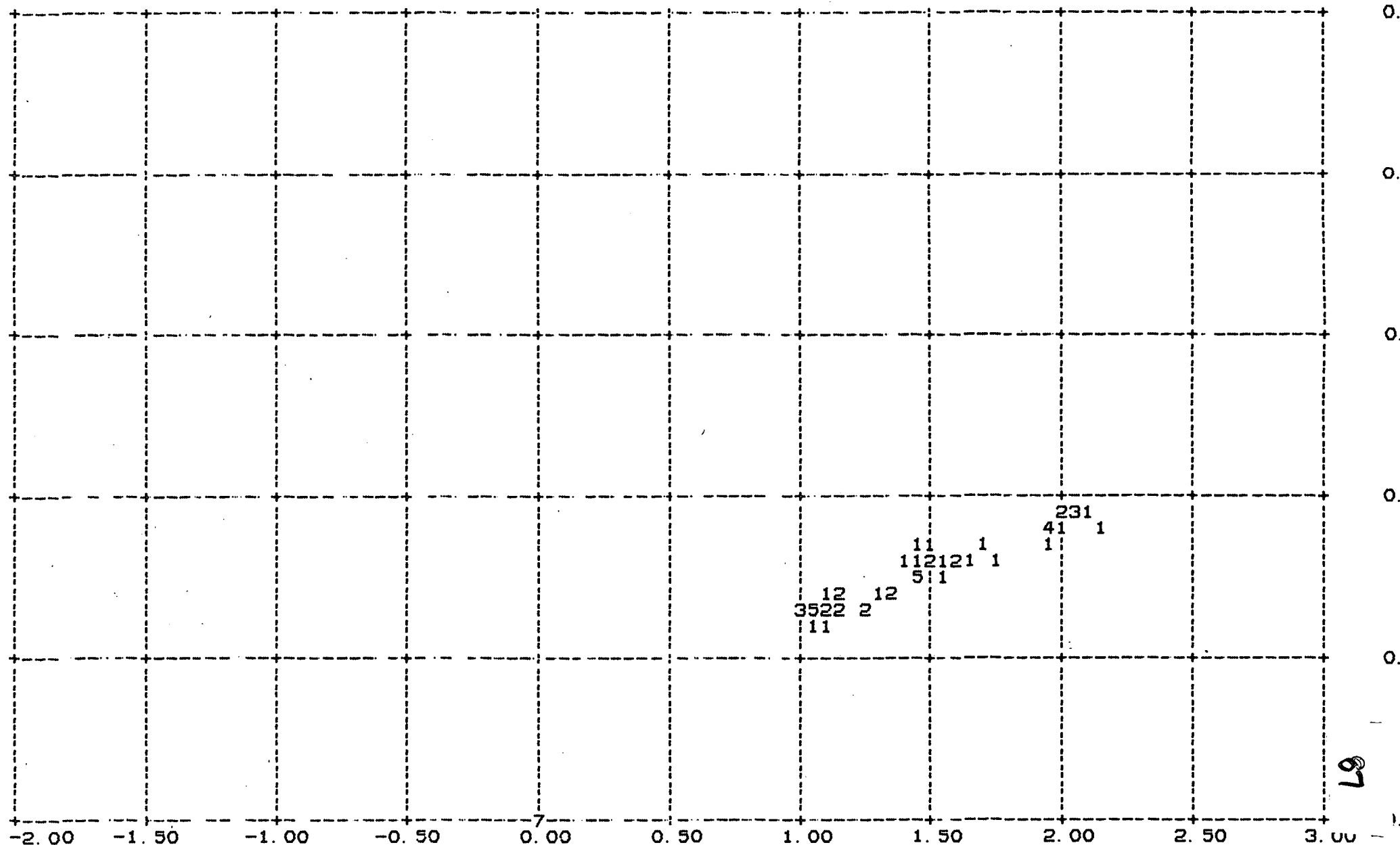
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17/01/83

FREQUENCY CUTOFF = 0 CALIPER CUTOFF = 1000.0

Z Axis =

Y Axis = LOG POROSITY (TOTAL)



LOG PERMEABILITY

KIDMAN #1

28-14-235/140-49-27E

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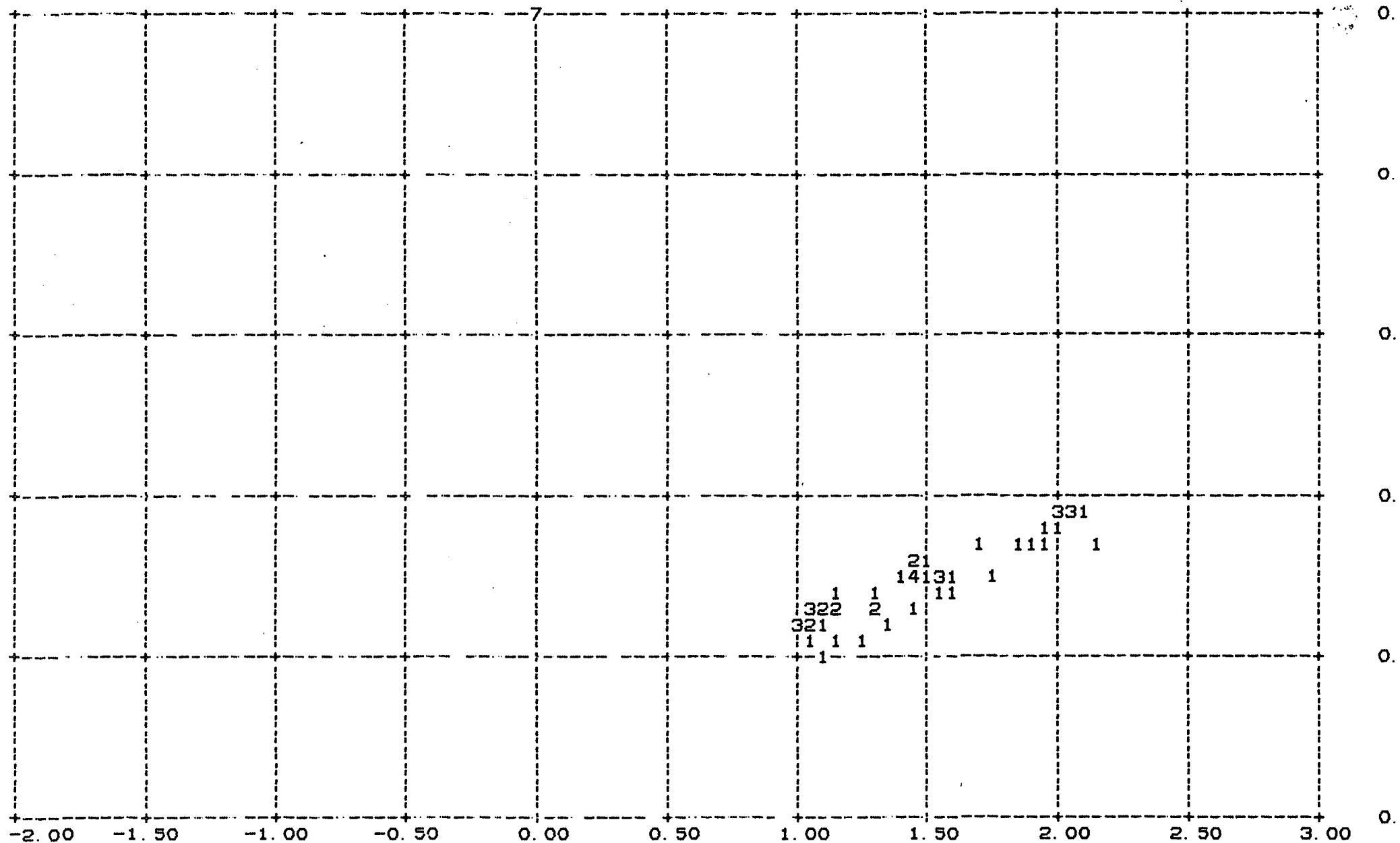
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17/01/83

FREQUENCY CUTOFF = 0 CALIPER CUTOFF =1000.0

Z Axis =

Y Axis = LOG POROSITY (EFFECTIVE)



LOG PERMEABILITY

KIDMAN #1

28-14-23S/140-49-27E

6600.0

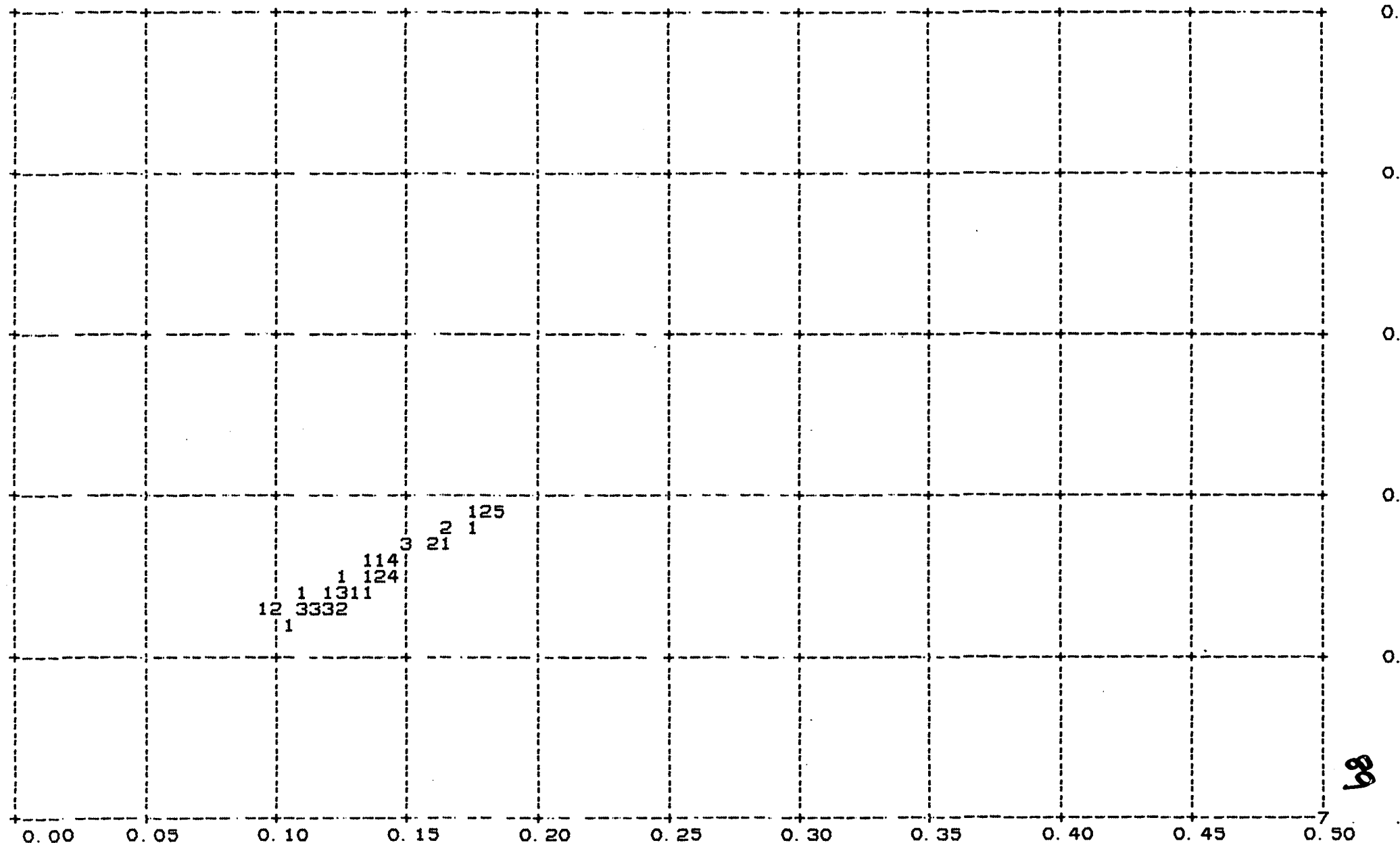
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17/01/83

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Z Axis =

Y Axis = LOG POROSITY (TOTAL)

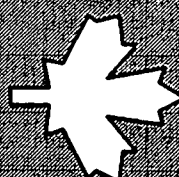


LOG POROSITY (EFFECTIVE)

121 34613383 23 225

7

COMENT
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LOG

INTERPRETATION

FOR

KIDMAN #1

28-14-23S/140-49-27E

07/12/82

FIRST FOLD HERE

ALL INTERPRETATIONS ARE OPINIONS BASED ON INFERENCES FROM ELECTRICAL OR OTHER MEASUREMENTS AND WE CANNOT, AND DO NOT, GUARANTEE THE ACCURACY OR CORRECTNESS OF ANY INTERPRETATIONS, AND WE SHALL NOT, EXCEPT IN THE CASE OF GROSS OR WILLFUL NEGLIGENCE ON OUR PART, BE LIABLE OR RESPONSIBLE FOR ANY LOSS, COSTS, DAMAGES OR EXPENSES INCURRED OR SUSTAINED BY ANYONE RESULTING FROM ANY INTERPRETATIONS MADE BY ANY OF OUR OFFICERS, AGENTS OR EMPLOYEES.

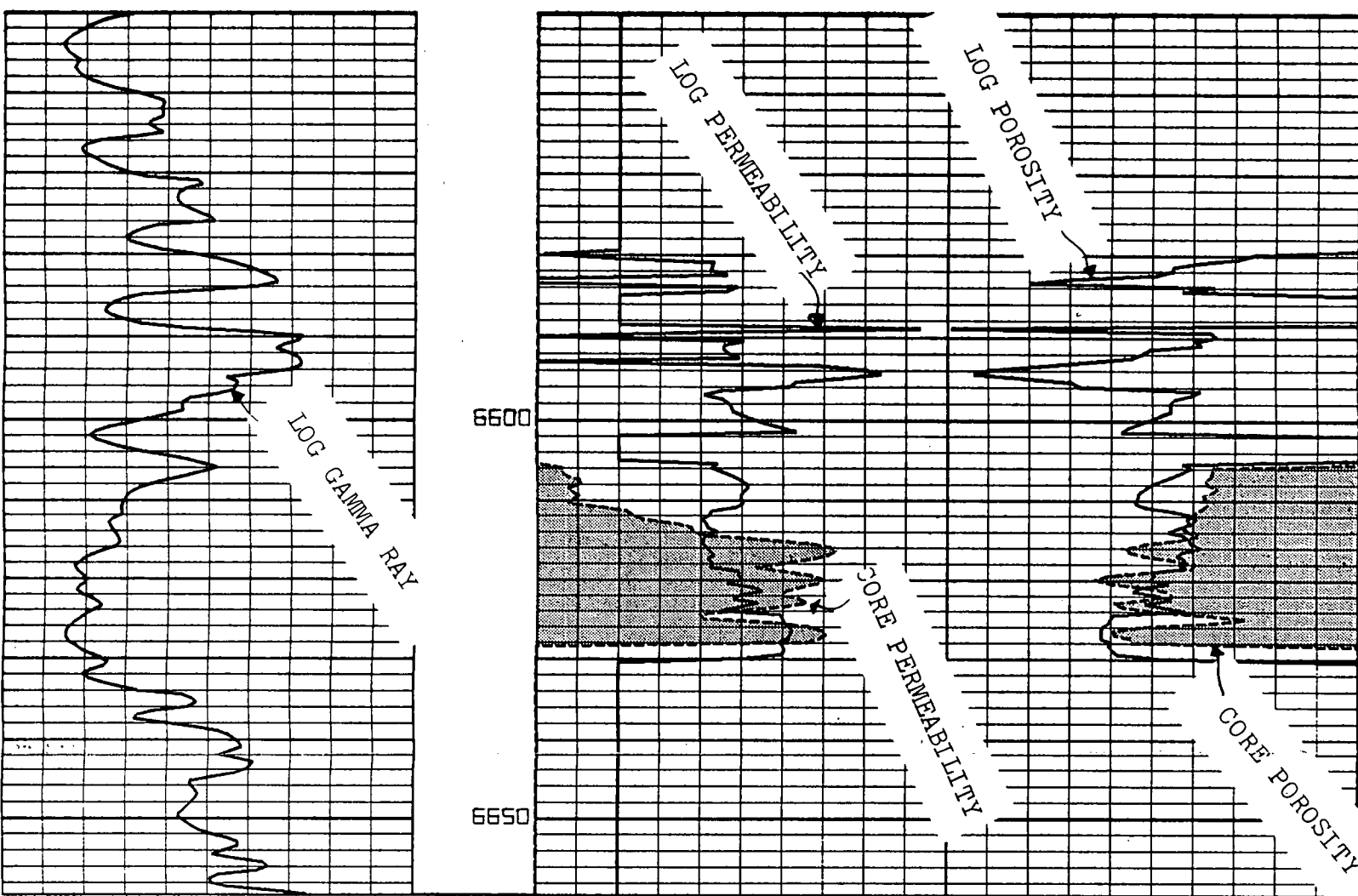
REMARKS
DATA STORED IN DKIDMAN-1

=====

= PLEASE NOTE THAT CORE DATA WAS SHIFTED DOWN 14 FEET =

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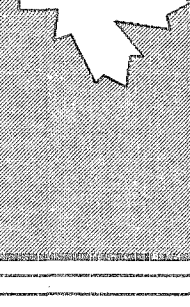
0-----GAMMA RAY-----200 .1-----PERMEABILITY-----10000 30-----POROSITY-----0



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28-14-23S/140-49-27E

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LOG

INTERPRETATION

FOR

KIDMAN #1

28-14-23S/140-49-27E

19/01/83

FIRST FOLD HERE
ALL INTERPRETATIONS ARE OPINIONS BASED ON INFERENCES FROM ELECTRICAL OR OTHER MEASUREMENTS AND WE CANNOT, AND DO NOT, GUARANTEE THE ACCURACY OR CORRECTNESS OF ANY INTERPRETATIONS. AND WE SHALL NOT, EXCEPT IN THE CASE OF GROSS OR WILLFUL NEGLIGENCE ON OUR PART, BE LIABLE OR RESPONSIBLE FOR ANY LOSS, COSTS, DAMAGES OR EXPENSES INCURRED OR SUSTAINED BY ANYONE RESULTING FROM ANY INTERPRETATIONS MADE BY ANY OF OUR OFFICERS, AGENTS OR EMPLOYEES.

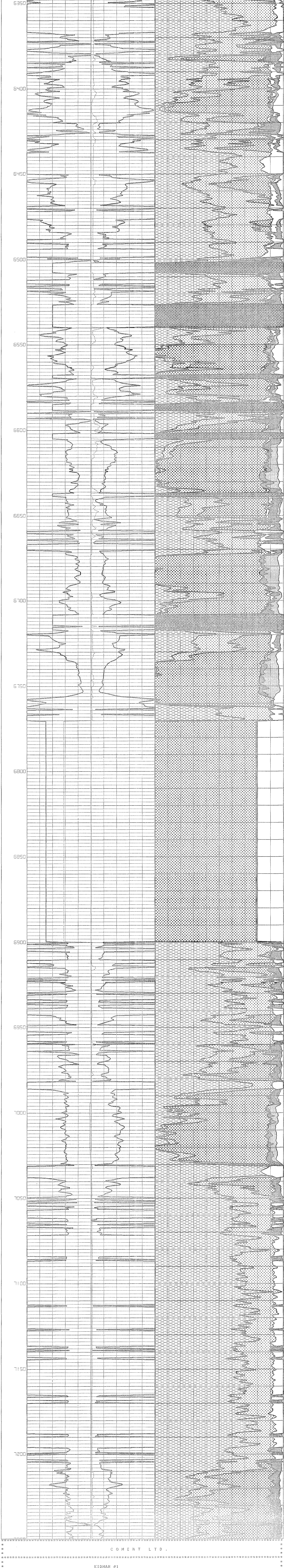
SANDSTONE ANALYSIS

FACTORS USED IN THIS INTERPRETATION

TOP	BASE	A	M	N	RK	TEMP	GRAD	GMAX	GMIN	RSH	COR	C	G	I	RHOG	RHOS	PHIS	PHIC
6340.00	6900.00	1.00	2.00	2.00	0.260	223.0	2.25	144.0	32.0	50.0	2	2	2	2	2.650	2.660	15.0	24.
6900.00	7250.00	1.00	2.00	2.00	0.180	235.0	2.25	140.0	48.0	56.0	2	2	2	2	2.650	2.760	14.0	24.

REMARKS
POROSITY DERIVED FROM NEUTRON/DENSITY XPLOT
DATA STORED IN AKIDMAN-1

DEPTH	PERMEABILITY	WATER SATURATION	BULK VOLUME ANALYSIS				
			0	100	0	100	0
			CLAY	SILT	SAND	ØZ	ØE ØESW



COMENT LTD.

KIDMAN #1

28-14-23S/140-49-27E

WP:3773N(1)

1120

SANTOS LIMITED
RESERVOIR ENGINEERING DEPARTMENT

KIDMAN #1
MODIFIED ISOCHRONAL
(TOOLACHEE FORMATION)

TEST PERFORMED: 15th - 20th MAY 1984

Report No.: RE: 207/84
Date: 6th December, 1984
Author: T.G. Paspaliaris

OK

WP:3773N (2)

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1. INTRODUCTION

2. RESULTS SUMMARY

3. CONCLUSIONS

4. RECOMMENDATIONS

5. DISCUSSION

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5.2 Simplified Analysis

5.3 LIT (Ψ) Flow Analysis

6. TABLES

Table 1 - Extended Buildup Data

Table 2 - Test Results

7. FIGURES

Figure 1 - Pseudo Pressure Horner Plot

Figure 1a - Pseudo Pressure Horner Plot with respect to Ψ_{wf}

Figure 1b - Pressure Squared Horner Plot

Figure 2 - Back Pressure Plot

Figure 3 - Deliverability Plot

8. APPENDIX A

Well Test Summary Sheets

Field and Deliverability Calculations

1. INTRODUCTION

Kidman #1 was drilled in September - October 1977 to a TD of 7720'KB (PBTD = 7079'KB). In July 1983, the well was completed as a single gas producer from the liquids-rich Toolachee Formation with 3-1/2" 9.3# J55 tubing.

This pre-production modified isochronal test was conducted between the 15th - 20th May 1984, for the purpose of determining initial reservoir parameters and to obtain representative fluid samples of the Toolachee Formation in order to establish a FWS composition.

The relevant perforated intervals and associated sands are:

<u>PERFORATED INTERVAL</u>	<u>SAND</u>	<u>NET PAY</u> <u>ft</u>	<u>POROSITY</u> <u>%</u>	<u>GAS SATURATION</u> <u>%</u>
TOOLACHEE FORMATION				
6606' - 6634'	66-1	17'	15.7	75.0
6673' - 6692'	66-7	<u>19'/30'</u>	<u>15.8</u>	<u>77.0</u>
		36'	15.8	76.1
			(Wt. ave)	(Wt. ave)

All perforations shot with 4" Casing Guns at 4 spf.

2. RESULTS SUMMARY

The pressure data was analysed using the Laminar Inertial Turbulence LIT(Ψ) method, giving the results below.

Reservoir Pressure	2912.6	psia @ 6554'KB (6313'SS)
Datum Pressure	2914.4	psia @ 6340'SS
Flow Capacity	1622.4	md-ft
Permeability	45.07	md
Apparent Skin	12.03	
Turbulence Coefficient	0.503	MMSCF/D ⁻¹
True Skin	8.22	
Damage Ratio	2.56	
Radius of Investigation	1150	ft
Absolute Open Flow Potential	29.1	MMSCFD
Stabilised Flow Constants a	9.8069	
b	0.3174	
Back Pressure Coefficients C	3.002 x 10 ⁻⁵	
n	0.8695	
Completion Efficiency	72.8%	

The Simplified Analysis gave an AOF = 31.8 MMSCF/D

The well was flowing gas at a rate of 7.573 MMSCF/D at FWHP = 2067 psig on a 28/64" choke, together with 172.5 BBLS/D condensate and 20.2 BBLS/D water, during the extended flow period.

3. CONCLUSIONS

1. The reservoir exhibited very good permeability, but the damage ratio and true skin indicate that moderate formation damage is present. This coupled with the medium turbulence coefficient of $0.503 \text{ MMSCF/D}^{-1}$ does not seriously impair deliverability.
2. The Horner slope indicates possible multilayering.
3. The completion efficiency of the well was determined to be 72.8%.
4. The well is performing adequately, and no remedial work is required at this point in time. It is anticipated that the completion efficiency of the well will decrease as production continues, and therefore some form of remedial work, such as an acid wash or reperforation, to improve flow characteristics, should be considered in the near future.

4. RECOMMENDATIONS

A pressure survey should be conducted within 6 months in order to monitor depletion under the current high decline conditions. This will also provide verification as to whether multilayering exists.

5. DISCUSSION

The test data sheets in Appendix A show the following pressure drops during the various flow periods:

<u>Flow Rate (MMSCF/D)</u>	<u>Pressure Drop (PSI)</u>
2.033	529.4
3.954	530.2
5.804	529.8
9.511	584.6
7.573	535.9

It appears that at flow rates up to 7.6 MMSCF/D flow is laminar. At 9.5 MMSCF/D, flow is beginning to enter the turbulent region.

Using the flow equation solver program, the completion efficiency was determined to be 72.8%, as outlined below:

FWHP = 2082 psia	FWHP = 2082 psia
D = 0.503	D = 0.3
S = 8.22	S = 0
yields Q = 8.53	yields Q = 11.71

A discussion on both the Simplified Analysis and the LIT(ψ) Flow Analysis for the determination of the stabilised flow constants is presented.

5.1 Horner Analysis

A Horner analysis was made based on pseudo pressures and the following equation:

$$\psi_i - \psi_{ws} = 1.632 \times 10^6 \frac{qT}{kh} \log \left(\frac{t + \Delta t}{\Delta t} \right)$$

The pressure data of the Extended Build-up (see Table 1) was used to construct a Horner Plot, a plot of

$$\psi_{ws} \text{ vs } (t + \Delta t) / \Delta t$$

on semi-logarithmic co-ordinates (see Figure 1).

This gave a best fit straight line of slope $m = 5.5 \times 10^6$ psia²/cp/cycle from which the flow capacity $kh = 1622.4$ md-ft was obtained.

The Horner slope did not behave in the conventional manner, and possibly indicates multilayering.

By extrapolation, the line yielded an average reservoir pseudo-pressure

$$\bar{\psi}_R = 553.6 \times 10^6 \text{ psia}^2/\text{cp, corresponding to an average reservoir pressure}$$

$$\bar{P}_R = 2912.6 \text{ psia}$$

This was corrected to a datum depth of 6340'SS using a gas gradient = 0.068 psi/ft (ex Static Gradient in Appendix A).

The radius of investigation of the well was determined to be 1150 ft, by means of matching the Horner plot slope.

The complete analysis is presented in Table 2.

5.2 Simplified Analysis

A back-pressure plot of

$$\Delta P^2 = \bar{P}_R^2 - P_{wf}^2 \text{ vs } q$$

was constructed on logarithmic co-ordinates as shown in Figure 2.

A straight line of slope $1/n = 1.150$, or reciprocal slope $n = 0.8695$, was drawn through the latter 3 transient flow points, and is called the transient deliverability line.

Thus flow 1 was identified as erroneous data, and was rejected from any further analysis.

A straight line parallel to the transient deliverability line was drawn through the stabilised extended flow point. This is called the stabilised deliverability line, and can be used to obtain the deliverability potential of the well against any sandface back-pressure.

It was used to calculate the Absolute Open Flow potential, AOF, which is the deliverability against a zero sandface pressure.

Based on $n = 0.8695$,

$$C = \frac{q}{(\bar{P}_R^2 - P_{wf}^2)^n} = 3.002 \times 10^{-5}$$

$$\text{Thus } q = 3.002 \times 10^{-5} (\bar{P}_R^2 - P_{wf}^2)^{0.8695}$$

giving an AOF $= C(\bar{P}_R^2)^n = 31.8 \text{ MMSCF/D}$, as can be seen in Figure 2.

5.3 LIT(Ψ) Flow Analysis

$$\text{LIT Flow Equation: } \Delta\Psi = \bar{\Psi}_R - \Psi_{wf} = aq + bq^2$$

From the Simplified Analysis, it was decided that Flow 1 was erroneous data.

The stabilised flow constants a and b were obtained from equations derived by the curve fitting method of least squares, based only on Flow 2, 3, 4 and the extended flow period.

$$\begin{aligned} \text{This yielded: } a &= 9.8069 \\ b &= 0.3174 \end{aligned}$$

A logarithmic plot of

$$(\Delta\Psi - bq^2) \text{ vs } q$$

was made (see Figure 3), where the ordinate represents the pseudo-pressure drop due to laminar flow effects.

Two lines are obtained, one for the isochronal data and one parallel through the stabilised point. This latter line is the stabilised deliverability line.

The deliverability potential of the well against any sandface pressure can be obtained by solving the above quadratic equation for the particular value of $\Delta\Psi$.

$$\text{i.e. } q = \frac{-a + \sqrt{a^2 + 4b \Delta\Psi}}{2b}$$

It was used to calculate the AOF of the well, which is the deliverability against a zero sandface pressure, i.e. $\Psi_{wf} = 0$.

$$\begin{aligned} \text{AOF} &= \frac{-a + \sqrt{a^2 + 4b \bar{\Psi}_R}}{2b} \\ &= 29.1 \cdot \text{MMSCF/D} \end{aligned}$$

6. TABLES

TABLE 1

0101

EXTENDED
BUILD UP PRESSURE DATA

Well Name: KIDMAN #1

Date Tested: 15-20 May 1984

Lubricator Pressure (psia)

Pressure Element: 60306

In Out

Depth Tested: 6554'KB

Amerada

2360.0 2350.2

Deadweight

2359.7 2359.7

$$t = \frac{\text{CUMULATIVE PRODUCTION}}{\text{LAST RATE BEFORE SHUT IN}} = \frac{5.563 \text{ MMSCF}}{7.573 \text{ MMSCF/D}} = 17.63 \text{ HOURS}$$

Δt hours	PRESSURE psia	PSEUDO PRESSURE $\text{psia}^2/\text{cp} \times 10^6$	$\Delta \psi$	$\frac{t + \Delta t}{\Delta t}$
0	2617.6	459.214	0.0	-
0.25	2873.2	540.737	81.523	71.5
0.5	2881.9	543.563	84.349	36.3
0.75	2887.5	545.382	86.168	24.5
1	2891.1	546.551	87.337	18.6
1.25	2892.4	546.974	87.760	15.1
1.5	2894.0	547.493	88.279	12.8
1.75	2895.5	547.980	88.766	11.1
2	2896.6	548.338	89.124	9.82
3	2899.4	549.247	90.033	6.88
4	2901.3	549.871	90.657	5.41
5	2902.4	550.234	91.020	4.53
6	2902.7	550.332	91.118	3.94
12	2906.1	551.454	92.240	2.47
18	2906.4	551.553	92.339	1.98
25.53	2906.8	551.685	92.471	1.69

TABLE 2
GAS WELL DELIVERABILITY TEST
RESULTS OF ISOCHRONAL 'LIT' ANALYSIS

0102

WELL NAME: KIDMAN #1 FORMATION: TOOLACHEE DATE OF TEST 15-20 MAY 1984
DEPTH TESTED: 6554 'K.B.

PRESSURE BUILD-UP INFORMATION

EXTRAPOLATED PRESSURE $P^* = \underline{8483.2} \times 10^3 \text{ psia}^2$
 $= \underline{2912.6} \text{ psia cf 2908 from STATIC GRAD}$
 $\psi^* = \underline{553.6} \times 10^6 \text{ psia}^2/\text{cp}$
 HORNER BUILD-UP SLOPE $m = \underline{97.0} \times 10^3 \text{ psia}^2/\text{cycle}$
 $m(\psi) = \underline{5.5} \times 10^6 \text{ psia}^2/\text{cp/cycle}$

WELL AND TEST PARAMETERS $S_g = 0.761$ $C_g = 0.318 \times 10^{-3}$

Porosity $\phi = \underline{0.158}$ Viscosity $\mu = \underline{0.0198} \text{ cp @ } P(\text{med}) = 2890 \text{ psia}$

Compressibility $C_t = \underline{0.242 \times 10^{-3}}$ well radius $r_w = \underline{0.3542} \text{ ft}$

Well drainage $r_e = \underline{1150} \text{ ft}$ thickness $h = \underline{36} \text{ ft}$

Final flow rate $q = \underline{7.573} \text{ MMcfd}$ Temperature $T = \underline{722} \text{ }^\circ\text{R}$

Sandface press. $P_o = \underline{2617.6} \text{ psia}$ Press 1 hr $P_1 = \underline{2891.4} \text{ psia}$
 $\psi_o = \underline{459.214} \times 10^6 \text{ psia}^2/\text{cp}$ $\psi_1 = \underline{546.64} \times 10^6 \text{ psia}^2/\text{cp}$

BACK PRESSURE COEFFICIENTS

$$\Delta\psi = a q + b q^2$$

$$a = \underline{9.8069} \times 10^6 \text{ psia}^2/\text{cp/MMcfd}$$

$$b = \underline{0.3174} \times 10^6 \text{ psia}^2/\text{cp/MMcfd}$$

FLOW CAPACITY

$$kh = \frac{1.632 \times 10^6}{m} \quad qT = \underline{1622.4} \text{ md-ft}$$

PERMEABILITY

$$k = \frac{kh}{h} = \underline{45.07} \text{ md}$$

APPARENT SKIN

$$S' = 1.151 \left[\frac{\psi_1 - \psi_o}{m} - \log \left(\frac{k}{\phi \mu C_t r_w^2} \right) + 3.23 \right] = \underline{12.03}$$

TURBULENCE COEFFICIENT

$$D = \frac{b kh}{1.417 \times 10^6 T} = \underline{0.503} \text{ MMcfd}^{-1}$$

TRUE SKIN

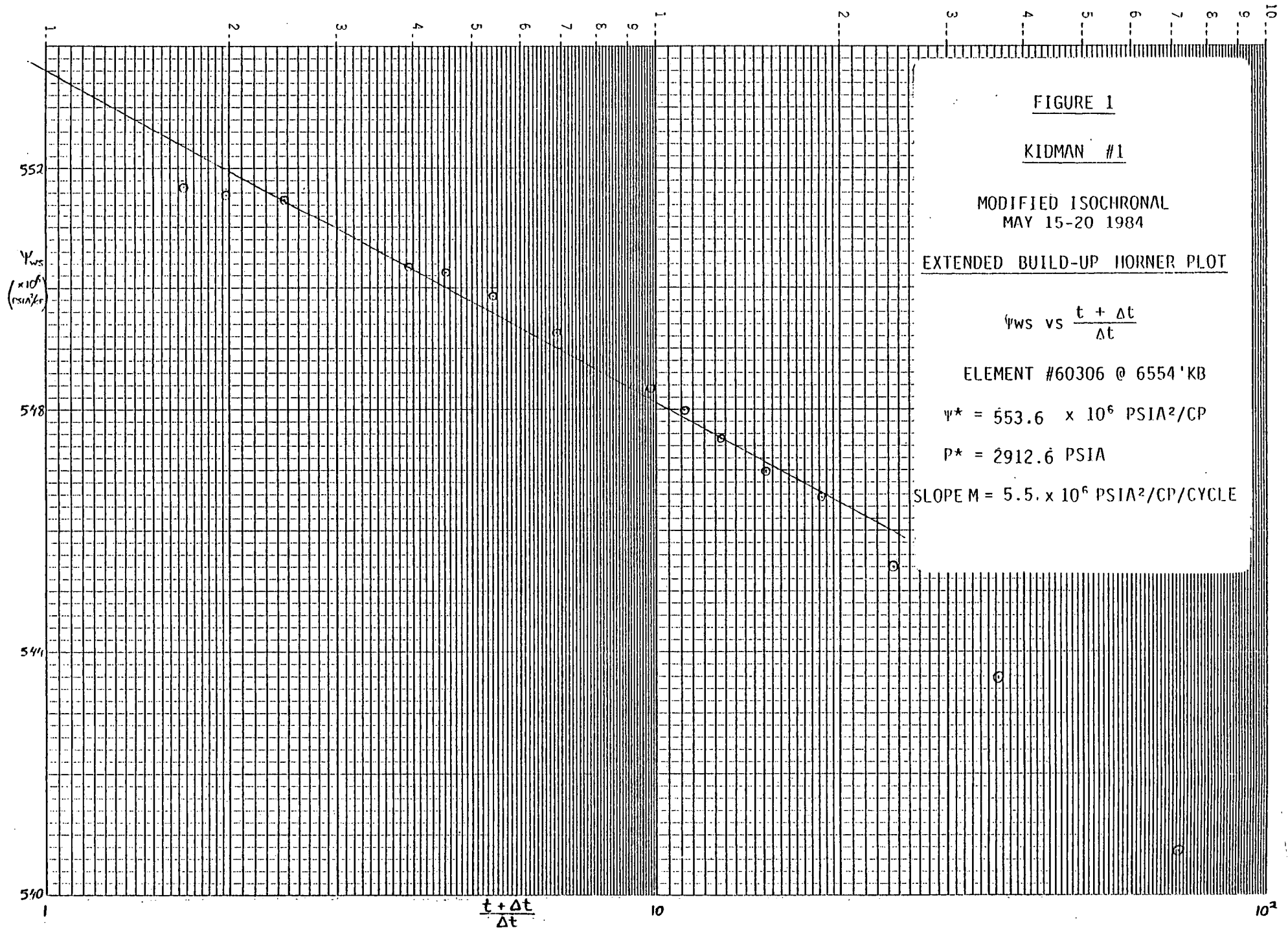
$$S = S' - Dq = \underline{8.22}$$

$$\Delta\psi_s' = 0.869 \text{ ms} = \underline{57.50}$$

$$DR = \frac{\psi^* - \psi_{wf}}{\psi^* - \psi_{wf} - \Delta\psi_s'} = \underline{2.56}$$

$$\psi^* - \psi_{wf} - \Delta\psi_s'$$

7. FIGURES



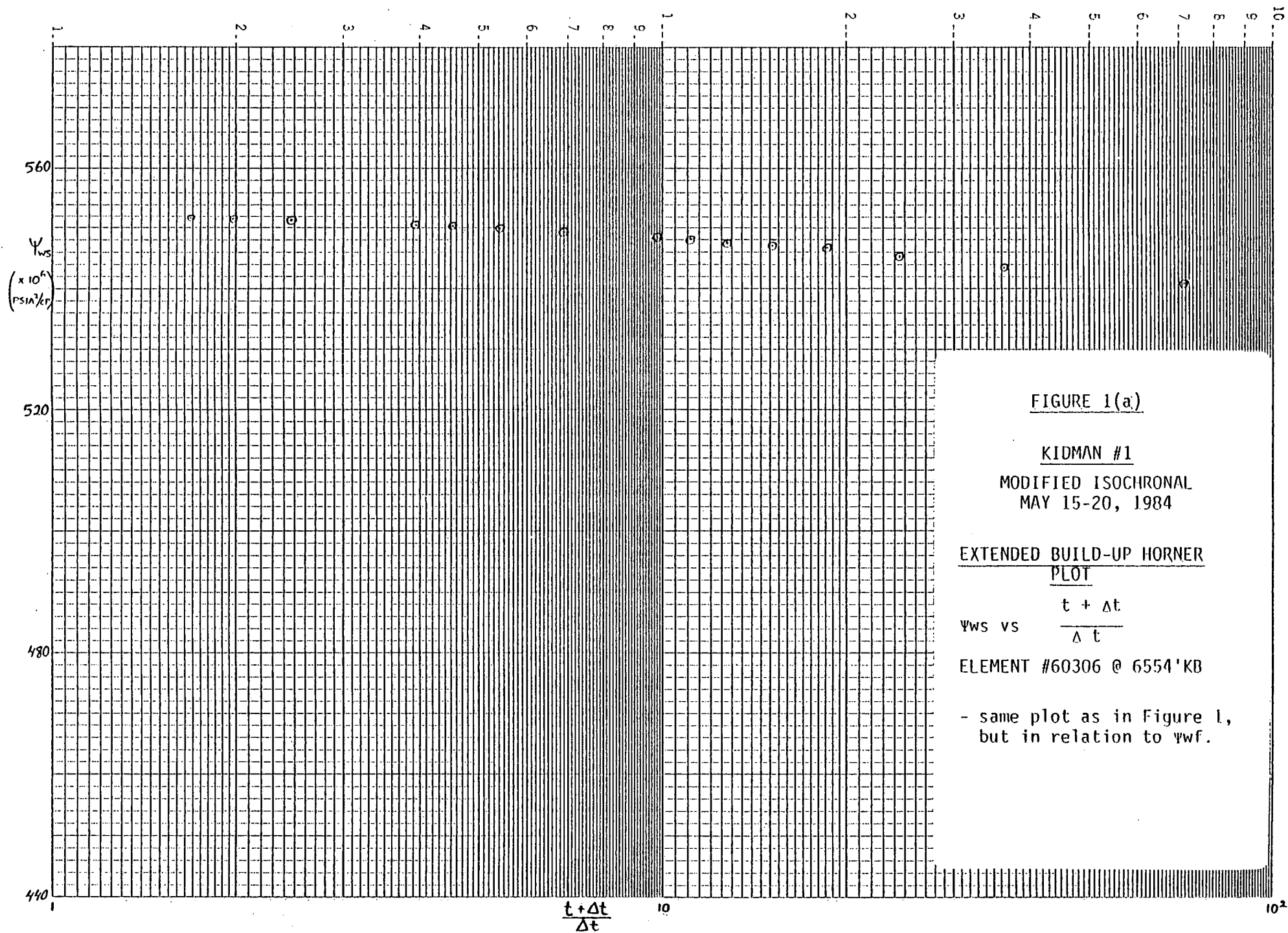


FIGURE 1(a)

KIDMAN #1

MODIFIED ISOCHRONAL
MAY 15-20, 1984

EXTENDED BUILD-UP HORNER
PLOT

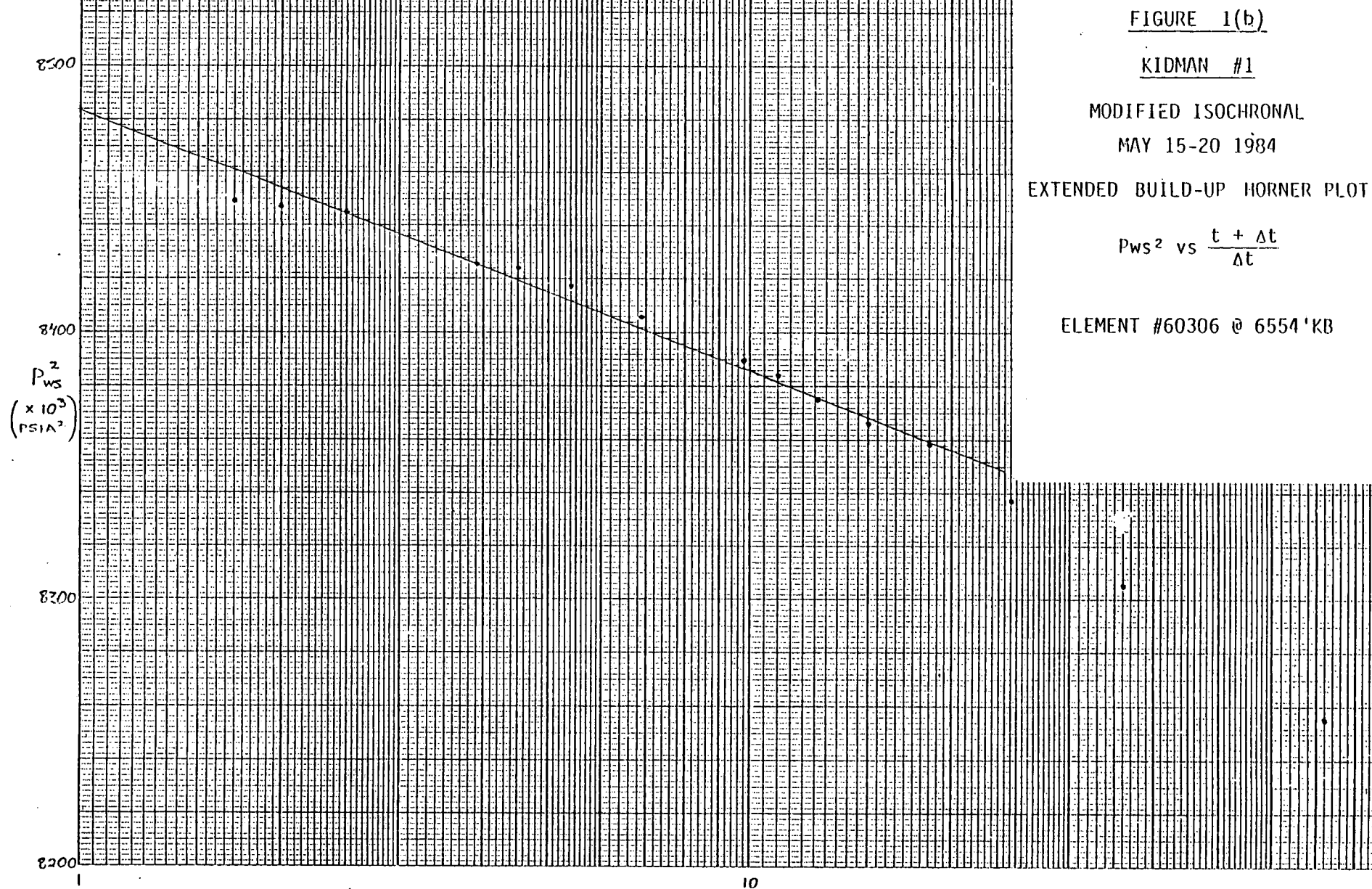
Ψ_{ws} vs $\frac{t + \Delta t}{\Delta t}$

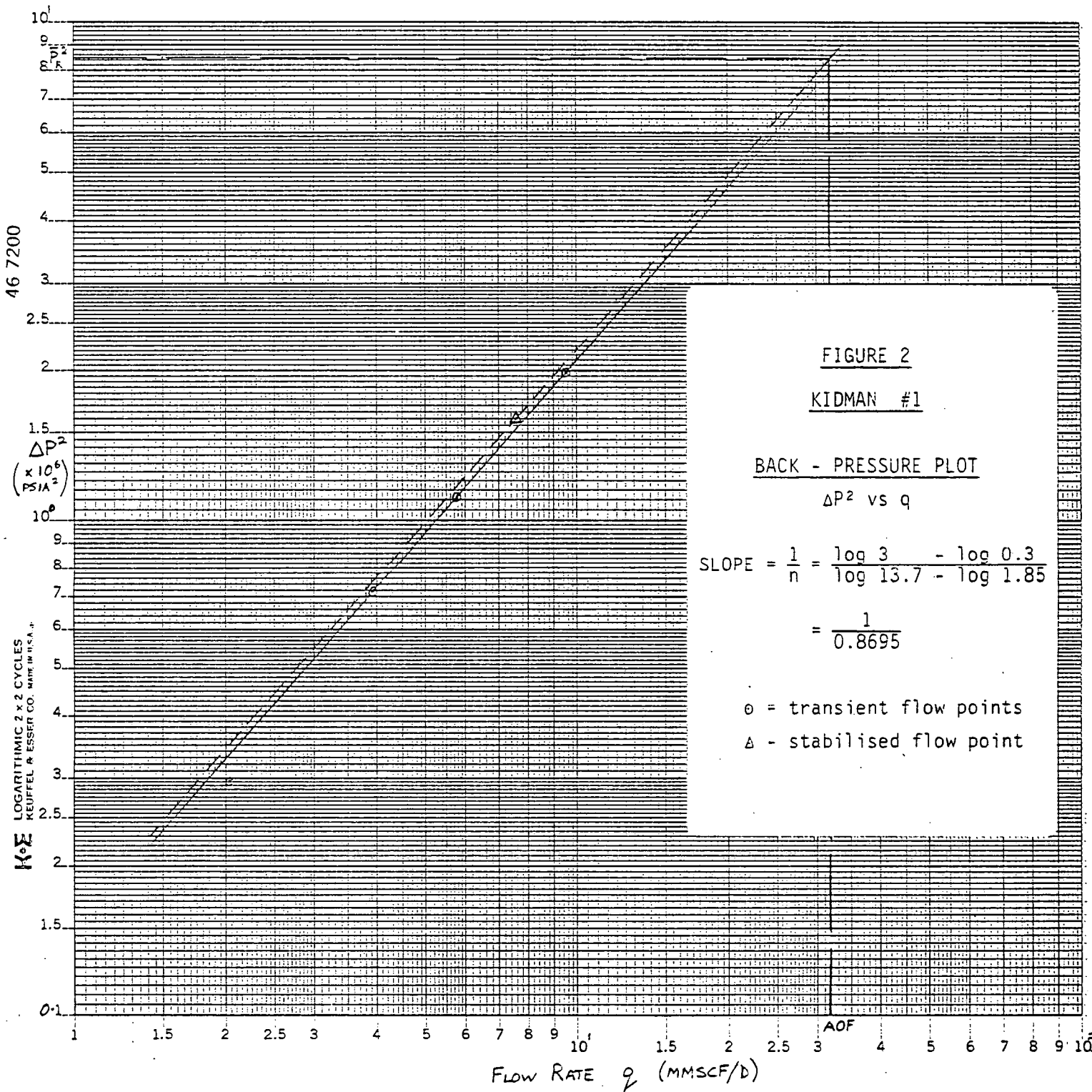
ELEMENT #60306 @ 6554'KB

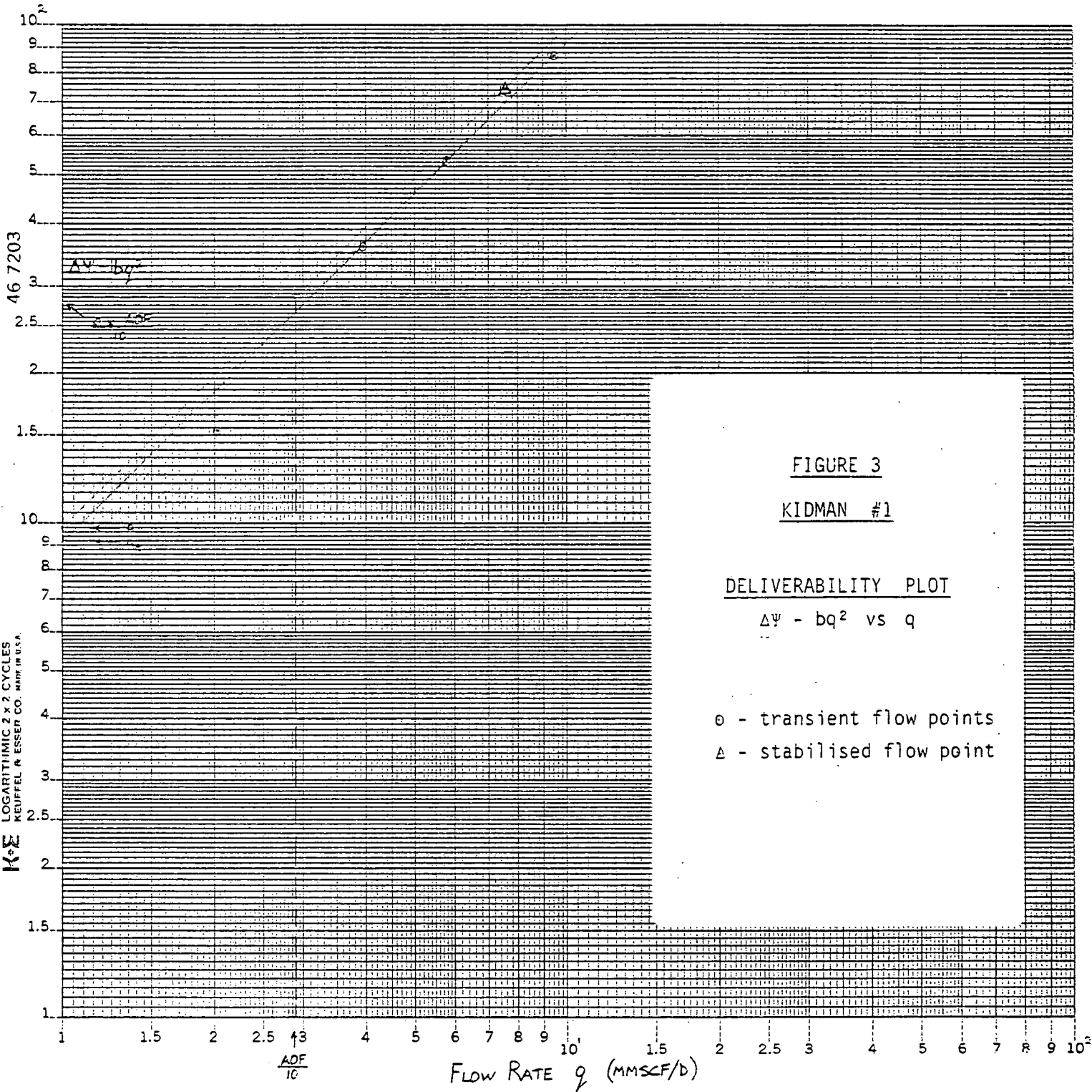
- same plot as in Figure 1,
but in relation to Ψ_{wf} .

0105

0106







8. APPENDIX A

WELL TEST SUMMARY SHEETS

- FIELD AND DELIVERABILITY CALCULATIONS

WELL: Kidman #1	Lat.: 28°14'24"S		
TESTED BY: L. Knox	LOCATION: Long: 140°49'27"E	DATE: May 15th - 20th 1984	FIELD Toolachee Formation
CASING SIZE: 7 ins	*PERFORATIONS: 6606-6692 ft	PRODUCING THROUGH: tubing	
TUBING SIZE: 3.5 ins	WEIGHT: 23 + 26 lb/ft	GRADE: J55 + N80	
	WEIGHT: 9.3 lb/ft	GRADE: J55	

DESCRIPTION OF TEST

INITIAL SHUT IN PERIOD

Time of Observations			Observed		Pressures	REMARKS
Date	Time	Shut In Time (Hours)	Tubing psig	Casing psig	Temp. °F	
15/5/84	1600	0				Shut well in
17/5/84	1011	42.18	2342			Ran Static Gradient
17/5/84	1600	48	2345	2070		Opened well on 1st rate

Flow Period

Run No.: 1	Duration of Run: 2	Hours.	Orifice Size: 1.250	ins
Flow Well On: 13/64"	Choke.		Meter Run: 3.826	ins

[illegible]

SANTOS LTD.
WELL TEST SUMMARY

Page 2.

2ND SHUT IN PERIOD

Time of Observations			Observed Pressures			REMARKS
Date	Time	Shut In Time (Hours)	Tubing	Casing	Temp.	
			psig	psig	°F	
17/5/84	1800	0	2323	2275	102	Shut well in
	1815	0.25	2358	2250		
	1830	0.5	2362	2240		
	1845	0.75	2363	2220		
	1900	1	2361	2210		
	1930	1.5	2361	2175		
	2000	2	2361	2175		Opened well on 2nd rate

Run No.: 2 Duration of Run: 2 Hours. Orifice Size: 1.500 ins
Flow Well On: 22/64" Choke. Meter Run: 3.826 ins

Date	Time	Flow Time (Hours)	Wellhead Readings			Meter or Prover Data			Condensate Production Bbls/d	Water Production Bbls/d
			Tubing	Casing	Temp.	Pf	Hw	Temp.		
			psig	psig	°F	psig	inches	°F		
17/5/84	2000	0	2361	2175						
	2030	0.5	2225	2290	100	605	160	94		
	2100	1	2225	2330	108	605	170	88	100.6	Nil
	2130	1.5	2238	2340	113	605	162	100		
	2200	2	2244	2340	117	610	156	86	80.4	Nil
	Choke appeared to be plugging throughout 2nd rate, upon inspection of choke pieces of steel were found edged between needle & seat, these were retained for inspection. No damage to choke.									

0111

SANTOS LTD.
WELL TEST SUMMARY

Page 3.

3RD SHUT IN PERIOD

Time of Observations			Observed Pressures			REMARKS
Date	Time	Shut In Time (Hours)	Tubing psig	Casing psig	Temp. °F	
17/5/84	2200	0	2244	2340	117	
	2215	0.25	2370	2330		Shut well in
	2230	0.5	2370	2330		
	2245	0.75	2370	2330		
	2300	1	2370	2310		
	2330	1.5	2370	2275		
	2400	2	2367	2240		Opened well

Run No.: 3 Duration of Run: 2 Hours. Orifice Size: 2.000 ins
Flow Well On: 23/64" Choke. Meter Run: 3.826 ins

Date	Time	Flow Time (Hours)	Wellhead Readings			Meter or Prover Data			Condensate Production Bbls/d	Water Production Bbls/d
			Tubing psig	Casing psig	Temp. °F	Pf psig	Hw inches	Temp. °F		
17/5/84	2400	0	2367	2240						
18/5/84	0030	0.5	2152	2410	111	600	99	83		
	0100	1	2163	2450	118	600	103	92	161.0	Nil
	0130	1.5	2168	2460	122	600	104	99		
	0200	2	2169	2465	127	600	105	99	80.4	Nil

0112

SANTOS LTD.
WELL TEST SUMMARY

Page 4.

4TH SHUT IN PERIOD

Time of Observations			Observed Pressures			REMARKS
Date	Time	Shut In Time (Hours)	Tubing psig	Casing psig	Temp. °F	
18/5/84	0200	0	2169	2465	127	Shut well in
	0215	0.25	2372	2450		
	0230	0.5	2370	2425		
	0245	0.75	2370	2385		
	0300	1	2370	2350		
	0330	1.5	2371	2300		
	0400	2	2370	2265		Opened well on 4th rate

Run No.: 4 Duration of Run: 2 Hours. Orifice Size: 2.500 ins
Flow Well On: 33/64" Choke. Meter Run: 3.826 ins

Date	Time	Flow Time (Hours)	Wellhead Readings			Meter or Prover Data			Condensate Production Bbls/d	Water Production Bbls/d
			Tubing	Casing	Temp.	Pf	Hw	Temp.		
			psig	psig	°F	psig	inches	°F		
18/5/84	0400	0	2370	2265						
	0430	0.5	1909	2470	120	600	101	90		
	0500	1	1930	2475	135	600	103	96	281.8	40.3
	0530	1.5	1943	2680	140	600	102	100		
	0600	2	1946	2690	145	605	102	104	241.4	40.3

0113

FINAL STABILIZATION FLOW PERIOD

Run No.:	5	Duration of Run:	12	Hours.	Orifice Size:	2.250 ins
Flow Well On:	28/64"	Choke.			Meter Run:	3.826 ins

[illegible]

0110

Page 6.

0115

FINAL BUILD-UP, SUBSURFACE PRESSURES

ELEMENT NO. 60306

BOMB DEPTH 6554

' KB

$$DWT_{in} = 2345 \text{ psig/out} = 2345 \text{ psig}$$
$$LUB_{in} = 2360.0 \text{ psig/out} = 2350.2 \text{ psig}$$
[illegible]

01167

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WELL TEST SUMMARY
CALCULATION SHEET

Page 8.

CASE 1: FLOW THROUGH METER RUN

Run No.	Hw (inches in water)	PF (psig)	Size Orifice Plate (inches)	Ft (°F)
1	91	590	1.250	90
2	156	610	1.500	86
3	105	600	2.000	99
4	102	605	2.500	104
5	109	600	2.250	111

(Taken from Kidman Toolachee Gaspac)

Specific Gravity = 0.8323

TC = 414.8 °R

PC = 694.2 psia

CO2 CONTENT = 8.845 mole %

Meter Run = 3.826 ins

FLOW THROUGH METER RUN (Continued)

Run No.	Q (MMscfd)
1	2.033
2	3.954
3	5.804
4	9.511
5	7.573

0117

GAS WELL DELIVERABILITY TEST CALCULATIONS
(Base Conditions = 14.65 psia and 60°F)

WELL NAME: KIDMAN #1 DATE: MAY 15th - 20th 1984 ELEMENT NO: 60306 DEPTH TESTED: 6554' KB
DWT IN: 2345 psig OUT: 2345 psig
LUB IN: 2360.0 psig OUT: 2350.2 psig

SIMPLIFIED ANALYSIS

	Duration (hours)	Sandface Pressure (psia)	Cal.	Meas.	Δp^2 ($\times 10^6$ psia ²)	Flow Rate (Mmscfd)	H/Carbon Prod. (BBLs/D)	Water Prod. (BBLs/D)	REMARKS
Initial Shut In	48	2918.2		X	/	/	/	/	$q = C(\bar{p}_R^2 - p_{wf}^2)^n$ reciprocal slope $n = 0.8695$ $\bar{p}_R = 2912.6$ psia $C = \frac{q}{(\bar{p}_R^2 - p_{wf}^2)^n}$ $= 3.002 \times 10^{-5}$ AOF (MMscfd) $= 31.75$
Flow 1	2	2867.1		X	0.296	2.033	10.1	Nil	
Shut In	2	2915.1		X	/	/	/	/	
Flow 2	2	2788.9		X	0.720	3.954	90.5	Nil	
Shut In	2	2912.3		X	/	/	/	/	
Flow 3	2	2713.5		X	1.118	5.804	120.7	Nil	
Shut In	2	2909.3		X	/	/	/	/	
Flow 4	2	2545.3		X	1.985	9.511	261.6	40.3	
Extended Flow	12	2617.6		X	1.598	7.573	172.5	20.2	
Final Shut In	25.53	2906.8		X	/	/	/	/	

0118

GAS WELL DELIVERABILITY TEST CALCULATIONS
(Base Conditions = 14.65 psia and 60°F)

LIT (ψ) ANALYSIS

	Duration (hours)	Sandface Pressure (psia)	ψ ($\times 10^6$ psia ² /cp)	$\Delta\psi$ ($\times 10^6$ psia ² /cp)	Flow Rate (q) (MMscfd)	$\Delta\psi/q$	q^2	$\Delta\psi - bq^2$
Initial Shut In	48	2918.2	555.444					
Flow 1	2	2867.1	538.756	16.688	2.033	8.209	4.133	15.376
Shut In	2	2915.1	554.422					
Flow 2	2	2788.9	513.417	41.005	3.954	10.371	15.634	36.043
Shut In	2	2912.3	553.498					
Flow 3	2	2713.5	489.338	64.160	5.804	11.054	33.686	53.468
Shut In	2	2909.3	552.509					
Flow 4	2	2545.3	436.919	115.590	9.511	12.153	90.459	86.878
Total=				237.443	21.302	41.787	143.912	
Extended Flow	12	2617.6	459.214	92.471	7.573	12.211	57.350	74.268
Final Shut In	25.53	2906.8	551.685					

TOTAL MINUS FLOW 1

220.755

19.269

33.578 139.779

0119

GAS WELL DELIVERABILITY TEST CALCULATIONSL.I.T. (Ψ) ANALYSISDISCARDED POINT FLOW #1

$$N = \underline{3} \quad \bar{\Psi}_R = \underline{553.6} \text{ MMpsia}^2/\text{cp}$$

$$a, a_t = \frac{\sum \frac{\Delta \Psi}{q} \sum q^2 - \sum q \sum \Delta \Psi}{N \sum q^2 - \sum q \sum q} = \underline{9.1538}$$

$$b = \frac{N \sum \Delta \Psi - \sum q \sum \frac{\Delta \Psi}{q}}{N \sum q^2 - \sum q \sum q} = \underline{0.3174}$$

(EXTENDED FLOW)

$$\Delta \Psi = \underline{92.471} \quad q = \underline{7.573} \quad b = \underline{0.3174}$$

$$a = \frac{\Delta \Psi - bq^2}{q} = \underline{9.8069}$$

RESULTS

$$\text{TRANSIENT FLOW: } \bar{\Psi}_R - \Psi_{wf} = a_t q + bq^2$$

$$\text{i.e. } \underline{553.6} - \Psi_{wf} = \underline{9.1538} q + \underline{0.3174} q^2$$

$$\text{STABILIZED FLOW: } \bar{\Psi}_R - \Psi_{wf} = a q + bq^2$$

$$\text{i.e. } \underline{553.6} - \Psi_{wf} = \underline{9.8069} q + \underline{0.3174} q^2$$

DELIVERABILITY:

$$q = \frac{1}{2b} [-a + \sqrt{a^2 + 4b (\bar{\Psi}_R - \Psi_{wf})}]$$

$$\text{FOR } \Psi_{wf} = 0, q = \text{AOF} = \underline{29.08} \text{ MMscfd}$$

$$\text{A.O.F.} = \underline{29.08} \text{ MMSCFD} \quad n = \underline{0.8695}$$

$$\text{Total Volume of Gas Produced During Test} = \underline{5.563} \text{ MMSCF}$$

$$\text{Condensate} = \underline{127.46} \text{ Bbls}$$

$$\text{Water} = \underline{15.12} \text{ Bbls}$$

REMARKS

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SUB-SURFACE PRESSURE SURVEY

CO. SANTOS	RUN 02 FIELD KIDMAN	WELL 01
EFF DEPTH	WELL STAT	TOOL HUNG
CASING 7" -	CASING PRESS	ON BOTTOM 17/5 1036
LINER -	TUBING PRESS	OFF BOTTOM
DATE 840517	ELEMENT RANGE 0 - 5108	ZERO POINT
ELEVATION	ZONE TOOLACHEE	SHUT-IN
MAX TEMP	PICK-UP	ON-PROD
PERF 6606'-6692'	CAL SER NO. 60306	MPP 6649' KB
TUBING 3-1/2" -		
UNITS ENGLISH	PURPOSE	STATIC PRESSURE GRADIENT

SURVEY DATA

CO. SANTOS				RUN 02 FIELD KIDMAN				WELL 01			
TIME	DEPTH	P/T	GRAD	TIME	DEPTH	P/T	GRAD	TIME	DEPTH	P/T	GRAD
10:40	0	2348.3	0.000	11:31	5000	2781.5	.076				
10:51	1000	2445.5	.097	11:42	6000	2854.9	.073				
11:00	2000	2536.1	.091	12:01	6649	2899.3	.068				
11:10	3000	2621.8	.086	12:07	6692	2910.7	.265				
11:21	4000	2705.1	.083	0:00	0	0.0	0.000				

LUB IN DWT = 2345 PSIG / OUT = 2348 PSIG
LUB IN AMERADA = 2348.3 PSIG / OUT = 2358.3 PSIG

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PAGE 1

SUB-SURFACE PRESSURE SURVEY

CO. SANTOS		RUN 01 FIELD KIDMAN		WELL 01	
EFF DEPTH		WELL STAT		TOOL HUNG	
CASING 7"	-	CASING PRESS		ON BOTTOM	17/5 1036
LINER	-	TUBING PRESS		OFF BOTTOM	
DATE	840517	ELEMENT RANGE	0 - 5168	ZERO POINT	
ELEVATION		ZONE	TOOLACHEE	SHUT-IN	
MAX TEMP		PICK-UP		ON-PROD	
PERF	6606'-6692'	CAL SER NO.	22581	MPP	6649' KB
TUBING 3-1/2"	-				
UNITS	ENGLISH	PURPOSE	STATIC PRESSURE GRADIENT		

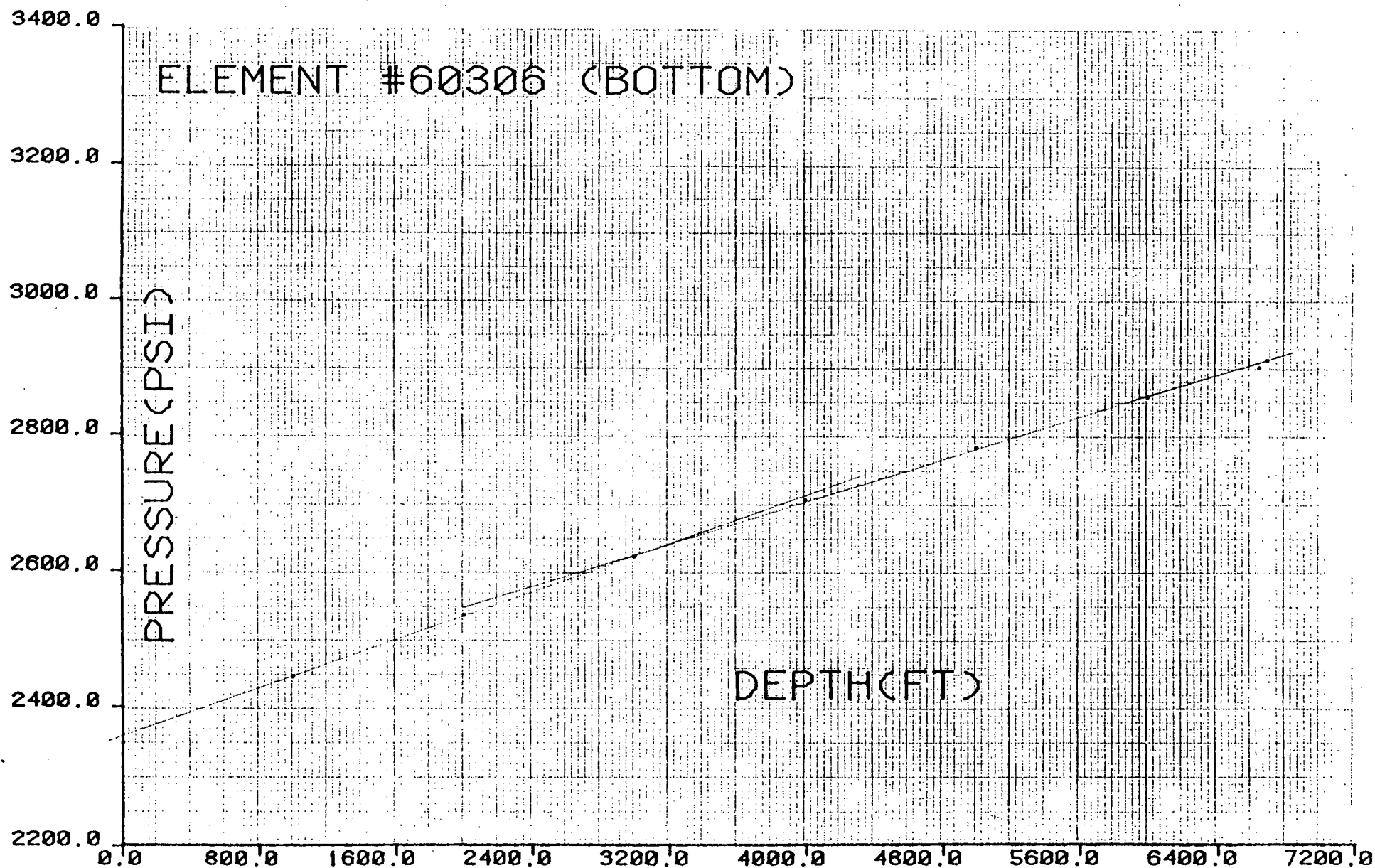
SURVEY DATA

CO. SANTOS			RUN 01 FIELD KIDMAN		WELL 01		
TIME	DEPTH	P/T	GRAD	TIME	DEPTH	P/T	GRAD
10:41	0	2355.3	0.000	11:32	5000	2791.0	.075
10:51	1000	2461.2	.106	11:43	6000	2864.2	.073
11:01	2000	2551.4	.090	12:03	6649	2906.7	.066
11:11	3000	2636.5	.085	12:09	6692	2912.0	.122
11:21	4000	2715.8	.079	0:00	0	0.0	0.000

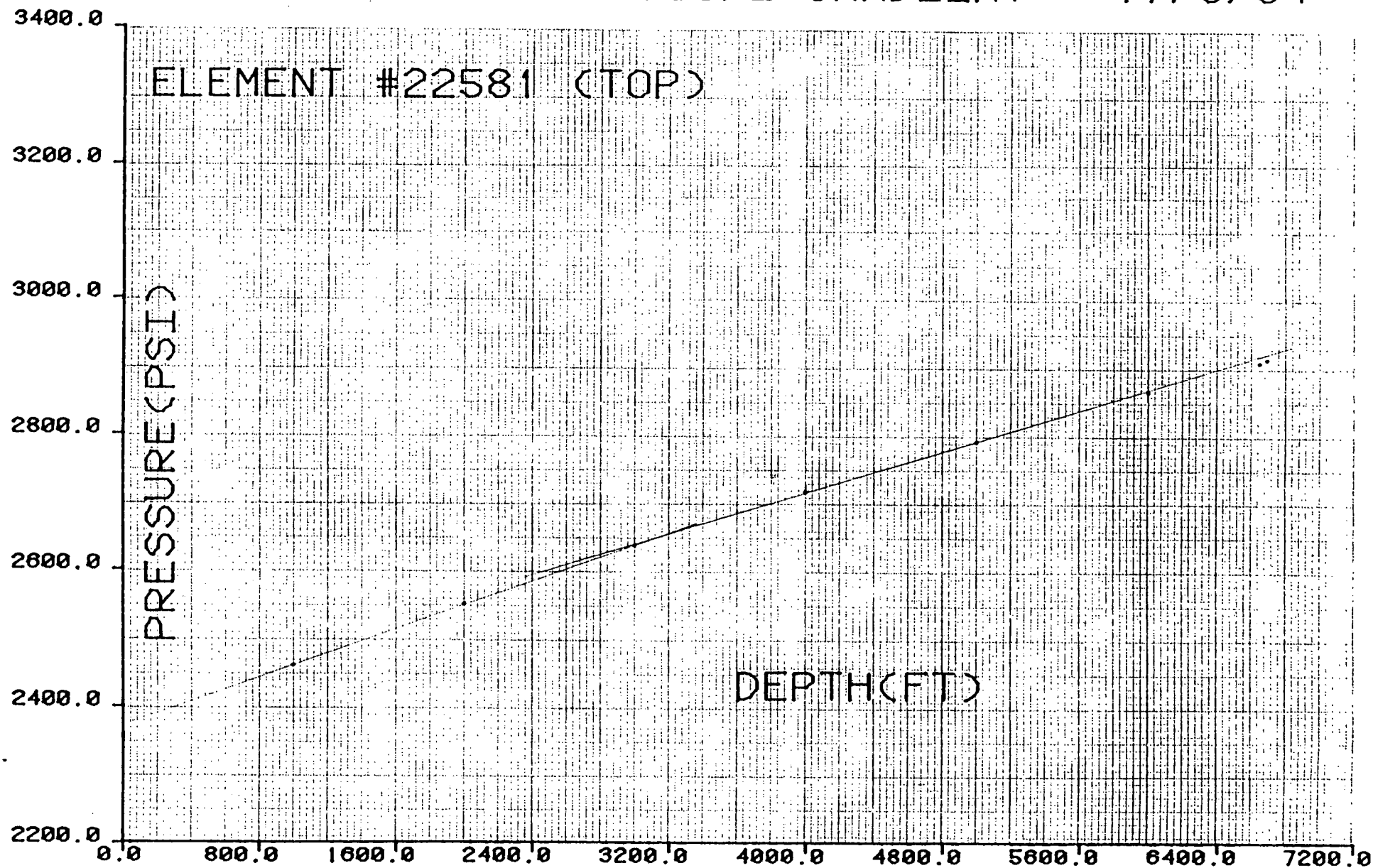
LUB IN DWT = 2345 PSIG / OUT = 2348 PSIG
LUB IN AMERADA = 2355.3 PSIG / OUT = 2364.8 PSIG

0122

KIDMAN #1 - STATIC PRESSURE GRADIENT - 17/5/84



KIDMAN #1 - STATIC PRESSURE GRADIENT - 17/5/84



ROLLING BOTTOMHOLE PRESSURE SURVEY GAS CALCULATION SHEET

WELL: Kidman # 1 Pf = 4200 kPa ✓
 ORIFICE SIZE: 76.200 mm 3.000 " ✓ T = 90 °C ✓
 LINE SIZE: 146.325 mm 5.761 " ✓ Diff = 10.5 kPa ✓

Cumulative Production to end of November = 262.596 m³ x 10⁶

Number of hours online in November = 718

Production in November = 6.724 m³ x 10⁶

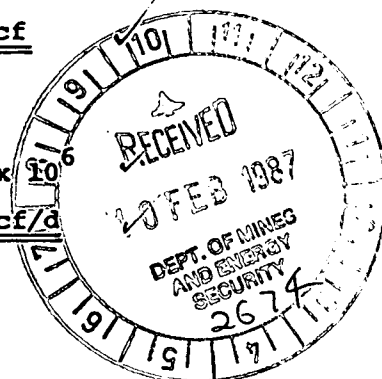
.. Average flow rate in November = (6.724 / 718) x 24 = 0.225 m³ x 10⁶ / d

Number of days online in December before Shut In 0855 hrs 16 / 12 / 86 ✓
 = 15.288 ✓

.. Production up to 0855 hrs 16 / 12 / 86 = 15.288 x 0.225 = 3.440 m³ x 10⁶ ✓

Total cumulative production = 3.440 + 262.596
 = 266.036 m³ x 10⁶
 = 9442.676 mmscf

Flow rate just prior to Shut In = 0.211 m³ x 10⁶
 = 7.503 mmscf/d



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39 GRENELL ST
ADELAIDE

SUB-SURFACE PRESSURE SURVEY

CO. SANTOS	RUN 01 FIELD KIDMAN	WELL 01
EFF DEPTH	WELL STAT	TOOL HUNG 6637'
CASING	CASING PRESS	DN BOTTOM 0615 16/12
LINER	TUBING PRESS	OFF BOTTOM 0900 19/12
DATE 861219	ELEMENT RANGE 0 - 4313	ZERO POINT
ELEVATION	ZONE	SHUT-IN 0855 16/12
MAX TEMP	PICK-UP	ON-PROD
PERF 6606'-6692'	CAL SER NO. 22420	MPP 6649'
TUBING 3-1/2"		
UNITS ENGLISH	PURPOSE BUILD-UP	

SURVEY DATA

CO. SANTOS				RUN 01 FIELD KIDMAN				WELL 01			
TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME
8:55	1136.8	0.0	0.0	10:06	1703.2	566.4	1.2				
8:59	1165.3	28.5	.1	10:29	1710.0	573.2	1.6				
9:06	1218.7	81.8	.2	11:41	1722.8	586.0	2.8				
9:17	1284.0	147.2	.4	13:18	1730.2	593.3	4.4				
9:20	1419.8	283.0	.4	15:51	1735.9	599.1	6.9				
9:24	1558.9	422.1	.5	19:44	1744.2	607.4	10.8				
9:27	1626.6	489.7	.5	2:14	1751.5	614.7	17.3				
9:29	1660.1	523.3	.6	11:43	1757.6	620.8	26.8				
9:32	1669.5	532.7	.6	20:23	1764.7	627.9	35.5				
9:35	1679.1	542.3	.7	6:00	1768.1	631.2	45.1				
9:41	1687.4	550.6	.8	17:09	1773.4	636.6	56.2				
9:50	1695.1	558.2	.9	9:00	1778.1	641.3	72.1				

LUB IN DWT = 647 PSI / OUT = 1464 PSI

LUB IN AMERADA = 637 PSI / OUT = 1464 PSI

SANTOS LTD
39 GRENELL ST
ADELAIDE

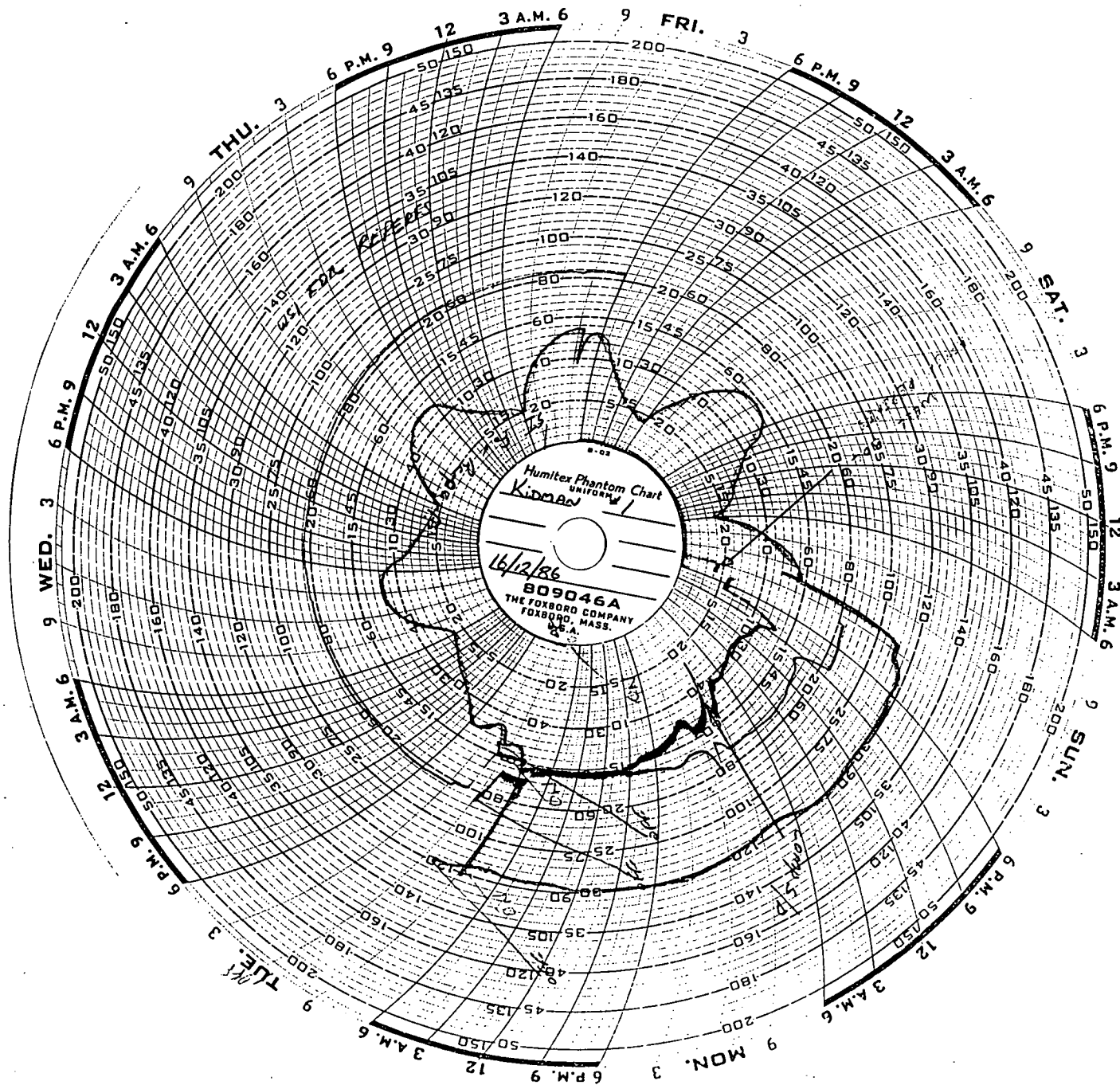
SUB-SURFACE PRESSURE SURVEY

CO. SANTOS	RUN 02 FIELD KIDMAN	WELL 01
EFF DEPTH	WELL STAT	TOOL HUNG 6643'
CASING	CASING PRESS	ON BOTTOM 0615 16/12
LINER	TUBING PRESS	OFF BOTTOM 0900 19/12
DATE 861219	ELEMENT RANGE 0 - 4013	ZERO POINT
ELEVATION	ZONE	SHUT-IN 0855 16/12
MAX TEMP	PICK-UP	ON-PROD
PERF 6606'-6692'	CAL SER NO. 29322	MPP 6649'
TUBING 3-1/2"		
UNITS ENGLISH	PURPOSE BUILD-UP	

SURVEY DATA

CO. SANTOS				RUN 02 FIELD KIDMAN				WELL 01			
TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME
8:55	1142.1	0.0	0.0	10:29	1711.1	569.0	1.6				
9:02	1194.7	52.6	.1	10:45	1713.8	571.7	1.8				
9:08	1244.8	102.7	.2	11:08	1716.9	574.8	2.2				
9:14	1288.4	146.3	.3	11:27	1720.6	578.5	2.5				
9:17	1442.7	300.6	.4	12:23	1725.5	583.4	3.5				
9:21	1590.9	448.8	.4	14:50	1733.7	591.6	5.9				
9:23	1628.8	486.7	.5	17:41	1738.9	596.8	8.8				
9:27	1659.7	517.6	.5	1:22	1748.8	606.7	16.5				
9:33	1678.5	536.4	.6	10:16	1755.7	613.6	25.4				
9:39	1686.4	544.3	.7	19:34	1761.1	619.0	34.7				
9:42	1692.4	550.3	.8	12:44	1769.2	627.1	51.8				
9:48	1696.4	554.2	.9	11:11	1773.4	631.2	64.3				
10:01	1702.1	560.0	1.1	9:00	1775.8	633.7	72.1				
10:15	1707.8	565.7	1.3	0:00	0.0	0.0	0.0				

LUB IN DWT = 647 PSI / OUT = 1464 PSI
LUB IN AMERADA = 648 PSI / OUT = 1470 PSI

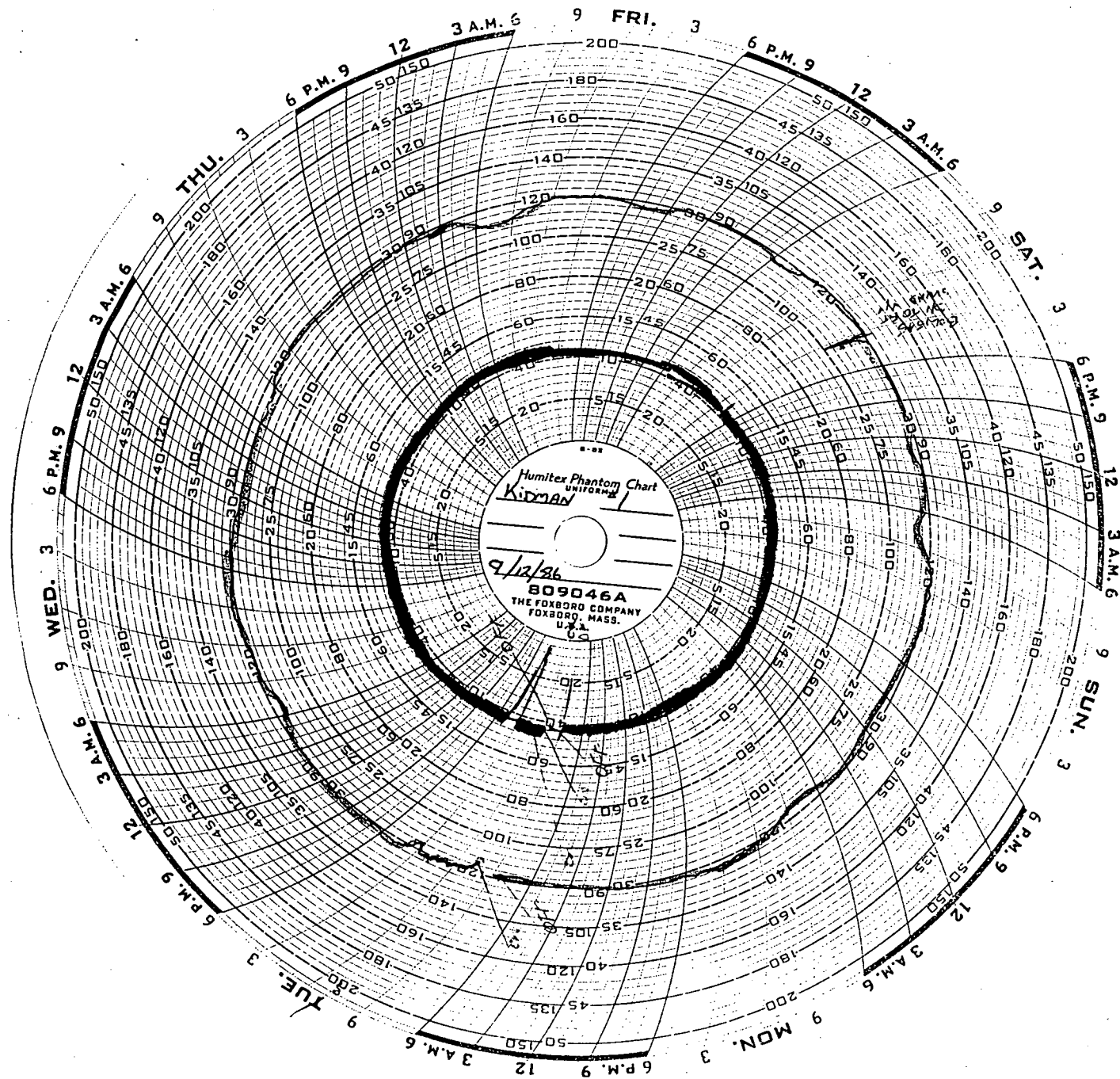


16/12/86. 0900

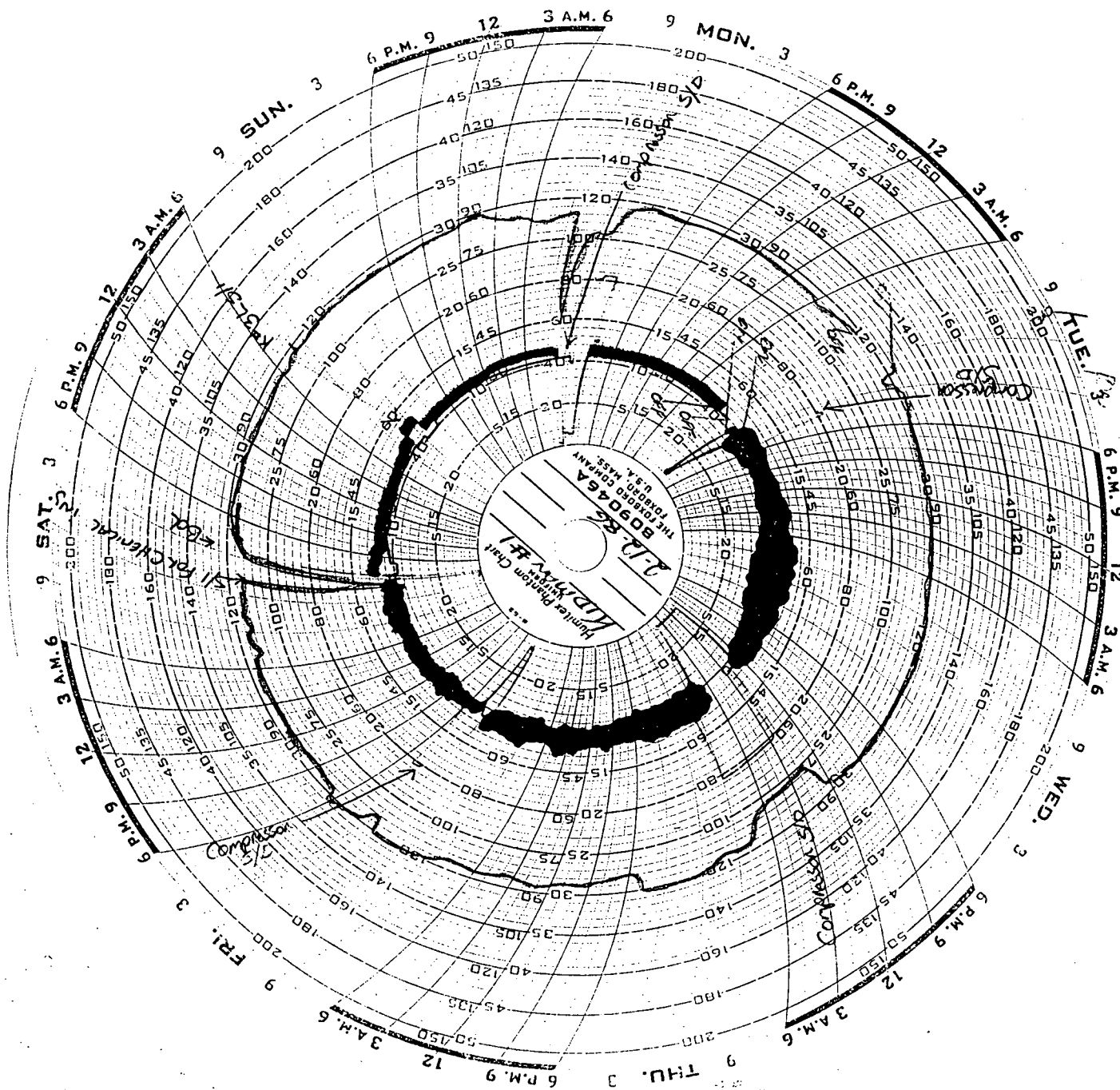
START

23/12/86 1137

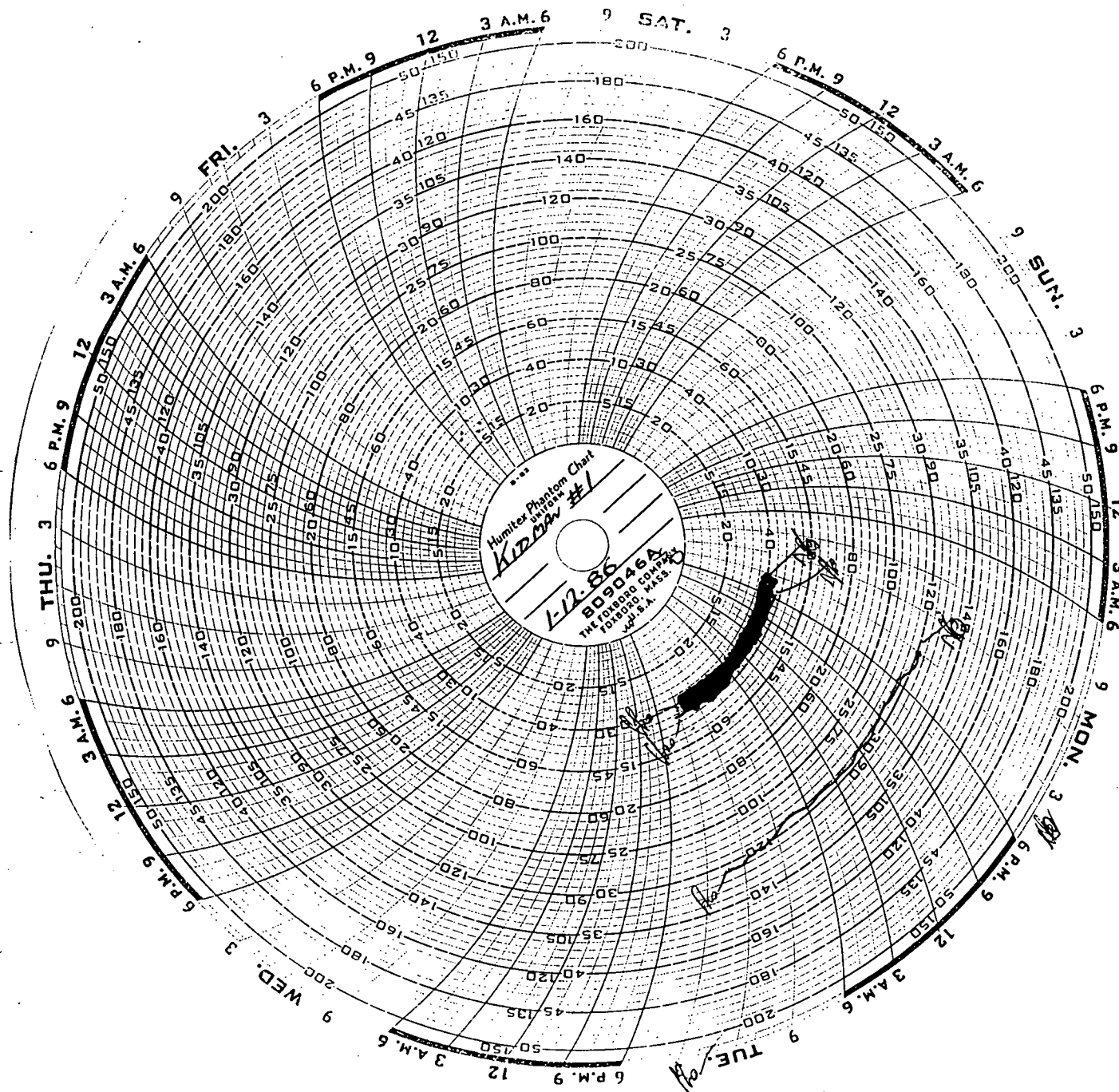
FINISH



9/12/86. 1053 STREET
16/12/86. 0900 FINISH



2/12/86 1338 START
 9/12/86 1057 FINISH



1/12/86 1515 START
2/12/86 1338 FINISH

146.30 Sannometer run diam
76200mm Orifice plate diam.

WELL: <u>K.I.D.MAN #1</u>						 SANTOS LTD. WELL TEST DATA SHEET										DATE: <u>13/12/86</u>				
TYPE OF TEST: <u>Flow & Build up</u>						PAGE No: <u>1</u>														
DATE TIME	WELLHEAD					GAS FLOW DATA					OIL/CONDENSATE PRODUCTION			WATER PRODUCTION		WELL TEST RESULTS				
	CASING PSI	TUBING PSI	TEMP. °F	CHOKE SIZE INS.	B.S.W. %	PI PSI	HW INS. H ₂ O	TEMP. °F	ORIFICE SIZE INS.	TANK DIP INS.	TANK PROD BBLs	API GRAVITY @ 60 °F	TANK DIP INS.	TANK PROD BBLs	FLOW RATE MMSCFD	FLOW RATE BBLs/ DAY	FLOW RATE BBLs/ DAY	TOTAL LIQUID FLOW RATE BBLs/ DAY	G.O.R. SCF/BBL	
13/12/86																				
1530																				
1540																				
1700																				
15/12/86																				
1700																				
1730	0	660		100%																
1745	0	657																		
1903																				
1923																				
1938	0	655																		
16/12/86																				
0415																				
0455																				
0555	0	647	176	100%																
0615																				

OPERATOR.....R. LARKIN.....

0132

[illegible]

WELL: K.I.D.MAN #1... (Toolbox)
 OPERATOR: R. LARKIN...



SANTOS LTD
 WELL TEST DATA
 METRIC SUMMARY SHEET

DATE: 16/12/86.....
 PAGE No: 2.....

DATE TIME	WELLHEAD						FLUID PRODUCTION				GAS PRODUCTION			
	CASING PSI	CASING KPA	TUBING PSI	TUBING KPA	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M3/D	FLOWRATE H2O BBL'S/D	FLOWRATE H2O M3/D	MMSCF/D	Mm3/D	G.O.R. Cu/FT BBL	G.O.R. M3/M3
0615	0	0	647	4461	176	80	START TEST.				choke	100%		
0715	0	0	647	4461	176	80								
0815	0	0	645	4447	180	82								
0845							Shut DOWN COMPRESSOR FOR REPAIRS.							
0855	0	0	910	6274	181	83	Shut IN FOR BUILD UP.							
0905	0	0	1355	9343										
0905	0	0	1400	9653										
0910	0	0	1410	9722										
0915	0	0	1414	9750										
0930	0	0	1420	9791										
0945	0	0	1423	9812										
1000	0	0	1426	9832										

CONVERSION FACTORS:

• BBL'S x 0.15899 = M³

• MMSCF x 28.174 = 10³ M³

• Cu/FT PER BBL x 0.1773 = M³/M³

• PSI x 6.895 = KPA

• °C x 9 ÷ 5 + 32 = °F

WELL: KIDMAN # 1 (Godakhe)
 OPERATOR: R. LARKIN



SANTOS LTD
 WELL TEST DATA
 METRIC SUMMARY SHEET

DATE: 16/12/86
 PAGE No: 3

DATE TIME	WELLHEAD						FLUID PRODUCTION				GAS PRODUCTION			
	CASING PSI	CASING KPA	TUBING PSI	TUBING KPA	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M3/D	FLOWRATE H2O BBL'S/D	FLOWRATE H2O M3/D	MMSCF/D	Mm3/D	G.O.R. Cu/FT BBL	G.O.R. M3/M3
1015	0	0	1420	9846										
1030	0	0	1430	9874										
1100	0	0	1430	9860										
1130	0	0	1433	9881										
1200	0	0	1435	9894										
1300	0	0	1440	9929										
1600	0	0	1446	9970										
1830	0	0	1446	9970										
2230	0	0	1448	9984										
17/12/86														
0230	0	0	1450	9998										
0630	0	0	1452	1002										

CONVERSION FACTORS:

• BBL'S x 0.15899 = M³

• MMSCF x 28.174 = 10³ M³

• Cu/FT PER BBL x 0.1773 = M³/M³

• PSI x 6.895 = KPA

• °C x 9 ÷ 5 + 32 = °F

WELL: *KIDMAN #1 (Goodrich)*
 OPERATOR: *R. LARKIN*



SANTOS LTD
WELL TEST DATA
METRIC SUMMARY SHEET

DATE: *17/12/86*
 PAGE No: *4*

DATE TIME	WELLHEAD						FLUID PRODUCTION				GAS PRODUCTION			
	CASING FSI	CASING KPA	TUBING PSI	TUBING KPA	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M3/D	FLOWRATE H2O BBL'S/D	FLOWRATE H2O M3/D	MMSCF/D	Mm3/D	G.O.R. Cu/FT BBL	G.O.R. M3/M3
<i>1030</i>	<i>0</i>	<i>0</i>	<i>1454</i>	<i>10025</i>										
<i>1430</i>	<i>0</i>	<i>0</i>	<i>1455</i>	<i>10031</i>										
<i>1830</i>	<i>0</i>	<i>0</i>	<i>1455</i>	<i>10031</i>										
<i>2030</i>	<i>0</i>	<i>0</i>	<i>1455</i>	<i>10031</i>										
<i>15/12</i>														
<i>0230</i>	<i>0</i>	<i>0</i>	<i>1455</i>	<i>10031</i>										
<i>0630</i>	<i>0</i>	<i>0</i>	<i>1459</i>	<i>10059</i>										
<i>1030</i>	<i>0</i>	<i>0</i>	<i>1460</i>	<i>10065</i>										
<i>1430</i>	<i>0</i>	<i>0</i>			<i>UNAVAILABLE</i>		<i>In</i>	<i>100038</i>						
<i>1830</i>	<i>0</i>	<i>0</i>	<i>1462</i>	<i>10079</i>										
<i>2230</i>	<i>0</i>	<i>0</i>	<i>1462</i>	<i>10079</i>										
<i>17/12</i>														

CONVERSION FACTORS:

• BBL'S. x 0.15899 = M³

• MMSCF x 28.174 = 10³ M³

• Cu/FT PER BBL x 0.1773 = M³/M³

• PSI x 6.895 = KPA

• °C x 9 ÷ 5 + 32 = °F

WELL: KIDMAN 1 (TOWERS)
 OPERATOR: A. Gillies



SANTOS LTD
WELL TEST DATA
METRIC SUMMARY SHEET

DATE: 19/12/96
 PAGE No: 5

DATE TIME	WELLHEAD						FLUID PRODUCTION				GAS PRODUCTION			
	CASING PSI	CASING KPA	TUBING PSI	TUBING KPA	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M3/D	FLOWRATE H2O BBL'S/D	FLOWRATE H2O M3/D	MMSCF/D	Mm3/D	G.O.R. Cu/FT BBL	G.O.R. M3/M3
19/12														
0230	0	0	1463	10086										
0630	0	0	1464	10093										
0700	0	0	1464	10093			P.O.H.							
1136	0	0	1464	10093			DE-PRESSURE	LUB	CHART'S	GOOD.				
1350							R.I.H.	STATIC	GRADIENT		2 x 4000 PSI		ELEMENT'S	
1451							ON	BOTTOM						
1456							P.O.H.							
1540	0	0	1465	10100			DE-PRESSURE	LUB	CHART'S	GOOD				
							RIG	DOWN	HAND	WELL	OVER	TO	PRODUCTION	

CONVERSION FACTORS:

• BBL'S. x 0.15899 = M³

• MMSCF x 28.174 = 10³ M³

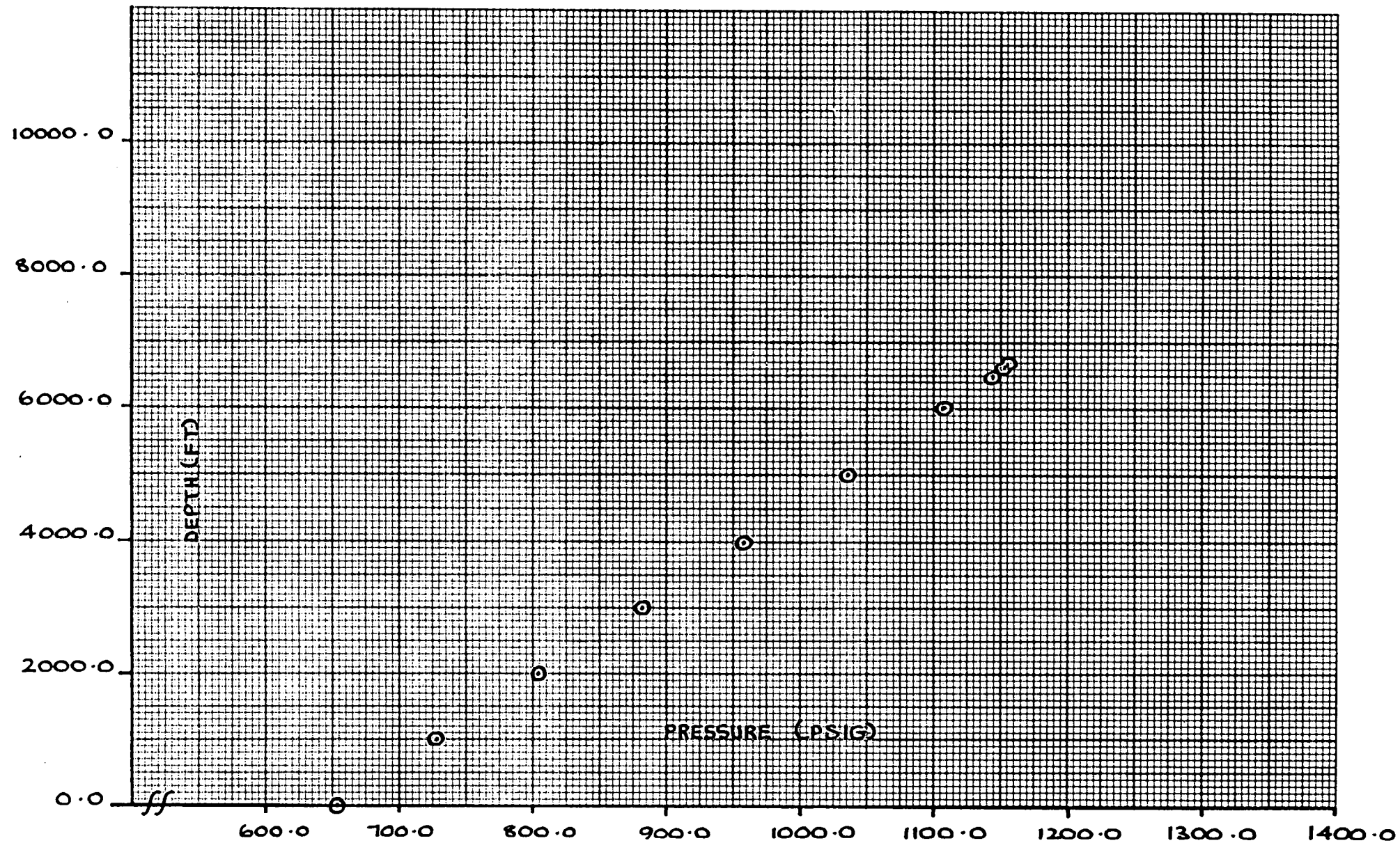
• Cu/FT PER BBL x 0.1773 = M³/M³

• PSI x 6.895 = KPA

• °C x 9 ÷ 5 + 32 = °F

KIDMAN # 1 - FLOWING PRESSURE GRADIENT - 15/12/86

ELEMENT # 29322/3950 (BOT)





**** KIDMAN 1 ****

FLOWING PRESSURE GRADIENT

TEST DATE: 15/12/86

DEPTH (FT.)	TOP PRESSURE ELEMENT 22420/4250			BOTTOM PRESSURE ELEMENT 29322/3950		
	DEFLECTION (INCHES)	PRESSURE (PSIG)	GRADIENT (PSI/FT)	DEFLECTION (INCHES)	PRESSURE (PSIG)	GRADIENT (PSI/FT)
LUB	0.3070	642.2	----	0.3270	653.0	----
1000	0.3410	714.6	0.0724	0.3650	728.7	0.0757
2000	0.3790	795.6	0.0810	0.4030	804.4	0.0757
3000	0.4150	872.3	0.0767	0.4420	882.1	0.0777
4000	0.4520	951.2	0.0789	0.4800	957.9	0.0757
5000	0.4880	1028.0	0.0768	0.5190	1035.6	0.0777
6000	0.5230	1102.8	0.0747	0.5550	1107.3	0.0717
6500	0.5410	1141.2	0.0769	0.5740	1145.2	0.0757
6649	0.5460	1151.9	0.0717	0.5780	1153.2	0.0535
6692	0.5460	1151.9	0.0000	0.5790	1155.2	0.0464
LUB	0.3090	646.4	----	0.3280	655.0	----

GENERAL REMARKS:

TEMP. ELEMENT 63256/150 F TO 400 F. REC. 61275/15 TLS. CLOCK 14053/3 HR

DWT IN: 657
 DWT OUT: 655
 MAX BHT: RAN TEMP. ELEMENT
 199.6°F

ELEMENT 22420/4250 CALIBRATED 30.11.86
 ELEMENT 29322/3950 CALIBRATED 30.11.86

WELL NAME: KIDMAN #1

Flowing

STATIC GRADIENT SURVEY

DATE:

DATE: 15/12/86

BOMB No. 1 DATA

ELEMENT No. 22420 ELEMENT RANGE: 4250

RECORDED No. 54651 CLOCK DATA: 16081 x 3Hr

ENGAGE STYLUS: 1723 DISENGAGE:

BOMB No. 2 DATA

ELEMENT No: 29322 ELEMENT RANGE: 3950..

RECORDED No. 14632... CLOCK DATA: 16086+34+

ENGAGE STYLUS: 17.23 DISENGAGE:

LUBRICATOR DATA

PRESSURE WITH D.W.T.: 657 PSI

TIME PRESSURED: 17:30

TIME DEPRESSURED: 19:38

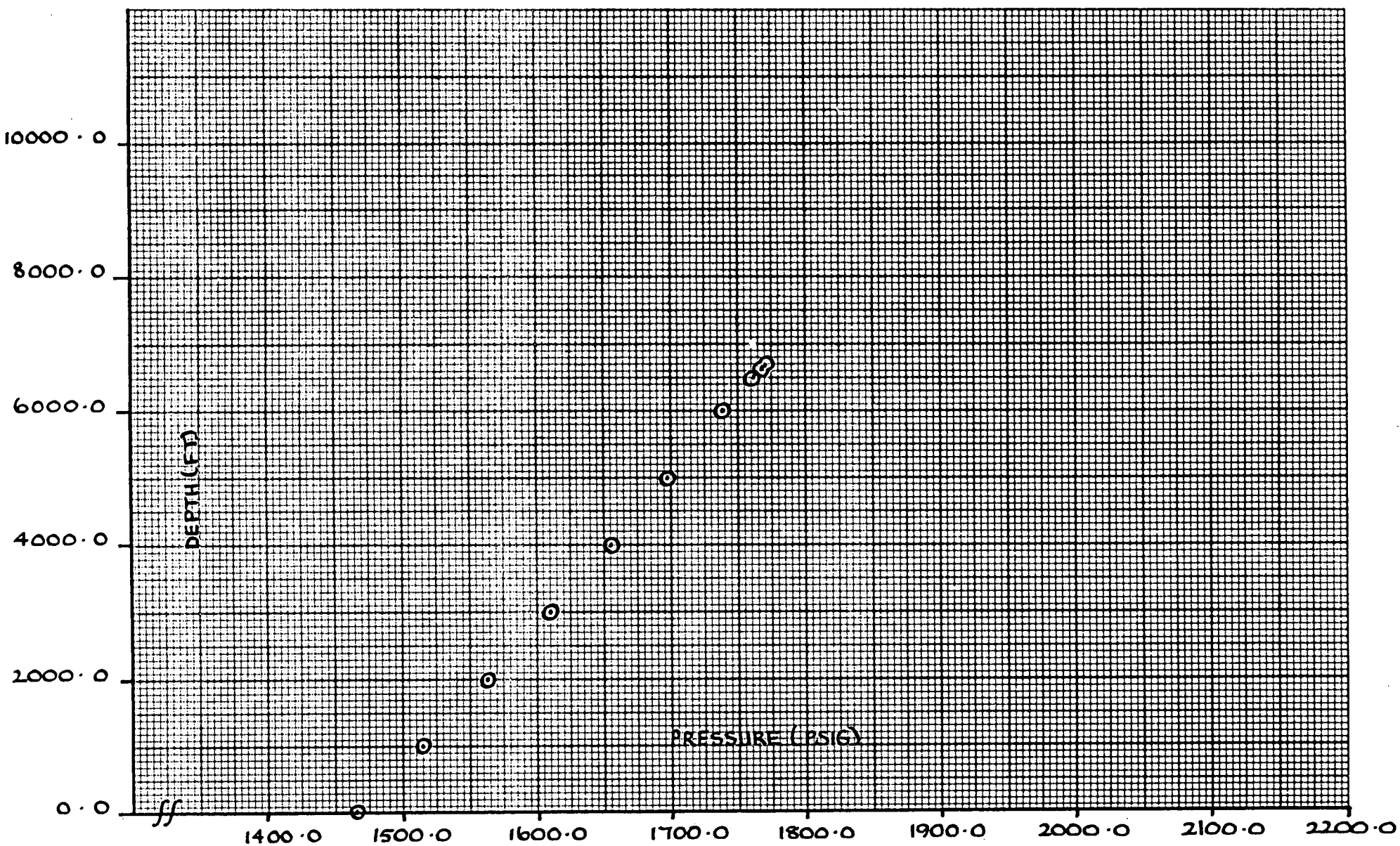
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General Comments:

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KIDMAN # 1 - STATIC PRESSURE GRADIENT - 19 / 12 / 86

ELEMENT # 29322 / 3950 (BOT)



0141



**** KIDMAN 1 # ****

STATIC PRESSURE GRADIENT

TEST DATE: 19-12-86

DEPTH (FT.)	TOP PRESSURE ELEMENT 22420/4250			BOTTOM PRESSURE ELEMENT 29322/3950		
	DEFLECTION (INCHES)	PRESSURE (PSIG)	GRADIENT (PSI/FT)	DEFLECTION (INCHES)	PRESSURE (PSIG)	GRADIENT (PSI/FT)
LUB	0.6873	1454.3	----	0.7350	1466.3	----
1000	0.7110	1505.1	0.0508	0.7595	1515.2	0.0489
2000	0.7336	1553.5	0.0485	0.7838	1563.6	0.0484
3000	0.7558	1601.2	0.0476	0.8070	1610.0	0.0464
4000	0.7775	1647.8	0.0466	0.8295	1655.0	0.0449
5000	0.7988	1693.5	0.0458	0.8505	1696.9	0.0420
6000	0.8200	1739.1	0.0456	0.8720	1739.9	0.0430
6500	0.8305	1761.7	0.0452	0.8830	1761.9	0.0440
6649	0.8343	1769.9	0.0549	0.8865	1768.9	0.0470
6692	0.8373	1776.3	0.1501	0.8905	1776.9	0.1860
LUB	0.6898	1459.6	----	0.7370	1470.3	----

GENERAL REMARKS:

NIL

DWT IN: 1468

DWT OUT: 1465

MAX BHT: TEMP NOT AVAILABLE CLOCK U/S

ELEMENT 22420/4250 CALIBRATED 30.11.86

ELEMENT 29322/3950 CALIBRATED 30.11.86

WELL NAME:

KIDMAN #1

STATIC GRADIENT SURVEY

DATE:

19/12/86

BOMB No. 1 DATA

ELEMENT No. 22420 ELEMENT RANGE: 4250
 RECORDER No. 54651 XISTV CLOCK DATA: 16081 x 342
 ENGAGE SYLUS: 1328 DISENGAGE: 15.47

BOMB No. 2 DATA

ELEMENT No. 29322 ELEMENT RANGE: 3950
 RECORDER No. 14632 CLOCK DATA: 14053 x 342
 ENGAGE SYLUS: DISENGAGE: 15.47

LUBRICATOR DATA

PRESSURE WITH D.W.T. IN 1468 OUT 1465
 TIME PRESSURED: 1340
 TIME DEPRESSURED: 1540

DATE	TIME	DEPTH	DEFLECTION	PRESSURE TEMP.	GRADIENT ps/VL	DEPTH	DEFLECTION	PRESSURE TEMP.	GRADIENT ps/VL	REMARKS
17/12/86	1340	LUB	.6873				.735			
	1350	R.T.H								DID NOT RUN TEMP ELEMENT CLOCK U/S.
	1355	1000	.711				.7595			
	1404	2000	.7336				.78375			
	1412	3000	.7558				.807			
	1421	4000	.7775				.8295			
	1429	5000	.7988				.8505			
	1437	6000	.820				.872			
	1444	6500	.8305				.883			
	1450	6649	.8343				.8865			
	1501	6692	.8373				.8905			
	1506	P.O.H								
	1530	IN LUB.	.6898				.737			
	1540	DE-PRESS								

General Comments:

0143

ROLLING BOTTOMHOLE PRESSURE SURVEY GAS CALCULATION SHEET

WELL: Kidmgn # 1 Pf = 5000 kPa
 ORIFICE SIZE: 76.200 mm 3.000 " / T = 90 °C
 LINE SIZE: 146.329 mm 5.761 " ✓ Diff = 29.7 kPa

Cumulative Production to end of April = $313.295 \text{ m}^3 \times 10^6$

Number of hours online in April = 673

Production in April = $11.355 \text{ m}^3 \times 10^6$

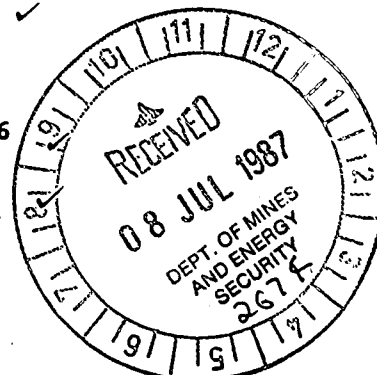
.. Average flow rate in April = $(11.355 / 673) \times 24 = 0.405 \text{ m}^3 \times 10^6 / \text{d}$

Number of days online in May before Shut In 1600 hrs 12 / 5 / 87
 = 11.667

.. Production up to 1600 hrs 12 / 5 / 87 = $0.405 \times 11.667 = 4.725 \text{ m}^3 \times 10^6$

Total cumulative production = $313.295 + 4.725$
 = $318.020 \text{ m}^3 \times 10^6$
 = 11287.802 mmscf ✓

Flow rate just prior to Shut In = $0.389 \text{ m}^3 \times 10^6$
 = 13.806 mmscf/d



SANTOS LTD
39 GRENFELL ST
ADELAIDE

SUB-SURFACE PRESSURE SURVEY

CO. SANTOS	RUN 02 FIELD KIDMAN	WELL 01
EFF DEPTH	WELL STAT	TOOL HUNG 6564'
CASING	CASING PRESS	ON BOTTOM 0955 12/5
LINER	TUBING PRESS	OFF BOTTOM 0800 16/5
DATE 870511	ELEMENT RANGE 0 - 4165	ZERO POINT
ELEVATION	ZONE	SHUT-IN 1600 12/5
MAX TEMP	PICK-UP	ON-PROD
PERF 6606'-6692'	CAL SER NO. 22410	MPP 6649'
TUBING 3-1/2"		
UNITS ENGLISH	PURPOSE BUILD-UP	

SURVEY DATA

CO. SANTOS				RUN 02 FIELD KIDMAN				WELL 01			
TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME				
16:00	1654.3	0.0	0.0	17:11	2160.9	506.6	1.2				
16:00	1704.3	50.0	0.0	17:37	2164.5	510.2	1.6				
16:02	1792.5	138.2	.0	18:22	2169.4	515.1	2.4				
16:04	1930.3	276.0	.1	19:07	2173.9	519.6	3.1				
16:07	2050.4	396.1	.1	20:44	2179.6	525.3	4.7				
16:08	2090.1	435.7	.1	22:53	2189.0	534.7	6.9				
16:09	2109.4	455.1	.2	1:29	2196.5	542.2	9.5				
16:11	2123.9	469.6	.2	3:53	2202.6	548.3	11.9				
16:14	2132.8	478.5	.2	10:33	2213.9	559.6	18.5				
16:17	2139.9	485.6	.3	20:29	2226.0	571.7	28.5				
16:20	2144.0	489.7	.3	8:30	2235.9	581.6	40.5				
16:26	2148.3	494.0	.4	21:38	2243.0	588.7	53.6				
16:33	2151.1	496.8	.6	10:22	2251.4	597.1	66.4				
16:43	2153.3	499.0	.7	1:29	2260.9	606.6	81.5				
16:56	2157.1	502.8	.9	8:00	2263.5	609.2	88.0				

LUB IN DWT = 776 PSI / OUT = 1897 PSI.

LUB IN AMERADA = 764 PSI / OUT = 1897 PSI

SANTOS LTD
39 GRENFELL ST
ADELAIDE

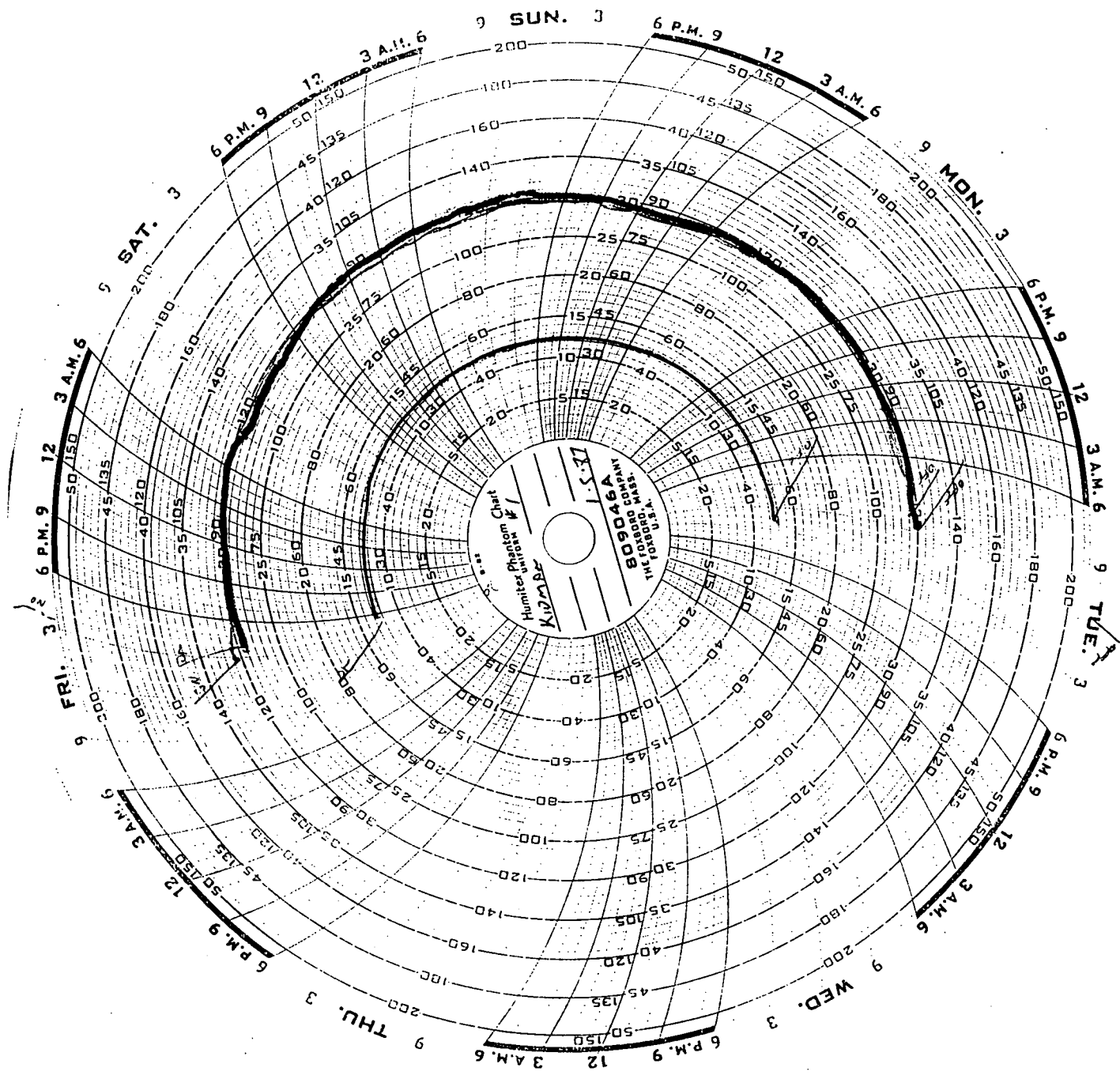
SUB-SURFACE PRESSURE SURVEY

CO. SANTOS	RUN 01 FIELD KIDMAN	WELL 01
EFF DEPTH	WELL STAT	TOOL HUNG 6558'
CASING	CASING PRESS	ON BOTTOM 0955 12/5
LINER	TUBING PRESS	OFF BOTTOM 0800 16/5
DATE 870511	ELEMENT RANGE 0 - 4107	ZERO POINT
ELEVATION	ZONE	SHUT-IN 1600 12/5
MAX TEMP	PICK-UP	ON-PROD
PERF 6606' - 6692'	CAL SER NO. 21374	MPP 6649'
TUBING 3-1/2"		
UNITS ENGLISH	PURPOSE BUILD-UP	

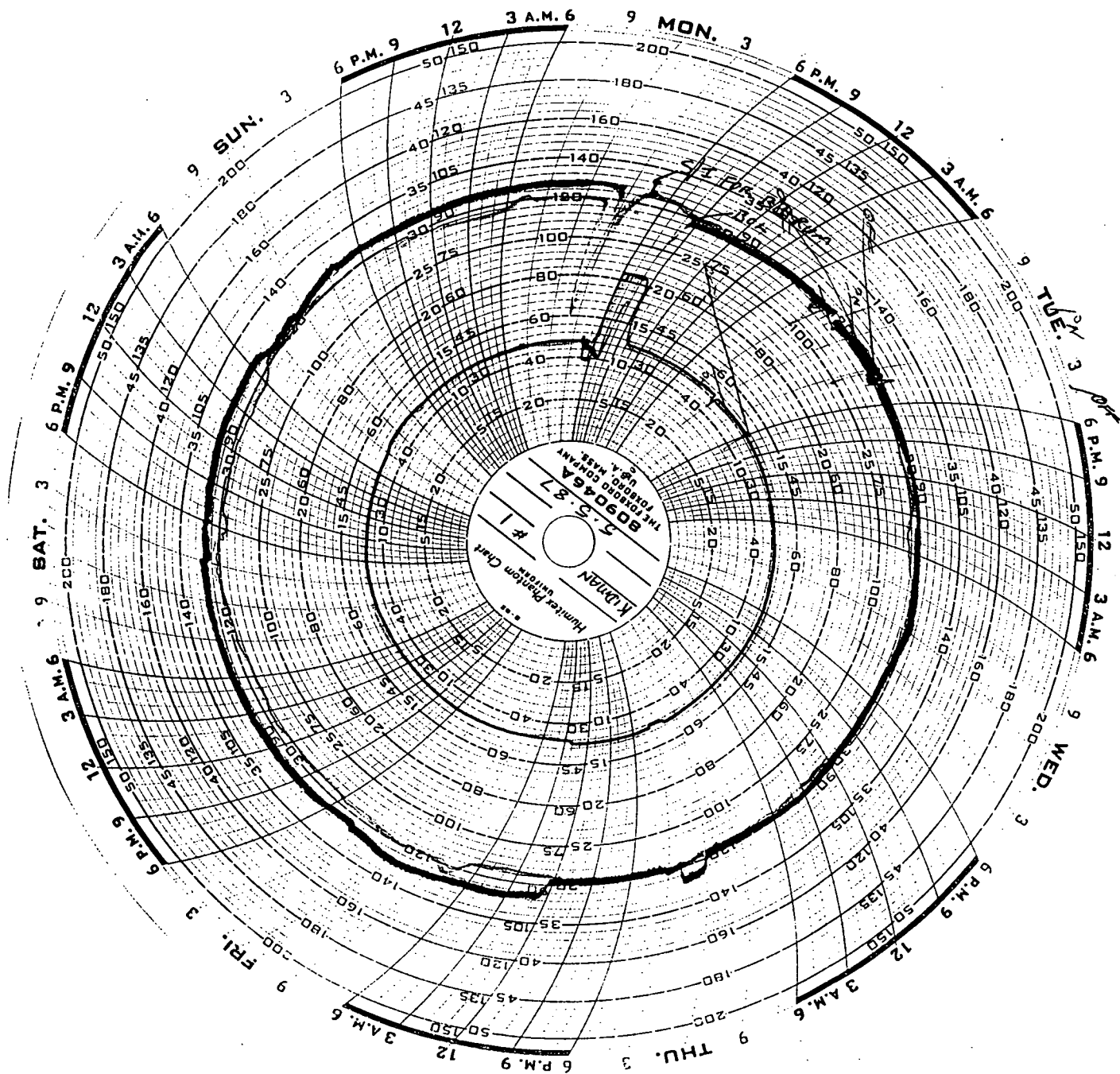
SURVEY DATA

CO. SANTOS				RUN 01 FIELD KIDMAN				WELL 01			
TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME
16:00	1647.3	0.0	0.0	17:31	2155.5	508.1	1.5				
16:02	1731.3	84.0	.0	18:02	2159.9	512.5	2.0				
16:02	1839.9	192.5	.0	18:38	2162.8	515.5	2.6				
16:04	1981.2	333.9	.1	19:31	2168.4	521.0	3.5				
16:07	2070.5	423.2	.1	20:41	2172.6	525.3	4.7				
16:07	2087.6	440.3	.1	22:22	2178.0	530.6	6.4				
16:08	2103.7	456.4	.1	0:22	2186.5	539.2	8.4				
16:11	2117.9	470.6	.2	4:14	2197.1	549.8	12.2				
16:14	2125.9	478.6	.2	11:43	2211.4	564.0	19.7				
16:16	2131.5	484.1	.3	23:20	2225.6	578.3	31.3				
16:20	2137.2	489.9	.3	12:48	2236.9	589.6	44.8				
16:27	2141.5	494.2	.4	21:35	2244.6	597.3	53.6				
16:37	2144.8	497.4	.6	8:28	2251.4	604.1	64.5				
16:50	2148.4	501.1	.8	23:19	2257.4	610.1	79.3				
17:06	2152.1	504.7	1.1	8:00	2261.2	613.9	88.0				

LUB IN DWT = 776 PSI / OUT = 1897 PSI
LUB IN AMERADA = 759 PSI / OUT = 1897 PSI

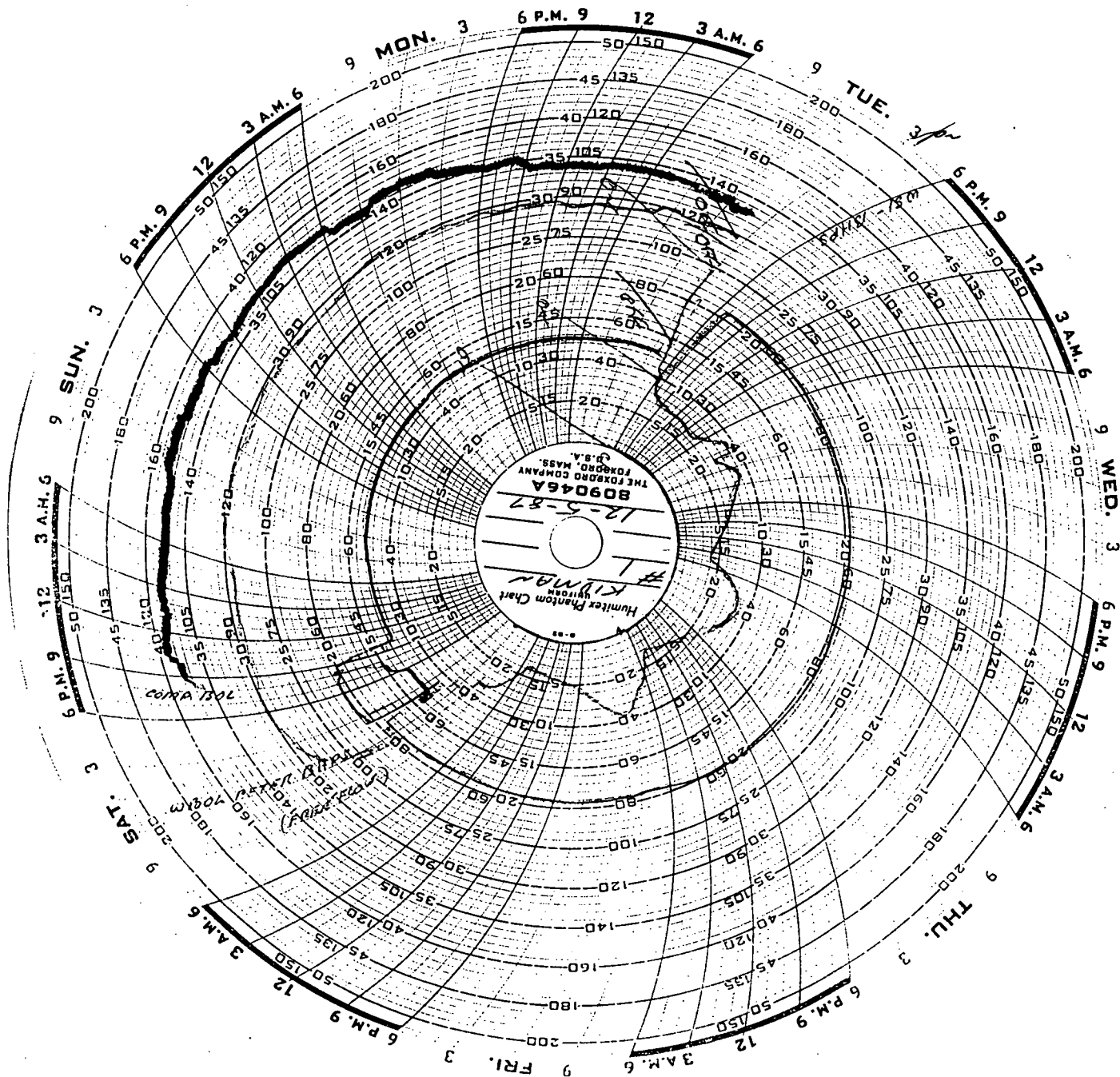


1-5-87. 1530 hrs.
 5-5-87. 1130hrs
 meter mm diam 146.329
 Office plate " 76.200



5.5.87
12.5.87

1130 hrs
1530 hrs



12-5-87

19-5-87

1530 L3

1600 L3



0150

Well: KIDMAN # 1 Date: 12-5-87

Lubricator Data: ① 759 1897 Operator M. SAUNDERS
② 764 1897

Pressure with D.W.T. In 776 psi Out 1897 psi

Time Pressured 0822 Time Depressed 0924

Time Run in Hole 0922 Time off Bottom 0800

Bomb No. 1 Data

Bomb No. 2 Data

Element No. and Range	<u>21374 x 4075</u>	<u>22410 x 4100</u>
Recorder No.	<u>14625</u>	<u>14627</u>
Clock and Lead Screw Data	<u>F-15683 x 120hr 15 Tls</u>	<u>F-15692 x 120hr 15 Tls</u>
Engage Stylus	Date: <u>12-5-87</u> Time: <u>0809</u>	Date: <u>12-5-87</u> Time: <u>0809</u>
Disengage	Date: <u>16-5-87</u> Time: <u>0933</u>	Date: <u>16-5-87</u> Time: <u>0933</u>

Remarks: TEMP ELEMENT N°; 63257 x 150-400° F
REC. N°; 59253
CLOCK N°; F-15693 x 120 hr

Well-Head Data for Final Build-up

Date	Time	Hours shut-in Time	Wellhead P.S.I.G.	Casing P.S.I.G.	Wellhead Temp. °F	Remarks
<u>12-5-87</u>						
	<u>0922</u>	<u>RUN</u>	<u>IN HOLE</u>			
			<u>776</u>	<u>0</u>	<u>183</u>	
	<u>0955</u>	<u>HANG</u>	<u>BOMBS</u>	<u>AT 6570' KB</u>		
	<u>1030</u>		<u>776</u>	<u>0</u>	<u>183</u>	
	<u>1100</u>		<u>777</u>		<u>183</u>	
	<u>1130</u>		<u>776</u>		<u>181</u>	
	<u>1200</u>		<u>777</u>		<u>183</u>	
	<u>1230</u>		<u>777</u>		<u>183</u>	
	<u>1300</u>		<u>777</u>		<u>185</u>	
	<u>1330</u>		<u>778</u>		<u>187</u>	
	<u>1400</u>		<u>780</u>		<u>188</u>	
	<u>1430</u>		<u>780</u>		<u>190</u>	
	<u>1500</u>		<u>780</u>		<u>190</u>	
	<u>1530</u>		<u>786</u>		<u>188</u>	
	<u>1600</u>		<u>786</u>		<u>188</u>	
		<u>SHUT WELL IN</u>				
	<u>1615</u>		<u>1824</u>	<u>0</u>	<u>164</u>	
	<u>1630</u>		<u>1827</u>		<u>149</u>	
	<u>1645</u>		<u>1829</u>		<u>136</u>	
	<u>1700</u>	<u>1</u>	<u>1830</u>		<u>127</u>	
	<u>1715</u>		<u>1831</u>		<u>120</u>	
	<u>1730</u>		<u>1831</u>		<u>116</u>	
	<u>1745</u>		<u>1831</u>		<u>114</u>	

Well: KIDMAN #1 Date: 12-5-87

Lubricator Data: Operator M. SAUNDERS

Pressure with D.W.T. In 776 psi Out 1897 psi

Time Pressured 0822 Time Depressed 0924

Time Run in Hole 0922 Time off Bottom 0800

Bomb No. 1 Data

Bomb No. 2 Data

Element No. and Range	<u>21374 x 4075 psi</u>	<u>22410 x 4100 psi</u>
Recorder No.	<u>14625</u>	<u>14627</u>
Clock and Lead Screw Data	<u>F-15683 x 120hr 15 TLS</u>	<u>F-15692 x 120hr 15 TLS</u>
Engage Stylus	Date: <u>12-5-87</u> Time: <u>0809</u>	Date: <u>12-5-87</u> Time: <u>0809</u>
Disengage	Date: <u>16-5-87</u> Time: <u>0933</u>	Date: <u>16-5-87</u> Time: <u>0933</u>

Remarks: Temp ELEMENT N°; 63257 x 150-400°K
REC N°; 59253
CLOCK N°; F-15693 x 120hr 15 TLS

Well-Head Data for Final Build-up

Date	Time	Hours shut-in Time	Wellhead P.S.I.G.	Casing P.S.I.G.	Wellhead Temp.	Remarks
12-5-87						
	1800	2	1831	0	113	
	1815		1832		109	
	1830		1835		106	
	1845		1836		102	
	1900	3	1837		98	
	1915		1838		95	
	1930		1838		93	
	1945		1838		90	
	2000	4	1838		88	
13-5-87						
	0000	8	1847	0	75	
	0400	12	1855		72	
	0800	16	1861		72	
	1200	20	1865		59	
	1600	24	1870			
	2000	28	1873			
14-5-87						
	0000	32	1875			
	0400	36	1876			
	0800	40	1879			
	1200	44	1881		72	
	1600	48	1883		79	
	2000	52	1883		66	



**** KIDMAN 1 ****

STATIC PRESSURE GRADIENT

TEST DATE: 16.5.87

TOP PRESSURE ELEMENT 21374/4075				BOTTOM PRESSURE ELEMENT 22410/4100		
DEPTH (FT.)	DEFLECTION (INCHES)	PRESSURE (PSIG)	GRADIENT (PSI/FT)	DEFLECTION (INCHES)	PRESSURE (PSIG)	GRADIENT (PSI/FT)
LUB	0.9283	1883.3	----	0.9188	1883.8	----
1000	0.9597	1947.8	0.0645	0.9492	1946.9	0.0632
2000	0.9888	2007.5	0.0598	0.9775	2005.8	0.0589
3000	1.0172	2065.9	0.0584	1.0053	2063.7	0.0579
4000	1.0442	2121.4	0.0555	1.0322	2119.7	0.0560
5000	1.0698	2174.1	0.0527	1.0573	2172.0	0.0523
6000	1.0952	2226.3	0.0523	1.0818	2223.1	0.0511
6500	1.1077	2252.1	0.0515	1.0945	2249.6	0.0530
6649	1.1125	2262.0	0.0663	1.0993	2259.6	0.0672
6692	1.1138	2264.6	0.0622	1.1002	2261.5	0.0437
LUB	0.9330	1893.0	----	0.9218	1890.0	----

GENERAL REMARKS:

DWT IN: 1897

DWT OUT: 1897

MAX BHT: TEMP ELEMENT No 63257 ALSO RUN.

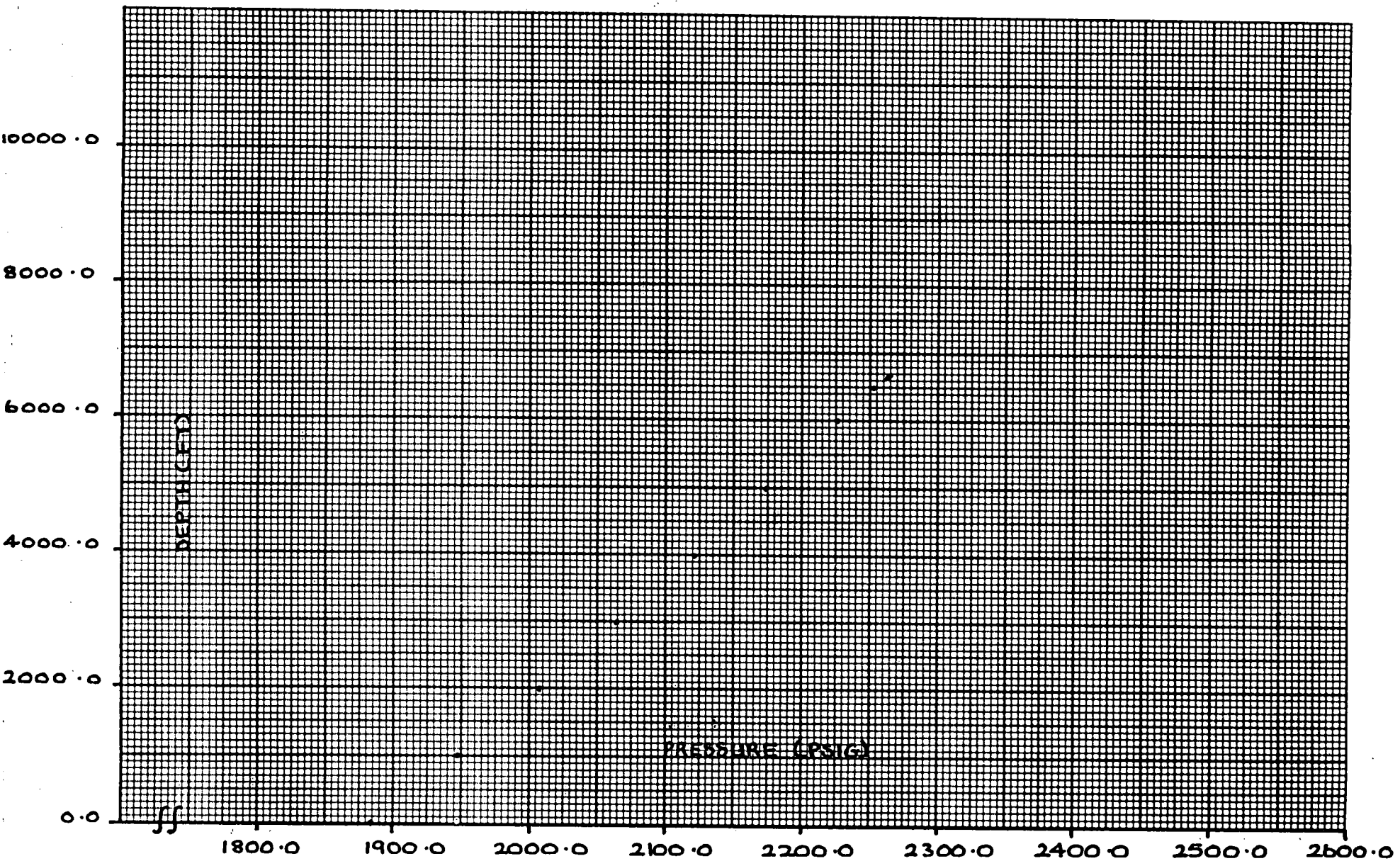
259°F

ELEMENT 21374/4075 CALIBRATED 12.3.87

ELEMENT 22410/4100 CALIBRATED 12.3.87

KIDMAN # 1 - STATIC PRESSURE GRADIENT - 16/5/87

ELEMENT # 21374 / 4075 (TOP)



WIRELINE REPORT

CLIENT Santos P.E. WELL Kidman #1

DATE 11th May 1981

PROGRAMME Blind box run flow build up and static gradient

PURPOSE OF WORK To check tubing is clear and tag P.B.T.D.

REPORT OF WORK PERFORMED 11.5.81 1330 Arrive on location rig up

1430 Shut well in pressure test OK

1450 Run in hole with 1.75" blind box tag P.B.T.D. 27070' KB

1510 Pull out of hole

1550 Bleed lubricator well back on line

12.5.81 0822 Pressure lubricator with 2 pressure elements
1x temperature element

0922 Run in hole to 6570' KB, shut well in on choke to
go through nipples

16.5.81 0800 Pull out of hole

0824 Arrive in lubricator

0924 Bleed lubricator - 3 good charts

0955 Pressure lubricator with 2 pressure 1x temperature
elements - run static gradient as per programme

1200 Bleed lubricator - 3 good charts, rig down

Secure well

1220 Hand well back to production

[Signature]
Operator's Signature

WORKED PERFORMED BY M. Saunders OF Expertest

WELL DATA:

Tubing Size 3 1/2" EVE FWHP 778 PSI SIWHP 1877 PSI

Subsurface S.V./Landing Nipple @ S.S.D. @

'X' Nipple @ 'N'/'XN' Nipple @ Other @

Min. I.D. @ Packer @

Perforated Interval:

WELL: ...KIDMAN # 1

OPERATOR: ...M. SAUNDERS...



SANTOS LTD WELL TEST DATA

METRIC SUMMARY SHEET

DATE: ...13-5-87...

PAGE No: ...4...

DATE TIME	WELLHEAD							FLUID PRODUCTION				GAS PRODUCTION			
	CASING PSI	CASING KPA	TUBING PSI	TUBING KPA	CHOKE SIZE INS.	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M3/D	FLOWRATE H2O BBL'S/D	FLOWRATE H2O M3/D	MMSCF/D	Mm3/D	G.O.R. Cu/FT BBL	G.O.R. M3/M3
1600	0	0	1870	12893	-										
2000			1873	12914											
14-5-87 0000			1875	12928											
0400			1876	12935											
0800			1879	12955											
1200			1881	12969		72	22								
1600			1883	12983		79	26								
2000			1883	12983		66	19								
15-5-87 0000			1884	12990		59	15								
0400			1884	12990		58	14.5								
0800			1885	12997		57	14								
1200			1890	13031		77	25								0157

CONVERSION FACTORS:

$$\bullet \text{BBL'S} \times 0.15899 = \text{M}^3$$

$$\bullet \text{MMSCF} \times 28.174 = 10^3 \text{M}^3$$

$$\bullet \text{Cu/FT PER BBL} \times 0.1773 = \text{M}^3/\text{M}^3$$

$$\bullet \text{PSI} \times 6.895 = \text{KPA}$$

$$\bullet ^\circ\text{C} \times 9 \div 5 + 32 = ^\circ\text{F}$$

WELL: ... KIDMAN # 1 ...
 OPERATOR: ... M. SAUNDERS ...



SANTOS LTD
 WELL TEST DATA
 METRIC SUMMARY SHEET

DATE: ... 12-5-87 ...
 PAGE No: ... 1 ...

DATE TIME	WELLHEAD							FLUID PRODUCTION				GAS PRODUCTION			
	CASING PSI	CASING KPA	TUBING PSI	TUBING KPA	CHOKE SIZE INS.	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M3/D	FLOWRATE H2O BBL'S/D	FLOWRATE H2O M3/D	MMSCF/D	Mm3/D	G.O.R. Cu/FT BBL	G.O.R. M3/M3
12-5-87															
0922	0	0	776	5350	100%	183	84	RUN IN HOLE							
0955			HANG		Bottoms		AT	6570' KB							
1030	0	0	776	5350	100%	183	84								
1100			777	5357		183	84								
1130			776	5350		181	83								
1200			777	5357		183	84								
1230			777	5357		183	84								
1300			777	5357		185	85								
1330			778	5364		187	86								
1400			780	5378		188	87								
1430			780	5378		190	88								0.58

CONVERSION FACTORS:

• BBL'S x 0.15899 = M³

• MMSCF x 28.174 = 10³ M³

• Cu/FT PER BBL x 0.1773 = M³/M³

• PSI x 6.895 = KPA

• °C x 9 ÷ 5 + 32 = °F

WELL: ...KIDMAN #1
 OPERATOR: ...M. SAUNDERS



SANTOS LTD
 WELL TEST DATA
 METRIC SUMMARY SHEET

DATE: ...12-5-87...
 PAGE No: ...2...

DATE TIME	WELLHEAD							FLUID PRODUCTION				GAS PRODUCTION			
	CASING PSI	CASING KPA	TUBING PSI	TUBING KPA	CHOKE SIZE INS.	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M3/D	FLOWRATE H2O BBL'S/D	FLOWRATE H2O M3/D	MMSCF/D	Mm3/D	G.O.R. Cu/FT BBL	G.O.R. M3/M3
1500	0	0	780	5378	100%	190	88								
1530	↓	↓	786	5419	↓	188	87								
1600	↓	↓	786	5419	↓	188	87								
	SHOT IN WELL														
1615	0	0	1824	12576	—	164	73.5								
1630			1827	12597		149	65								
1645			1829	12610		136	58								
1700			1830	12617		127	53								
1715			1831	12624		120	49								
1730			1831	12624		116	47								
1745	↓	↓	1831	12624		114	45								
1800	↓	↓	1831	12624	↓	113	45								

CONVERSION FACTORS:

• BBL'S x 0.15899 = M³

• MMSCF x 28.174 = 10³ M³

• Cu/FT PER BBL x 0.1773 = M³/M³

• PSI x 6.895 = KPA

• °C x 9 ÷ 5 + 32 = °F

0151

WELL: ...KIDMAN #1
 OPERATOR: ...M. SAUNDERS



SANTOS LTD
 WELL TEST DATA
 METRIC SUMMARY SHEET

DATE: ...12-5-87
 PAGE No: ...3

DATE TIME	WELLHEAD							FLUID PRODUCTION				GAS PRODUCTION			
	CASING PSI	CASING KPA	TUBING PSI	TUBING KPA	CHOKE SIZE INS.	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M3/D	FLOWRATE H2O BBL'S/D	FLOWRATE H2O M3/D	MMSCF/D	Mm3/D	G.O.R. Cu/FT BBL	G.O.R. M3/M3
1815	0	0	1832	12631	—	109	43								
1830			1835	12652		106	41								
1845			1836	12659		102	39								
1900			1837	12666		98	37								
1915			1838	12673		95	35								
1930			1838	12673		93	34								
1945			1838	12673		90	32								
2000			1838	12673		88	31								
13-5-87 0000			1847	12735		75	24								
0400			1855	12790		72	22								
0800			1861	12831		72	22								
1200			1865	12859		59	15								0160

CONVERSION FACTORS:

• BBL'S x 0.15899 = M³

• MMSCF x 28.174 = 10³ M³

• Cu/FT PER BBL x 0.1773 = M³/M³

• PSI x 6.895 = KPA

• °C x 9 ÷ 5 + 32 = °F

WELL: KIDMAN #1
 OPERATOR: M. SAUNDERS



SANTOS LTD
WELL TEST DATA
METRIC SUMMARY SHEET

DATE: 15-5-87
 PAGE No: 5

DATE TIME	WELLHEAD							FLUID PRODUCTION				GAS PRODUCTION			
	CASING PSI	CASING KPA	TUBING PSI	TUBING KPA	CHOKE SIZE INS.	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M3/D	FLOWRATE H2O BBL'S/D	FLOWRATE H2O M3/D	MMSCF/D	Mm3/D	G.O.R. Cu/FT BBL	G.O.R. M3/M3
1600	0	0	1890	13031	-	77	25								
2000			1890	13031	1	66	19								
1658/0000			1891	13038		59	15								
0400			1891	13038		57	14								
0800	↓	↓	1893	13052	↓	59	15								
	PULL OUT OF HOLE.														
0824	ON SURFACE														
0924	0	0	1897	13079		59	15								
	DEPRESSURE LUBRICATOR														

CONVERSION FACTORS:

• BBL'S x 0.15899 = M³

• MMSCF x 28.174 = 10³ M³

• Cu/FT PER BBL x 0.1773 = M³/M³

• PSI x 6.895 = KPA

• °C x 9 ÷ 5 + 32 = °F

0161

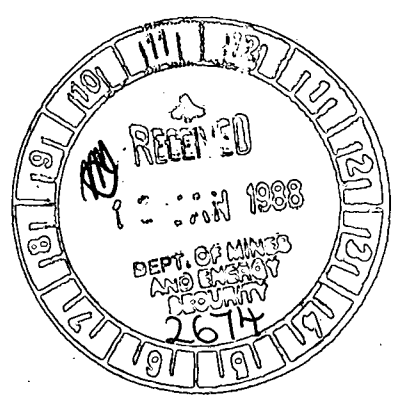
0162

CHIED HOLE



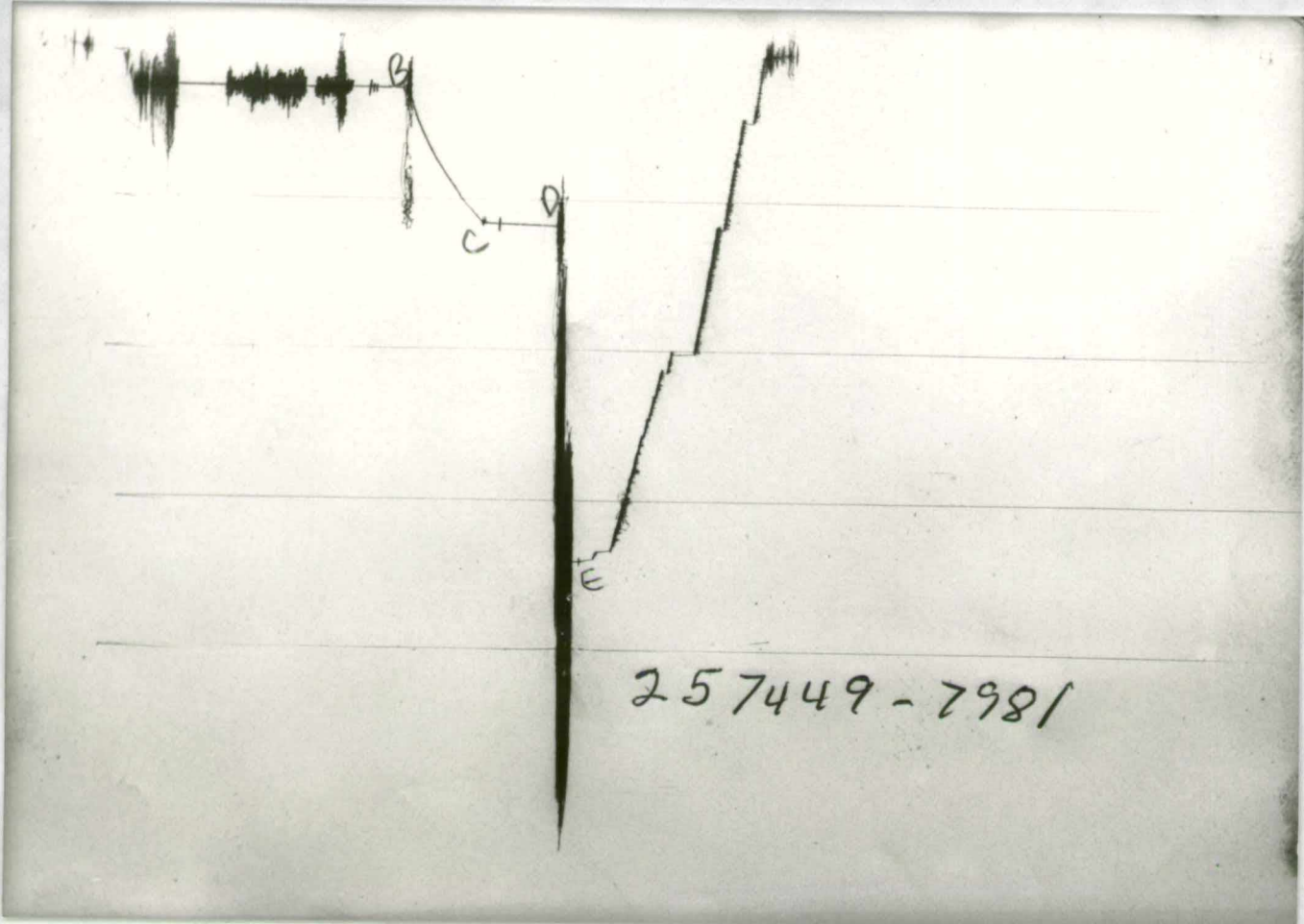
HALLIBURTON SERVICES

TICKET NO. 25744900
11-JAN-88
MOOMBA



FORMATION TESTING SERVICE REPORT

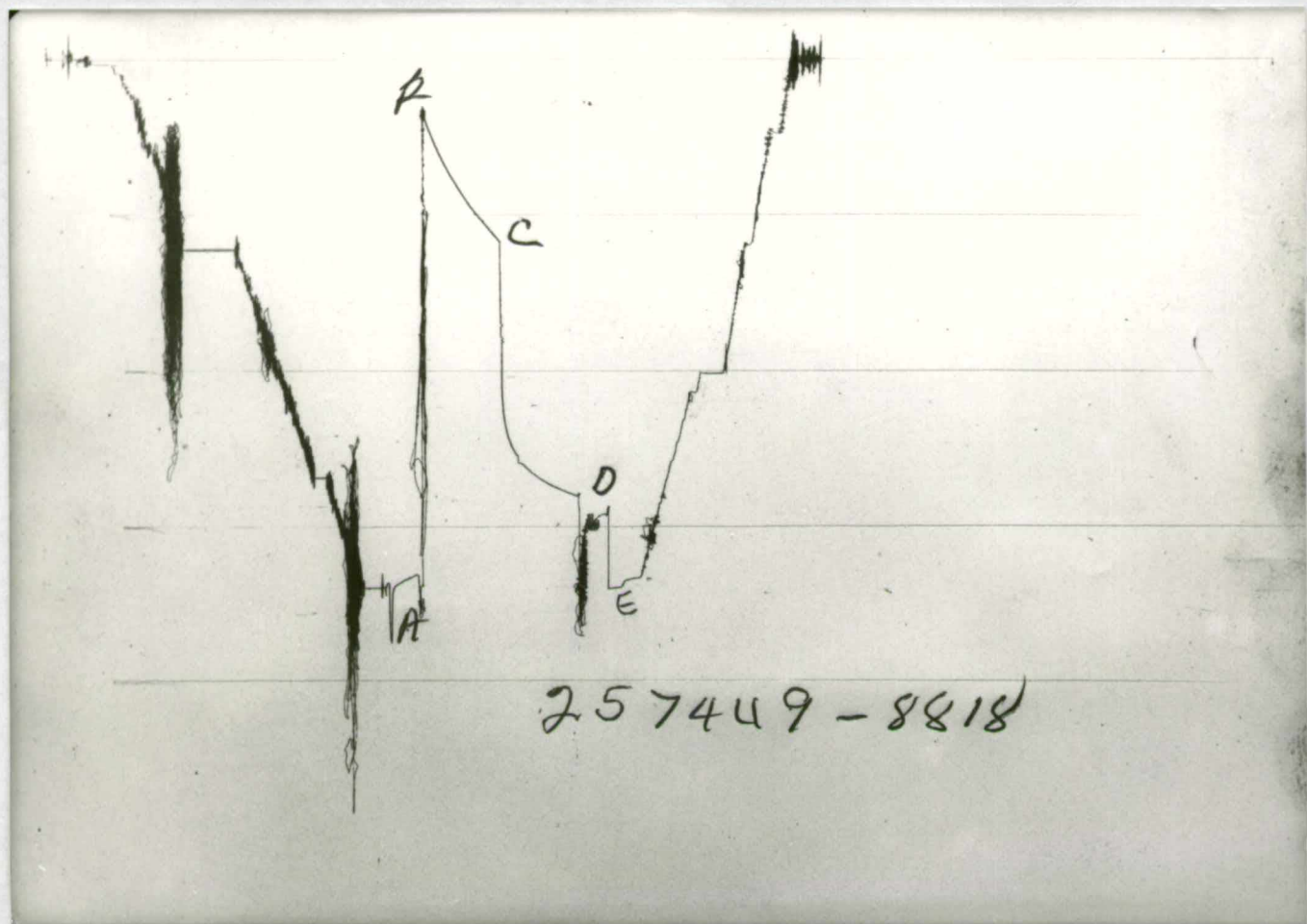
LEASE NAME		WELL NO.		TEST NO.		TESTED INTERVAL		LEASE OWNER/COMPANY NAME	
KIDMBN		1		1		7240.0 - 7515.0		SRANTOS LIMITED	
LEGAL LOCATION		SEE REMARKS		FIELD AREA		COOPER BASIN		COUNTY QUEENSLAND	
SEC. - TWP. - RING.								STATE AUSTRALIA	
								DR	



257449-7981

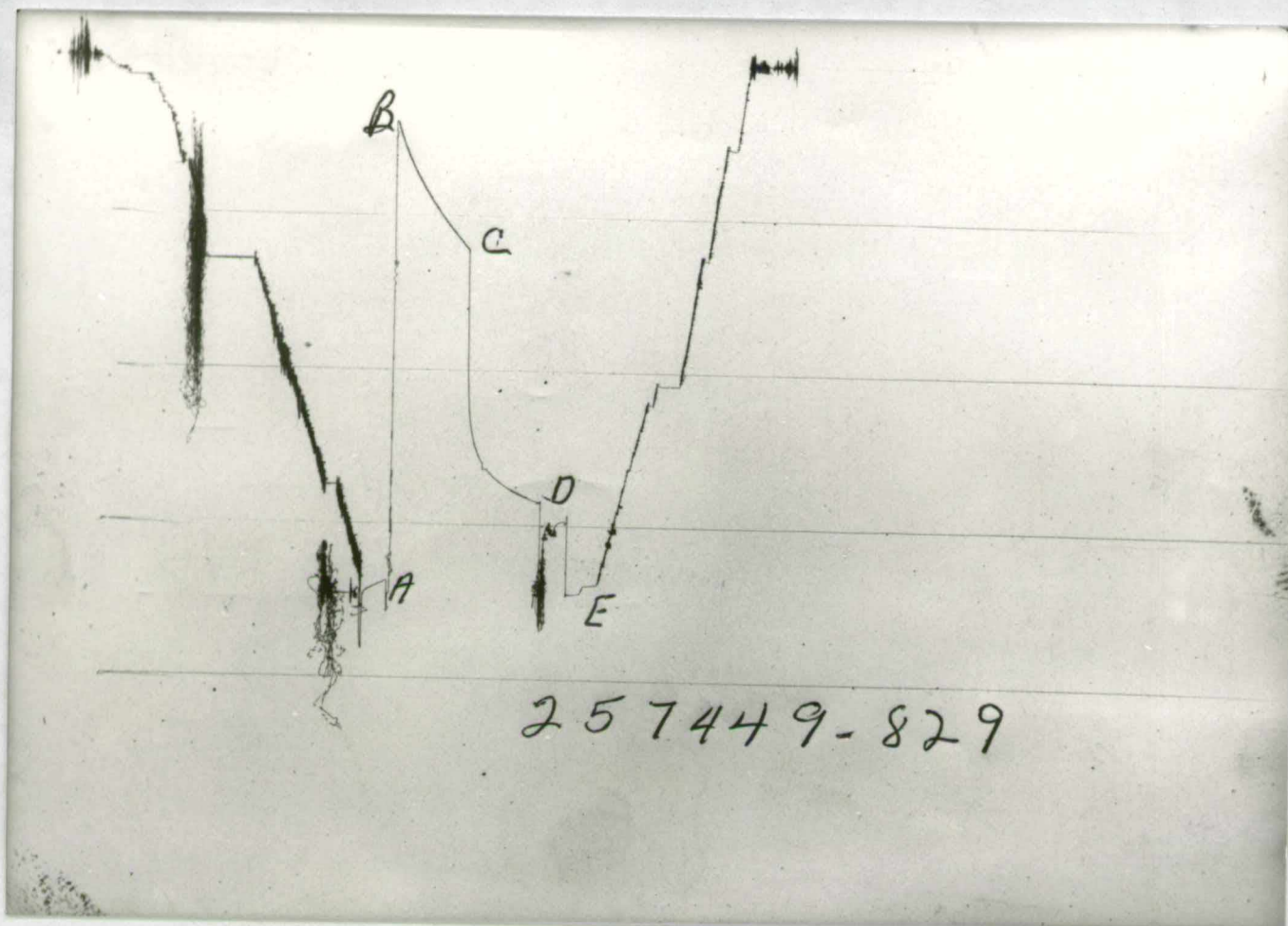
GAUGE NO: 7981 DEPTH: 7080.0 BLANKED OFF: NO HOUR OF CLOCK: 48

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC					
B	INITIAL FIRST FLOW	252	246.4	180.0	179.5	F
C	FINAL FIRST FLOW		1145.6			
C	INITIAL FIRST CLOSED-IN		1145.6	180.0	180.5	C
D	FINAL FIRST CLOSED-IN	1163	1160.6			
E	FINAL HYDROSTATIC		3318.3			



GAUGE NO: 8818 DEPTH: 7091.0 BLANKED OFF: NO HOUR OF CLOCK: 48

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	3382	3298.7			
B	INITIAL FIRST FLOW	315	295.7	180.0	179.5	F
C	FINAL FIRST FLOW	1160	1160.3			
C	INITIAL FIRST CLOSED-IN	1160	1160.3	180.0	180.5	C
D	FINAL FIRST CLOSED-IN	2791	2791.9			
E	FINAL HYDROSTATIC	3382	3318.2			



GAUGE NO : 829 DEPTH : 7252.0 BLANKED OFF : YES HOUR OF CLOCK : 48

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	3438	3352.6			
B	INITIAL FIRST FLOW	388	386.5			
C	FINAL FIRST FLOW	1204	1208.5	180.0	179.5	F
C	INITIAL FIRST CLOSED-IN	1204	1208.5			
D	FINAL FIRST CLOSED-IN	2833	2839.9	180.0	180.5	C
E	FINAL HYDROSTATIC	3422	3359.9			

EQUIPMENT & HOLE DATAFORMATION TESTED: PATCHAWARRANET PAY (ft): 13.0 (PERF. INTERVAL)GROSS TESTED FOOTAGE: 275.0ALL DEPTHS MEASURED FROM: RKBCASING PERFS. (ft): 7296-7309'HOLE OR CASING SIZE (in): 7.000ELEVATION (ft): 257.0TOTAL DEPTH (ft): 7515.0PACKER DEPTH(S) (ft): 7240FINAL SURFACE CHOKE (in): 0.50000BOTTOM HOLE CHOKE (in): 0.620MUD WEIGHT (lb/gal): 9.50

MUD VISCOSITY (sec): _____

ESTIMATED HOLE TEMP. (°F): _____

ACTUAL HOLE TEMP. (°F): 282 @ 7226.0 ftTICKET NUMBER: 25744900DATE: 7-11-87 TEST NO: 1TYPE DST: CASED HOLEHALLIBURTON CAMP:
MOOMBATESTER: TREVOR BURKEWITNESS: WARREN BOERDRILLING CONTRACTOR:
RICHTER RIG #16**FLUID PROPERTIES FOR
RECOVERED MUD & WATER**

SOURCE	RESISTIVITY	CHLORIDES
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm
_____	_____ @ _____ °F	_____ ppm

SAMPLER DATA

Psig AT SURFACE: _____
 cu.ft. OF GAS: _____
 cc OF OIL: _____
 cc OF WATER: _____
 cc OF MUD: _____
 TOTAL LIQUID cc: _____

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): _____ @ _____ °F
 GAS/OIL RATIO (cu.ft. per bbl): _____
 GAS GRAVITY: _____

CUSHION DATA

TYPE	AMOUNT	WEIGHT
<u>WATER (FT.)</u>	<u>500.0</u>	<u>8.33</u>

RECOVERED :

31.29 BBLS. OF FORMATION WATER
 3.71 BBLS. OF WATER CUSHION

 MEASURED FROM
TESTER VALVE
REMARKS :

LEGAL LOCATION: 28 DEG. 12' 30" S. LAT. & 140 DEG. 48' 36.1" E. LONG.

0167

TYPE & SIZE MEASURING DEVICE : 6" CERAMIC CHOKE					TICKET NO: 25744900
TIME	CHOKE SIZE	SURFACE PRESSURE PSI	GAS RATE MCF	LIQUID RATE BPD	REMARKS
7-10-87					
1700					LOADED BT'S
1715					MADE UP B.H.A. OF TOOL
1730					RUN DRILL COLLARS
1810					MADE UP TOOLS
1835					TOOLS MADE UP, RUN IN HOLE
7-11-87					
0555					SET PACKER
0605					PRESSURE TESTED SEP. LINE,
					ANNULUS AND HOWCO
0711					SET 15,000# ON TOOL
0716					OPENED TOOL WITH NO BLOW
0717					TOOL CLOSED TO FLARE
0739					VERY, VERY WEAK BLOW
0743					SURGING WEAK BLOW
0746	.5				SURGING WEAK TO MODERATE BLOW
					OPENED TO FLARE
0750					MODERATE TO STRONG BLOW UNTIL
					0830
0800		2			
0805		2			
0810		2			
0815		2			
0830		2			
0839		1			BLOW SURGING SLOW DECREASE
0845		1			SAME
0900		1			
0915		1			
0919		1			CONSTANT MODERATE BLOW
0930		1			SAME
0945		1			
1000		1			
1016					CLOSED TOOL
1316					BYPASS OPENED
1322					DROPPED BAR TO REVERSE
1324					BEGAN REVERSE CIRCULATION
1353					FINISHED

0169

TICKET NO: 25744900

CLOCK NO: 23497 HOUR: 48



GAUGE NO: 7981

DEPTH: 7080.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	245.4			
2	30.0	522.9	276.5		
3	60.0	693.9	171.0		
4	90.0	827.8	134.0		
5	120.0	951.5	123.7		
6	150.0	1059.8	108.2		
C 7	179.5	1145.6	85.9		
FIRST CLOSED-IN					
C 1	0.0	1145.6			
D 2	180.5	1160.6	15.0	90.0	0.300

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$

REMARKS:

0170

TICKET NO: 25744900

CLOCK NO: 10878 HOUR: 48



GAUGE NO: 8818

DEPTH: 7091.0

REF	MINUTES	PRESSURE	AP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	295.7			
2	30.0	549.5	253.8		
3	60.0	716.7	167.2		
4	90.0	852.4	135.7		
5	120.0	968.3	115.9		
6	150.0	1065.7	97.4		
C 7	179.5	1160.3	94.6		
FIRST CLOSED-IN					
C 1	0.0	1160.3			
2	10.0	2312.7	1152.4	9.5	1.277
3	20.0	2428.9	1268.7	18.0	0.999
4	30.0	2496.0	1335.7	25.7	0.844
☒ 5	38.1	2581.6	1421.3	31.4	0.757
6	40.0	2579.3	1419.0	32.7	0.739
7	50.0	2587.2	1427.0	39.1	0.662
8	60.1	2611.7	1451.4	45.0	0.601
9	70.0	2637.4	1477.1	50.4	0.552
10	80.0	2658.7	1498.5	55.4	0.511
11	90.0	2679.6	1519.4	60.0	0.476
12	100.0	2698.1	1537.8	64.2	0.446
13	110.0	2714.4	1554.1	68.2	0.420
14	120.0	2727.5	1567.3	71.9	0.397
15	130.0	2741.3	1581.0	75.4	0.377
16	140.0	2752.6	1592.3	78.6	0.358
17	150.0	2765.2	1605.0	81.7	0.342
18	160.0	2776.7	1616.4	84.6	0.327
19	170.0	2786.2	1626.0	87.3	0.313
D 20	180.5	2791.9	1631.7	90.0	0.300

REF	MINUTES	PRESSURE	AP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$

LEGEND:

☒ STAIR-STEP

REMARKS:

0171

TICKET NO: 25744900

GAUGE NO: 829

CLOCK NO: 14113 HOUR: 48

DEPTH: 7252.0



REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	386.5			
2	30.0	591.3	204.8		
3	60.0	760.5	169.2		
4	90.0	898.7	138.2		
5	120.0	1011.5	112.8		
6	150.0	1112.6	101.1		
C 7	179.5	1208.5	95.8		
FIRST CLOSED-IN					
C 1	0.0	1208.5			
2	10.0	2368.3	1159.9	9.4	1.280
3	20.0	2482.5	1274.0	18.0	0.998
4	30.0	2551.6	1343.1	25.7	0.844
☒ 5	38.1	2631.6	1423.1	31.4	0.757
6	40.0	2627.1	1418.6	32.7	0.739
7	50.0	2637.7	1429.2	39.1	0.662
8	60.0	2654.3	1455.8	45.0	0.601
9	70.0	2688.6	1480.2	50.3	0.552
10	80.0	2711.1	1502.6	55.4	0.511
11	90.0	2730.9	1522.5	59.9	0.476
12	100.0	2747.0	1538.5	64.2	0.447
13	110.0	2762.2	1553.7	68.2	0.420
14	120.0	2775.2	1566.7	71.9	0.397
15	130.0	2787.0	1578.6	75.4	0.377
16	140.0	2798.7	1590.3	78.7	0.358
17	150.0	2810.9	1602.4	81.7	0.342
18	160.0	2822.9	1614.5	84.6	0.327
19	170.0	2832.7	1624.2	87.3	0.313
D 20	180.5	2839.9	1631.4	90.0	0.300

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$

LEGEND:

☒ STAIR-STEP

REMARKS:

		O.D.	I.D.	LENGTH	DEPTH	
1		DRILL PIPE.....	3.500	2.764	7069.4	
5		CROSSOVER.....	4.750	2.000	1.0	
50		IMPACT REVERSING SUB.....	3.750	2.000	1.2	7077.0
5		CROSSOVER.....	3.400	2.000	0.7	
258		BAR CATCHER SUB.....	4.750	1.120	0.7	
80		AP RUNNING CASE.....	5.000	2.250	4.1	7080.0
5		CROSSOVER.....	4.750	2.000	1.0	
61		INDEXING HYDROSPRING TESTER.....	3.870	0.620	6.0	7089.0
80		AP RUNNING CASE.....	3.870	2.000	4.6	7091.0
14		EXTENSION JOINT.....	3.880	0.880	4.2	
14		EXTENSION JOINT.....	3.880	0.880	4.2	
5		CROSSOVER.....	3.800	2.250	1.0	
5		CROSSOVER.....	4.750	2.500	0.9	
3		DRILL COLLARS.....	4.750	2.310	124.6	
5		CROSSOVER.....	4.750	2.250	0.8	
5		CROSSOVER.....	3.800	0.900	1.0	
15		JAR.....	3.870	1.250	5.0	
16		VR SAFETY JOINT.....	3.870	0.750	2.5	
76		RTTS PACKER.....	5.650	2.400	3.7	7240.0
5		CROSSOVER.....	3.500	1.750	0.6	
21		PERFORATED TAIL PIPE.....	3.870	1.750	8.0	
81		BLANKED-OFF RUNNING CASE.....	3.870		4.2	7252.0
TOTAL DEPTH					7515.0	

EQUIPMENT DATA

ROLLING BOTTOMHOLE PRESSURE SURVEY GAS CALCULATION SHEET

0173

WELL: Kidman # 1 Pf = 4400 kPa
 ORIFICE SIZE: 76.200 mm 3.000 " T = 89 °C
 LINE SIZE: 146.329 mm 5.761 " ✓ Diff = 27 kPa

Cumulative Production to end of July = $454.360 \text{ m}^3 \times 10^6$

Number of hours online in July = 637 ✓

Production in July = $9.060 \text{ m}^3 \times 10^6$ ✓

.. Average flow rate in July = $(9.060/637) \times 24 = 0.341 \text{ m}^3 \times 10^6/\text{d}$

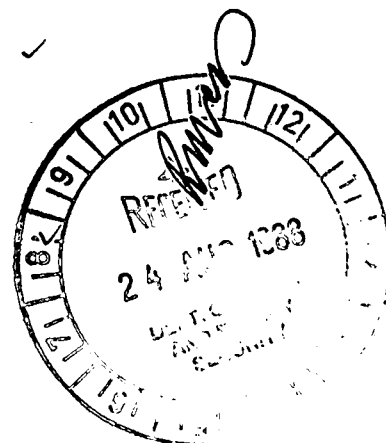
Number of days online in July ^{after} before Shut In 0800 hrs 28 / 7 /88
 = NIL

.. Production up to 0800 hrs 28 / 7 /88 = July Production $\text{m}^3 \times 10^6$

Total cumulative production =
 = $454.360 \text{ m}^3 \times 10^6$
 = 16127.054 mmscf ✓

Flow rate just prior to Shut In = $0.347 \text{ m}^3 \times 10^6$
 = 12.333 mmscf/d

2674



SANTOS LTD
39 GRENFELL ST
ADELAIDE

SUB-SURFACE PRESSURE SURVEY

CO. SANTOS	RUN 01 FIELD KIDMAN	WELL 01
EFF DEPTH	WELL STAT	TOOL HUNG 6569'
CASING -	CASING PRESS	ON BOTTOM 1800 27/7
LINER -	TUBING PRESS	OFF BOTTOM 0800 1/8
DATE 880801	ELEMENT RANGE 0 - 4164	ZERO POINT
ELEVATION	ZONE	SHUT-IN 0800 28/7
MAX TEMP 262	PICK-UP	ON-PROD
PERF -	CAL SER NO. 22410	MDP
TUBING -		
UNITS ENGLISH	PURPOSE BUILD-UP	

SURVEY DATA

CO. SANTOS				RUN 01 FIELD KIDMAN				WELL 01			
TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME				
8:00	1700.6	0.0	0.0	9:09	2195.8	495.3	1.1				
8:01	1764.1	63.5	.0	9:38	2197.6	497.0	1.6				
8:02	1833.9	133.3	.0	10:30	2197.3	496.8	2.5				
8:03	1938.9	238.3	.1	12:08	2196.9	496.3	4.1				
8:05	2055.0	354.5	.1	15:04	2196.1	495.6	7.1				
8:06	2116.3	415.7	.1	19:33	2197.0	496.4	11.6				
8:09	2160.7	460.2	.2	3:44	2196.4	495.9	19.7				
8:11	2173.9	473.4	.2	13:29	2195.7	495.2	29.5				
8:15	2178.1	477.5	.3	23:17	2196.0	495.4	39.3				
8:20	2183.4	482.9	.3	10:13	2198.5	497.9	50.2				
8:26	2186.7	486.1	.4	23:14	2201.2	500.6	63.2				
8:32	2190.0	489.4	.5	11:55	2201.7	501.2	75.9				
8:41	2192.9	492.3	.7	2:05	2204.4	503.8	90.1				
8:51	2194.7	494.1	.9	8:00	2204.2	503.7	96.0				

LUB IN DWT = 1297 PSI / OUT = 1859 PSI

LUB IN AMERADA = 1286 PSI / OUT = 1853 PSI

SANTOS LTD
39 GRENELL ST
ADELAIDE

SUB-SURFACE PRESSURE SURVEY

CO. SANTOS	RUN 02 FIELD KIDMAN	WELL 01
EFF DEPTH	WELL STAT	TOOL HUNG 6575'
CASING	CASING PRESS	ON BOTTOM 1800 27/7
LINER	TUBING PRESS	OFF BOTTOM 0800 1/8
DATE 880801	ELEMENT RANGE 0 - 4099	ZERO POINT
ELEVATION	ZONE	SHUT-IN 0800 28/7
MAX TEMP 262	PICK-UP	ON-PROD
PERF	CAL SER NO. 21374	MPP
TUBING		
UNITS ENGLISH	PURPOSE BUILD-UP	

SURVEY DATA

CO. SANTOS				RUN 02 FIELD KIDMAN				WELL 01			
TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME				
8:00	1684.6	0.0	0.0	8:52	2179.7	495.1	.9				
8:01	1720.1	35.4	.0	9:13	2180.3	495.7	1.2				
8:02	1763.7	79.1	.0	9:37	2180.9	496.2	1.6				
8:03	1821.9	137.3	.1	10:40	2181.9	497.3	2.7				
8:04	1880.3	195.7	.1	12:18	2181.7	497.0	4.3				
8:05	1962.1	277.5	.1	15:05	2181.2	496.6	7.1				
8:07	2067.9	383.3	.1	18:44	2182.9	498.3	10.7				
8:08	2117.2	432.6	.1	0:07	2182.7	498.1	16.1				
8:11	2144.7	460.1	.2	8:37	2182.9	498.2	24.6				
8:13	2155.0	470.3	.2	19:11	2184.1	499.5	35.2				
8:16	2160.5	475.9	.3	5:08	2187.4	502.7	45.1				
8:19	2167.5	482.9	.3	15:41	2187.0	502.3	55.7				
8:22	2171.0	486.3	.4	3:10	2188.9	504.3	67.2				
8:32	2173.8	489.2	.5	20:21	2190.8	506.2	84.3				
8:41	2176.9	492.2	.7	8:00	2193.1	508.5	96.0				

LUB IN DWT = 1297 PSI / OUT = 1859 PSI

LUB IN AMERADA = 1276 PSI / OUT = 1847 PSI

0176

1240 7 ADJ " 0.

1112MAN #1

1305
146.329

Mixing

0.20 MPA
0.80 KPA
0.150°C

WILL ON TEST YES

19-7-88 76.200

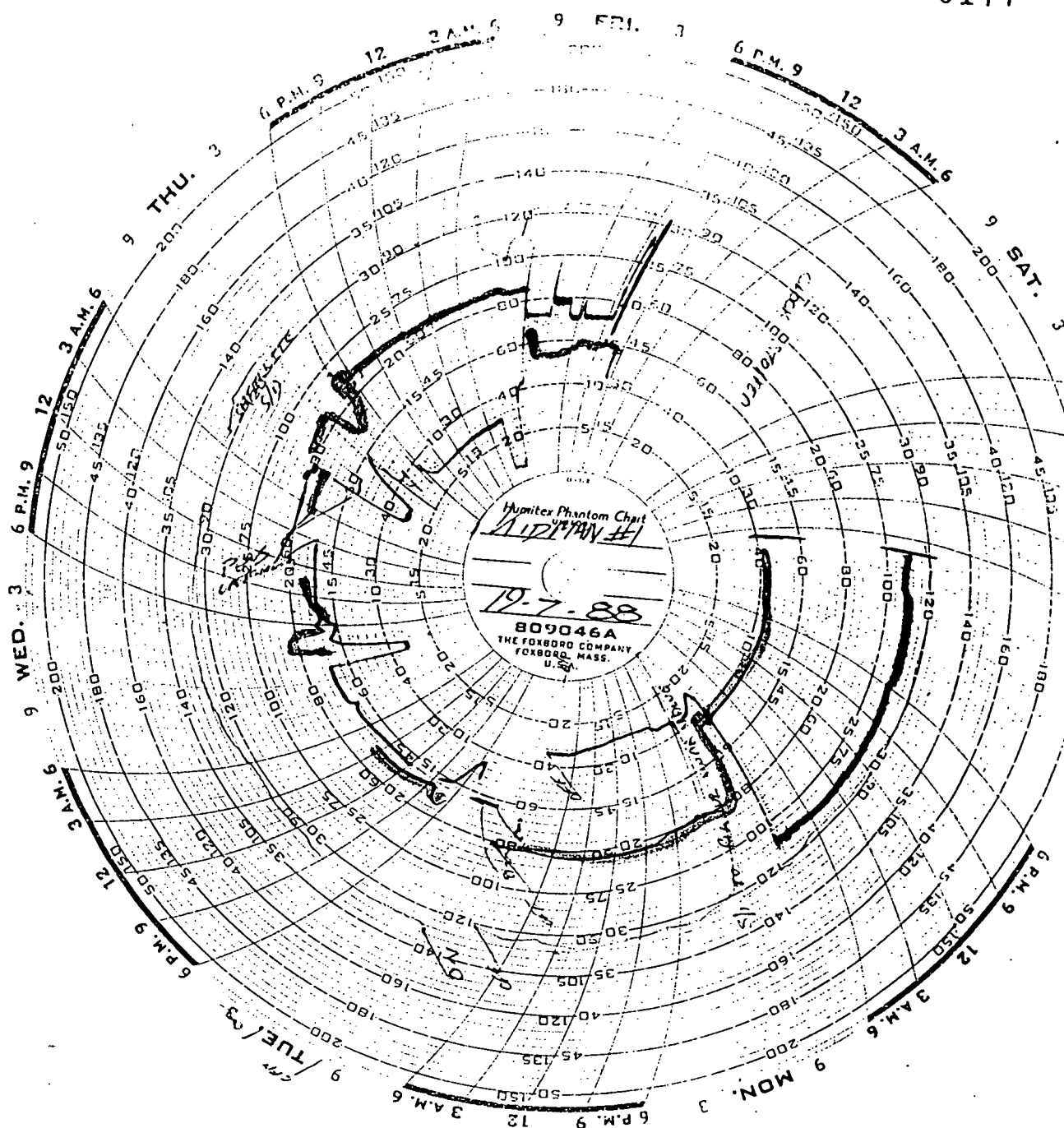
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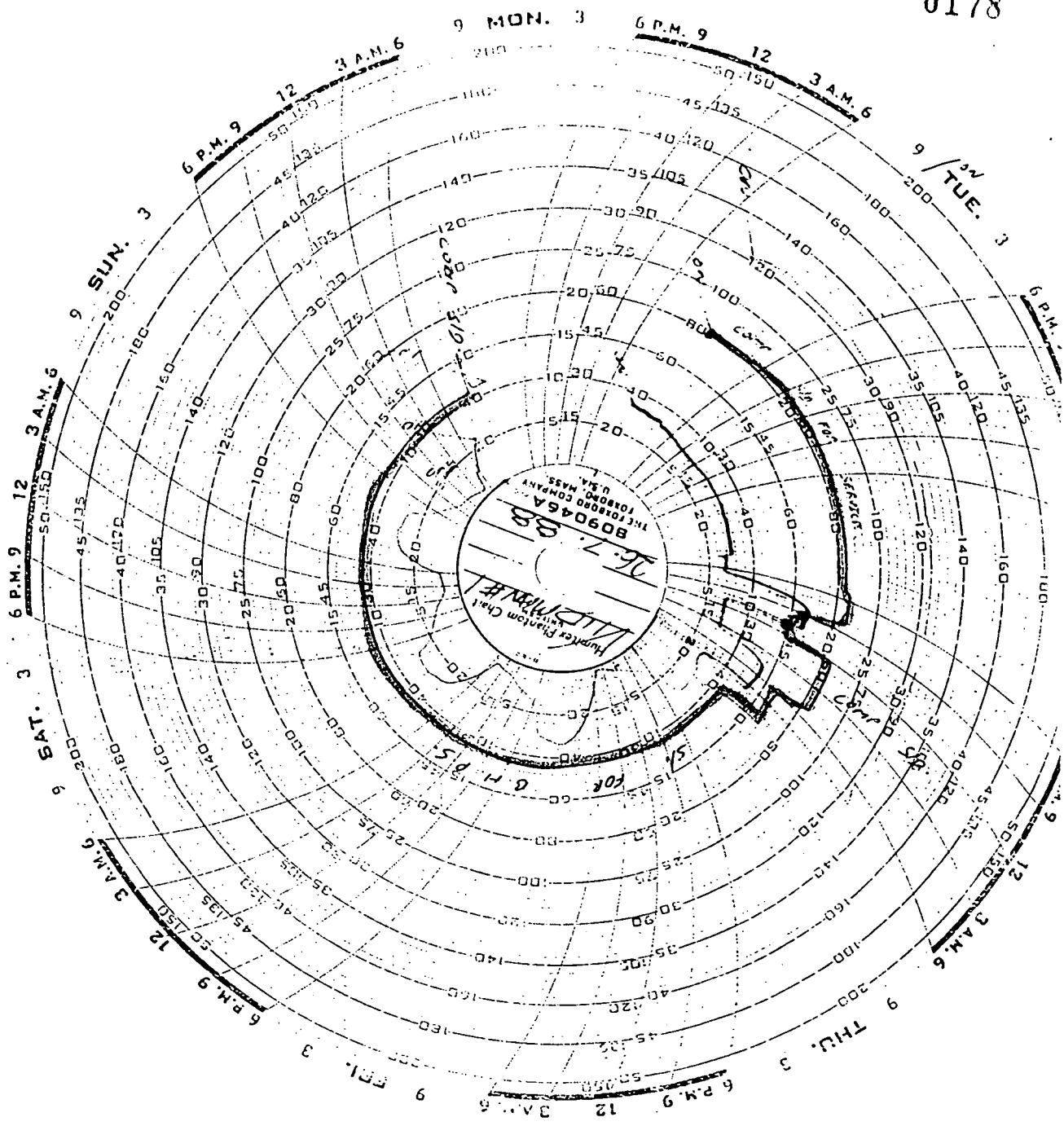
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CHECK MARKING







WELL: KIDMAN #1						SANTOS LTD.										DATE: 27-7-88				
TYPE OF TEST: P.B.U. SURVEY						WELL TEST DATA SHEET										PAGE No: #1				
DATE TIME	WELLHEAD					GAS FLOW DATA					OIL/CONDENSATE PRODUCTION			WATER PRODUCTION		WELL TEST RESULTS				
	CASING KPA	TUBING KPA	TEMP. °C	CHOKE SIZE INS.	B.S.W. %	PI PSI	HW INS. H ₂ O	TEMP. °F	ORIFICE SIZE INS.	TANK DIP INS.	TANK PROD BBLs	API GRAVITY @ 60 °F	TANK DIP INS.	TANK PROD BBLs	FLOW RATE MMSCFD	FLOW RATE BBLs/ DAY	FLOW RATE BBLs/ DAY	TOTAL LIQUID FLOW RATE BBLs/ DAY	G.O.R. SCF/BBL	
27 TH JULY 1988																				
1540																				
1740	0	8943	87																	
1800	0	8998	88																	
2400	0	8895	88	100%																
28 TH JULY 1988																				
0600	0	7067	88																	
0630		7033	89																	
0700		7102	90																	
0730		7136	90																	
0800		7171	90	100%																
0815		12804																		
0830		12825																		
0845		12838																		
0900		12832																		
0915		12825																		
0930		12825																		
0945		12825																		
1000		12825																		
1015	0	12825																		

OPERATOR: A. SMITH

0150

WELL: <u>KIDMAN #1</u>						SANTOS LTD.										DATE: <u>28-7-88</u>				
TYPE OF TEST: <u>P.B.U SURVEY</u>						WELL TEST DATA SHEET										PAGE No: <u>#2</u>				
DATE TIME	WELLHEAD					GAS FLOW DATA				OIL/CONDENSATE PRODUCTION			WATER PRODUCTION		WELL TEST RESULTS					
	CASING KPA	TUBING KPA	TEMP. °C	CHOKE SIZE INS.	B.S.W. %	PI PSI	HW INS. H ₂ O	TEMP. °F	ORIFICE SIZE INS.	TANK DIP INS.	TANK PROD BBLs	API GRAVITY @60 °F	TANK DIP INS.	TANK PROD BBLs	GAS FLOW RATE MMSCFD	OIL FLOW RATE BBLs/ DAY	WATER FLOW RATE BBLs/ DAY	TOTAL LIQUID FLOW RATE BBLs/ DAY	G.O.R. SCF/BBL	
28 TH JULY 1988																				
1030	0	12825																		
1045	↑	↑																		
1100	↑	↑																		
1115	↑	↑																		
1130	↑	↑																		
1200		12825																		
1600		12811																		
2000	↓	12825																		
2400	0	12832																		
29 TH JULY 1988																				
0400	0	12811																		
0800	↑	12811																		
1200		IN MOOMBA																		
1600		IN MOOMBA																		
2000	↓	12811																		
2400	0	12825																		
30 TH JULY 1988																				
0400	0	12811																		
0800	0	12811																		

OPERATOR: A. SMITH

0181



**** KIDMAN #1 ****

STATIC PRESSURE GRADIENT

TEST DATE: 1-8-88

TOP PRESSURE ELEMENT 22410/4100				BOTTOM PRESSURE ELEMENT 21374/4075		
DEPTH (FT.)	DEFLECTION (INCHES)	PRESSURE (PSIG)	GRADIENT (PSI/FT)	DEFLECTION (INCHES)	PRESSURE (PSIG)	GRADIENT (PSI/FT)
LUB	0.8970	1841.9	----	0.9060	1831.9	----
1000	0.9240	1898.0	0.0561	0.9360	1893.5	0.0616
2000	0.9520	1956.1	0.0582	0.9630	1948.9	0.0555
3000	0.9790	2012.3	0.0562	0.9900	2004.4	0.0555
4000	1.0040	2064.3	0.0520	1.0160	2057.9	0.0535
5000	1.0290	2116.4	0.0521	1.0410	2109.3	0.0514
5500	1.0400	2139.4	0.0459	1.0550	2138.1	0.0576
6000	1.0530	2166.5	0.0542	1.0660	2160.8	0.0453
6500	1.0640	2189.4	0.0459	1.0780	2185.5	0.0494
6674	1.0680	2197.8	0.0480	1.0830	2195.8	0.0592
6742	1.0720	2206.1	0.1228	1.0890	2208.1	0.1817
LUB	0.8970	1841.9	----	0.9100	1840.1	----

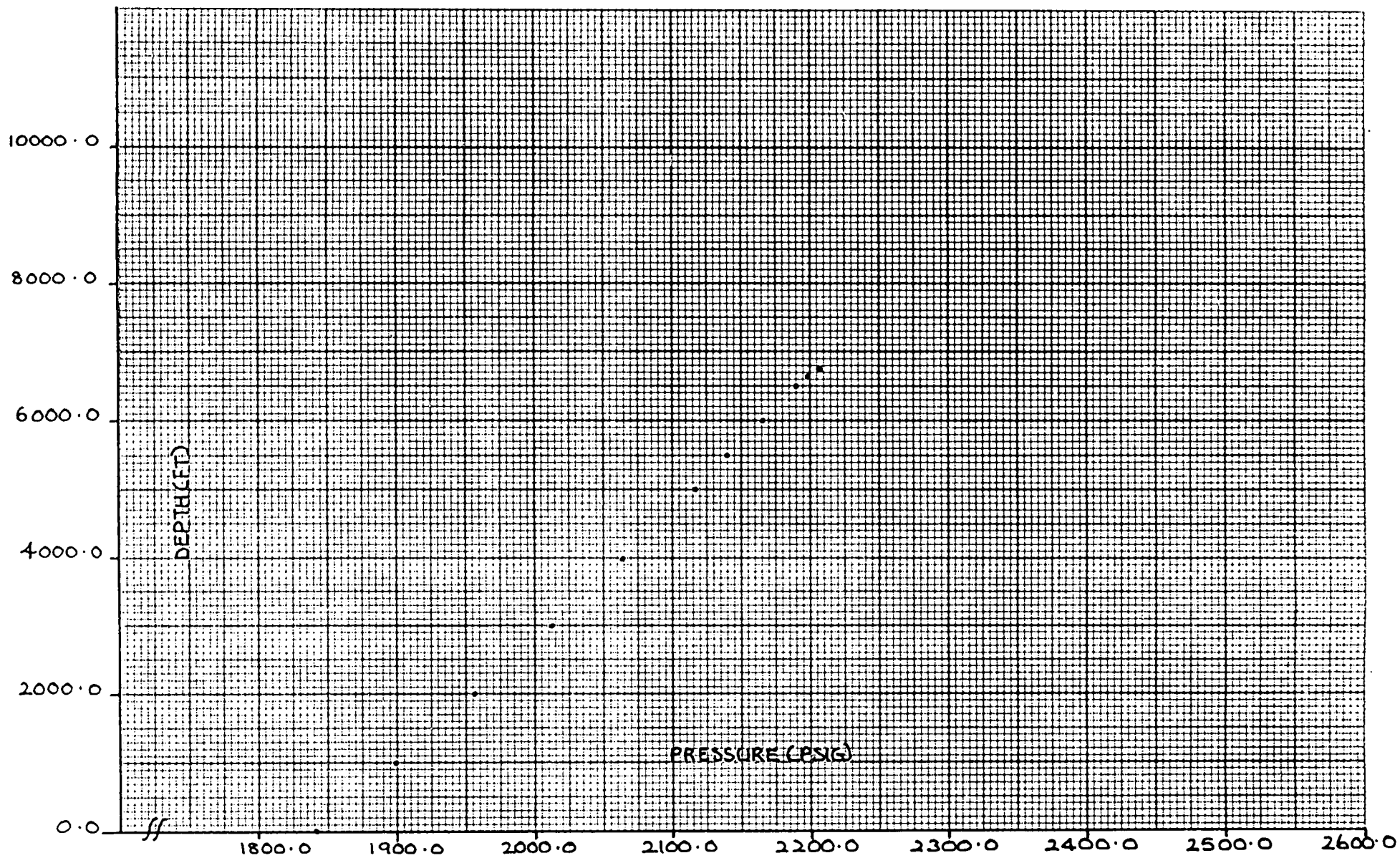
GENERAL REMARKS:

DWT IN: 1859
DWT OUT: 1859
MAX BHT: 270 F

ELEMENT 22410/4100 CALIBRATED 16.7.88
ELEMENT 21374/4075 CALIBRATED 16.7.88

KIDMAN # 1 - STATIC PRESSURE GRADIENT - 1/8/88

ELEMENT # 22410/4100(TOP)



BOMB No. 1 DATA						BOMB No. 2 DATA				LUBRICATOR DATA	
ELEMENT No. 22410						ELEMENT No. 21374				PRESSURE WITH D.W.T. IN 12818 KPA OUT 12818 K	
RECORDER No. 14627 x 15 TLS						RECORDER No. 14623 x 15				TIME PRESSURED: 1033	
ENGAGE SYLUS: 1029						ENGAGE SYLUS: 1029				TIME DEPRESSURED: 1249	
ELEMENT RANGE: 4100 PSI						ELEMENT RANGE: 4075 PSI					
CLOCK DATA: 2360 x 3 HR						CLOCK DATA: 2387 x 3 HR					
DISENGAGE: 1253						DISENGAGE: 1253					
DATE	TIME	DEPTH	DEFLECTION	PRESSURE TEMP.	GRADIENT ps/ft	DEPTH	DEFLECTION	PRESSURE TEMP.	GRADIENT ps/ft	REMARKS	
1ST	AUGUST	1988		KPA				KPA			
	1033	LUB	.897			LUB	.906			PRESSURE LUBRICATOR.	
	1048	R.I.H				R.I.H				RUN IN HOLE.	
	1053	1000	.924			1000	.936				
	1101	2000	.952			2000	.963				
	1109	3000	.979			3000	.990				
	1117	4000	1.004			4000	1.016			NOTE: CLOCK #2360 FAILED TO RUN ON THE FIRST 2 STOP	
	1126	5000	1.029			5000	1.041				
	1124	5500	1.040			5500	1.055				
	1135	6000	1.053			6000	1.066				
	1142	6500	1.064			6500	1.078				
	1148	6674	1.068	15155.8		6674	1.083	151400		M.P.P	
	1204	6742	1.072			6742	1.089				
	1209	P.O.O.H				P.O.O.H				PULL OUT OF HOLE.	
	1234	LUB	.897			LUB	.910			@ LUBRICATOR.	
	1249	BLEED				BLEED				DEPRESSURE LUBRICATOR.	

WIRELINE REPORT

CLIENT Santos Ltd WELL Kidman # 1

DATE 25.07.88

PROGRAMME Flow & Build up Survey.

PURPOSE OF WORK Well evaluation

REPORT OF WORK PERFORMED 25th July 1988

12:30 Move onto location and rig in a wire line unit

14:00 Well shut in by production to fit a swab valve
Problems sealing 3 1/2 EUE swage in the tree connection check threads for possible bruising. OK

After third attempt washed up threads and applied yellow thread tape

14:18 Well back on production

14:20 Pressure test B.O.P.S

14:25 RIH with a 1.75" Blind box
Cut well back to 50% choke to travel tools through the N nipple. Note :- compressor not on line during survey.

14:48 Pick up was made at 7065' KA which is 5' less than previous survey.
POOH

15:10 Tools at surface. Depressure the Lub and secure well.

Graham R Peterson
Operator's Signature

WORKED PERFORMED BY G. Peterson R. Sullivan OF Expertest

WELL DATA:

Tubing Size 3 1/2" FWHP 8500 kpa. SIWHP

Subsurface S.V./Landing Nipple @ S.S.D. @

'X' Nipple @ 'N' ~~N~~ Nipple @ 6534' Other @

Min. I.D. 2.205" @ 6534' Packer @ 6516'

Perforated Interval: 6606' - 6692' Toolachee.

WIRELINE REPORT

CLIENT **SANTOS**

WELL **KIDMAN #1**

DATE **27.7.88**

PROGRAMME **P.B.U SURVEY**

PURPOSE OF WORK **TO DEFINE BOTTOM HOLE PRESSURE**

REPORT OF WORK PERFORMED

27TH JULY 1988

1540 : PRESSURE LUBRICATOR FOR P.B.U SURVEY

**1740 : R.I.H WITH 2 PRESSURE ELEMENTS & M.B.H -
- THERMOMETER**

1800 : @ HANG DEPTH 6575' K.B

28TH JULY 1988

0800 : S.W.I FOR BUILD UP.

1ST AUGUST 1988

0800 : 96 HR SHUT IN TIME P.O.O.H.

0817 : @ LUBRICATOR

**1017 : DEPRESSURE LUBRICATOR, RELOAD FOR
STATIC GRADIENT**

**1048 : R.I.H WITH 2 PRESSURE ELEMENTS FOR STATIC
GRADIENT.**

**1830 : STATIC GRADIENT COMPLETED, RIG DOWN EQU-
- IPMENT & HAND WELL BACK TO PRODUCTION
(CHARTS GOOD).**

A.S.M.

Operator's Signature

WORKED PERFORMED BY **A.S.MITH** OF **EXPERTEST**

WELL DATA:

Tubing Size **3 1/2"** FWHP **8500 KPA** SIWHP **-**

Subsurface S.V./Landing Nipple @ **S.S.D. @**

'X' Nipple @ **'N' Nipple @ 6534' K.B** Other @

Min. I.D. **2.205"** @ **6534' K.B** Packer @ **6516**

Perforated Interval: **6606' - 6692' K.B**

ROLLING BOTTOMHOLE PRESSURE SURVEY GAS CALCULATION SHEET

WELL: Kidman #1 Pf = 7150 kPa
 ORIFICE SIZE: 64.000 mm 2.520 " T = 89 °C
 LINE SIZE: 146.329 mm 5.761 " Diff = 5.2 kPa

Cumulative Production to end of August = $553.876 \text{ m}^3 \times 10^6$

Number of hours online in August = 744

Production in August = $4.294 \text{ m}^3 \times 10^6$

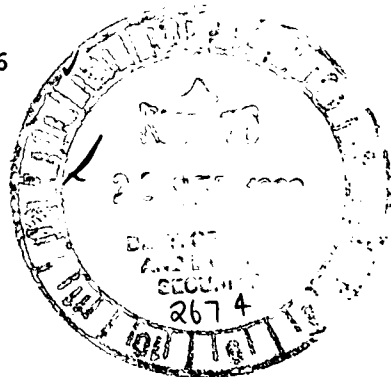
.. Average flow rate in August = $(4.294/744) \times 24 = 0.139 \text{ m}^3 \times 10^6/\text{d}$

Number of days online in Sept. before Shut In 0700 hrs 10 / 9 / 89
 = 9.167 days.

.. Production up to 0700 hrs 10 / 9 / 89 = $9.167 \times 0.139 = 1.270 \text{ m}^3 \times 10^6$

Total cumulative production = $1.270 + 553.876$
 = $555.146 \text{ m}^3 \times 10^6$
 = 19704.344 mmscf ✓

Flow rate just prior to Shut In = $0.138 \text{ m}^3 \times 10^6$
 = 4.896 mmscf/d



SUB-SURFACE PRESSURE SURVEY

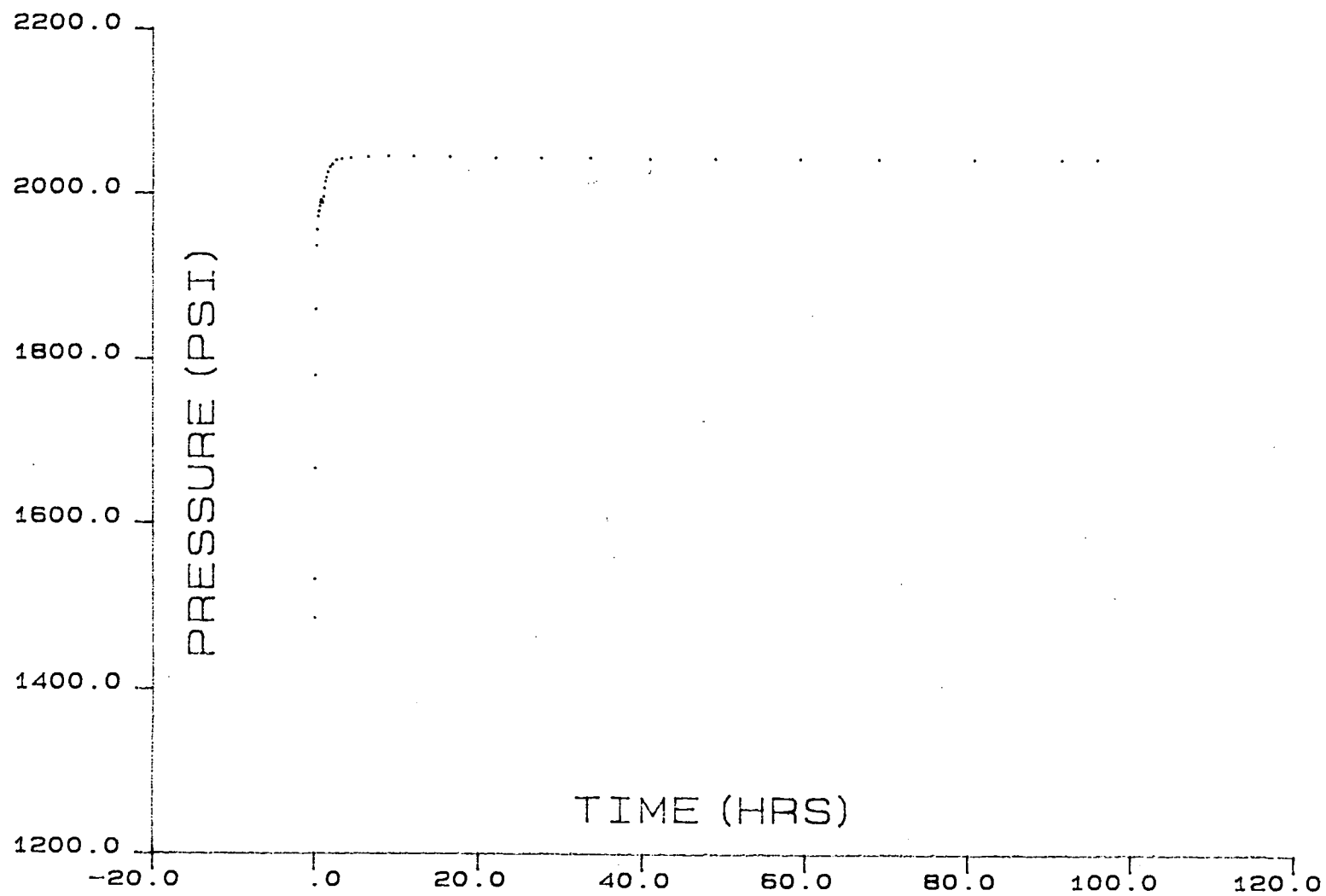
CO.		RUN 01 FIELD KIDMAN	WELL 01
EFF DEPTH		WELL STAT	TOOL HUNG 6573'
CASING	-	CASING PRESS	ON BOTTOM 1044 9/9
LINER	-	TUBING PRESS	OFF BOTTOM 0700 14/9
DATE	890914	ELEMENT RANGE 0 - 3042	ZERO POINT
ELEVATION		ZONE	SHUT-IN 0700 10/9
MAX TEMP	N/A	PICK-UP	ON-PROD
PERF	-	CAL SER NO. 29388	MPP
TUBING	-		
UNITS	ENGLISH	PURPOSE	BUILD-UP

SURVEY DATA

CO.	TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME
	7:00	1485.7	1485.7	.0	8:52	2031.8	2031.8	1.9
	7:00	1532.1	1532.1	.0	9:08	2035.2	2035.2	2.1
	7:03	1666.7	1666.7	.0	9:37	2039.9	2039.9	2.6
	7:05	1780.1	1780.1	.1	10:17	2041.6	2041.6	3.3
	7:08	1860.2	1860.2	.1	11:24	2043.0	2043.0	4.4
	7:11	1937.0	1937.0	.2	13:32	2044.4	2044.4	6.5
	7:17	1956.0	1956.0	.3	15:59	2045.3	2045.3	9.0
	7:24	1971.9	1971.9	.4	19:00	2045.1	2045.1	12.0
	7:29	1978.3	1978.3	.5	23:26	2043.9	2043.9	16.4
	7:34	1984.5	1984.5	.6	5:02	2042.4	2042.4	22.0
	7:38	1989.1	1989.1	.6	10:31	2043.0	2043.0	27.5
	7:42	1991.7	1991.7	.7	16:34	2042.6	2042.6	33.6
	7:47	1991.7	1991.7	.8	23:55	2041.6	2041.6	40.9
	7:51	1989.7	1989.7	.8	7:57	2042.7	2042.7	49.0
	7:56	1988.3	1988.3	.9	18:24	2042.3	2042.3	59.4
	8:01	1995.9	1995.9	1.0	4:10	2041.8	2041.8	69.2
	8:09	2005.8	2005.8	1.2	15:53	2041.9	2041.9	80.9
	8:17	2014.4	2014.4	1.3	2:36	2041.3	2041.3	91.6
	8:23	2018.8	2018.8	1.4	7:00	2042.6	2042.6	96.0
	8:34	2025.3	2025.3	1.6	0:00	.0	.0	.0

LUB IN DWT = 1112 PSI / OUT = 1732 PSI
 LUB IN AMERADA = 1104 PSI / OUT = 1734 PSI

KIDMAN #1 BUILD-UP 10-14/9/89
ELEMENT #29388 (top)



SUB-SURFACE PRESSURE SURVEY

CO. SANTOS		RUN 02 FIELD KIDMAN	WELL 01
EFF DEPTH		WELL STAT	TOOL HUNG 6579'
CASING	-	CASING PRESS	ON BOTTOM 1044 9/9
LINER	-	TUBING PRESS	OFF BOTTOM 0700 14/9
DATE 890914		ELEMENT RANGE 0 - 3020	ZERO POINT
ELEVATION		ZONE	SHUT-IN 0700 10/9
MAX TEMP N/A		PICK-UP	ON-PROD
PERF	-	CAL SER NO. 29386	MPP
TUBING	-		
UNITS ENGLISH		PURPOSE BUILD-UP	

SURVEY DATA

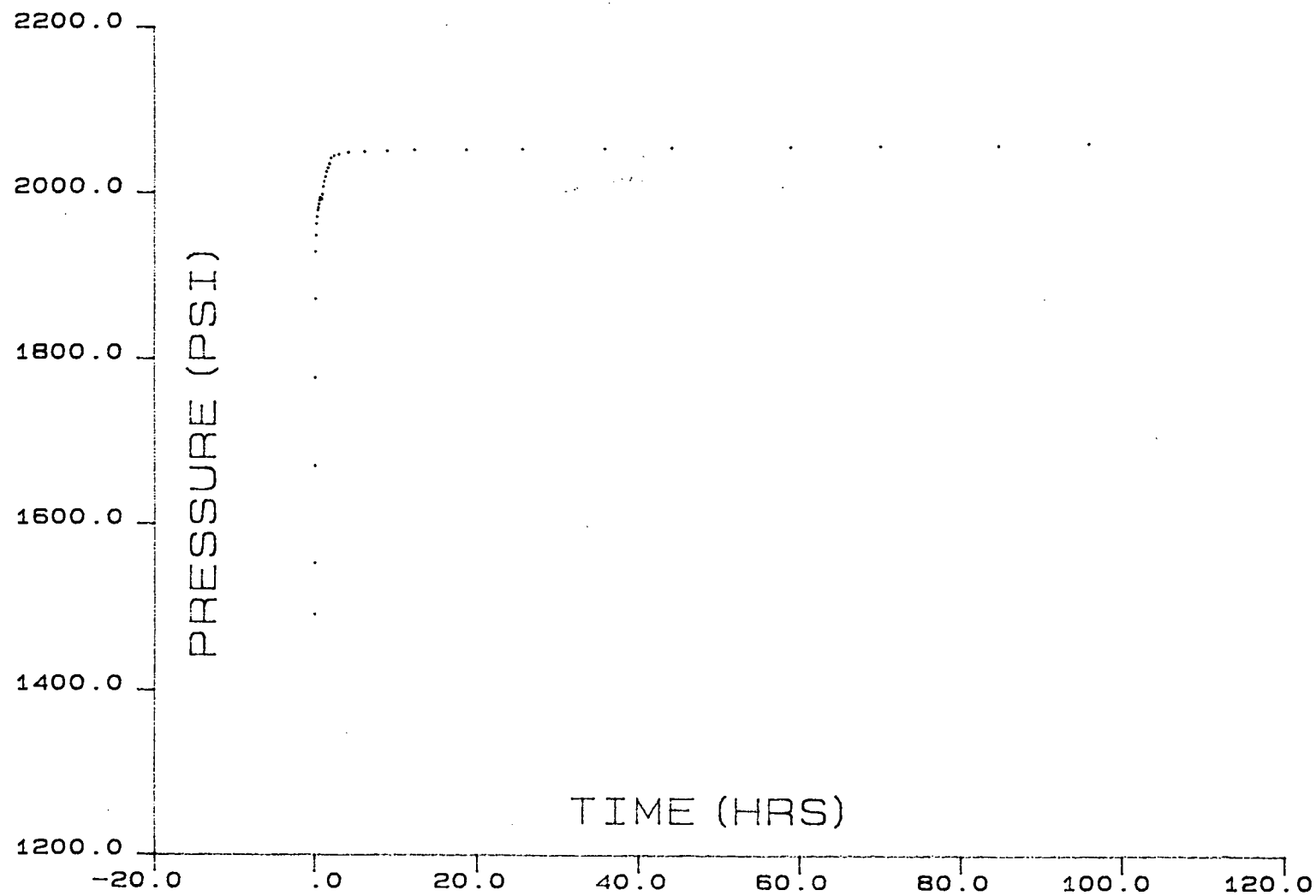
CO. SANTOS		RUN 02 FIELD KIDMAN	WELL 01
TIME	P-T	DP-DT	DTIME
7:00	1490.9	1490.9	.0
7:01	1552.9	1552.9	.0
7:02	1670.3	1670.3	.0
7:05	1777.1	1777.1	.1
7:06	1872.6	1872.6	.1
7:07	1929.2	1929.2	.1
7:10	1948.9	1948.9	.2
7:15	1962.4	1962.4	.2
7:18	1971.1	1971.1	.3
7:23	1978.9	1978.9	.4
7:27	1982.0	1982.0	.5
7:31	1985.9	1985.9	.5
7:35	1990.8	1990.8	.6
7:39	1994.0	1994.0	.7
7:44	1992.8	1992.8	.7
7:49	1992.8	1992.8	.8
7:53	1991.6	1991.6	.9
7:58	1997.7	1997.7	1.0
8:05	2006.7	2006.7	1.1
8:11	2013.4	2013.4	1.2

TIME	P-T	DP-DT	DTIME
8:20	2018.7	2018.7	1.3
8:29	2025.0	2025.0	1.5
8:40	2029.6	2029.6	1.7
8:50	2034.4	2034.4	1.8
9:02	2041.0	2041.0	2.0
9:24	2043.8	2043.8	2.4
10:01	2045.6	2045.6	3.0
11:10	2048.2	2048.2	4.2
13:09	2048.9	2048.9	6.2
15:55	2049.9	2049.9	8.9
19:18	2051.1	2051.1	12.3
1:40	2051.0	2051.0	18.7
8:32	2052.2	2052.2	25.5
18:48	2052.9	2052.9	35.8
3:07	2054.4	2054.4	44.1
17:57	2055.9	2055.9	58.9
5:13	2057.1	2057.1	70.2
19:52	2057.5	2057.5	84.9
7:00	2060.1	2060.1	96.0
0:00	.0	.0	.0

LUB IN DWT = 1112 PSI / OUT = 1732 PSI

LUB IN AMERADA = 1100 PSI / OUT = 1751 PSI

KIDMAN #1 BUILD-UP 10-14/9/89
ELEMENT # 29386 (BOT)



EXPRESS PTX LTD

WIRELINE & WELL TESTING SERVICE

PO BOX 354 COWANDILLA 5033

PH. (08) 354 0488 TELEX AA87183

FAX (08) 43 7408

138 RICHMOND ROAD MARLESTON

SOUTH AUSTRALIA 5033

Tested Thursday, 14th September 1989.

CLIENT	LOCATION	FORMATION
Santos Ltd.	KIDMAN#1	TOOLACHEE

STATIC PRESSURE GRADIENT REPORT

PRESSURE ELEMENT DATA			
POSITION	SERIAL NO.	RANGE	CALIBRATED
Top	29388	3000	12/ 8/89
Bottom	29386	2975	12/ 8/89

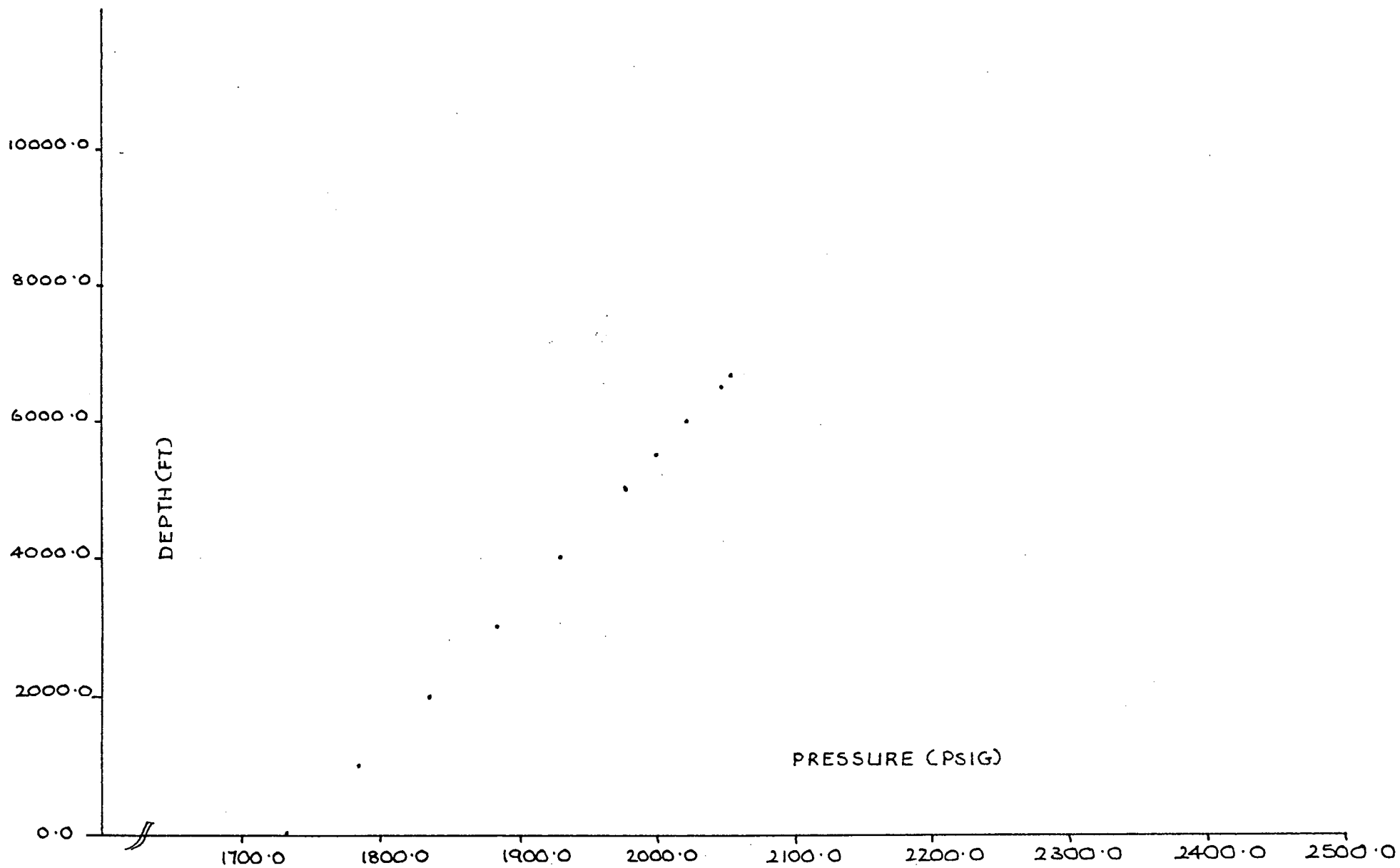
WELL DATA	
PARAMETER	VALUE
DWT In	1732PSI
DWT Out	1732PSI
Max BHT	254°F

DEPTH FT KB	TOP ELEMENT			BOTTOM ELEMENT		
	DEFLECTION INCHES	PRESSURE PSIG	GRADIENT PSI/FT	DEFLECTION INCHES	PRESSURE PSIG	GRADIENT PSI/FT
LUB.	1.1440	1732.1	-----	1.1500	1729.2	-----
1000	1.1780	1784.1	0.052	1.1850	1782.2	0.053
2000	1.2110	1834.6	0.051	1.2190	1833.7	0.052
3000	1.2430	1883.5	0.049	1.2510	1882.2	0.049
4000	1.2740	1930.9	0.047	1.2820	1929.2	0.047
5000	1.3040	1976.8	0.046	1.3140	1977.6	0.049
5500	1.3190	1999.8	0.046	1.3300	2001.9	0.049
6000	1.3340	2022.7	0.046	1.3460	2026.2	0.049
6500	1.3500	2047.2	0.049	1.3620	2050.4	0.049
6674	1.3550	2054.9	0.044	1.3670	2058.0	0.044
LUB.	1.1490	1739.8	-----	1.1540	1735.3	-----

GENERAL REMARKS

TEMP ELEMENT RAN

KIDMAN # 1 — STATIC PRESSURE GRADIENT — 14/9/89
ELEMENT # 29388 / 3000 (TOP)





CLIENT SANTOS

WELL KIDMAN #1

STATIC GRADIENT SURVEY

OPERATOR A. SMITH

DATE 14.9.89

BOMB No 1 DATA						BOMB No 2 DATA				DWT IN 11942 KPA DWT OUT 11942 KPA	
ELEMENT No. <u>29388</u>		ELEMENT RANGE <u>3000 PSI</u>				ELEMENT No. <u>29386</u>		ELEMENT RANGE <u>2975 PSI</u>			
RECORDER No. <u>61001</u>		CLOCK DATA <u>2360 x3HR</u>				RECORDER No. <u>61373</u>		CLOCK DATA <u>2279 x3HR</u>			
ENGAGE STYLUS <u>0935</u>		DISENGAGE <u>1130</u>				ENGAGE STYLUS <u>0935</u>		DISENGAGE <u>1130</u>			
PRESSURE LUBRICATOR <u>0938</u>						BLEED LUBRICATOR <u>1126</u>					
DATE	TIME	DEPTH'	DEFLEC- TION	PRESSURE TEMP.	GRADIENT psi/ft	DEPTH'	DEFLEC- TION	PRESSURE TEMP.	GRADIENT psi/ft	REMARKS	
14 TH	SEPTEMBER 1989			KPA				KPA			
	0938	LUB	1.144	11943		LUB	1.150	11923		PRESSURE LUBRICATOR.	
	0953	R.I.H				R.I.H				RUN IN HOLE.	
	0955	1000	1.178			1000	1.185				
	1001	2000	1.211			2000	1.219				
	1007	3000	1.243			3000	1.251				
	1013	4000	1.274			4000	1.282				
	1019	5000	1.304			5000	1.314				
	1025	6000	1.319			5500	1.330				
	1031	6000	1.334			6000	1.346				
	1037	6500	1.350			6500	1.362				
	1043	6674	1.355	14169		6674	1.367	14190		M.P.P.	
	1058	P.O.O.H				P.O.O.H				PULL OUT OF HOLE.	
	1111	LUB	1.149	11996		LUB	1.154	11965		@ LUBRICATOR.	
	1126	BLEED				BLEED				DEPRESSURE LUBRICATOR.	

GENERAL REMARKS: RAN TEMPERATURE ELEMENT 63256 $\times 150^{\circ} \rightarrow 400^{\circ}F$
 RECORDER 61275 $\times 15TLS$
 CLOCK 16080 $\times 3HR$



Well: KIDMAN #1.

Date: 9-9-89

Lubricator Data:

① 1105 / 1749
② 1100 / 1751
C1112 (psi)

Operator A. SMITH

Pressure with D.W.T. In

7667 KPA

Out

11942 C1732 (psi) KPA

Time Pressured

0833

9-9-89

Time Depressed

0917

14-9-89

Time Run in Hole

1033

-11-

Time off Bottom

0700

-1-

Bomb No. 1 Data

Bomb No. 2 Data

Element No. and Range	29388 x 3000 PSI	29386 x 2975 PSI
Recorder No.	61001 x 15 TLS	61373 x 15 TLS
Clock and Lead Screw Data	15306 x 120 HR	15695 x 120 HR
Engage Stylus	Date: 9.9.89 Time: 0826	Date: 9.9.89 Time: 0826
Disengage	Date: 14.9.89 Time: 0920	Date: 14.9.89 Time: 0920

Remarks: RAN TEMPERATURE ELEMENT 63256 x 150° → 400°F
 RECORDER 61275 x 15 TLS
 CLOCK 24703 x 120 HR

Well-Head Data for Final Build-up

Date	Time	Hours shut-in Time	KPA Wellhead	KPA Casing	°C Wellhead Temp.	Remarks
9TH	SEPTEMBER 1989					
	0826					
	0833		7612	0	77	ENGAGE STYLUS
	1033		7667		78	PRESSURE LUBRICATOR
	1044		7681		79	R.I.H.
	1100		7722		79	@ HANG DEPTH 6585' KB.
	1130		7771		78	(WELL FLOWING 100%)
	1200		7826		77	
	1230		7860		78	
	1300		7895		77	
	1330		7550		75	
	1400		7171		72	
	1430		7033		74	
	1500		6998		74	
	1530		7033		73	
	1600		5999		75	
	2200		7343		81	FLOW WELL OVERNIGHT
10TH	SEPTEMBER 1989.					DUE TO UNSTABLE WELLHEAD PRESSURE.
	0200		7136		80	
	0600		7067		79	
	0630		7019		78	
	0700		6998		80	S.W.I FOR 96HR BUILDUP.
	0705		10756		78	
	0710		10998	0	71	



0197

Well: KIDMAN #1.Date: 10-9-89

Lubricator Data:

Operator A. SMITH

Pressure with D.W.T. In

Out

Time Pressured

Time Depressed

Time Run in Hole

Time off Bottom

Bomb No. 1 Data

Bomb No. 2 Data

Element No. and Range					
Recorder No.					
Clock and Lead Screw Data					
Engage Stylus	Date:	Time:	Date:	Time:	
Disengage	Date:	Time:	Date:	Time:	

Remarks: REFER TO PAGE # 1. FOR ELEMENT INFORMATION.

Well-Head Data for Final Build-up

Date	Time	Hours shut-in Time	KPA Wellhead	KPA Casing	°C Wellhead Temp.	Remarks
10 TH	SEPTEMBER 1989					
	0715		11204	0	63	
	0730	.5	11446	↑	50	
	0745		11687		46	
	0800	1	11825		42	
	0815		11873		40	
	0830		11915		38	
	0845		11949		36	
	0900	2	11977		34	
	0915		11997		30	
	0930		11997		29	
	0945		11997		29	
	1000	3	11997		28	
	1015		12004		29	
	1030		12004		30	
	1045		12004		31	
	1100	4	12004		31	
	1500		12011		33	
	1900	12	12011		28	
	2300		12018		15	
11 TH	SEPTEMBER 1989					
	0300		12018		11	
	0700	24	12018	↓	13	
	1100		11984	0	17	



0198

Well: KIDMAN #1.Date: 11-9-89

Lubricator Data:

Operator A. SMITH

Pressure with D.W.T. In

Out

Time Pressured

Time Depressed

Time Run in Hole

Time off Bottom

Bomb No. 1 Data

Bomb No. 2 Data

Element No. and Range					
Recorder No.					
Clock and Lead Screw Data					
Engage Stylus	Date:	Time:	Date:	Time:	
Disengage	Date:	Time:	Date:	Time:	

Remarks: REFER TO PAGE #1. FOR ELEMENT INFORMATION.

Well-Head Data for Final Build-up

Date	Time	Hours shut-in Time	KPA Wellhead	KPA Casing	°C Wellhead Temp.	Remarks
11 TH	SEPTEMBER 1989.					
	1500		11962	0	25	
	1900	36	11915		15	
	2300		11942		12	
12 TH	SEPTEMBER 1989.					
	0300		11949		11	
	0700	48	11956		10	
	1100		11956		19	
	1500		11963		25	
	1900	60	11963		18	NOTE: RECORDER
	2300		11956		9	#61275 ON TEMPER-
13 TH	SEPTEMBER 1989.					-ATURE ELEMENT
	0300		11963		9	STOP RUNNING AFTER
	0700	72	11970		10	RUNNING IN THE
	1100		11970		18	HOLE DUE TO STICKY
	1500		11956		29	LEAD SCREW & -
	1900	84	11949		17	PROBLEM REPAIRED.
	2300		11942		11	
14 TH	SEPTEMBER 1989.					
	0300		11942		10	
	0700	96.	11935		9	P.O.O.H. (BUILDUP FINISHED).
	0717		11935		9	@ LUBRICATOR.
	0917		11942		17	DEPRESSURE LUBRICATOR.
	0920					DISENGAGE STYLUS,

RECOVER CHARTS, RELOAD ELEMENTS WITH 3HR.

CLOCKS & PERFORM STATIC GRADIENT SURVEY

WIRELINE REPORT

CLIENT SANTOS WELL KIDMAN #1 DATE 8-9-89

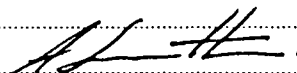
PROGRAMME DUMMY RUN.
PURPOSE OF WORK TO ENSURE TUBING IS FREE OF ANY OBSTRUCTION
FOR B.H.P. SURVEY.

REPORT OF WORK PERFORMED 8TH SEPTEMBER 1989.
1320 : ARRIVE ON LOCATION, S.W.I & RIG UP WIRELINE EQUIPMENT.
1340 : R.I.H WITH 1.75 " BLIND BOX
1355 : TAG P.B.T.D @ 7084' KB. (TUBING CLEAR) & P.O.O.H.
1415 : @ LUBRICATOR, RIG OUT TOOLSTRING & OPEN WELL 100%.
9TH SEPTEMBER 1989.

1033 : R.I.H WITH 2 PRESSURE ELEMENTS & 1 TEMPERATURE
ELEMENT FOR B.H.P SURVEY.
1044 : @ HANG DEPTH 6585' KB. (WELL FLOWING 100%).
10TH SEPTEMBER 1989.

0700 : S.W.I FOR 96 HR BUILD UP AS PER PROGRAMME.
14TH SEPTEMBER 1989.

0700 : P.O.O.H. (BUILD UP COMPLETED).
0717 : @ LUBRICATOR
0917 : DEPRESSURE LUBRICATOR, RECOVER CHARTS, (GOOD) & RELOAD
ELEMENTS WITH 3 HR CLOCKS FOR STATIC GRADIENT.
0953 : R.I.H WITH 2 PRESSURE ELEMENTS & 1 TEMPERATURE ELEMENT
FOR STATIC GRADIENT SURVEY.
1130 : SURVEY COMPLETED, RIG DOWN WIRELINE EQUIPMENT
& HAND WELL BACK TO PRODUCTION.



Operator's Signature

WORKED PERFORMED BY A. SMITH OF EXPERTEST

WELL DATA:

Tubing Size 3 1/2" FWHP 6800 KPA SIWHP
Subsurface S.V./Landing Nipple @ S.S.D. @
'X' Nipple @ 'N'/'X' Nipple @ 6535' KB Other @
Min. I.D. 2.205" @ 6535' KB Packer @ 6517' KB
Perforated Interval: TOOLACHEE F.M 6605' KB → 6742' KB.