

SOUTH AUSTRALIA
DEPARTMENT OF MINES AND ENERGY



OPEN FILE ENVELOPE NO. 2007

PPL 4, MOOMBA BLOCK
EROMANGA AND COOPER BASINS

BIG LAKE 4
TEST REPORTS

Submitted by
Delhi International Oil Corporation

1989

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SCANNED

ENVELOPE 2007

TENEMENT: PPL 4, Moomba Block; Eromanga and Cooper Basins

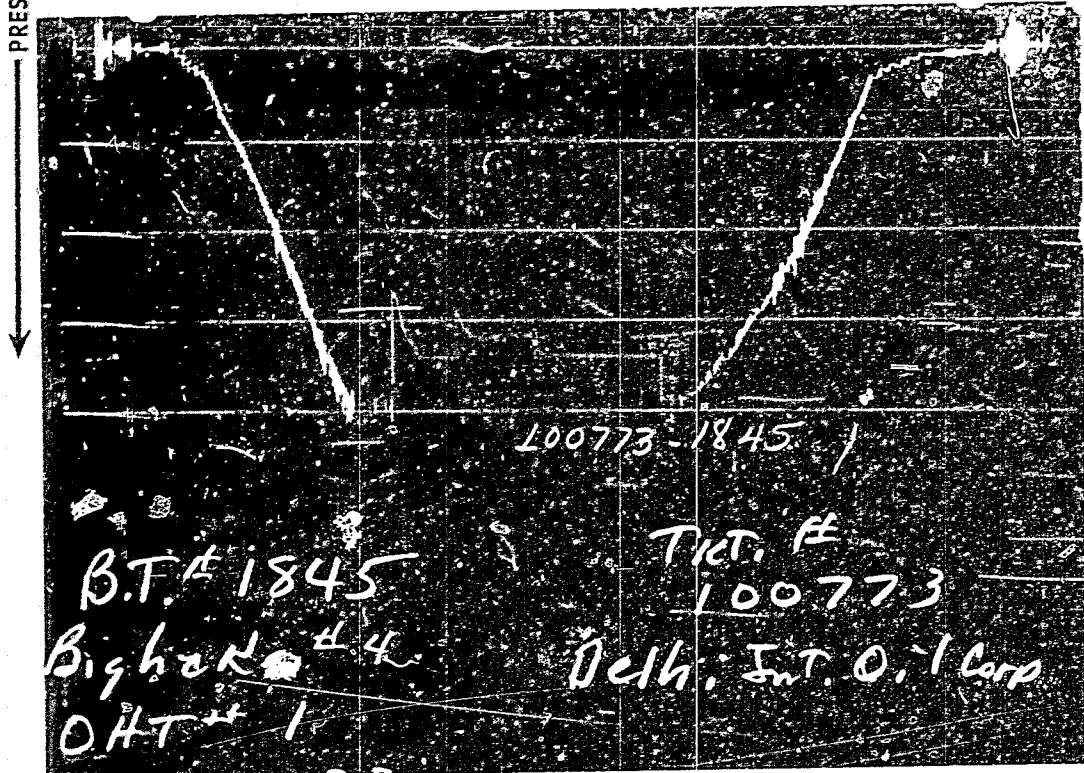
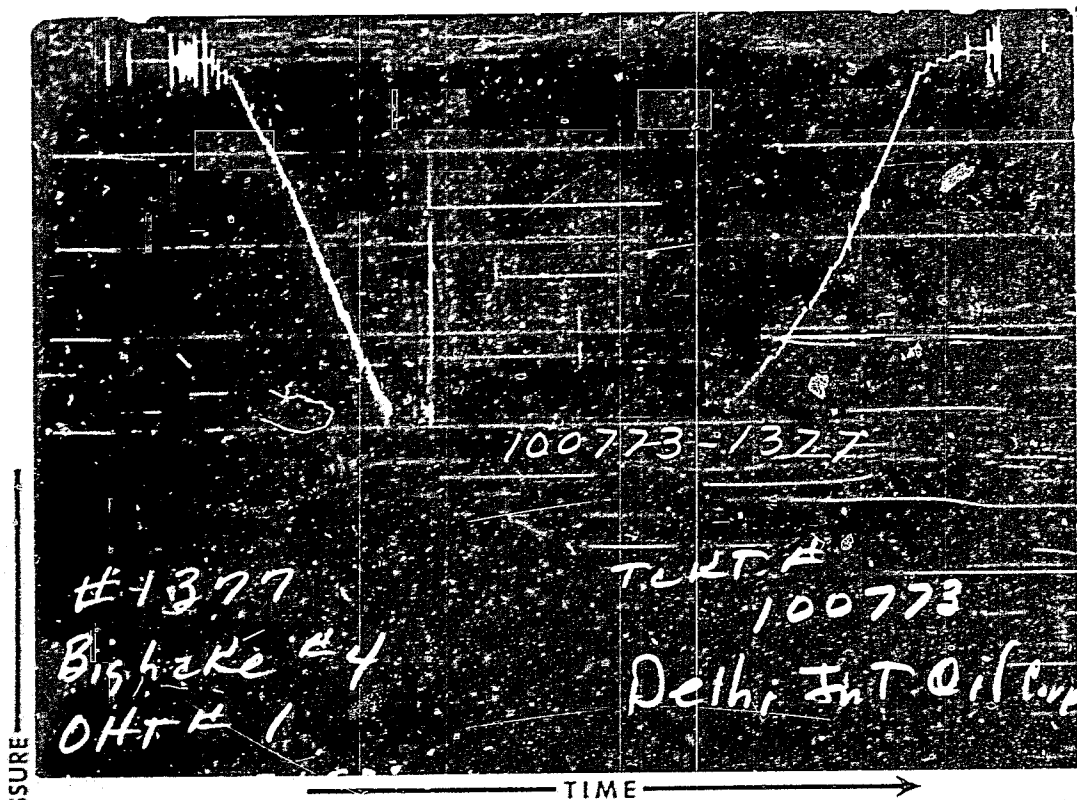
TENEMENT HOLDER: Delhi International Oil Corporation (operator), Santos Ltd and Vamgas Ltd

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	SADME NO.
REPORTS:	
Halliburton Services, 1972. Formation testing service report - DST 1 (31 July 1972).	2007 R 1 Pgs 3-7
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Halliburton Services, 1972. Formation testing service report - DST 3 (8 August 1972).	2007 R 3 Pgs 13-18
Halliburton Services, 1972. Formation testing service report - DST 4 (14 August 1972).	2007 R 4 Pgs 19-23
Delhi International Oil Corporation, 1972. DST evaluation - DST 1 (31 July 1972).	2007 R 5 Pgs 24-27
Delhi International Oil Corporation, 1972. DST evaluation - DST 2 (2 August 1972).	2007 R 6 Pgs 28-31
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Delhi International Oil Corporation, 1972. DST evaluation - DST 4 (14 August 1972).	2007 R 8 Pgs 34-37
Delhi International Oil Corporation, 1973. Summary of gas production test conducted during 27-30 January 1973.	2007 R 9 Pgs 38-57
Delhi International Oil Corporation, 1977. Results of pressure build-up survey and static pressure/temperature gradient, 29 September 1977.	2007 R 10 Pgs 58-60
Kay, B. and Dove, K., 1986. Results of pressure build-up survey and static pressure/temperature gradient, 22 August - 4 September 1986 (Expertest Pty Ltd).	2007 R 11 Pgs 61-75
Santos Ltd, 1987. DST and production water analyses, Toolachee/Daralingie reservoir (July 1972 - June 1987).	2007 R 12 Pgs 76-84
Pidcock, C.L., 1988. Production logging survey, 6 February 1987 (Santos Ltd Reservoir Engineering Department report no. RE:077/87, January 1988).	2007 R 13 Pgs 85-101
Johns, D., 1987. Results of pressure build-up and static pressure gradient survey , 26 August - 4 September 1987 (Expertest Pty Ltd).	2007 R 14 Pgs 102-114

	SADME NO.
REPORTS:	
Douglas, P. and Bond, W., 1989. Results of pressure build-up survey and static pressure/temperature gradient, 1-7 September 1989 (Expertest Pty Ltd).	2007 R 15 Pgs 115-127
Challenger Geological Services. Core photographs, cores 1 and 2.	2007 R 16 Pgs 128-129

END OF CONTENTS



Each Horizontal Line Equal to 1000 p.s.i.

00004

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FORMATION TEST DATA

LITTLE'S

00005

Date Time		Choke Size	Surface Pressure psi	Gas Rate MCF	Liquid Rate BPD	Remarks
14:07						Start B.T. 1845 and clock 10813
14:12						Start BT 1377 and clock 6743'
17:47		1/4				Hydrospring opened in 2 minutes, with a good blow.
17:50		"	1060			Gas to surface in 3 minutes.
17:53		"	1700			
17:56		"	2000			
17:59		"	2290			
18:03		"	2400	3,048	Trace	Closed tool
18:03						Reopened tool with a strong blow.
18:33		7/16"	1050			
18:38		"	1760			
18:43		"	2180			
18:48		"	2200			
18:53		"	2180			
18:58		"	2110			
19:03		"	2080			
19:08		"	2100			
19:13		"	2090			
19:18		"	2110			
19:23		"	2100			
19:28		"	2100			
19:33		"	2100	8,573	Trace	
19:33						Closed tool
21:03						Off bottom

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PRODUCTION TEST DATA

LITTLE'S

Gauge No.		1377	Depth		7514'	Clock No.		6743	12	hour	Ticket No.	100773
First Flow Period		Closed In Pressure		Second Flow Period		Closed In Pressure		Third Flow Period		Closed In Pressure		Time Defl.
Time Defl.	PSIG Temp. Corr.	Time Defl.	PSIG Temp. Corr.	Time Defl.	PSIG Temp. Corr.	Time Defl.	PSIG Temp. Corr.	Time Defl.	PSIG Temp. Corr.	Time Defl.	PSIG Temp. Corr.	Time Defl.
.003"		.000"		.000"		.000"		.000"		.000"		.000"
0	.000 2202	.000	3101	.000	2314	.000	2850	.000	2850			
1	.008 2224*	.0070	3301	.0687	2915	.0069	3288	.0069	3288			
2	.031 2344	.0140	3317	.1374	2910	.0138	3301	.0138	3301			
3	.054 2617	.0210	3324	.2061	2823	.0208	3308	.0208	3308			
4	.077 2913	.0280	3328	.2748	2859	.0277	3312	.0277	3312			
5	.100 3040	.0350	3330	.3435	2859	.0347	3315	.0347	3315			
6	.121 3101	.0420	3335	.4120	2850	.0416	3319	.0416	3319			
7		.0490	3335			.0485	3321	.0485	3321			
8		.0560	3337			.0555	3324	.0555	3324			
9		.0630	3339			.0624	3326	.0624	3326			
10		.0700	3342			.0693	3328	.0693	3328			
11		.0980	3344			.2080	3339	.2080	3339			
12		.1260	3346			.3467	3344	.3467	3344			
13		.1540	3348			.4853	3346	.4853	3346			
14		.1820	3348			.6240	3348	.6240	3348			
15		.2030	3348			.6310	3348	.6310	3348			

Gauge No.		1845	Depth		7681'	Clock No.		10813	12	hour	Minutes
First Flow Period		Closed In Pressure		Second Flow Period		Closed In Pressure		Third Flow Period		Closed In Pressure	
Time Defl.	PSIG Temp. Corr.	Time Defl.	PSIG Temp. Corr.	Time Defl.	PSIG Temp. Corr.	Time Defl.	PSIG Temp. Corr.	Time Defl.	PSIG Temp. Corr.	Time Defl.	PSIG Temp. Corr.
.003"		.000"		.000"		.000"		.000"		.000"	
0	.000 2686	.000	3286	.000	2886	.000	3168	.000	3168		
1	.007 2707*	.0068	3370	.0673	3148	.0068	3343	.0068	3343		
2	.029 2852	.0136	3382	.1346	3198	.0135	3355	.0135	3355		
3	.051 3084	.0204	3389	.2019	3182	.0203	3361	.0203	3361		
4	.073 3180	.0273	3391	.2692	3166	.0271	3366	.0271	3366		
5	.095 3259	.0341	3395	.3365	3177	.0338	3370	.0338	3370		
6	.117 3286	.0410	3398	.4040	3168	.0406	3373	.0406	3373		
7		.0478	3400			.0474	3375	.0474	3375		
8		.0546	3402			.0542	3377	.0542	3377		
9		.0614	3404			.0609	3380	.0609	3380		
10		.0683	3407			.0676	3382	.0676	3382		
11		.0955	3409			.2031	3389	.2031	3389		
12		.1229	3411			.3384	3391	.3384	3391		
13		.1502	3411			.4738	3395	.4738	3395		
14		.1775	3411			.6092	3398	.6092	3398		
15		.1980	3411			.6160	3399	.6160	3399		

Reading Interval .3 ** 10 ***

REMARKS: * First interval equal to 1 minute ** First 10 intervals equal to 1 minute each; next 4 intervals equal to 4 minutes each; last interval equal to 3 minutes. *** First 10 intervals equal to 1 minute each; next 4 intervals equal to 20 minutes each; last interval equal to 1 minute.

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SPECIAL PRESSURE DATA

LITTLE'S

100773

00007

	O.D.	I.D.	LENGTH	DEPTH
Reversing Sub	6"	3"	1.00'	
Water Cushion Valve				
Drill Pipe	5"	4.276"	7116'	
Drill Collars	6.00"	2 7/8"	383'	
Handling Sub & Choke Assembly	5.87"	5/8"	2.60'	
Dual CIP Valve	5"	.87"	4.00'	
Dual CIP Sampler				
Hydro-Spring Tester	5"	.75"	5.00'	7512'
Multiple CIP Sampler				
Extension Joint				
AP Running Case	5"		4.05'	7514'
Hydraulic Jar	5"	.87"	3.30'	
VR Safety Joint	5"	1.00"	2.30'	
Pressure Equalizing Crossover				
Packer Assembly	7 3/4"	1.68"	6.15'	7528'
Distributor				
Packer Assembly	7 3/4"	1.68"	6.15'	7534'
Flush Joint Anchor				
Pressure Equalizing Tube				
Blanked-Off B.T. Running Case				
Drill Collars				
Anchor Pipe Safety Joint	5"	1.50"	4.10'	
Packer Assembly X-Over			1.00'	
Packer Assembly				
Anchor Pipe Safety Joint				
Side Wall Anchor				
Drill Collars X Over	6"	2 7/8"	113.00'	
Flush Joint Anchor	5"	2.37"	.85'	
Blanked-Off B.T. Running Case	5"		27.00'	
			4.00'	7681'

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EQUIPMENT DATA

LITTLE B 90216 SM 2/72

00009

FLUID SAMPLE DATA				Date 8-2-72		Ticket Number 100774	
Pressure _____ P.S.I.G. at Surface				Kind of Job OPEN HOLE		Halliburton District MOONBA	
cc Oil _____				Tester F. HARRIS		Witness P. WOOLDRIGE	
cc Water _____						C. MC KAY	
cc Mud _____				Drilling Contractor DRILCON # 2		NM	
Test Liquid cc _____				EQUIPMENT & HOLE DATA			
Gravity _____ ° API @ _____ °F.				Formation Tested Upper Gidgealea			
Gas Oil Ratio _____ cu. ft./bbl.				Elevation 128' Ft.			
RESISTIVITY _____ CHLORIDE CONTENT _____				Net Productive Interval 155' Ft.			
Recovery Water _____ @ _____ °F. _____ ppm				All Depths Measured From Kelly Bushing			
Recovery Mud _____ @ _____ °F. _____ ppm				Total Depth 7840' Ft.			
Recovery Mud Filtrate _____ @ _____ °F. _____ ppm				Main Hole/Casing Size 8 1/2"			
Mud Pit Sample _____ @ _____ °F. _____ ppm				Drill Collar Length 402' I.D. 2 7/8"			
Mud Pit Sample Filtrate _____ @ _____ °F. _____ ppm				Drill Pipe Length 7248' I.D. 4 2/6"			
Mud Weight 10 vis 44 cp				Packer Depth(s) 7679' - 7685' Ft.			
				Depth Tester Valve 7665' Ft.			
Cushion		TYPE	AMOUNT	Depth Back Pres. Valve	Surface Choke	Bottom Choke	
		NONE	NONE	NONE	1 1/4" - 7/16"	5/8"	
Recovered	105	Feet of slightly condensate cut muddy water					
Recovered		Feet of					
Recovered		Feet of					
Recovered		Feet of					
Recovered		Feet of					
Remarks Tool opened @0631; had gas to the surface in 3 minutes. Closed CIP @ 0647; closed for 25 minutes - changed from 1/2" to 7/16" choke - choke manifold was leaking - repaired manifold - closed in for a 93 minute fix closed in pressure. Tool reopened for a 60 minute second flow. Took a 90 minute second closed in pressure. Off bottom @ 10:52..							
TEMPERATURE		Gauge No. 1377		Gauge No. 1845		Gauge No.	
		Depth: 7667' Ft.		Depth: 7836' Ft.		Depth: Ft.	
		12 Hour Clock		12 Hour Clock		Hour Clock	
Est _____ °F.		Blanked Off NO		Blanked Off YES		Blanked Off	
7836' @						Tool A.M.	
Actual 246 °F.						Opened 06:31 P.M.	
		Pressures		Pressures		Tool A.M.	
						Closed 10:52 P.M.	
		Field Office		Field Office		Reported Computed	
						Minutes Minutes	
Initial Hydrostatic		3928	3952	4075	4082		
First Period	Flow Initial	2081	1991	2706	2716		
	Flow Final	3108	3111	3220	3230		
	Closed in	3378	3385	3443	3441	16	17
Second Period	Flow Initial	2516	2577	2807	2843		
	Flow Final	2812	2815	3070	3082	95	93
	Closed in	3383	3372	3448	3434	60	60
Third Period	Flow Initial					90	90
	Flow Final						
	Closed in						
Final Hydrostatic		3928	3930	4075	4043		

Legal Location
Sec. - Twp. - Rng.

BIG LAKE

Lease Name

4

Well No.

2

Test No.

7685' - 7840'

Tested Interval

DEITH INTERNATIONAL OIL CORPORATION

Lease Owner/Company Name

Field Area

COOPER BASIN

County

State SOUTH AUSTRALIA

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FORMATION TEST DATA

LITTLE'S

Date		Choke	Surface	Gas	Liquid	Remarks
Time	a m p m	Size	Pressure psi	Rate MCF	Rate BPD	
0121						B.T. # 1845 - clock 10813 - started
0204						B.T. # 1377 - clock 6743 - started
						Run tool to 5100'
						Waited for daylight
0515						Run tool to the bottom.
0631		1/2"				Hydrospring opened
0634		"	650			Gas to the surface
0637		"	1400			
0640		"	1800			
0643		"	2100			
0646		"	2380	3,023		
0647		"				Closed CIP - REPAIRED CHOKE MANIFOLD.
0822		7/16"	850			Opened CIP
0827		"	1575			
0832		"	2125			
0837		"	2140			
0842		"	2100			
0847		"	2050			
0852		"	2050			
0857		"	2060			
0902		"	2040			
0907		"	2030			
0912		"	2075			
0917		"	2050			
0922		"	2040	8,331		Closed CIP
1052						Off bottom.

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PRODUCTION TEST DATA

LITTLE'S

Gauge No. 1377			Depth 7667'			Clock No. 6743			12 hour Ticket No. 100774								
First Flow Period			First Closed In Pressure			Second Flow Period			Second Closed In Pressure			Third Flow Period			Third Closed In Pressure		
	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.		
0	.000	1991	.000		3111	.000	2577	.000		2815							
1	.021	2095*	.0209		3324	.0695	2901	.0208		3283							
2	.035	2185	.0418		3342	.1390	2856	.0416		3306							
3	.049	2439	.0627		3351	.2085	2838	.0624		3320							
4	.063	2658	.0836		3361	.2780	2845	.0832		3329							
5	.077	2811	.1045		3363	.3475	2820	.1040		3336							
6	.091	2955	.1254		3370	.4170	2815	.1248		3340							
7	.105	3057	.1463		3372			.1456		3347							
8	.119	3111	.1672		3374			.1664		3349							
9			.1881		3376			.1872		3351							
10			.2090		3379			.2080		3354							
11			.2925		3381			.2912		3361							
12			.3760		3383			.3744		3365							
13			.4595		3385			.4576		3367							
14			.5430		3385			.5408		3370							
15			.6470		3385			.6240		3372							

Gauge No. 1845			Depth 7836'			Clock No. 10813			hour 12		
	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	
0	.000	2716	.000		3230	.000	2843	.000		3082	
1	.0206	2759*	.0204		3377	.0682	3093	.0203		3343	
2	.0344	2777	.0408		3395	.1364	3095	.0406		3366	
3	.0482	2891	.0612		3407	.2046	3082	.0609		3377	
4	.0620	2982	.0816		3411	.2728	3084	.0812		3386	
5	.0758	3080	.1020		3418	.3410	3098	.1015		3393	
6	.0896	3145	.1224		3423	.4090	3082	.1218		3400	
7	.1034	3195	.1428		3425			.1421		3405	
8	.1170	3230	.1632		3427			.1624		3409	
9			.1836		3430			.1827		3411	
10			.2040		3432			.2030		3414	
11			.2854		3436			.2842		3420	
12			.3668		3439			.3654		3427	
13			.4482		3439			.4466		3430	
14			.5296		3441			.5278		3432	
15			.6310		3441			.6090		3434	

Reading Interval 2 ** 10 ***

REMARKS: * INTERVAL = 3 MINUTES. ** FIRST 10 READINGS = 3 MINUTES EACH - NEXT 4 READINGS = 12 MINUTES EACH AND THE LAST READING = 15 MINUTES. *** FIRST 10 READINGS = 3 MINUTES EACH AND THE LAST READING = 12 MINUTES.

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SPECIAL PRESSURE DATA

LITTLE'S

00011

	O. D.	I. D.	LENGTH	DEPTH
Reversing Sub	6"	3"	1.00'	
Water Cushion Valve				
Drill Pipe X-OVER	5"	4.276"	7248'	
Drill Collars	6 1/2"	2 7/8"	402'	
Handling Sub & Choke Assembly	5.87"		2.60'	
Dual CIP Valve	5"	.87"	4.00'	
Dual CIP Sampler				
Hydro-Spring Tester	5"	.75"	5.00'	7665'
Multiple CIP Sampler				
Extension Joint				
AP Running Case	5"		4.05'	7667'
Hydraulic Jar	5"	.87"	3.30'	
VR Safety Joint	5"	1.00"	2.30'	
Pressure Equalizing Crossover				
Packer Assembly	7 3/4"	1.68"	6.15'	7679'
Distributor				
Packer Assembly	7 3/4"	1.68"	6.15'	7685'
Flush Joint Anchor				
Pressure Equalizing Tube				
Blanked-Off B.T. Running Case				
Drill Collars				
Anchor Pipe Safety Joint				
Packer Assembly				
Packer Assembly				
Anchor Pipe Safety Joint	5"	1.50"	4.10'	
X-OVER	6"	1.05'		
Side Wall Anchor				
Drill Collars	6 1/2"	2 7/8"	113.00'	
X-OVER	6"		.85'	
Flush Joint Anchor	5"	2.37"	31.00'	
Blanked-Off B.T. Running Case	5"		4.00'	7836'

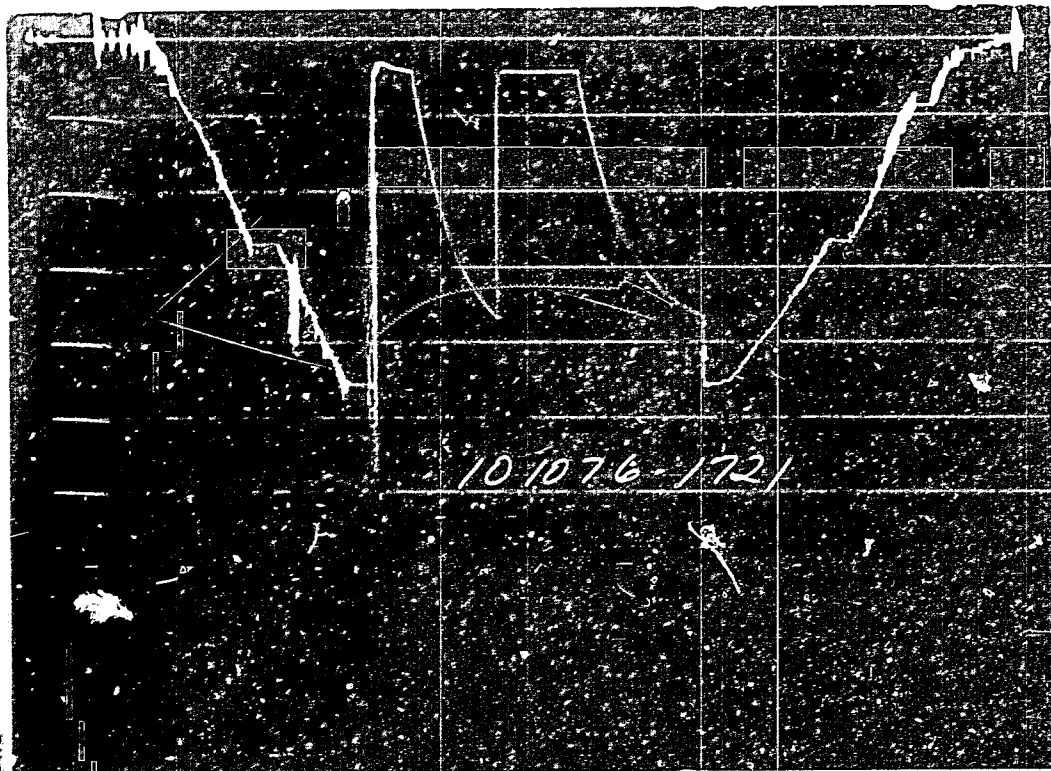
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EQUIPMENT DATA

LITTLE 90216 SM 2/72

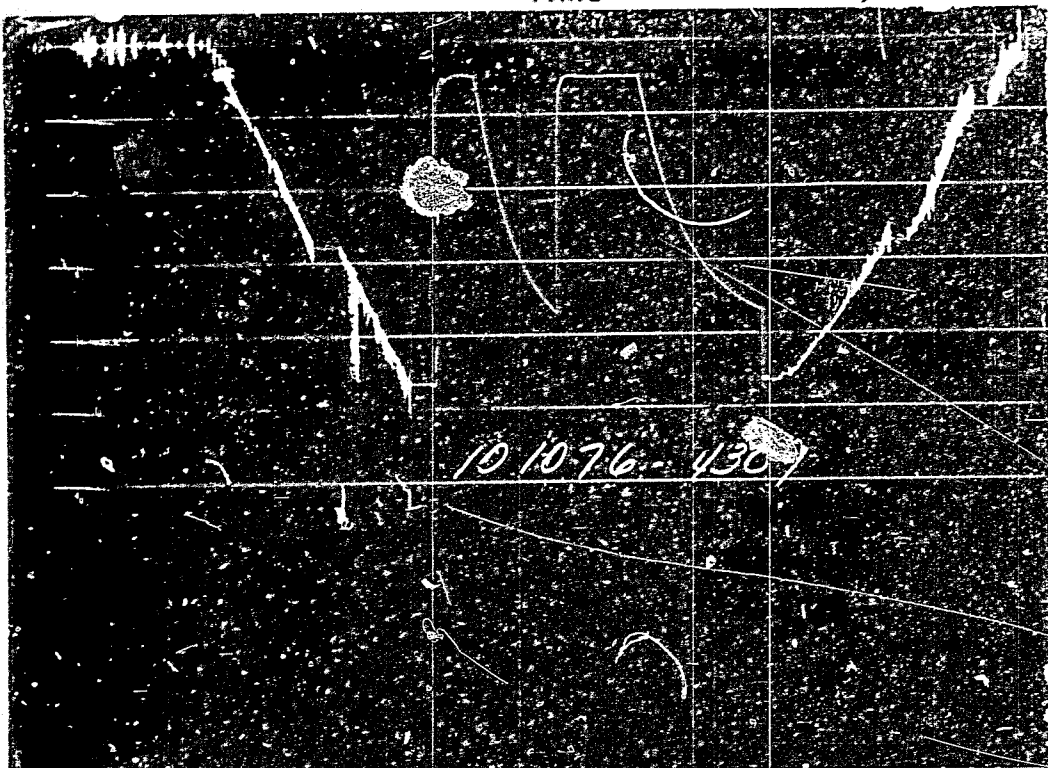
8

PRESSURE



10 1076-1721

TIME



10 1076-430

Each Horizontal Line Equal to 1000 p.s.i.

00014

FLUID SAMPLE DATA				Date 8-8-72		Ticket Number 101076	
Pressure _____ P.S.I.G. at Surface				Kind of Job OPEN HOLE		Halliburton District MOOMBA	
Recovery Cu Ft Gas _____				Tester A. PALMER		Witness G. MC KAY	
cc Oil _____				Drilling Contractor DRILCON R/G # 2 sm S			
cc Water _____				EQUIPMENT & HOLE DATA			
cc Mud _____				Formation Test Patchawarra			
Tot. Liquid cc _____				Elevation 111.1' Gr. 128' KB Ft.			
Gravity _____ * API @ _____ *F.				Net Productive Interval 48' Ft.			
Gas Oil Ratio _____ cu. ft./bbl.				All Depths Measured From Kelly bushing			
RESISTIVITY _____ CHLORIDE CONTENT _____				Total Depth 9200' Ft.			
Recovery Water _____ @ _____ *F. _____ ppm				Main Hole/Casing Size 8 1/2"			
Recovery Mud _____ @ _____ *F. _____ ppm				Drill Collar Length 380' I.D. 2.87"			
Recovery Mud Filtrate _____ @ _____ *F. _____ ppm				Drill Pipe Length 8586' I.D. 3.826"			
Mud Pit Sample _____ @ _____ *F. _____ ppm				Packer Depth(s) 8995-9003' Ft.			
Mud Pit Sample Filtrate _____ @ _____ *F. _____ ppm				Depth Tester Valve 8979' Ft.			
Mud Weight 9.7 vis 47 cp							
TYPE		AMOUNT		Depth Back Pres. Valve		Surface Choke 1/4 & 7/16" Choke 5/8"	
Cushion None							
Recovered 740		Feet of gas cut drilling mud		Meas. from Tester Valve			
Recovered		Feet of					
Recovered		Feet of					
Recovered		Feet of					
Recovered		Feet of					
Remarks Tool opened for 30 minute first flow with moderate blow after 1 minute, flow increased with gas to the surface at 6:35 AM thru 1/4" choke. Closed tool for 60 minute first closed in pressure. Tool reopened for 61 minute second flow thru 7/16" choke, formation flowed for 61 minutes. Closed tool for 91 minute second closed in pressure. SEE PRODUCTION TEST DATA SHEET							
TEMPERATURE		Gauge No. 1721		Gauge No. 4309		Gauge No.	
Depth: 8980 Ft.		Depth: 9197 Ft.		Depth: Ft.		TIME	
12 Hour Clock		12 Hour Clock		Hour Clock		Tool Opened 6:27 A.M.	
Est. *F. Blanked Off no		Blanked Off yes		Blanked Off		Tool Closed 8:57 1/2 P.M.	
Actual 276 *F.		Pressures		Pressures		Pressures	
Field		Office		Field		Office	
Initial Hydrostatic 4552		4563		4639		4667	
Initial 303		4630		475		8020	
Flow Final 386		419		475		480	
Closed in 3677		3679		3686		3745	
Initial 413		512		503		615	
Flow Final 413		413		503		486	
Closed in 3677		3674		3686		3725	
Initial							
Flow Final							
Closed in							
Final Hydrostatic 4552		4557		4639		4633	
Q = Questionable							

Lease Location

BIG LAKE

Lease Name

Well No. 4

Test No. 3

9003 - 9200'

Tested Interval

Field Area

COOPER BASIN

County

State

SOUTH AUSTRALIA

DEIHI INTERNATIONAL OIL CORPORATION

Lease Owner/Company Name

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FORMATION TEST DATA

LITTLE'S

8

00015

Casing perf.		Bottom choke		5/8"		Surf. temp		*F		Ticket No.		101076	
Gas gravity		Delhi GI factor		21		GOR							
Spec gravity		Chlorides		ppm		Res.		@				*F	
Date	8-8-72	Choke	Size	Surface	Pressure	Gas	Rate	Liquid	Rate	Remarks			
Time	a.m. p.m.			psi		MCF		BPD					
1:39 AM		1/4"								Engaged stylus on Bt 4309 and started in hole.			
2:23		"								Engaged stylus on BT 1721.			
3:25		"								Tool through floor.			
6:26		"								Tool on bottom. Packer set.			
6:27		"								Tool opened with moderate blow.			
6:33		"								Blow increased to strong.			
6:35		"		40		69.4				Gas to the surface.			
6:38		"		65		101.1							
6:41		"		85		126.3							
6:44		"		90		132.6							
6:47		"		100		145.2							
6:50		"		115		164.1							
6:53		"		120		170.5							
6:55		"		130		183.0							
6:57		"								Rotated DCIP for closed in period.			
6:59		"		135		189.5							
7:05		"		120		170.5							
7:11		"		100		145.2							
7:14		"		95		138.8							
7:21		"		85		126.3							
7:27		"		70		107.4							
7:30		"		60		94.7							
7:35		"		50		82.1							
7:57		7/16"								Rotated DCIP for second flow period.			
8:02		7/16"		90		425.5							
8:07		7/16"		100		466.0							
8:17		7/16"		100		466.0							

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PRODUCTION TEST DATA

LITTLE'S

8

00016

[illegible]

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PRODUCTION TEST DATA

LITTLE'S

8

Gauge No. 1721			Depth 8980'			Clock No. 6615			12 hour Ticket No. 101076								
First Flow Period			First Closed In Pressure			Second Flow Period			Second Closed In Pressure			Third Flow Period			Third Closed In Pressure		
	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	$\log \frac{t + \theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	$\log \frac{t + \theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	$\log \frac{t + \theta}{\theta}$	PSIG Temp. Corr.		
0	.0000	463	.0000		419	.0000	512	.0000		413							
1	.0328	306	.0412		1101	.0730*	413	.0680**		1312							
2	.0656	328	.0824		1658	.1394	421	.1292		1907							
3	.0984	361	.1236		2107	.2058	419	.1904		2367							
4	.1312	380	.1648		2482	.2722	416	.2516		2723							
5	.1640	397	.2060		2805	.3386	416	.3128		2995							
6	.1970	419	.2472		3057	.4050	413	.3740		3208							
7			.2884		3266			.4352		3367							
8			.3296		3433			.4964		3496							
9			.3708		3570			.5576		3595							
10			.4120		3679			.6190		3674							
11																	
12																	
13																	
14																	
15																	

Gauge No. 4309			Depth 9197'			Clock No. 10813			12 hour		
	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	$\log \frac{t + \theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	$\log \frac{t + \theta}{\theta}$	PSIG Temp. Corr.	
0	.0000	802	.0000		480	.0000	486				
1	.0335	528	.0404		1145	.0738*	480	.0668**		1370	
2	.0670	506	.0808		1696	.1408	492	.1269		1958	
3	.1005	461	.1212		2159	.2079	494	.1870		2413	
4	.1340	455	.1616		2534	.2749	489	.2471		2763	
5	.1675	469	.2020		2852	.3419	489	.3072		3059	
6	.2010	480	.2424		3134	.4090	486	.3673		3269	
7			.2828		3336			.4274		3429	
8			.3232		3501			.4875		3549	
9			.3636		3639			.5476		3650	
10			.4040		3745			.6080		3725	
11											
12											
13											
14											
15											

Reading Interval	5	6	10	9	Minutes
REMARKS:	*First interval is equal to 11 minutes. **10 minutes.				

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SPECIAL PRESSURE DATA

LITTLE'S

00017

101076

00018

	O. D.	I. D.	LENGTH	DEPTH
Reversing Sub	7.10"	3"	.98'	
Water Cushion Valve				
Drill Pipe	4 1/2"	3.826"	8586'	
Drill Collars	6.50"	2.87"	380'	
Cross over sub	6.75"	2.80"	1'	
Handling Sub & Choke Assembly	5.87"	5/8"	2.68'	
Dual CIP Valve	5.03"	.87"	4'	
Dual CIP Sampler				
Hydro-Spring Tester	5"	.75"	5.01'	8979'
Multiple CIP Sampler				
Extension Joint				
AP Running Case	5"	3.06"	4.05'	8980'
Hydraulic Jar	5.03"	1.75"	5'	
VR Safety Joint	5"	1"	2.23'	
Pressure Equalizing Crossover				
Packer Assembly	7 3/4"	1.68"	5.95'	8995'
Distributor	5"	1.68"	1.99'	
Packer Assembly				
Flush Joint Anchor				
Pressure Equalizing Tube				
Blanked-Off B.T. Running Case				
Drill Collars				
Anchor Pipe Safety Joint				
Packer Assembly	7 3/4"	1.68"	5.95'	9003'
Packer Assembly				
Anchor Pipe Safety Joint	5"	1.50"	4'	
Side Wall Anchor				
Cross over sub	6.50"	2.50"	1.05'	
Drill Collars	6.50"	2.87"	140.25'	
Cross over sub	6.60"	2.38"	.82'	
Flush Joint Anchor	5.00"	2.37"		
Blanked-Off B.T. Running Case	5"	2.44"	4.05'	9197'

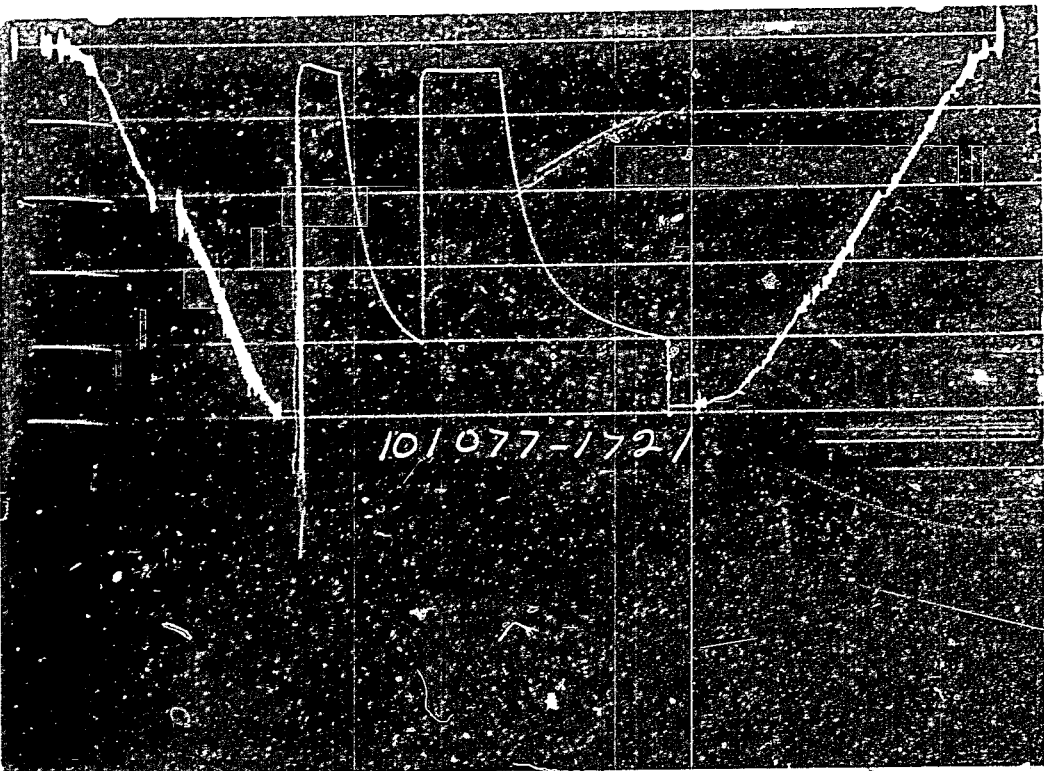
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EQUIPMENT DATA

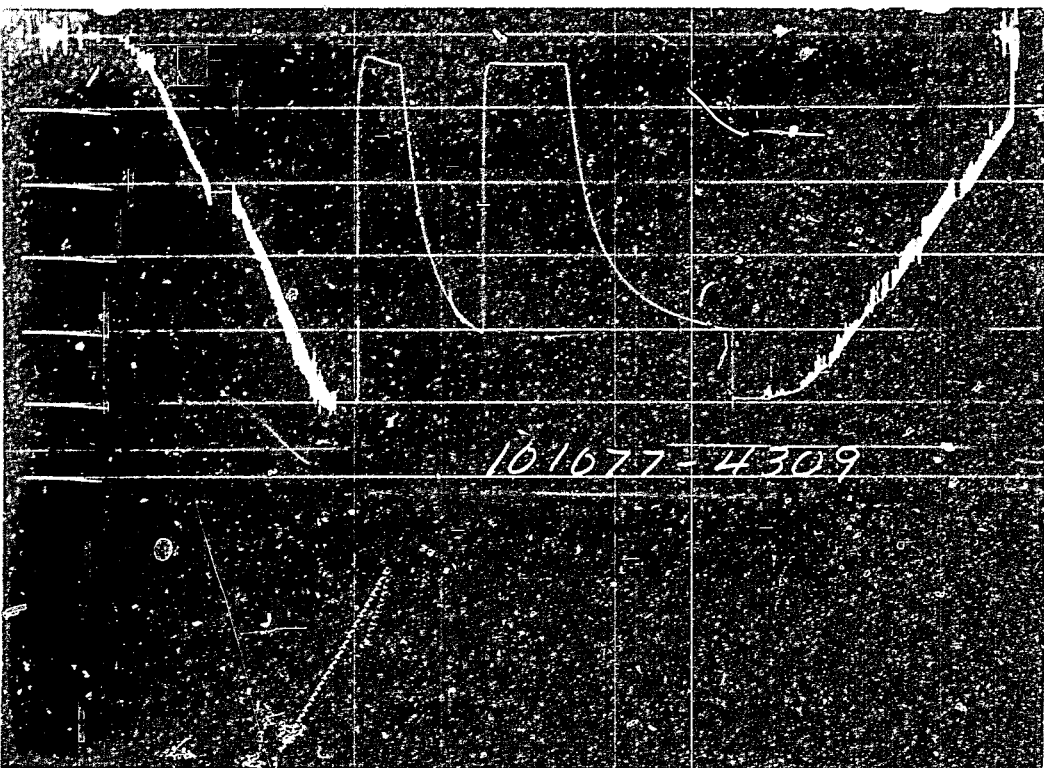
LITTLE'S 90216 SH 2/72

8

PRESSURE



PRESSURE



Each Horizontal Line Equal to 1000 p.s.i.

00020

FLUID SAMPLE DATA						Date 8-14-72		Ticket Number 101077	
Pressure _____ S.I.G. at Surface						Kind of Job OPEN HOLE		Halliburton District MOOMBA	
Cu Ft Gas _____						Tester MR. SCOTT		Witness MR. GALE	
cc Oil _____						Drilling Contractor DRILLING CONTRACTORS RIG # 2 DR 9			
cc Water _____						EQUIPMENT & HOLE DATA			
cc Mud _____						Formation Tested Tirrawarra			
Tot Liquid cc _____						Elevation 128' KB 111.1' Ground Ft.			
Gravity _____ * API @ _____ * F.						Net Productive Interval 119' Ft.			
Gas Oil Ratio _____ cu. ft./bbl.						All Depths Measured From Kelly Bushing			
						Total Depth 9905' Ft.			
RESISTIVITY CHLORIDE CONTENT						Main Hole/Casing Size 8 1/2"			
Recovery Water @ _____ *F. _____ ppm						Drill Collar Length 430' I.D. 2.87"			
Recovery Mud @ _____ *F. _____ ppm						Drill Pipe Length 9299' I.D. 3.826"			
Recovery Mud Filtrate @ _____ *F. _____ ppm						Packer Depth(s) 9757'-9765' Ft.			
Mud Pit Sample @ _____ *F. _____ ppm						Depth Tester Valve 9740' Ft.			
Mud Pit Sample Filtrate @ _____ *F. _____ ppm									
Mud Weight 9.8 vis 40 cp									
TYPE AMOUNT Cushion None						Depth Back Pres. Valve		Surface Choke 1/4-7/16" Bottom Choke 5/8"	
Recovered 700 Feet of slightly gas cut mud						Med. from Tester Valve			
Recovered _____ Feet of _____									
Recovered _____ Feet of _____									
Recovered _____ Feet of _____									
Recovered _____ Feet of Q-QUESTIONABLE									
Remarks SEE PRODUCTION TEST DATA SHEET									
TEMPERATURE		Gauge No. 1721 Depth 9742 Ft. 12 Hour Clock Blanked Off NO	Gauge No. 4309 Depth 9901 Ft. 12 Hour Clock Blanked Off YES	Gauge No. _____ Depth _____ Ft. Hour Clock Blanked Off	TIME				
Est. _____ *F.						Tool _____ A.M. Opened 13:40 P.M.			
Actual 295 *F.		Pressures		Pressures		Tool _____ A.M. Closed 18:11 P.M.			
		Field Office	Field Office	Field Office		Reported Computed			
Initial Hydrostatic 4907		4923	5003	5003			Minutes Minutes		
First Period	Flow Initial 248	873Q	307	1064Q					
	Final 413	408	419	422					
	Closed In 4060	4041	4078	4050					
Second Period	Flow Initial 358	713Q	391	712Q					
	Final 386	388	419	402					
	Closed In 4005	4003	3994	4011					
Third Period	Flow Initial								
	Final								
	Closed In								
Final Hydrostatic 4907		4915	4947	4950					

BIG LAKE
 Lease Name
 Well No. 4
 Test No. 4
 Field Area COOPER BASIN
 Tested Interval
 County AUSTRALIA
 State SOUTH AUSTRALIA
 DEIHI INTERNATIONAL OIL CORPORATION
 Lease Owner/Company Name

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 FORMATION TEST DATA

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FORMATION TEST DATA

LITTLE'S

8

00021

Date		Choke	Surface	Gas	Liquid	Remarks
Time	a.m. p.m.	Size	Pressure psi	Rate MCF	Rate BPD	
09:45						Stylus engaged bottom BT 4309'
						Clock #7588
10:32						Stylus engaged top BT 1721
						Clock # 7582
10:40						Start tools in hole
13:22						Tag bottom and make up head
13:40		1/4"				Hydrospring open with a weak blow
		1/4"				developing into a fair blow
13:49		1/4"	20	44		Gas to surface
13:55		1/4"	40	69		After this reading I exchanged the
						3000 lbs. gauge with 600 lbs. gauge on
						the control head.
14:00		1/4"	80	120		
14:03		1/4"	100	146		
14:06		1/4"	110	158		
14:09		1/4"	125	177		
14:11						Closed tool for initial closed in period
15:11		7/16"				Opened tool for second flow
15:16		7/16"	90	426		
15:21		7/16"	105	436		
15:26		7/16"	110	507		
15:31		7/16"	110	507		The surface pressure stabilized at 110
						PSI for the remainder of flow period.
16:11						Closed tool for final closed in
18:11						Came off bottom, dismantled head and
						started out of hole.

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PRODUCTION TEST DATA

LITTLE'S

8

Gauge No. 1721			Depth 9742'			Clock No. 7582			12 hour Ticket No. 101077								
First Flow Period			First Closed In Pressure			Second Flow Period			Second Closed In Pressure			Third Flow Period			Third Closed In Pressure		
	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	Temp. Corr.		
0	.000	873 Q	.000		408	.000	713 Q	.000		388							
1	.0459	284*	.0342		1293**	.0667	380	.0815		1951							
2	.0787	295	.0753		2107	.1334	388	.1630		2740							
3	.1115	331	.1164		2677	.2001	388	.2445		3186							
4	.1443	353	.1575		3096	.2668	388	.3260		3452							
5	.1771	383	.1986		3394	.3335	388	.4075		3622							
6	.2100	408	.2397		3597	.4000	388	.4890		3740							
7			.2808		3759			.5705		3830							
8			.3219		3877			.6520		3901							
9			.3630		3967			.7335		3956							
10			.4040		4041			.8150		4003							
11																	
12																	
13																	
14																	
15																	

Gauge No. 4309			Depth 9901'			Clock No. 7588			12 hour						
	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $\frac{t+\theta}{\theta}$	Temp. Corr.
0	.000	10640	.000		422	.000	712 Q	.000		402					
1	.0473	304*	.0342		1368*	.069	391	.0826		2017					
2	.0811	316	.0753		2156	.138	402	.1652		2791					
3	.1149	346	.1164		2729	.207	402	.2478		3213					
4	.1487	374	.1575		3120	.276	402	.3304		3468					
5	.1825	399	.1986		3412	.345	402	.4130		3636					
6	.2160	422	.2397		3625	.414	402	.4956		3756					
7			.2808		3773			.5782		3843					
8			.3219		3894			.6608		3910					
9			.3630		3980			.7434		3966					
10			.4040		4050			.8260		4011					
11															
12															
13															
14															
15															

Reading Interval 5 6 10 12 Minutes

REMARKS: * First interval equal to 7 minutes **-5 minutes.
Q-QUESTIONABLE

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SPECIAL PRESSURE DATA

LITTLE'S

00022

101077

00023

	O.D.	I.D.	LENGTH	DEPTH
Reversing Sub	7.10"	3.00"	.98'	
Water Cushion Valve				
Drill Pipe	4½"	3.826"	9299'	
Drill Collars	6.50"	2.87"	430'	
X.O. SUB	6.75"	2.80"	1.00'	
Handling Sub & Choke Assembly	5.87"	5/8"	2.68'	
Dual CIP Valve	5.03"	.87"	4.00'	
Dual CIP Sampler				
Hydro-Spring Tester	5.00"	.75"	5.01'	9740'
Multiple CIP Sampler				
Extension Joint				
AP Running Case	5.00"	3.06"	4.05'	9742'
Hydraulic Jar	5.03"	1.75"	5.00'	
VR Safety Joint	5.00"	1.00"	2.23'	
Pressure Equalizing Crossover				
Packer Assembly	7.75"	1.68"	5.95'	9757'
Distributor	5.00"	1.68"	1.99'	
Packer Assembly	7.75"	1.68"	5.95'	9765'
Flush Joint Anchor				
Pressure Equalizing Tube				
Blanked-Off B.T. Running Case				
Drill Collars				
Anchor Pipe Safety Joint				
Packer Assembly				
Packer Assembly				
Anchor Pipe Safety Joint	5.00"	1.50"	4.00'	
Side Wall Anchor X.O. Sub	6.50"	2.50"	1.05'	
Drill Collars	6.50"	2.87"	85.20'	
X.O. SUB	6.60"	2.38"	.82'	
Flush Joint Anchor	5.00"	2.37"	43.00'	
Blanked-Off B.T. Running Case	5.00"	2.44"	4.05'	9901'

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EQUIPMENT DATA

LITTLE'S 90216 SM 2/72

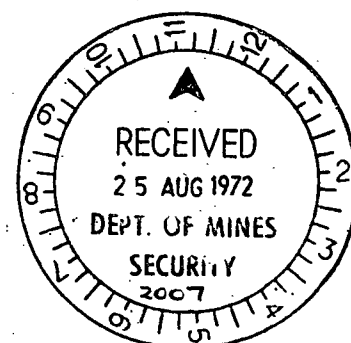
BIG LAKED.S.T. EVALUATION (GAS)Date July 31, 1972 Well No .4 D.S.T. No1Interval Tested .7534' - .7685' Recorder Depth: Top ..7514.. ft.
Bottom ..7682.. ft.Recorder Used: ~~xxx~~ Bottom

COMMENTS:

Valid D.S.T. Unstabilised second flow period. Calculations
have been done and are as follows:

DATA:

Elevation (EL)		<u>..128..</u> ft.
Surface Pressure (P) (1)		<u>.2400..</u> psia
	(2)	<u>.2100..</u> psia
Choke Sizes	(1)	<u>1/4</u> in.
	(2)	<u>7/16</u> in.
Gas Gravity (G)		<u>.0.756</u>
Compressibility Factor (z)		<u>.0.8932</u>
Slopes (m)	Initial	<u>251.000</u> psi ² /cycle
	Final	<u>210.000</u> psi ² /cycle
Well bore Radius (rw)		<u>.0.354</u> ft.
Gas Compressibility (C)		<u>0.000293</u> psi ⁻¹
Surface Temperature (Ts)		<u>...520.</u> °R
Choke Factor (Fp)	(1)	<u>1.143.</u>
	(2)	<u>3.672.</u>



Final Flow Pressure (Pf)	Initial	3279... psig
	Final	3164... psig
Extrapolated Static Pressure (Ps)		
	Initial	3414... psig
	Final	3403... psig
Flow Time (t)		0.0118 days
Total Flow Time (to)		0.0528 days
Gas Viscosity (μ)		0.0204 cps
Temperature (T)		..704. °R
Porosity (ϕ)		...13. %

PRODUCT	EQUATION	INITIAL	FINAL	UNIT
Flow Rate	$Q_g = \frac{F_p \times P}{\sqrt{G} \times T_s} \times 24$	...3308	..9299	MCFD
Transmissability	$\frac{K_h}{\mu} = \frac{1637 \times Q_g z T}{m}$	..13566	45581	md-ft/ cps.
Theoretical Flow Capacity	$K_h = \frac{K_h}{\mu} \times \mu$	277	...930	md-ft
Average Effective Permeability	$K = \frac{K_h}{h}$			
Based on gross sand of: 74 ft.		...3.74	..12.57	md
Based on net sand of: 45 ft.		...6.16	..20.67	md
Indicated Flow Capacity				
$(K_h)_2 = \frac{3200 Q_g \mu z T \text{ Log}(0.472^b / r_w)}{P_s^2 - P_f^2}$		...272	...588	md-ft
Damage Ratio	$\frac{\text{Theoretical Flow Cap}}{\text{Indicated Flow Cap}}$	1.0**	1.5	-

** Not real value

<u>PRODUCT</u>	<u>EQUATION</u>	<u>INITIAL</u>	<u>FINAL</u>	<u>UNIT</u>
Indicated Absolute Open Flow Rate				
Max. OF_1	$= \frac{Q_g P_s^2}{P_s^2 - P_f^2}$	...42669	...69029	MCFD
Min. OF_2	$= \frac{Q_g P_s}{\sqrt{P_s^2 - P_f^2}}$	...11875	...25316	MCFD
Theoretical Absolute Open Flow Potential Rate				
Max. OF_3	$= OF_1 \times DR$	...42669	...103544	MCFD
Min. OF_4	$= OF_2 \times DR$	...11875	...37974	MCFD
Approx. Radius of Investigation				
$b = \sqrt{\frac{Kt}{39.2 \phi \mu c}} \text{ or } \sqrt{\frac{Kt_o}{39.2 \phi \mu c}}$				
Based on gross sand:	74 ft.	...38...	...147...	ft.
Based on net sand:	45 ft.	...49...	...190...	ft.
Potentiometric Surface	$Pot = (EL - GD) + (2.319 P_s)$	...363...	...338...	ft.
Barrier Distance				
$-Ei \frac{(-3793 \text{ ra}^2 \phi \mu c)}{KT} = 2.303 \text{ Log } \frac{T + \theta_a}{\theta_a}$				
		...N/A...	...N/A...	ft.

Where -ra = distance to anomaly in feet

T = flow time in hours

θ_a = shut-in-time at intercept point of two
slopes describing anomaly, hours.

00027

DELHI INTERNATIONAL OIL CORPORATION

WELL BIG LAKE N°4

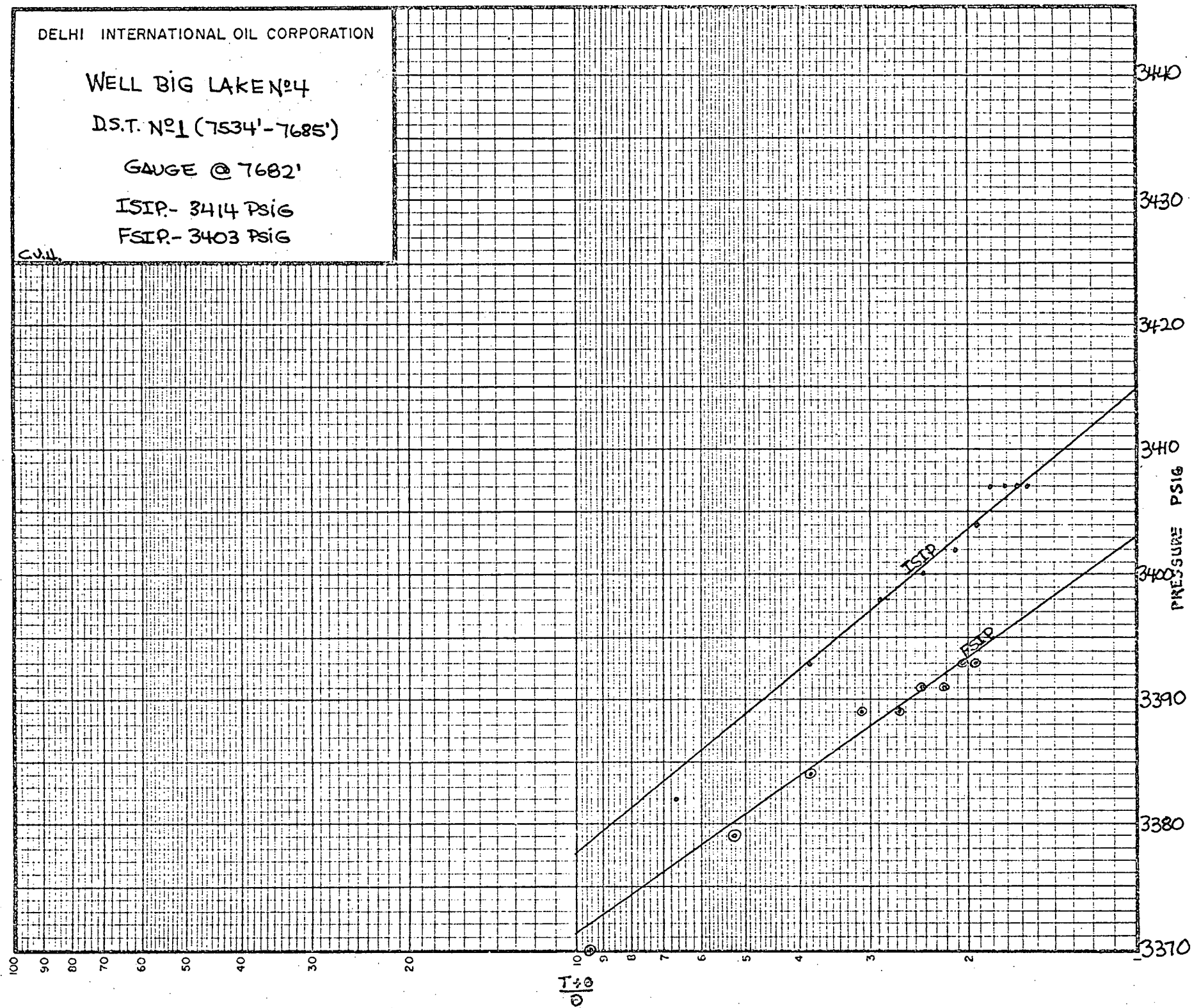
D.S.T. N°1 (7534'-7685')

GAUGE @ 7682'

ISIP- 3414 PSIG

FSIP- 3403 PSIG

C.V.I.



BIG LAKED.S.T. EVALUATION (GAS)

Date August 2, 1972 Well No ...4... D.S.T. No ...2...
Interval Tested 7685-.7840 Recorder Depth: Top ...7667. ft.
Bottom ...7837. ft.
Recorder Used: ~~xxx~~/Bottom

COMMENTS:

Valid D.S.T. Unstabilised second flow period. Calculations
have been done and are as follows:

DATA:

Elevation (EL)	..128. ft.
Surface Pressure (P) (1)	.2380. psia
(2)	.2040. psia
Choke Sizes (1)	.1/4. in.
(2)	.7/16. in.
Gas Gravity (G)	0.756.
Compressibility Factor (z)	0.8959
Slopes (m) Initial	524,000. $\text{psi}^2/\text{cycle}$
Final	443,600. $\text{psi}^2/\text{cycle}$
Well bore Radius (rw)	0.354. ft.
Gas Compressibility (C)	0.000290. psi^{-1}
Surface Temperature (Ts)	..560. $^{\circ}\text{R}$
Choke Factor (Fp) (1)	1.143.
(2)	3.672.

Final Flow Pressure (Pf)	Initial	3227.. psig
	Final	3078.. psig
Extrapolated Static Pressure (Ps)	Initial	3444.. psig
	Final	3445.. psig
Flow Time (t)		0.0118. days
Total Flow Time (to)		0.0535. days
Gas Viscosity (μ)		0.0204. cps
Temperature (T)		706 °R
Porosity (ϕ)		13. %

<u>PRODUCT</u>	<u>EQUATION</u>	<u>INITIAL</u>	<u>FINAL</u>	<u>UNIT</u>
Flow Rate	$Q_g = \frac{Fp \times P}{V_G \times T_s} \times 24$	.3280..	.2034..	MCFD
Transmissability	$\frac{Kh}{\mu} = \frac{1637 \times Q_g zT}{m}$	.6481..	21086..	md-ft/ cps.
Theoretical Flow Capacity	$Kh = \frac{Kh}{\mu} \times \mu$	..132..	..430..	md-ft
Average Effective Permeability	$K = \frac{Kh}{h}$			
Based on gross sand of:	95 ft.	...1.39	..4.53	md
Based on net sand of:	70 ft.	...1.89	..6.14	md
Indicated Flow Capacity	$(Kh_2) = \frac{3200 Q_g \mu zT \text{Log}(0.472^b/rw)}{P_s^2 - P_f^2}$	...147..	...335..	md-ft
Damage Ratio	$\frac{\text{Theoretical Flow Cap}}{\text{Indicated Flow Cap}}$	0.9**	1.2	-

** Not real value

<u>PRODUCT</u>	<u>EQUATION</u>	<u>INITIAL</u>	<u>FINAL</u>	<u>UNIT</u>
Indicated Absolute Open Flow Rate				
Max. OF_1	$= \frac{Q_g P_s^2}{P_s^2 - P_f^2}$	...26886	...44860	MCFD
Min. OF_2	$= \frac{Q_g P_s}{\sqrt{P_s^2 - P_f^2}}$	9414	...20209	MCFD
Theoretical Absolute Open Flow Potential Rate				
Max. OF_3	$= OF_1 \times DR$	...26886	...53832	MCFD
Min. OF_4	$= OF_2 \times DR$	9414	...24251	MCFD
Approx. Radius of Investigation				
$b = \sqrt{\frac{Kt}{39.2 \phi \mu C}} \text{ or } \sqrt{\frac{Kt_o}{39.2 \phi \mu C}}$				
Based on gross sand:	95 ft.	24	90	ft.
Based on net sand:	70 ft.	28	104	ft.
Potentiometric Surface	$Pot = (EL-GD) + (2.319Ps)$	.278...	.280...	ft.
Barrier Distance				
$-Ei \frac{(-3793 \text{ ra}^2 \phi \mu C)}{KT} = 2.303 \text{ Log } \frac{T+\theta_a}{\theta_a}$				
		...N/A..	...N/A..	ft.
Where -ra = distance to anomaly in feet T = flow time in hours θ_a = shut-in-time at intercept point of two slopes describing anomaly, hours.				

00031

DELHI INTERNATIONAL OIL CORPORATION

WELL BIG LAKE N°4

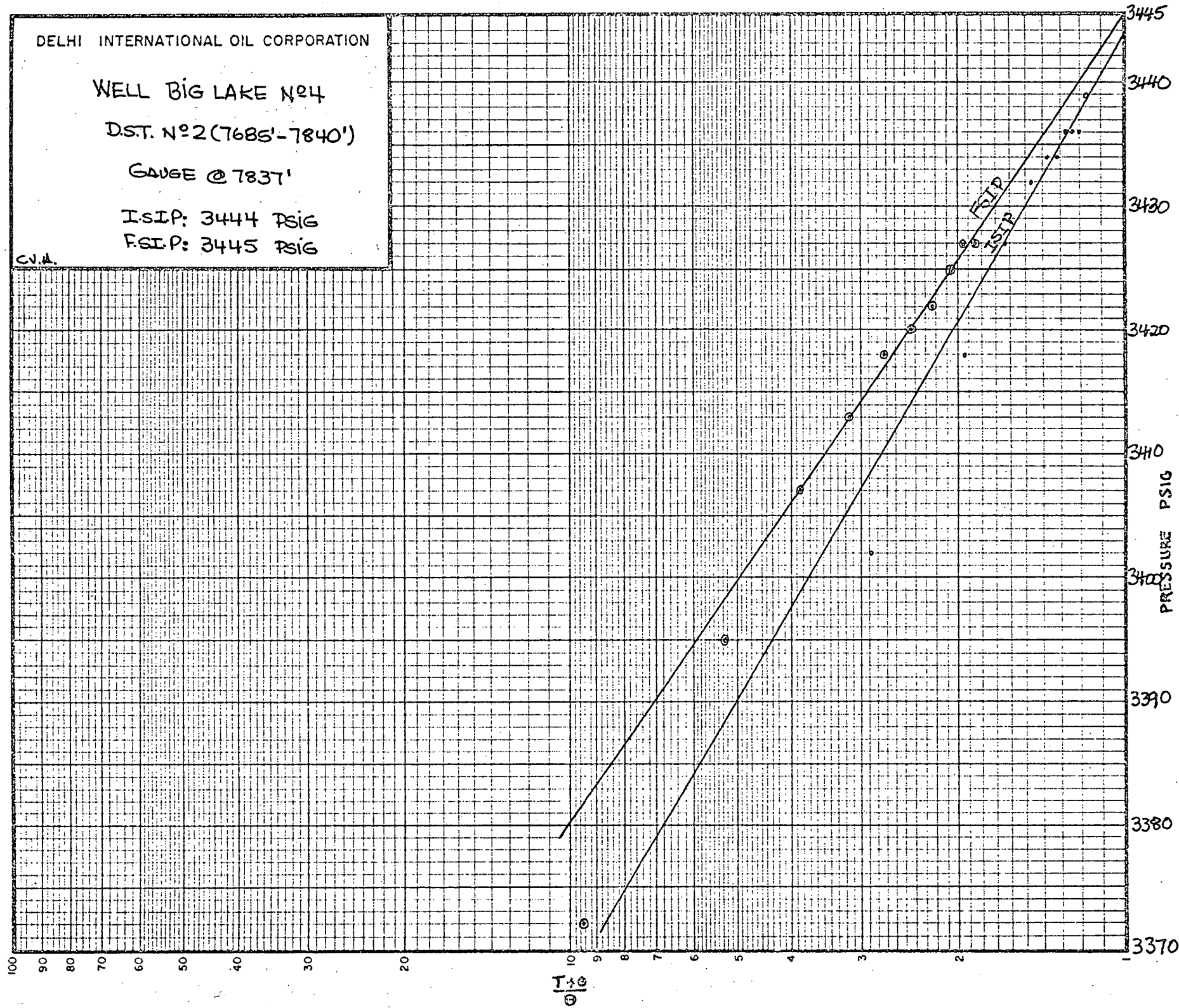
DST. N°2 (7685'-7840')

GAUGE @ 7837'

ISIP: 3444 PSIG

F.S.I.P: 3445 PSIG

C.V.M.



BIG LAKED.S.T. EVALUATION (GAS)

Date August 8, 1972. Well No ...4... D.S.T. No ...3...
Interval Tested 9003.7-9200 Recorder Depth: Top ..8980. ft.
Bottom ..9197.. ft.
Recorder Used: ~~Top~~/Bottom

COMMENTS:

Charts indicated very tight formation. Gas Faro 466 MCFD in last flow period stabilized. Recovered 740 feet of gas cut drilling mud. Calculations have not been done due to insufficient closure in the pressures build-up.

DATA:

Elevation (EL)	..128..	ft.
Surface Pressure (P) (1)		psia
(2)		psia
Choke Sizes (1)	<u>1/4</u>	in.
(2)	<u>7/16</u>	in.
Gas Gravity (G)		
Compressibility Factor (z)		
Slopes (m) Initial		psi ² /cycle
Final		psi ² /cycle
Well bore Radius (rw)	<u>.0.354</u>	ft.
Gas Compressibility (C)		psi ⁻¹
Surface Temperature (Ts)		°R
Choke Factor (Fp) (1)	<u>.1.143</u>	
(2)	<u>.3.672</u>	
Final Flow Pressure (1)	466	psig
(2)	475	psig
Temperature (T)	736	°R

00033

DELHI INTERNATIONAL OIL CORPORATION

WELL BIG LAKE N°4

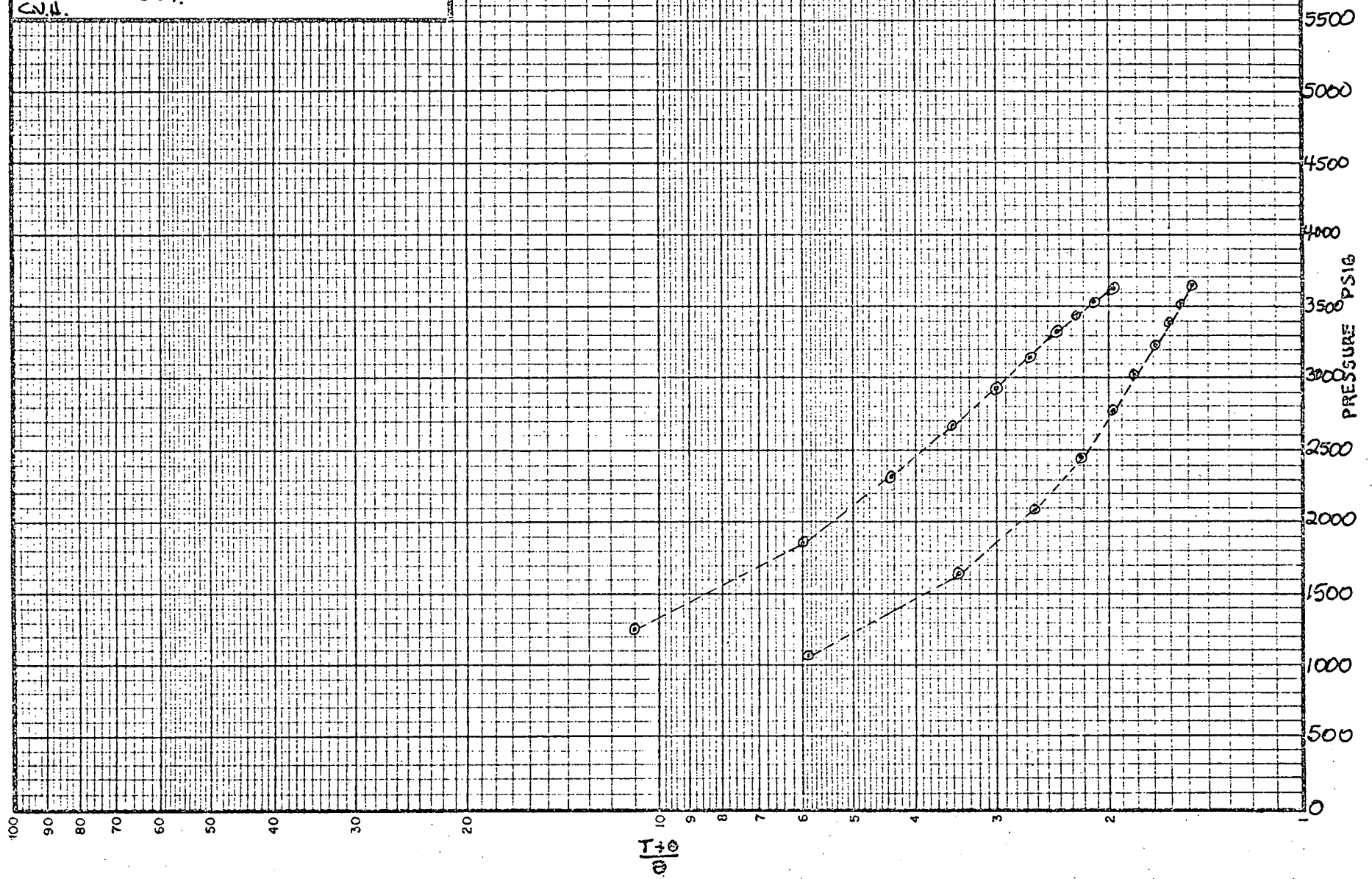
D.S.T. N°3 (9003'-9200')

GAUGE @ 9197'

ISIP —

FSIP —

C.N.



BIG LAKED.S.T. EVALUATION (GAS)

Date August 14, 1972 Well No ...4... D.S.T. No ...4...
 Interval Tested .9765-.9905 Recorder Depth: Top .9742.. ft.
 Bottom .9902... ft.

Recorder Used: ~~Top~~/Bottom

COMMENTS:

Charts indicated very tight formation. Calculations have been done. Recovered 700 feet of slightly gas cut mud.

DATA:

Elevation (EL)		.128.. ft.
Surface Pressure (P) (1)		.140.. psia
	(2)	.125.. psia
Choke Sizes	(1)	.1/4.. in.
	(2)	.7/16.. in.
Gas Gravity (G)		0.756..
Compressibility Factor (z)		0.997..
Slopes (m)	Initial	22,000.000. psi ² /cycle
	Final	17,622.000. psi ² /cycle
Well bore Radius (rw)		0.354. ft.
Gas Compressibility (C)		0.000213. psi ⁻¹
Surface Temperature (Ts)		..580. °R
Choke Factor (Fp)	(1)	1.143.
	(2)	3.672.

Final Flow Pressure (Pf)	Initial	..425. psig
	Final	..397. psig
Extrapolated Static Pressure (Ps)		
	Initial	.4740. psig
	Final	.4650. psig
Flow Time (t)		0.0215. days
Total Flow Time (to)		0.0632. days
Gas Viscosity (μ)		0.0204. cps
Temperature (T)		..755. °R
Porosity (ϕ)		...12. %

<u>PRODUCT</u>	<u>EQUATION</u>	<u>INITIAL</u>	<u>FINAL</u>	<u>UNIT</u>
Flow Rate	$Q_g = \frac{F_p \times P}{\sqrt{G \times T_s}} \times 24$	...183..	..525..	MCFD
Transmissability	$\frac{K_h}{\mu} = \frac{1637 \times Q_g z T}{m}$	11..	...37..	md-ft/ cps.
Theoretical Flow Capacity	$K_h = \frac{K_h}{\mu} \times \mu$	...0.22	..0.75	md-ft
Average Effective Permeability	$K = \frac{K_h}{h}$			
Based on gross sand of:	65 ft.	.0.0034	.0.0115	md
Based on net sand of:	39 ft.	.0.0056	.0.0192	md
Indicated Flow Capacity				
	$(K_h)_2 = \frac{3200 Q_g \mu z T \text{ Log}(0.472^b / r_w)}{P_s^2 - P_f^2}$	.0.20...	1.2...	md-ft
Damage Ratio	$\frac{\text{Theoretical Flow Cap}}{\text{Indicated Flow Cap}}$	1.1	0.6	-

<u>PRODUCT</u>	<u>EQUATION</u>	<u>INITIAL</u>	<u>FINAL</u>	<u>UNIT</u>
Indicated Absolute Open Flow Rate				
Max.	$OF_1 = \frac{Q_g P_s^2}{P_s^2 - P_f^2}$	...184.	...529.	MCFD
Min.	$OF_2 = \frac{Q_g P_s}{\sqrt{P_s^2 - P_f^2}}$	...184.	...527.	MCFD
Theoretical Absolute Open Flow Potential Rate				
Max.	$OF_3 = OF_1 \times DR$	...202.	...529.	MCFD
Min.	$OF_4 = OF_2 \times DR$	...202.	...527.	MCFD
Approx. Radius of Investigation				
$b = \sqrt{\frac{Kt}{39.2 \phi \mu c}} \text{ or } \sqrt{\frac{Kt_o}{39.2 \phi \mu c}}$				
Based on gross sand:	65 ft.	...1:9.	...5:9.	ft.
Based on net sand:	39 ft.	...2:4.	...7:7.	ft.
Potentiometric Surface	$Pot = (EL-GD) + (2.319Ps)$	...1218.	...1009.	ft.
Barrier Distance				
$-Ei \frac{(-3793 \text{ ra}^2 \phi \mu c)}{KT} = 2.303 \text{ Log } \frac{T+\theta_a}{\theta_a}$				
		...N/A...	...N/A...	ft.

Where :-ra = distance to anomaly in feet

T = flow time in hours

θ_a = shut-in-time at intercept point of two
slopes describing anomaly, hours.

00037

DELHI INTERNATIONAL OIL CORPORATION

WELL BIG LAKE N°4

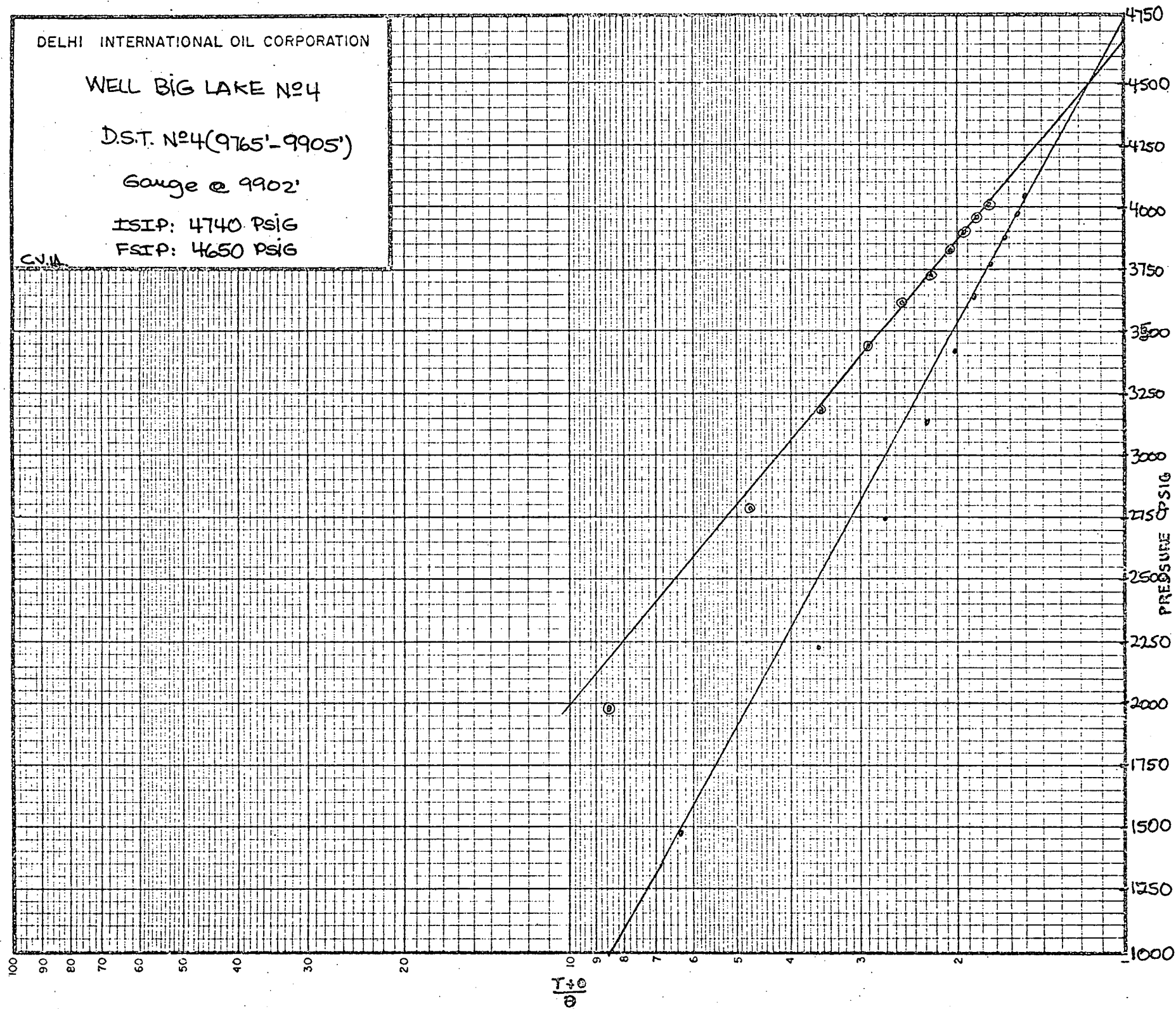
D.S.T. N°4(9765'-9905')

Gauge @ 9902'

ISIP: 4740 PSIG

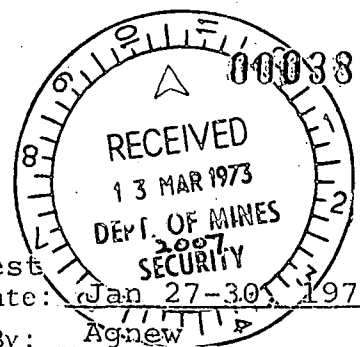
FSIP: 4650 PSIG

C.V. II



DELHI INTERNATIONAL OIL CORPORATION

WELL TEST SUMMARY PAGE 1



Lat $28^{\circ} 15' 29''$ S Test Date: Jan 27-30, 1973
 Well: Big Lake #4 Location: Long 140 14' 18" E
 Field: Big Lake Pool: Toolachee Tested By: Agnew
 Casing Size: 7" OD Weight: 26#/ft Grade: Mxd. Producing Interval: 7586-7914
 Tubing Size: 3 1/2" OD Weight: 9.3#/ft Grade: J55 Producing Through: Tubing
 Well Blown 48 hours Description of Blow: None

Gas Gravity: 0.761 Source: Calc. Mean Annual Surface Temp °F
 Liquid Gravity: Source: B.H. Temp: 282 °F Source: Max. Thermom
 INITIAL SHUT-IN PERIOD Date Shut-In: Jan 25 Time: 1400 Tot. Shut-In 48 hrs.

Time of Observation			Observed Pressures				Wellhead Temp.-OF	Remarks
Date	Time	Shut-In Time Hrs.	Tubing		Casing			
			psig	psia	psig	psia		
Jan 27 1973	1400	48.0	2829	2844				

FLOW PERIODS Approximate Duration of Flow Periods 2 hours

Run No. 1 Duration of Run 2 hrs. Orifice Size 1.75 Meter Run 3.068" ID
 High Pressure Separator - Operating Pressure psig Temp. °F
 Low Pressure Separator - Operating Pressure psig Temp. °F
 Flowed well on 16/64" choke

Date	Time	Flow Time Hours	Wellhead Readings			Meter or Prover Data			Condensate Prod.-Bbls	Water Prod.-Bbls
			Tubing psig	Casing psig	Temp. °F	Pf psia	Hw Ins	Temp. °F		
Jan 27	1430	0.5	2619		110	490	104	60		
	1500	1.0	2608		110	490	108	68		
	1530	1.5	2601		109	490	107	73		
	1600	2.0	2608		113	490	108	83	Nil	1.500

INTERMEDIATE SHUT-IN PERIOD (For use with Isochronal Type Tests)

Date	Time	Shut-In Time Hrs.	Tubing Pressure		Casing Pressure		Wellhead Temp. °F
			psig	psia	psig	psia	
Jan 27	1630	0.5	2836	2851	NOT GIVEN		113
	1700	1.0	2841	2856	"	"	112
	1730	1.5	2845	2860	"	"	111
	1800	2.0	2842	2857	"	"	109

Run No. 2 Duration of Run 2 Hrs. Orifice Size 1.75 Meter Run or Prover Size 3.068
 High Pressure Separator - Operating Pressure psig Temp. °F
 Low Pressure Separator - Operating Pressure psig Temp. °F
 Flowed well on 20/64" choke

Date	Time	Flow Time Hours	Wellhead Readings			Meter or Prover Data			Condensate Prod.-Bbls	Water Prod.-Bbls
			Tubing psig	Casing psig	Temp. °F	Pf psia	Hw Ins	Temp. °F		
Jan 27	1830	0.5	2463		106	585	144	84		
	1900	1.0	2479		108	585	143	82		
	1930	1.5	2491		110	585	143	82		
	2000	2.0	2500		110	585	144	84	1.308	1.500

WELL TEST SUMMARY PAGE 2

For Use with Isochronal Tests

Date	Time	Shut-In Time Hrs.	Tubing Pressure		Casing Pressure		Wellhead Temp. °F
			psig	psia	psig	psia	
Jan 27	2030	0.5	2839	2854	NOT	GIVEN	104
	2100	1.0	2848	2863	"	"	99
	2130	1.5	2848	2863	"	"	98
	2200	2.0	2848	2863	"	"	94

Run No. 3 Duration of Run 2 hrs. Orifice Size 2.25" Meter Run: 3.068"
 High Pressure Separator - Operating Pressure _____ psig Temp. _____ °F
 Low Pressure Separator - Operating Pressure _____ psig Temp. _____ °F
 Flowed Well on 24/64" choke

Date	Time	Flow Time Hours	Wellhead Readings			Meter or Prover Data			Condensate Prod-Bbls	Water Prod- Bbls
			Tubing psig	Casing psig	Temp. °F	Pf psia	Hw Ins	Temp. °F		
Jan 27	2230	0.5	2326		106	495	60	72		
	2300	1.0	2352		107	495	60	74		
	2330	1.5	2366		112	495	61	76		
	2400	2.0	2376		115	495	62	78	1.667	1.591

For Use with Isochronal Type Tests

Date	Time	Shut-In Time Hrs.	Tubing Pressure		Casing Pressure		Wellhead Temp. °F
			psig	psia	psig	psia	
Jan 28	0030	0.5	2844	2859			107
	0100	1.0	2850	2865			100
	0130	1.5	2848	2863			96
	0200	2.0	2848	2863			92

Run No. 4 Duration of Run 2 hrs. Orifice Size 2.250 Meter Run or Prover
 Size: 3.068
 High Pressure Separator - Operating Pressure _____ psig Temp. _____ °F
 Low Pressure Separator - Operating Pressure _____ psig Temp. _____ °F
 Flowed well on 28/64" choke setting

Date	Time	Flow Time Hours	Wellhead Readings			Meter or Prover Data			Condensate Prod-Bbls	Water Prod- Bbls
			Tubing psig	Casing psig	Temp. °F	Pf psia	Hw Ins	Temp. °F		
Jan 28	0230	0.5	2026		110	495	124	78		
	0300	1.0	2071		116	495	126	81		
	0330	1.5	2078		120	495	129	84		
	0400	2.0	2088		124	495	130	86	1.350	2.383

For Use with Isochronal Type Tests

Date	Time	Shut-In Time Hrs.	Tubing Pressure		Casing Pressure		Wellhead Temp. °F
			psig	psia	psig	psia	
Jan 28	0430	0.5	2847	2862			114
	0500	1.0	2852	2867			106
	0530	1.5	2853	2868			100
	0600	2.0	2852	2867			100

Remarks :

00040

WELL TEST SUMMARY PAGE 3

FINAL STABILIZATION FLOW PERIOD

Run No. 5 Duration of Run 24.25 Hrs. Orifice Size 2.25 Meter Run 3.068" ID
Flowed well on 24/64" choke

[illegible]

FINAL BUILD-UP PERIOD

[illegible]

CALCULATION SHEET

CASE 1: FLOW THROUGH METER RUN

Run No.	HW(in wtr)	Pf (psia)	Size Orifice Plate (inches)	F _t of	b	$\frac{H_w}{P_f}$
1	108	490	1.750	83	.0524	.220
2	144	585	1.750	84	.0524	.246
3	62	495	2.250	78	.0706	.125
4	130	495	2.250	86	.0706	.263
5	72	495	2.250	99	.0706	.145

CASE 2: FLOW THROUGH METER RUN 3.068" I.D.

Run No.	F _b	F _g	F _{tf}	F _{pv}	F _{pb}	F _{tb}
1	663.42	1.1463	0.9786	1.0331	1.0068	1.0000
2	663.42	"	0.9777	1.0398	"	"
3	1223.2	"	0.9831	1.0347	"	"
4	1223.2	"	0.9759	1.0328	"	"
5	1223.2	"	0.9645	1.0298	"	"

FLOW THROUGH METER RUN (Continued)

Run No.	F _r	Y	C'	$\frac{H_w P_f}{Q}$	$\frac{Q}{MCF/Hour}$	$\frac{Q}{MCFD}$
1	1.0002	.9973	771.956	230.043	177.583	4262
2	1.0002	.9972	776.135	290.241	225.266	5406
3	1.0004	.9983	1433.590	175.186	251.145	6027
4	1.0003	.9963	1417.689	253.673	359.630	8631
5	1.0004	.9980	1399.463	188.786	264.198	6341

BACK PRESSURE TEST - SUMMARY SHEET

00043

Lat 28° 15' 29" S

Well: Big Lake #4 Location: Long 140° 14' 18"E Field: Big Lake
 Pool: Toolachee Tested by: Agnew Calculated by: DG
 Casing Size: 6.276" I.D. Tubing Size: 2.992 I.D. Produced Through: Tubing
 Perforations: 7586 - 7914 Length of Flow String: 7527'
 Properties of Well Effluent. Spec. Gravity _____ Pc _____ Tc _____

H₂S N/A p.p.m.A. FLOW TEST DATA

Run No.	Tubing psia	Casing psia	Calculated Sandface Press. psia	Gas Flow Rate MMCFD	Condensate Prod- Bbl/d	Total Flow Rate MMCFD	Water Prod. Bbl/d
1	2623		Measured	4.262	Nil	4.262	18.0
2	2515		"	5.406	15.7	5.420	18.0
3	2391		"	6.027	20.0	6.045	19.1
4	2103		"	8.631	16.2	8.646	28.6
5	2442		"	6.341	11.4	6.351	21.5

B. BOMB MEASURED PRESSURES Datum from KB 7700'

Flow Rate No.	Date	Time	Depth	Corr. Press. @ Run Depth - psia	Corr. Press. @ Datum - psia	Remarks
1	Jan 27	1600	7500	3210.48	3223.06	
2	"	2000	"	3085.72	3098.30	
3	"	2400	"	2960.67	2973.25	
4	Jan 28	0400	"	2692.36	2704.94	
5	Jan 29	0615	"	2954.90	2967.48	

C. SHUT-IN DATA

Shut-In No.	Pressure - psia		Shut-In Time-Hrs.	Shut-In No.	Pressure - psia		Shut-In Time-hrs.
	Wellhead	Sandface			Wellhead	Sandface	
Initial	2844	3460.91	48				
1	2857	3465.42	2				
2	2863	3461.41	2				
3	2863	3455.91	2				
4	2867	3448.90	2				

D. PLOTTING DATA

P_f	$P_f^2 \times 10^3$	P_s	$P_s^2 \times 10^3$	$P_f^2 - P_s^2 \times 10^3$	Q Total-MMCFD
3460.91	11.978	3223.06	10.388	1590	4.262
3465.42	12.009	3098.30	9.599	2410	5.420
3461.41	11.981	2973.25	8.840	3141	6.045
3455.91	11.943	2704.94	7.317	4626	8.646
3448.90	11.895	2967.48	8.806	3089	6.351

A.O.F. 16.7 MMCFD, n 0.72654Total Volume of Gas Produced During Test 8.30 MMCF/CONDENSATE 17.6 Bbls.

Remarks: TWO STAGE SEPARATION UTILIZED, BUT LOW PRESSURE FLOW RATES WERE
BELOW METERING SENSITIVITY.

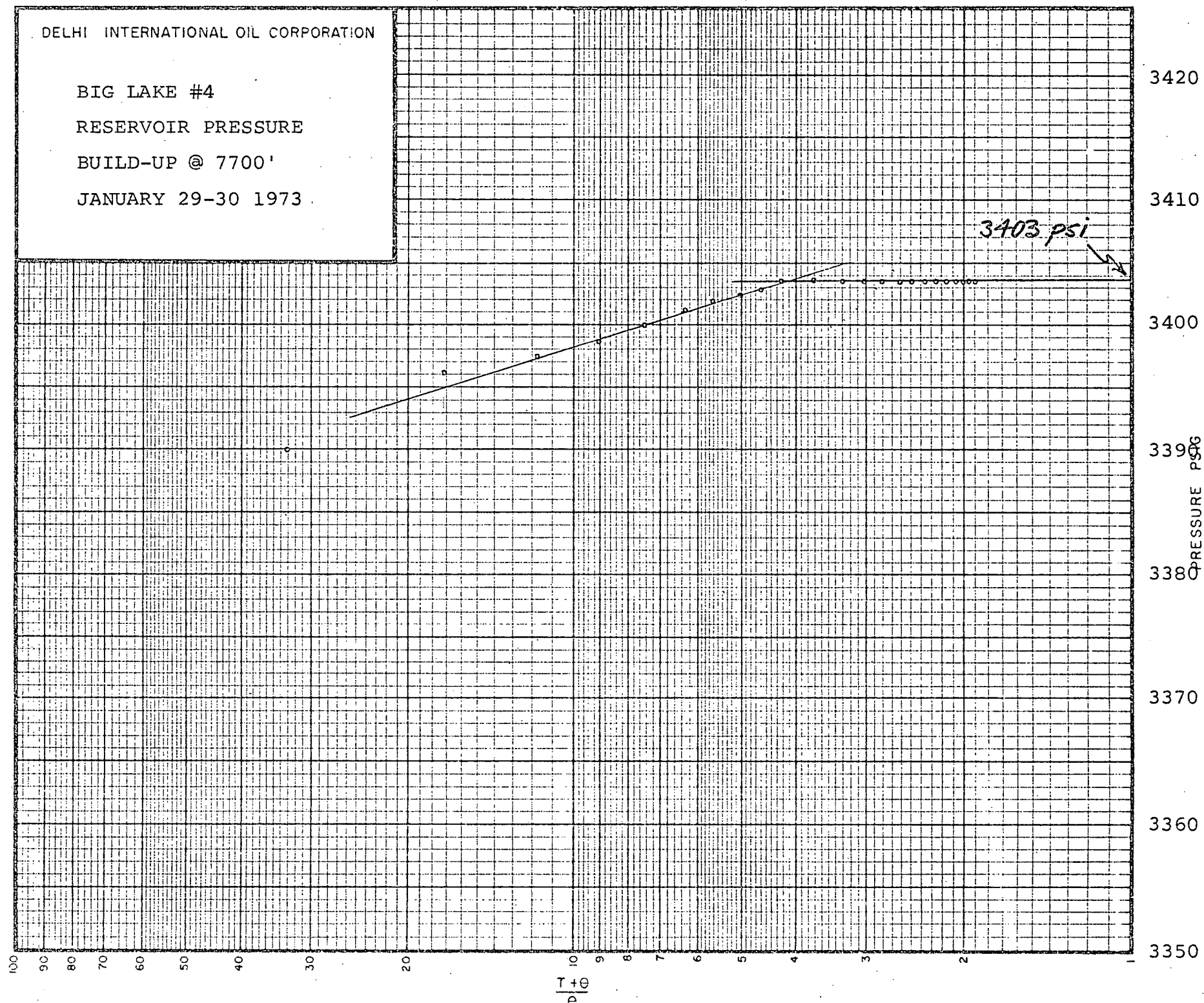
DELHI INTERNATIONAL OIL CORPORATION

BIG LAKE #4

RESERVOIR PRESSURE

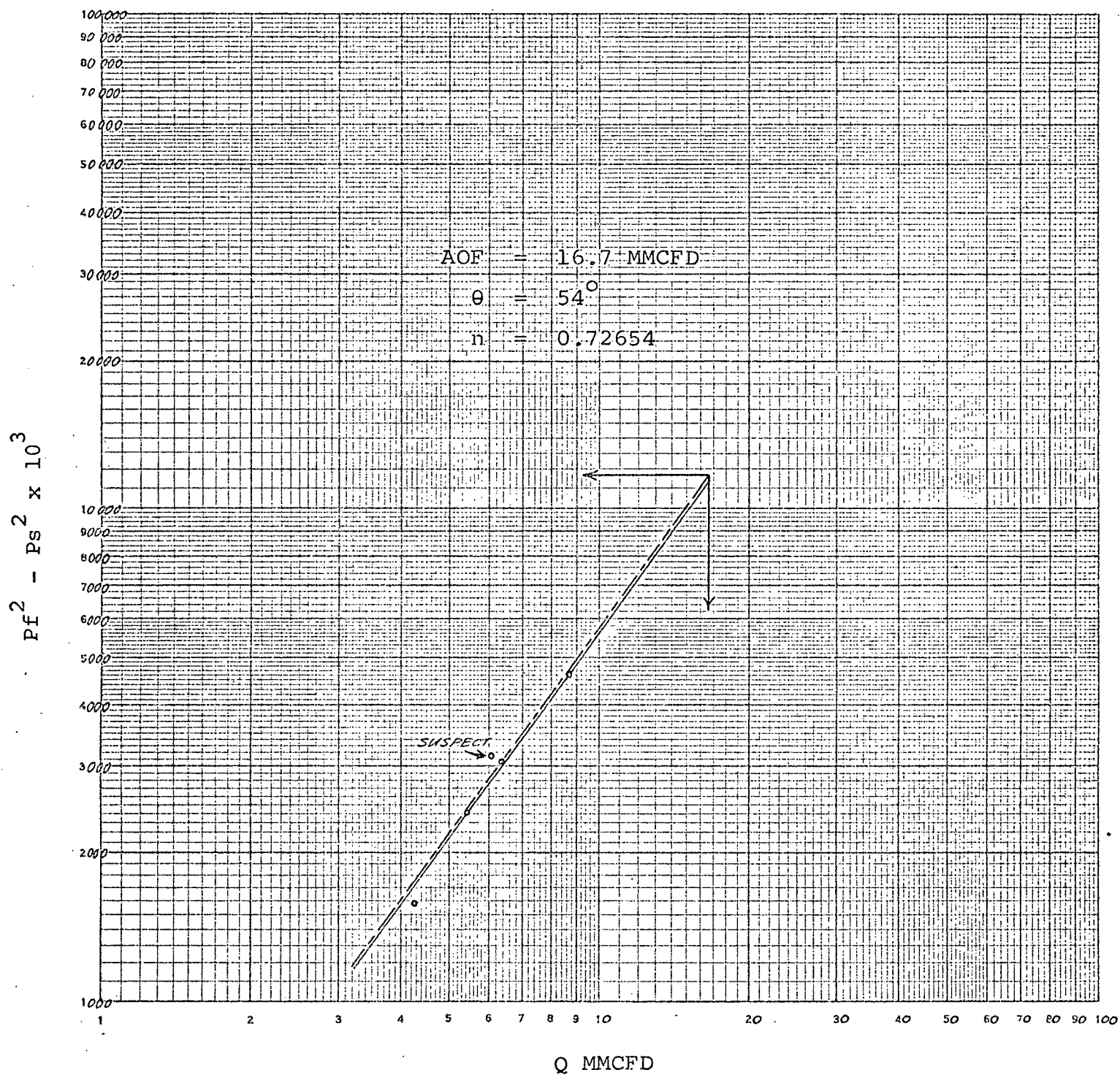
BUILD-UP @ 7700'

JANUARY 29-30 1973



0004

BIG LAKE #4
OPEN FLOW POTENTIAL TEST
JANUARY 27-30 1973





amdel

00046

The Australian Mineral Development Laboratories

Flemington Street, Frewville, South Australia 5063
Phone 79 1662, telex AA82520

Please address all correspondence to the Director
In reply quote: AN3/51/0 - 3301/73

PART REPORT 1

NATA CERTIFICATE

27 February 1973

Mr H.J. Hannah
Production Manager
Delhi International Oil Corporation
GPO Box 2364
ADELAIDE SA 5001

REPORT AN 3301/73

YOUR REFERENCE:	Purchase Order A 19337
LOCATION:	Big Lake 4
IDENTIFICATION:	As listed
DATE RECEIVED:	7/2/73

Enquiries quoting AN 3301/73 to Officer in Charge please

Officer in Charge, Analytical Section: A.B. Timms

for F.R. Hartley
Director

pkm



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AN 3301/73

2.

Well tested:	Big Lake No. 4	Ex 27
Date tested:	29/1/73	0330 hrs
Type of test:	-	
Type of sample:	High pressure gas	
Source of sample:	-	
Field sampling conditions:	Press. 480 psi	Temp. 99°F
Reference:	Purchase Order A19337	

RESULTS OF ANALYSIS

Oxygen plus argon	<0.02 % mol vol
Nitrogen	0.20
Hydrogen	-
Helium	-
Carbon dioxide	16.5
Methane	76.6
Ethane	4.89
Propane	1.21
i Butane	0.122
n Butane	0.200
i Pentane	0.055
n Pentane	0.052
Hexanes	0.048
Heptanes	0.060
Octanes and higher hydrocarbons	0.063
Calculated Gas Density (relative air = 1)	0.761 ✓

REMARKS:



AN 3301/73

00048

3.

Well tested:	Big Lake No. 4	Ex 34
Date tested:	19/1/73	0245 hrs
Type of test:	-	
Type of sample:	High pressure gas	
Source of sample:	-	
Field sampling conditions:	Press. 480 psi	Temp. 100 ^o F
Reference:	Purchase Order A19337	

RESULTS OF ANALYSIS

Oxygen plus argon	<0.02 % mol vol
Nitrogen	0.22
Hydrogen	-
Helium	-
Carbon dioxide	15.9
Methane	77.1
Ethane	4.88
Propane	1.18
i Butane	0.145
n Butane	0.230
i Pentane	0.075
n Pentane	0.064
Hexanes	0.055
Heptanes	0.063
Octanes and higher hydrocarbons	0.088
Calculated Gas Density (relative air = 1)	0.758

REMARKS:



00049

AN 3301/73

4.

Well tested:	Big Lake No. 4 PD 53
Date tested:	29/1/73 0330 hrs'
Type of test:	-
Type of sample:	Low pressure separator gas
Source of sample:	-
Field sampling conditions:	Press. 6 psig Temp. 92°F
Reference:	Purchase Order A 19337

RESULTS OF ANALYSIS

Oxygen plus argon	<0.02 % mol vol
Nitrogen	0.05
Hydrogen	-
Helium	-
Carbon dioxide	32.3
Methane	41.3
Ethane	11.1
Propane	6.85
i Butane	1.33
n Butane	2.54
i Pentane	0.980
n Pentane	0.925
Hexanes	0.830
Heptanes	0.935
Octanes and higher hydrocarbons	0.860
Calculated Gas Density (relative air = 1)	1.156

REMARKS:



AN 3301/73

00050

5.

Well tested:	Big Lake No. 4	PD 64
Date tested:	29/1/72	0300 hrs
Type of test:	-	
Type of sample:	Low Pressure separator gas	
Source of sample:	-	
Field sampling conditions:	Press. 6 psig	Temp. 92°F
Reference:	Purchase Order A 19337	

RESULTS OF ANALYSIS

Oxygen plus argon	<0.02 % mol vol
Nitrogen	0.05
Hydrogen	-
Helium	-
Carbon dioxide	32.3
Methane	40.8
Ethane	11.1
Propane	6.80
i Butane	1.38
n Butane	2.58
i Pentane	1.01
n Pentane	0.97
Hexanes	0.90
Heptanes	1.04
Octanes and higher hydrocarbons	1.07
Calculated Gas Density (relative air = 1)	1.169

REMARKS:



AN 3301/73

6.

Well tested:	Big Lake No. 4	Ex 31
Date tested:	29/1/73	0245 hrs
Type of test:	-	
Type of sample:	Low pressure condensate	
Source of sample:	-	
Field sampling conditions:	Press. 6 psig	Temp. 93°F
Reference:	Purchase Order A19337	

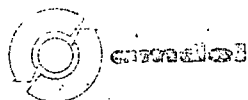
RESULTS OF ANALYSIS

The sample was released to air pressure and temperature by displacement with saturated brine solution to yield gas and liquid. The relative volume of each was measured, both fractions were then analysed chromatographically and the results combined mathematically to give an analysis of the sample as submitted.

The sample yielded oil and gas in the ratio of 410 millilitres oil and 0.05 litres of gas at 27 °C and 765.2 mm pressure.

Flash Gas Analysis

Hydrogen	1.20	
Nitrogen	14.2	% mol vol
Carbon dioxide	8.90	
Methane	44.6	
Ethane	13.0	
Propane	8.50	
i Butane	1.76	
n Butane	3.10	
i Pentane	1.23	
n Pentane	1.07	
Hexanes	1.00	
Heptanes	0.87	
Octanes and higher hydrocarbons	0.57	



Calculated Composition of Sample as Received

Hydrogen	<0.002	
Nitrogen	0.002	% by Weight
Carbon dioxide	0.002	
Methane	0.005	
Ethane	0.002	
Propane	0.066	
Butanes	0.54	
Pentanes	1.03	
Hexanes	1.78	
Benzene	0.96	
Heptanes	4.64	
Toluene	6.72	
Octanes	10.4	
Xylenes plus ethyl benzene	11.42	
Nonanes	8.53	
C ₉ aromatics	7.05	
Decanes plus C ₁₀ aromatics	10.16	
Undecanes plus aromatics	6.83	
Dodecanes plus aromatics	6.45	
Tridecanes plus aromatics	6.41	
Tetradecanes plus aromatics	4.85	
Pentadecanes plus aromatics	2.87	
Hexadecanes plus aromatics	2.55	
Heptadecanes and higher hydrocarbons	6.93	

Specific Gravity of C₁₇ + (from A.S.T.M. Distillation)

= To follow when oil received.

REMARKS:



00053

AN 3301/73

8.

Well tested:	Big Lake No 4	PD 74
Date tested:	29/1/73	0230 hrs
Type of test:	-	
Type of sample:	Low pressure condensate	
Source of sample:	-	
Field sampling conditions:	Press. 6 psig	Temp. 94° F
Reference:	Purchase Order A19337	

RESULTS OF ANALYSIS

The sample was released to air pressure and temperature by displacement with saturated brine solution to yield gas and liquid. The relative volume of each was measured, both fractions were then analysed chromatographically and the results combined mathematically to give an analysis of the sample as submitted.

The sample yielded oil and gas in the ratio of 411 millilitres oil and 0.05 litres of gas at 27 °C and 765.2 mm pressure.

Flash Gas Analysis

		% mol vol
Nitrogen	4.00	
Carbon dioxide	33.5	
Methane	35.2	
Ethane	11.2	
Propane	6.80	
i Butane	1.58	
n Butane	2.80	
i Pentane	1.06	
n Pentane	0.95	
Hexanes	0.88	
Heptanes	1.00	
Octanes and higher hydrocarbons	1.03	

AN 3301/73

Calculated Composition of Sample as Received

9.

Nitrogen	0.001	% by Weight
Carbon dioxide	0.01	
Methane	0.003	
Ethane	0.002	
Propane	0.20	
Butanes	0.69	
Pentanes	1.12	
Hexanes	1.95	
Benzene	1.05	
Heptanes	4.79	
Toluene	7.00	
Octanes	10.43	
Xylenes plus ethyl benzene	11.72	
Nonanes	8.66	
C ₉ aromatics	6.84	
Decanes plus C ₁₀ aromatics	10.22	
Undecanes plus aromatics	6.90	
Dodecanes plus aromatics	6.06	
Tridecanes plus aromatics	6.03	
Tetradecanes plus aromatics	4.49	
Pentadecanes plus aromatics	2.97	
Hexadecanes plus aromatics	2.04	
Heptadecanes and higher hydrocarbons	6.83	

Specific Gravity of C₁₇ + (from A.S.T.M. Distillation)

= To follow when oil received.

REMARKS:

1973 APR 30 AM 10:25

00055



amdel

The Australian Mineral Development Laboratories

Flemington Street, Frewville, South Australia 5063
Phone 79 1662, telex AA82520

Please address all correspondence to the Director
In reply quote: AN3/51/0 - 3301/73

REPORT COMPLETE

NATA CERTIFICATE

27 April 1973

The Production Manager
Delhi International Oil Corporation
GPO Box 2364

ADELAIDE SA 5001

REPORT AN 3301/73

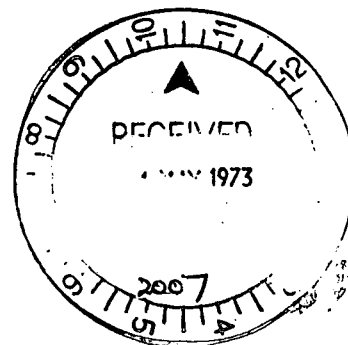
YOUR REFERENCE:	Purchase Order A19337
LOCATION:	Big Lake 4
MATERIAL:	Condensate and water
IDENTIFICATION:	As listed
DATE RECEIVED:	7/2/73

Enquiries quoting AN 3301/73 to Officer in Charge please

Officer in Charge, Analytical Section: A.B. Timms

for F.R. Hartley
Director

pkm



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Well tested:	Big Lake 4
Date tested:	29/1/73
Type of test:	-
Type of sample:	Condensate
Source of sample:	Stock tank
Field sampling conditions	-
Reference:	Purchase Order No. A19337

RESULTS OF ANALYSIS

Kinematic Viscosity	1.049	centistokes/second at 37.8°C
		(100°F)
Specific Gravity at 15.6°C (60°F)	0.818	
A.P.I. Gravity at 15.6°C (60°F)	41.5	

A.S.T.M. Distillation

Initial Boiling Point	74	°C
10% recovery	111	
20	127	
30	136	
40	146	
50	163	
60	180	
70	204	
80	236	
90	280	
94.0	300	

Weight distillate	75.9	grams
Weight residue	5.10	grams
Loss	1.35	grams
Recovery	98.3	%
Residue after distillation		
Specific Gravity at 15.6°C (60°F)	0.83	
Pour Point	< -5	°C
Flash Point	8	°C
Aniline Point	30	°C
Sulphur (X.R.F.)	0.012	% by weight



00057

WATER ANALYSIS REPORT

SAMPLE NO.

JOB NO. 3301/73

CHEMICAL COMPOSITION

		Milligrams per litre mg/l	Milliequivalents per litre me/l
<i>Cations</i>			
Calcium	(Ca)	20	1.0
Magnesium	(Mg)	12	1.0
Sodium	(Na)	2400	104.4
Potassium	(K)	29	0.7
Iron	(Fe)	4	0.1
<i>Anions</i>			
Carbonate	(CO ₃)		
Bicarbonate	(HCO ₃)	225	3.7
Sulphate	(SO ₄)	240	5.2
Chloride	(Cl)	3420	96.4
Fluoride	(F)		
Nitrate	(NO ₃)		
Phosphate	(PO ₄)		

TOTALS and BALANCE

Cations me/l	Anion me/l
107.2	105.3

diff Δ 1.9 sum Σ 212.5 % $(\frac{\Delta \times 100}{\Sigma})$ 0.9

DERIVED AND OTHER DATA

Conductivity (E.C.) μ S/cm at 25°C	10,700	Milligrams per litre mg/l
Total Dissolved Solids:		
a. Based on E.C.		
b. Calculated (HCO ₃ =CO ₃)	6236	
c. Residue on evaporation at 180°C		
Total Hardness as CaCO ₃	105	
Carbonate Hardness as CaCO ₃	105	
Non-carbonate Hardness as CaCO ₃	5	
Total Alkalinity as CaCO ₃	180	
Free Carbon Dioxide (CO ₂)		
Suspended Solids		
Silica (SiO ₂)		
Boron (B)		
Reaction-pH	6.5	Units
Turbidity (Jackson)		
Colour (Hazen)		
Sodium Absorption Ratio SODIUM / TOTAL CATION RATIO	97.4	

Name	Hundred	Supply
	Section	Depth Hole
Address	Hole No.	Date Collected
	Water Cut	Sample Collected by
	Water Level	Date Received

REMARKS:

for Director

PRESSURE BUILD UP SURVEYBIG LAKE #4

Date: September 26-29, 1977

Depth Tested: 7747' KB

Lubricator
Pressure:

In	Amerada	= 1337 psig (9219 KPA)
	Deadweight	= 1358 psig (9363 KPA)
Out	Amerada	= 2158 psig (14877 KPA)
	Deadweight	= 2143 psig (14775 KPA)

SHUT IN
TIME HRS.

PSIG

KPA

REMARKS

-3.1	2105.9	14520	Flow
Ø	2105.9	14520	S.W.I. 2100 Hrs 26/9/77
1	2496.6	17214	
2	2504.8	17270	
3	2507.5	17289	
4	2513.0	17327	
5	2513.0	17327	
6	2515.7	17346	
7	2518.5	17365	
8	2521.2	17384	
9	2521.2	17384	
10	2523.9	17402	
20	2532.1	17459	
40	2543.1	17535	
60	2551.3	17591	
64.5	2554.0	17610	POH 1330 Hrs 29/9/77

STATIC PRESSURE

GRADIENT

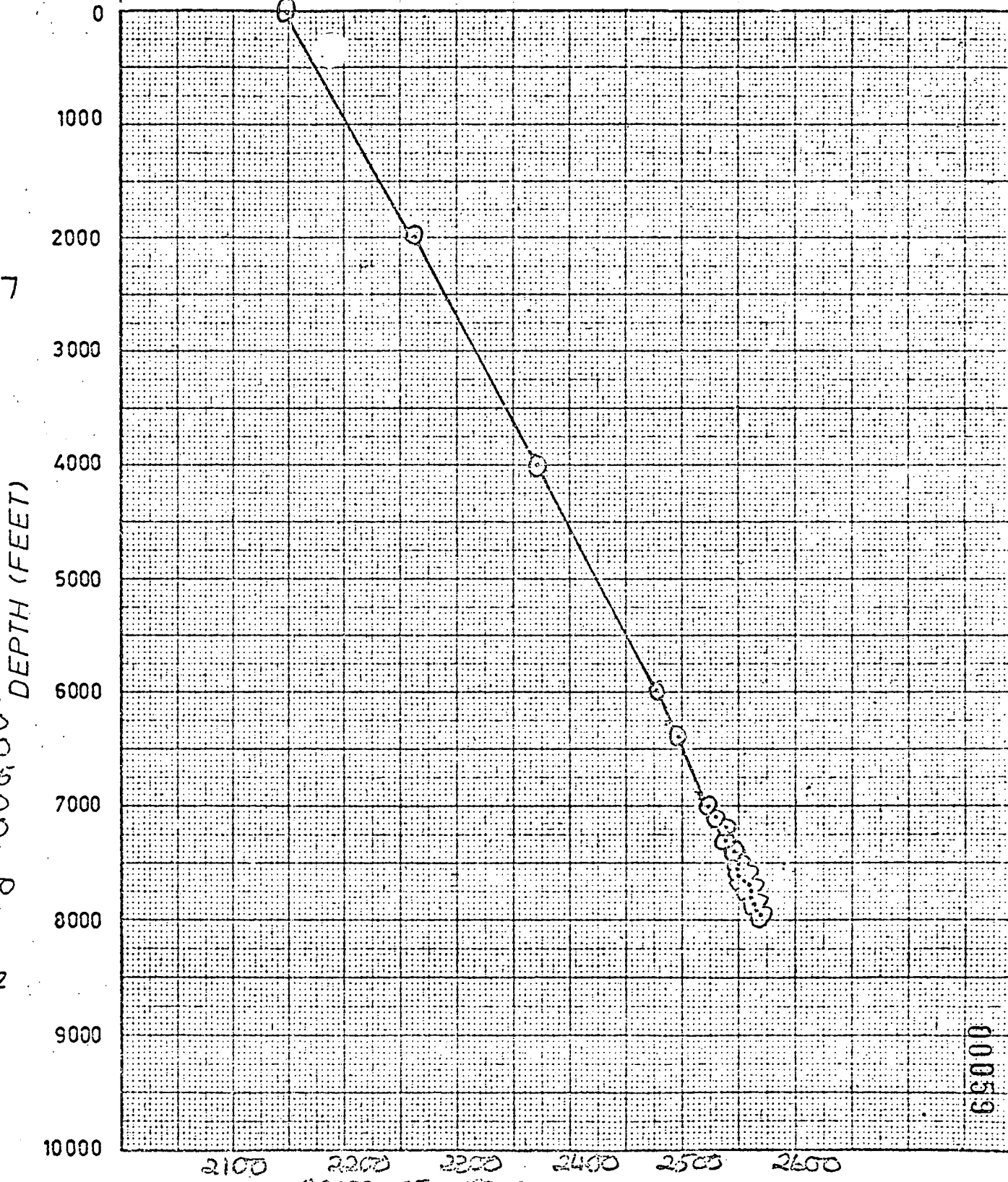
WELL BIG LAKE 4

TEST DATE 29th SEPTEMBER 1977

DEPTH (FEET)	PRESSURE (PSIG)	GRADIENT PSI / FT	DEPTH (METRES)	PRESSURE KPa	GRADIENT KPa / M
LUBRICATOR	2146.8	—	LUBRICATOR	14806	—
2000	2261.5	0.0574	609.6	15597	1.2976
4000	2370.9	0.0547	1219.2	16351	1.2369
6000	2477.5	0.0533	1828.8	17086	1.2057
6387	2496.6	0.0494	1946.8	17218	1.1186
6974	2523.9	0.0465	2125.7	17406	1.0509
7074	2529.4	0.0550	2156.2	17444	1.2459
7174	2537.6	0.0820	2186.6	17501	1.8750
7274	2537.6	0.0000	2217.1	17501	0.0000
7374	2545.8	0.0820	2247.6	17578	2.6246
7474	2548.5	0.0000	2278.1	17578	0.0000
7524	2548.5	0.0000	2293.3	17578	0.0000
7574	2551.3	0.0560	2308.6	17595	4.6405
7624	2554.0	0.0540	2323.8	17614	1.2500
7674	2556.8	0.0560	2339.0	17633	1.2500
7724	2559.5	0.0540	2354.3	17652	1.2418
7774	2559.5	0.0000	2369.5	17652	0.0000
7824	2562.2	0.0540	2384.8	17670	1.1765
7874	2565.0	0.0560	2400.0	17690	1.3158
7924	2570.4	0.1080	2415.2	17727	2.4342

DEAD WEIGHT

PRESSURE = 2143 PSIG
= 14779 KPa



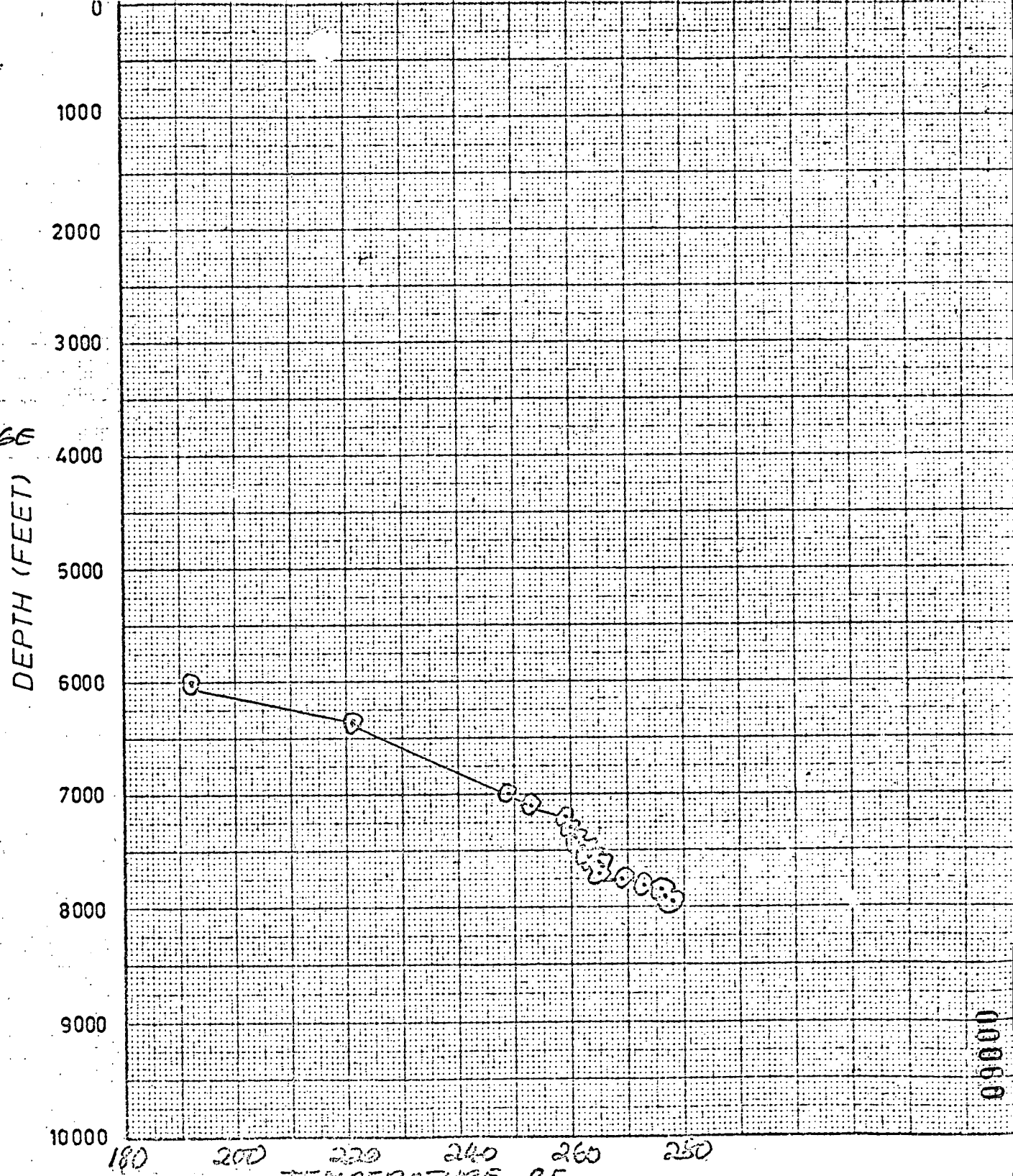
STATIC TEMPERATURE

GRADIENT

WELL BIG LAKE 4

TEST DATE 29th SEPTEMBER 1977

DEPTH (FEET)	TEMP °F	GRADIENT /FT	DEPTH (METRES)	TEMP °C	GRADIENT /M
LUBRICATOR	BELOW	RANGE	LUBRICATOR	BELOW	RANGE
2000	BELOW	RANGE	609.6	BELOW	RANGE
4000	BELOW	RANGE	1219.2	BELOW	RANGE
6000	187.0		1828.8	86.1	
6387	221.4		1946.8	105.2	
6974	249.3		2125.7	120.7	
7074	253.3		2156.2	123.0	
7174	258.6		2186.6	125.9	
7274	259.6		2217.1	126.5	
7374	260.9		2247.6	127.2	
7474	262.2		2278.1	127.9	
7524	263.4		2293.3	128.6	
7574	264.5		2308.6	129.2	
7624	265.4		2323.8	129.7	
7674	265.4		2339.0	129.7	
7724	268.5		2354.3	131.4	
7724	272.9		2369.5	133.8	
7824	275.6		2384.8	135.3	
7874	276.4		2400.0	135.8	
7924	277.8		2415.2	136.6	



WELL : Big Lake # 4 $P_f = 36.00 \text{ Kpa}$

ORIFICE SIZE : 34.925 mm 1.375 "

 $T = 21 ^\circ\text{C}$

LINE SIZE : 87.325 mm 3.438 "

 $\text{Diff} = 0.2 \text{ Kpa}$ Cumulative Production to end of August = $1251.962 \text{ m}^3 \times 10^6$

Number of hours online in August = 691 hours

Production in August = $0.567 \text{ m}^3 \times 10^6$ $\therefore$ Average flow rate in August = $(0.567 / 691) \times 24 = 0.020 \text{ m}^3 \times 10^6 / \text{d}$

Number of days online in August before shut in 0700 hrs 30/8/86

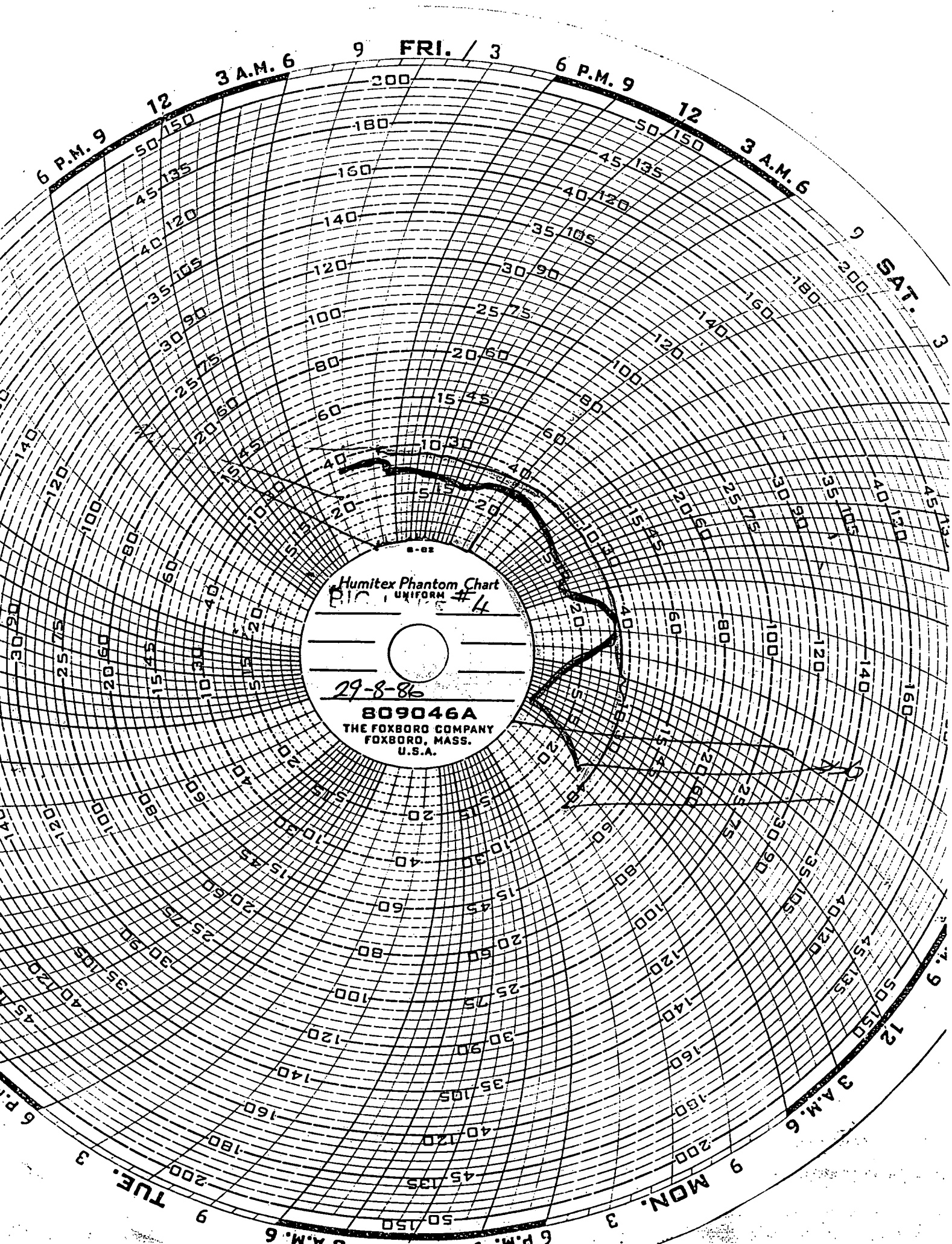
= 28.792 = 691 hrs. Well remained shut in from 0700 30/8/86 to after midnight 31/8/86

 $\therefore$ Production upto 0700hrs 30/8/86 = August cumulative production, $\Rightarrow$ Total cumulative Production= $1251.962 \text{ m}^3 \times 10^6$ = 44437.139 mmscf Flow Rate just prior to Shut In = $0.007 \text{ m}^3 \times 10^6 / \text{d}$ * = $0.231 \text{ mmscf} / \text{d}$

* N.B. Accuracy of flow rate is questionable due to difficulty in obtaining confident differential pressure reading from attached charts.



00062



00064

DATE 11/11/77
TO 12/11/77
ADSLDIDE

SUB-SURFACE PRESSURE SURVEY

CO. SANTOS	RUN 01 FIELD BIG LAKE	WELL 04
EFF DEPTH	WELL STAT	TOOL HUNG 7486'
CASING 7"	CASING PRESS	ON BOTTOM 1630 30/8
LINER	TUBING PRESS	OFF BOTTOM 0830 4/5
DATE 860630	ELEMENT RANGE 0 - 3110	ZERO POINT
ELEVATION	ZONE	SHUT-IN 0730 30/8
MAX TEMP	PICK-UP	ON-PROD
PERF 7586' - 7514'	CAL SER NO. 26515	MPP 7750'
TUBING 2-7/8"		
UNITS ENGLISH	PURPOSE BUILD-UP	

SURVEY DATA

CO. SANTOS				RUN 01 FIELD BIG LAKE				WELL 04			
TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME
16:30	1516.7	0.0	0.0	7:22	1545.1	28.3	14.9				
17:20	1515.3	-1.4	0.8	7:25	1542.5	25.8	14.9				
18:56	1526.6	9.9	2.4	7:31	1539.7	22.9	15.0				
19:56	1533.7	17.0	3.4	7:40	1541.1	24.4	15.2				
20:34	1533.4	16.6	4.1	7:47	1545.0	28.2	15.3				
21:11	1523.1	6.3	4.7	8:02	1549.5	32.8	15.5				
22:58	1525.0	8.3	6.5	8:53	1551.4	34.7	16.4				
23:37	1523.1	6.4	7.1	10:19	1548.1	31.4	17.8				
1:28	1531.3	14.6	9.0	11:14	1539.2	22.4	18.7				
3:41	1530.1	13.3	11.2	12:59	1534.9	18.2	20.5				
4:44	1527.0	10.3	12.2	15:41	1538.3	21.6	23.2				
5:07	1534.3	17.5	12.6	21:10	1539.0	22.3	28.7				
5:25	1541.0	24.2	12.9	6:04	1541.3	24.6	37.6				
5:43	1535.5	18.8	13.2	8:16	1541.3	24.6	49.8				
6:29	1536.7	19.9	14.0	8:09	1542.5	25.8	63.7				
7:11	1536.3	19.5	14.7	0:33	1543.2	26.4	80.1				
SWI 7:17	1536.2	19.5	14.8	15:52	1544.9	28.2	95.4				
7:19	1539.0	22.3	14.8	8:30	1543.7	27.0	112.0				
7:20	1543.0	26.3	14.8	0:00	0.0	0.0	0.0				

LUB IN DWT = 537 PSI / OUT = 1205 PSI
LUB IN AMERADA = 525 PSI / OUT = 1222 PSI

60-100-100
75 GREENFIELD ST
ADELAIDE

00065

SUB-SURFACE PRESSURE SURVEY

CO. SANTOS		RUN 02 FIELD BIG LAKE		WELL 04
EFF DEPTH		WELL STAT		TOOL HUNG 7494'
CASING 7"	-	CASING PRESS		ON BOTTOM 1630 30/8
LINER	-	TUBING PRESS		OFF BOTTOM 0830 4/8
DATE	860830	ELEMENT RANGE	0 - 3108	ZERO POINT
ELEVATION		ZONE		SHUT-IN 0700 30/8
MAX TEMP		PICK-UP		ON-PROD
PERF	7586'-7914'	CAL. SER NO.	56429	MPD
TUBING 2-7/8"	-			7750'
UNITS	ENGLISH	PURPOSE	BUILD-UP	

SURVEY DATA

CO. SANTOS				RUN 02 FIELD BIG LAKE				WELL 04			
TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME				
16:30	1528.0	0.0	0.0	7:15	1559.6	31.6	14.7				
17:22	1526.9	-1.2	9	7:18	1558.1	30.0	14.8				
18:45	1536.3	8.3	2.2	7:22	1556.5	28.4	14.9				
19:55	1546.3	18.3	3.4	7:27	1555.2	27.2	14.9				
20:29	1547.1	19.1	4.0	7:37	1559.6	31.6	15.1				
21:10	1537.2	9.2	4.7	7:51	1562.9	34.9	15.4				
23:35	1537.5	9.5	7.1	8:11	1565.8	37.8	15.7				
23:56	1542.6	14.6	7.4	8:54	1567.4	39.4	16.4				
0:43	1542.3	14.3	8.2	10:28	1562.3	34.3	18.0				
2:29	1543.7	15.6	10.0	12:02	1552.8	24.8	19.5				
4:31	1540.7	12.7	12.0	15:08	1555.7	27.7	22.6				
4:39	1540.2	12.2	12.1	21:17	1555.3	27.3	28.8				
4:53	1548.0	20.0	12.4	3:17	1556.9	28.9	34.8				
5:14	1554.8	26.8	12.7	11:47	1558.8	30.8	43.3				
5:34	1552.6	24.6	13.1	20:19	1559.3	31.3	51.8				
6:17	1551.8	23.8	13.8	5:38	1559.1	31.1	61.1				
SWI 7:09	1551.3	23.3	14.6	19:19	1560.3	32.3	74.8				
7:11	1553.6	25.6	14.7	9:37	1561.2	33.1	89.1				
7:12	1556.2	28.2	14.7	22:26	1560.5	32.4	101.9				
7:13	1558.4	30.4	14.7	8:30	1560.4	32.4	112.0				

LUB IN DWT = 537 PSI / OUT = 1205 PSI

LUB IN AMERADA = 532 PSI / OUT = 1221 PSI

Well:.....BIG LAKE #4.....Date: 30/8/86.....
 ① 525 1222
 Lubricator Data: ② 532 1221
 Pressure with D.W.T. 537 PSI OUT=1205 psi
 Time Pressured 1400 HRS Time Depressed 10:45
 Time Run in Hole 1600 HRS Time off Bottom 0830

Bomb No. 1 Data

Bomb No. 2 Data

Element No. and Range	28515 x 3000 PSI	56429 x 3000 PSI
Recorder No.	13027 x 15 TKS	14628 x 15 TKS
Clock and Lead Screw Data	F-15307	F-15293
Engage Stylus	Date: 3/8/86 Time: 13:48	Date: 3/8/86 Time: 13:48
Disengage	Date: 4/9/86 Time: 10:56	Date: 4/9/86 Time: 10:56

Remarks: RAN TEMP ELEMENT EVER 29216 149 / 351 OF
.....
.....
.....
Max S.L.B.H. Temperature = 282.4°F

Well-Head Data for Final Build-up

[illegible]

BUILD UP DATA

WELL:BIG LAKE # 4.....

OPERATOR: ..DAVID...KAY.....



SANTOS LTD
WELL TEST DATA
METRIC SUMMARY SHEET

DATE: ...31./8./86.....

PAGE No: ..ONE.....

DATE TIME	WELLHEAD						FLUID PRODUCTION				GAS PRODUCTION			
	CASING PSI	CASING KPA	TUBING PSI	TUBING KPA	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M ³ /D	FLOWRATE H ₂ O BBL'S/D	FLOWRATE H ₂ O M ³ /D	MMSCF/D	Mm ³ /D	G.O.R. Cu/FT BBL	G.O.R. M ³ /M ³
0830	9	62	635	4378										
0845	9	62	649	4474										
0900	9	62	654	4509										
0915	9	62	663	4571										
0930	9	62	670	4619										
0945	9	62	676	4661										
1000	9	62	681	4695										
1015	9	62	685	4723										
1030	9	62	686	4729										
1045	9	62	685	4723										
1100	9	62	683	4709										
1115	9	62	683	4709										

CONVERSION FACTORS:

• BBL'S x 0.15899 = M³

• MMSCF x 28.174 = 10³ M³

• Cu/FT PER BBL x 0.1773 = M³/M³

• PSI x 6.895 = KPA

• °C x 9 ÷ 5 + 32 = °F

000068

WELL:BIG LAKE # 4.....

OPERATOR:DAVID KAY.....



SANTOS LTD
WELL TEST DATA
METRIC SUMMARY SHEET

DATE:31/8/86.....

PAGE No: TWO.....

DATE TIME	WELLHEAD						FLUID PRODUCTION				GAS PRODUCTION			
	CASING PSI	CASING KPA	TUBING PSI	TUBING KPA	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M3/D	FLOWRATE H2O BBL'S/D	FLOWRATE H2O M3/D	MMSCF/D	Mm3/D	G.O.R. Cu/FT BBL	G.O.R. M3/M3
1130	9	62	683	4709										
1145	9	62	683	4709										
1200	9	62	682	4702										
1215	9	62	682	4702										
1230	9	62	682	4702										
1630	9	62	706	4867										
2030	8	55	724	4991										
0030	8	55	743	5122										
0430		N/A												
0830	8	55	794	5474										
1230	8	55	821	5660										
1630	8	55	841	5798										

CONVERSION FACTORS:

• BBL'S. x 0.15899 = M³

• MMSCF x 28.174 = 10³ M³

• Cu/FT PER BBL x 0.1773 = M³/M³

• PSI x 6.895 = KPA

• °C x 9 ÷ 5 + 32 = °F

WELL: ...BIG LAKE #4.....

OPERATOR: ...DAVID KAY.....



SANTOS LTD
WELL TEST DATA
METRIC SUMMARY SHEET

DATE: ...4/9/86.....

PAGE No: ...THREE.....

DATE TIME	WELLHEAD						FLUID PRODUCTION				GAS PRODUCTION			
	CASING PSI	CASING KPA	TUBING PSI	TUBING KPA	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M ³ /D	FLOWRATE H ₂ O BBL'S/D	FLOWRATE H ₂ O M ³ /D	MMSCF/D	Mm ³ /D	G.O.R. Cu/FT BBL	G.O.R. M ³ /M ³
2030	6	41	863	5950										
			2 ND /9/86											
0030	6	41	885	6102										
0430	6	41	907	6253										
0830	6	41	930	6419										
1230	6	41	954	6577										
1630	6	41	978	6743										
2030	6	41	1001	6901										
			3 RD /9/86											
0030	7	48	1022	7046										
0430	7	48	1044	7198										
0830	5	34	1059	7301										

CONVERSION FACTORS:

• BBL'S. x 0.15899 = M³

• MMSCF x 28.174 = 10³ M³

• Cu/FT PER BBL x 0.1773 = M³/M³

• PSI x 6.895 = KPA

• °C x 9 ÷ 5 + 32 = °F

WELL:BIG LAKE #4.....

OPERATOR: ...DAVID KAY.....



SANTOS LTD
WELL TEST DATA
METRIC SUMMARY SHEET

DATE:4TH/9/86.....

PAGE No: ...FOUR.....

DATE TIME	WELLHEAD						FLUID PRODUCTION				GAS PRODUCTION			
	CASING PSI	CASING KPA	TUBING PSI	TUBING KPA	TEMP °F	TEMP °C	FLOWRATE OIL-COND BBL'S/D	FLOWRATE OIL-COND M3/D	FLOWRATE H2O BBL'S/D	FLOWRATE H2O M3/D	MMSCF/D	Mm3/D	G.O.R. Cu/FT BBL	G.O.R. M3/M3
1230	4	27	1097	7563										
1630	4	27	1120	7722										
2030	4	27	1144	7887										
0030	4	27	1161	8005			4 TH /9/86.							
0430	4	27	1180	8136										
0830	4	27	1205	8308										
0830			PULL AMERADAS END TEST.											

CONVERSION FACTORS:

• BBL'S x 0.15899 = M³

• MMSCF x 28.174 = 10³ M³

• Cu/FT PER BBL x 0.1773 = M³/M³

• PSI x 6.895 = KPA

• °C x 9 ÷ 5 + 32 = °F



WIRELINE REPORT

00071

WELL: BIG LAKE # 4

DATE: 6-9-86

PROGRAM: REMOVE OBSTRUCTION FROM TUBING

PURPOSE OF WORK: TO CLEAR TUBING

REPORT OF WORK PERFORMED:

11:00 TO 12:00 RIGED UP 3 SECTIONS LUB TO FISH WIRE.
13:00 TO 13:45 R.H. 2.170 L.B. TO 7524' W/L POOH
(NO IMPRESSION)
13:45 TO 14:30 R.H. 2.170 L.B. 7524 W/L POOH
IMPRESSION AROUND EDGE OF L.B. MAY BE SCALE
14:30 TO 15:00 CHANGE TO 1 1/2" TOOL STRING R.H. 1.75 BLIND BOX
TO 7574 W/L 7588 KB POOH
15:00 TO 1530 RIGED DOWN

Karl Dove
OPERATOR'S SIGNATURE

WORK PERFORMED BY: K. DOVE OF EXPERTEST

WELL DATA:

Tubing Size: 3 1/2" FWHP: 6,700 KPA SIWHP: 6700 KPA

Sub Surface S.V./Landing Nipple @ S.S.D. @: 7477'

"X" Nipple @ "N"/"X" Nipple @ 7524' other

Min I.D. 2.205 " @ 7524' Packer @ 7511'

Perforated Interval:

Forward to: Petroleum Engineering — Adelaide
Production Department — Moomba



00072

WIRELINE REPORT

WELL: BIG LAKE #4

DATE: 30/8/86

PROGRAM: BHP SURVEY

PURPOSE OF WORK: TAG PBTD

REPORT OF WORK PERFORMED: 0830 CONTINUE RIGGING UP W/L UNIT

0930 RTH WITH 1.9" LUB AND
HANG UP AT 7509 LBS POOR
POSSIBLY SOME WIRE IN HOLE
POOR RUN AMERADAS FOR BHP
SURVEY.

1400, PRESSURE LUB FOR BHP SURVEY.


OPERATOR'S SIGNATURE

WORK PERFORMED BY: DAVID KAY OF EXPERTEST

WELL DATA:

Tubing Size: 3 1/2" EUE FWHP: 540 PSI SIWHP: —

Sub Surface S.V./Landing Nipple @ S.S.D. @:

"X" Nipple @ "N"/"XN" Nipple @ 7526 other

Min I.D. 2.205" @ 7526 Packer @ 7512

Perforated Interval: 7586 - 7914

Forward to: Petroleum Engineering — Adelaide
Production Department — Moomba



**** BIG LAKE #4 ****

STATIC PRESSURE GRADIENT

TEST DATE: 4.9.86

DEPTH (FT.)	TOP PRESSURE ELEMENT 28515/3000			BOTTOM PRESSURE ELEMENT 56429/3000		
	DEFLECTION (INCHES)	PRESSURE (PSIG)	GRADIENT (PSI/FT)	DEFLECTION (INCHES)	PRESSURE (PSIG)	GRADIENT (PSI/FT)
LUB	0.7890	1219.5	----	0.7900	1221.5	1----
1000	0.8125	1256.0	0.0366	0.8130	1257.2	0.0357
2000	0.8355	1291.8	0.0358	0.8350	1291.4	0.0342
3000	0.8578	1326.6	0.0347	0.8580	1327.1	0.0357
4000	0.8792	1359.9	0.0333	0.8800	1361.3	0.0342
5000	0.9002	1392.6	0.0327	0.9010	1394.0	0.0326
6000	0.9200	1423.4	0.0308	0.9235	1428.9	0.0350
7000	0.9420	1457.7	0.0343	0.9450	1462.4	0.0334
7500	0.9970	1543.5	0.1715	1.0010	1549.4	0.1741
LUB	0.7950	1228.8	----	0.7940	1227.7	----

GENERAL REMARKS:

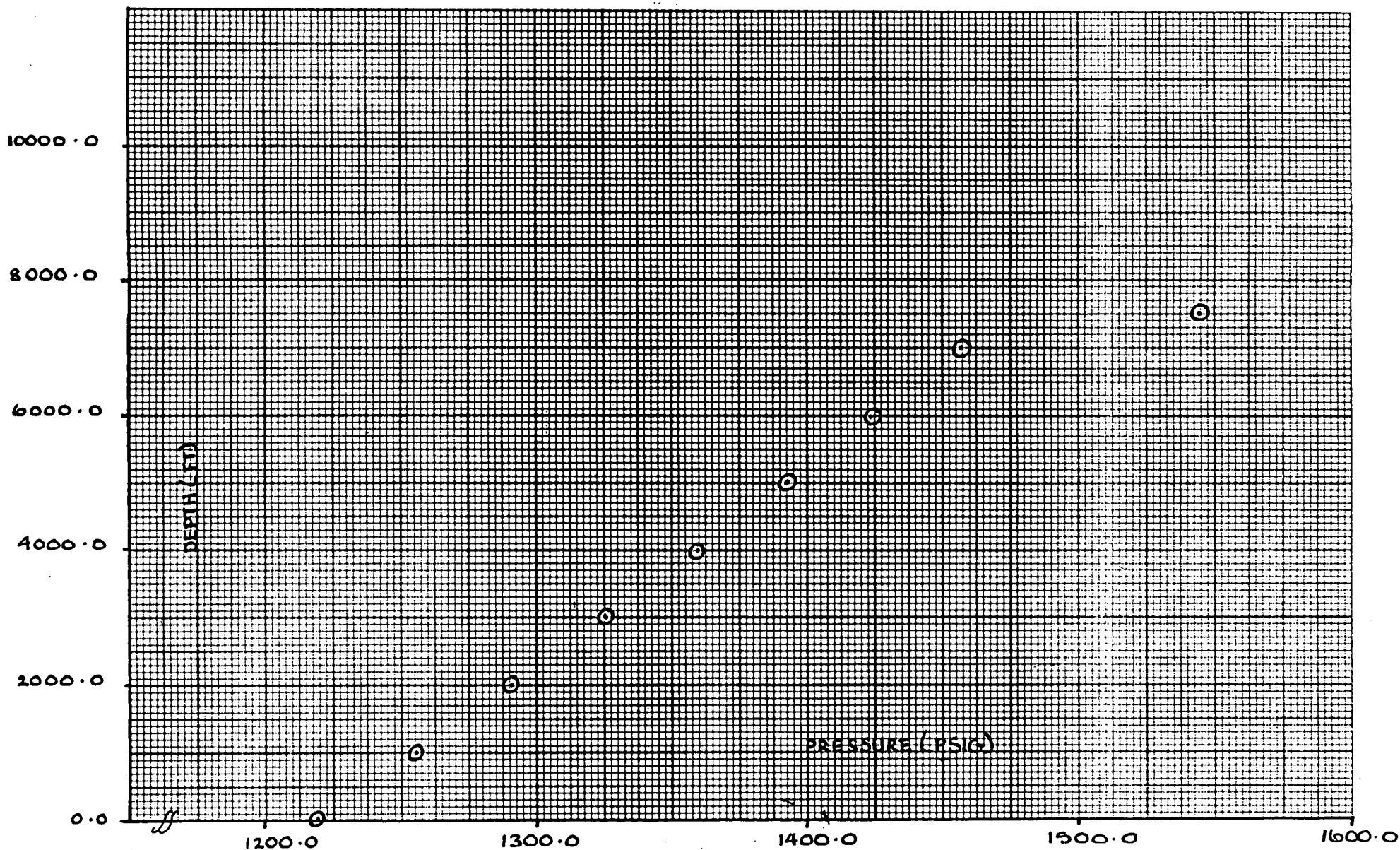
AN TEMP ELEMENT 29216

DWT IN: 1227
DWT OUT: 1229
MAX BHT: N/A 279.3°F

ELEMENT 28515/3000 CALIBRATED 24.8.86.
ELEMENT 56429/3000 CALIBRATED 24.8.86.

BIG LAKE # 4 - STATIC PRESSURE GRADIENT - 4/9/86

ELEMENT # 28515/3000 (TOP)



BIG LAKE II 4

STATIC GRADIENT SURVEY

DATE: 4/9/86

BOMB No. 1 DATA

ELEMENT No. 28515 ELEMENT RANGE: x 3000
RECORDER No. 13027 x 1545 CLOCK DATA: 2395 x 3 hr.
ENGAGE STYLUS: 11:09 DISENGAGE: 13:40

BOMB No. 2 DATA

ELEMENT No. 56429 ELEMENT RANGE: x3000
RECORDER No. 14628 CLOCK DATA: 2131 x3HR
ENGAGE SYLUS: 1109 DISENGAGE: 13.40

LUBRICATOR DATA

PRESSURE WITH D.W.T.: 1227 PSI
TIME PRESSURED: 11:21
TIME DEPRESSURED: 13:33

[illegible]

General Comments:

G O I O

00075

SANTOS EXPLORATION DATA BASE

WATER ANALYSIS

WELL: BIG LAKE

4

LAB: AMDEL

TEST: DST 1

DATE: / /19

SAMPLE: .

DEPTH: 7534. - 7689. FT (KB)

FT (SUBSEA)

FORMATION: TOOLACHEE

TOOLACHEE COAL

COMMENT: REC: 95' MW: RW(RIG)=1.1 @ 74 DEG F: 8.6 MMCFD: NAEL EQUIV=3602 PPM: TOOLACHEE

CATIONS	MG/L	MEQ/L	ANIONS	MG/L	MEQ/L
SODIUM	1140.0	49.6	CHLORIDE	1150.0	32.4
POTASSIUM	100.0	2.6	BICARBONATE	1025.0	16.8
CALCIUM	77.0	3.8	CARBONATE		
MAGNESIUM	36.0	3.0	SULPHATE	735.0	15.3
IRON	200.0	7.2	NITRATE	0.0	0.0
			HYDROXIDE		
TOTAL CATIONS	1553.0	66.1	TOTAL ANIONS	2910.0	64.5

ION BALANCE: 1.2 %

TOTAL DISSOLVED SOLIDS: 3942.0 MG/L

MEASURED RESISTIVITY: 1.770 OHM-M AT TEMP 77. F 25. C

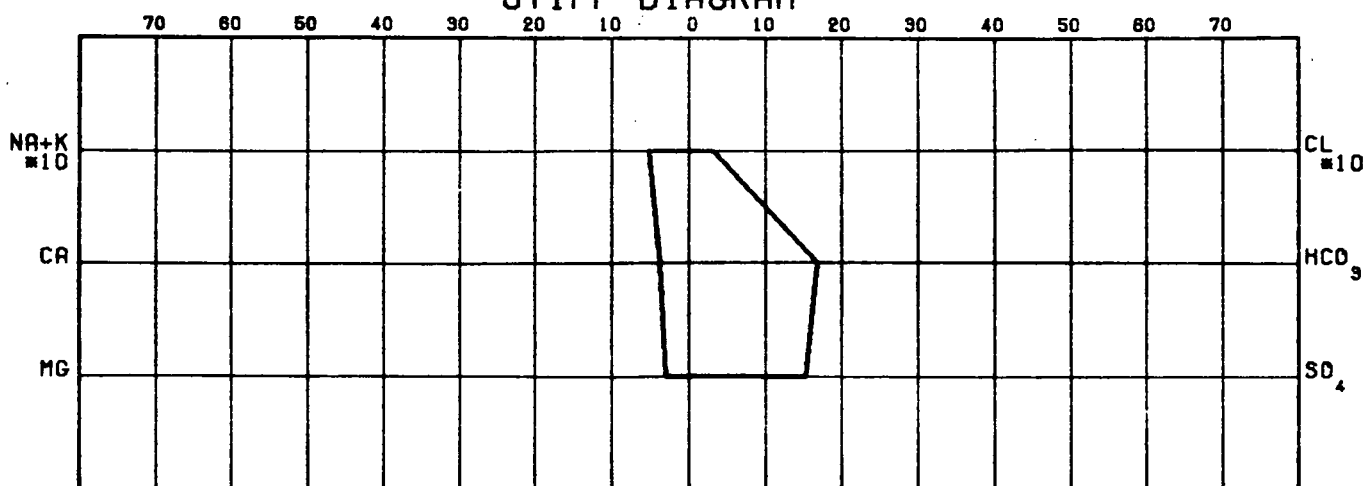
SODIUM TO TOTAL CATION RATIO: 75.0 %

PH: 7.5

SODIUM CHLORIDE EQUIVALENT: 3223.

EQUIVALENT RW AT 75 F: 1.71

STIFF DIAGRAM



00077

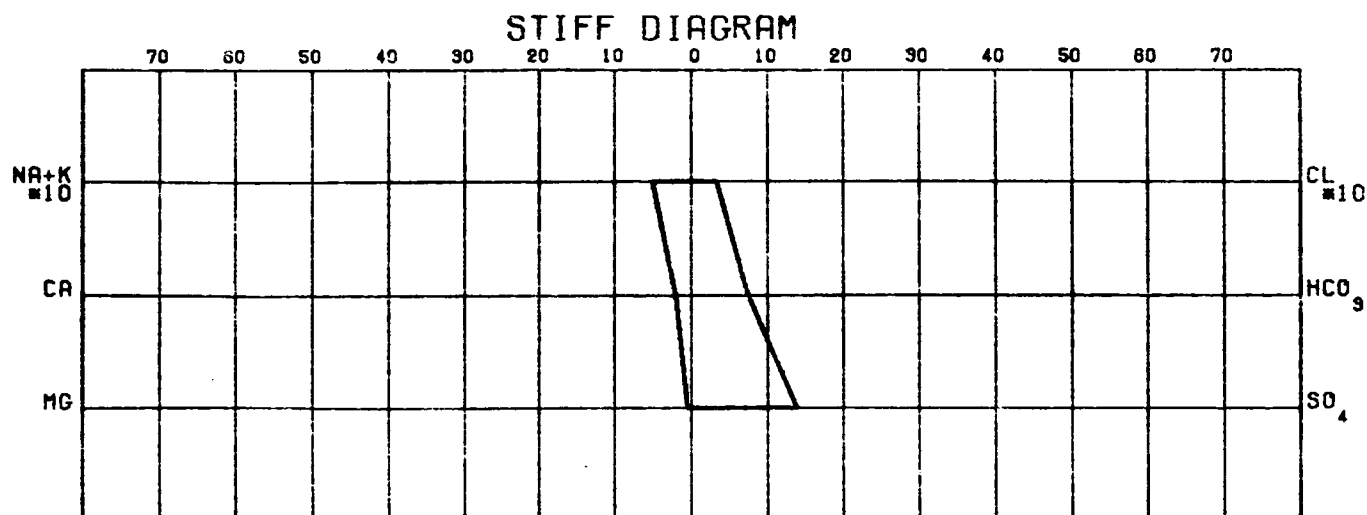
SANTOS EXPLORATION DATA BASE

WATER ANALYSIS

WELL: BIG LAKE 4 LAB: AMDEL
 TEST: DST 2 DATE: / /19
 SAMPLE: .
 DEPTH: 7685. - 7840. FT (KB) - FT (SUBSEA)
 FORMATION: TOOLACHEE TOOLACHEE COAL DARALINGIE
 COMMENT: REC: 105' W; RW(RIG)=1.1 @ 74 DEG F; 8.3 MMCFD: TOOLACHEE/DARALINGIE

CATIONS	MG/L	MEQ/L	ANIONS	MG/L	MEQ/L
SODIUM	1100.0	47.8	CHLORIDE	1195.0	33.7
POTASSIUM	100.0	2.6	BICARBONATE	455.0	7.5
CALCIUM	40.0	2.0	CARBONATE		
MAGNESIUM	6.0	0.5	SULPHATE	665.0	13.9
IRON	79.0	2.8	NITRATE	0.0	0.0
			HYDROXIDE		
TOTAL CATIONS	1325.0	55.7	TOTAL ANIONS	2315.0	55.0

ION BALANCE: 0.7 %
 TOTAL DISSOLVED SOLIDS: 3409.0 MG/L
 MEASURED RESISTIVITY: 1.934 OHM-M AT TEMP 77. F 25. C
 SODIUM TO TOTAL CATION RATIO: 85.9 %
 PH: 7.1
 SODIUM CHLORIDE EQUIVALENT: 2961.
 EQUIVALENT RW AT 75 F: 1.86



00078

SANTOS EXPLORATION DATA BASE

WATER ANALYSIS

WELL: BIG LAKE

4

LAB: AMDEL

TEST: PROD

DATE: 18/10/1984

SAMPLE: .

DEPTH: - FT (KB)

- FT (SUBSEA)

FORMATION:

COMMENT: LET 16-18/10/84: G05HMSCFD, W093.6BPD, WGR=18.72; IMBAL DUE TO NH3: TOOL/DARAL

CATIONS	MG/L	MEQ/L	ANIONS	MG/L	MEQ/L
SODIUM	4220.0	183.5	CHLORIDE	7870.0	221.7
POTASSIUM	76.0	1.9	BICARBONATE	517.0	8.5
CALCIUM	150.0	7.5	CARBONATE		
MAGNESIUM	42.0	9.5	SULPHATE	4.4	0.1
IRON			NITRATE	4.0	0.1
			HYDROXIDE		
TOTAL CATIONS	4488.0	196.4	TOTAL ANIONS	8395.4	230.3

ION BALANCE: -8.0 %

TOTAL DISSOLVED SOLIDS: 12600.0 MG/L

MEASURED RESISTIVITY: 0.426 OHM-M AT TEMP 77. F 25. C

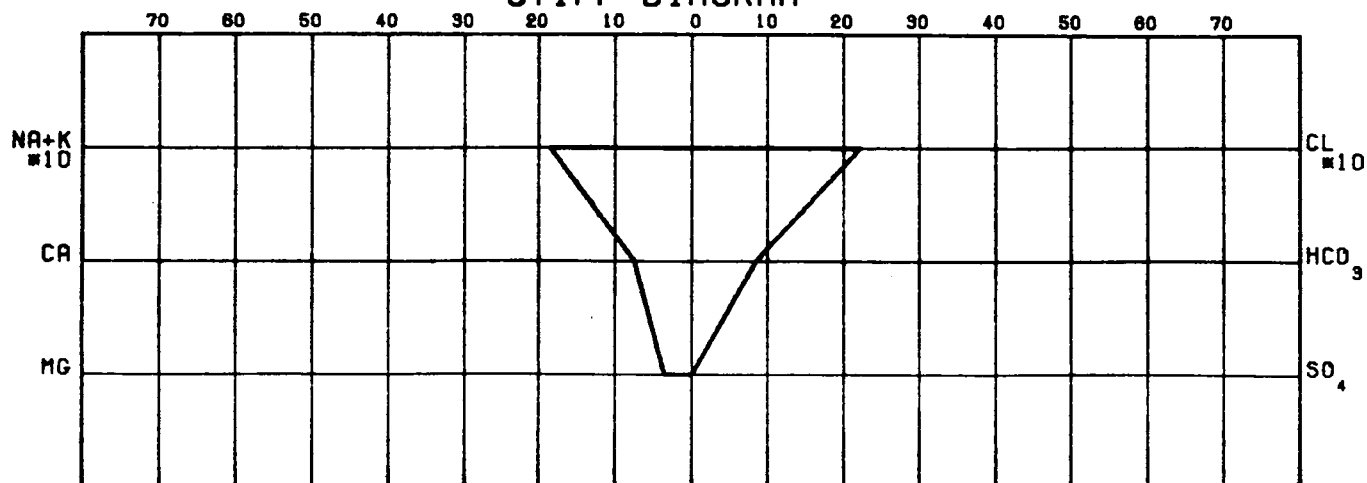
SODIUM TO TOTAL CATION RATIO: 93.4 %

PH: 6.9

SODIUM CHLORIDE EQUIVALENT: 12470.

EQUIVALENT RW AT 75 F: 0.47

STIFF DIAGRAM



OF env. 2007

00079

SANTOS EXPLORATION DATA BASE

WATER ANALYSIS

WELL: BIG LAKE

4

LAB: RMDEL

TEST: PROD

DATE: 23/02/1985

SAMPLE: .

DEPTH: - FT (KB)

- FT (SUBSEA)

FORMATION:

COMMENT: LET 21-23/2/85; G00.7MMSCFD, H/C01.3BPD, W04.5BPD, WGR=6.57; NH3: T00L/DARAL

CATIONS	MG/L	MEQ/L	ANIONS	MG/L	MEQ/L
SODIUM	1100.0	47.8	CHLORIDE	1800.0	50.7
POTASSIUM	41.0	1.0	BICARBONATE	186.0	3.0
CALCIUM	18.0	0.9	CARBONATE		
MAGNESIUM	9.4	0.8	SULPHATE	57.0	1.2
IRON			NITRATE	4.0	0.1
			HYDROXIDE		
TOTAL CATIONS	1168.4	50.5	TOTAL ANIONS	2047.0	55.0

ION BALANCE: -4.2 %

TOTAL DISSOLVED SOLIDS: 3120.0 MG/L

MEASURED RESISTIVITY: 1.670 OHM-M AT TEMP 77. F 25. C

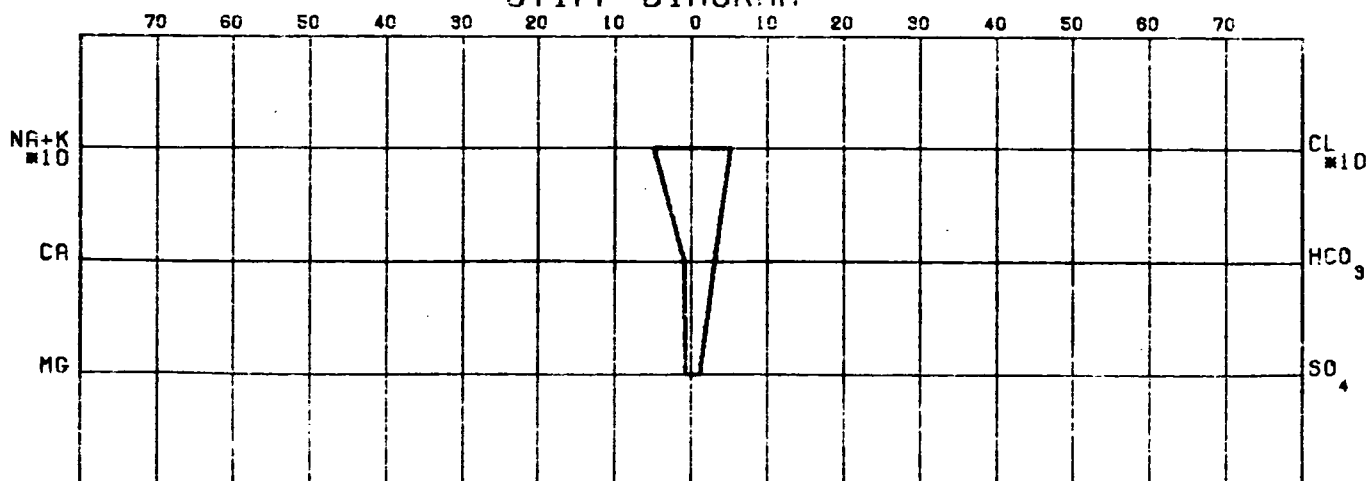
SODIUM TO TOTAL CATION RATIO: 94.6 %

PH: 5.7

SODIUM CHLORIDE EQUIVALENT: 3061.

EQUIVALENT RW AT 75 F: 1.80

STIFF DIAGRAM



SANTOS EXPLORATION DATA BASE

WATER ANALYSIS

WELL: BIG LAKE

4

LAB: AMDEL

TEST: PROD

DATE: 27/04/1986

SAMPLE: .

DEPTH: - FT (KB)

- FT (SUBSEA)

FORMATION:

COMMENT: LET 26-27/4/86: G=0.801MMSCFD. H/C=8BPD. W=32.6BPD. WGR=40.7: TOOL/DARAL

CATIONS	MG/L	MEQ/L	ANIONS	MG/L	MEQ/L
SODIUM	5700.0	247.8	CHLORIDE	9420.0	265.4
POTASSIUM	12.0	0.3	BICARBONATE	521.0	8.5
CALCIUM	190.0	9.5	CARBONATE		
MAGNESIUM	190.0	15.6	SULPHATE	5.7	0.1
IRON			NITRATE	4.0	0.1
			HYDROXIDE		
TOTAL CATIONS	6092.0	273.3	TOTAL ANIONS	9950.7	274.1

ION BALANCE: -0.2 %

TOTAL DISSOLVED SOLIDS: 15800.0 MG/L

MEASURED RESISTIVITY: 0.417 OHM-M AT TEMP 77. F 25. C

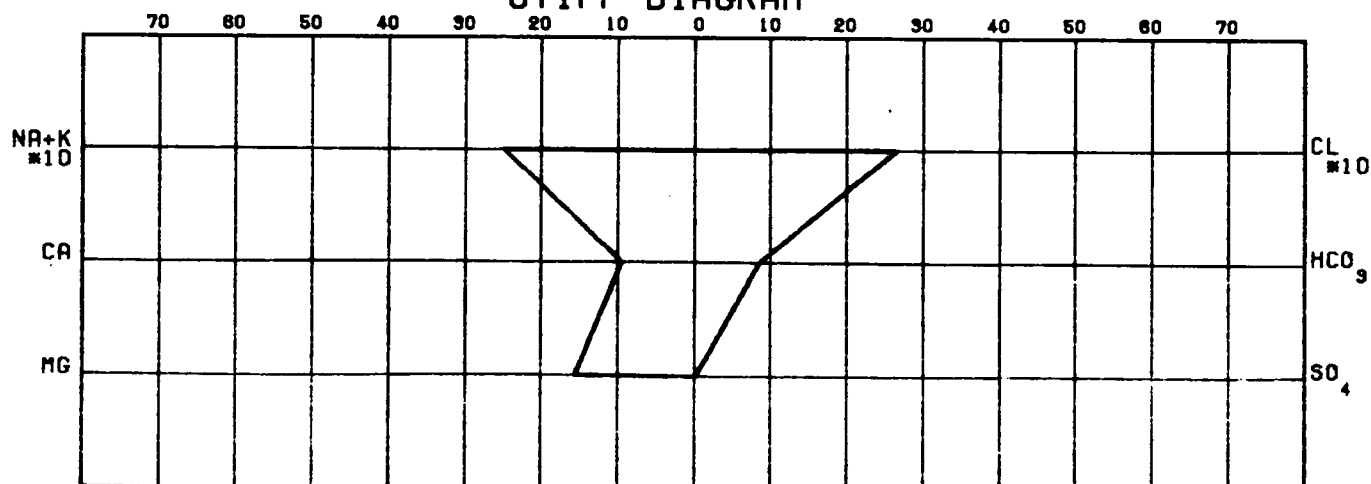
SODIUM TO TOTAL CATION RATIO: 90.7 %

PH: 6.3

SODIUM CHLORIDE EQUIVALENT: 15650.

EQUIVALENT RW AT 75 F: 0.39

STIFF DIAGRAM



00081

SANTOS EXPLORATION DATA BASE

WATER ANALYSIS

WELL: BIG LAKE

4

LAB: RMDEL

TEST: PROD

DATE: 12/05/1986

SAMPLE:

DEPTH:

FT (KB)

FT (SUBSEA)

FORMATION:

COMMENT:

CATIONS	MG/L	MEQ/L	ANIONS	MG/L	MEQ/L
SODIUM	5700.0	247.8	CHLORIDE	9420.0	265.4
POTASSIUM	12.0	0.3	BICARBONATE	521.0	8.5
CALCIUM	190.0	9.5	CARBONATE		
MAGNESIUM	190.0	15.6	SULPHATE	5.7	0.1
IRON			NITRATE	4.0	0.1
			HYDROXIDE		
TOTAL CATIONS	6092.0	273.3	TOTAL ANIONS	9950.7	274.1

ION BALANCE: -0.2 %

TOTAL DISSOLVED SOLIDS: 15800.0 MG/L

MEASURED RESISTIVITY: 0.417 OHM-M AT TEMP 77. F 25. C

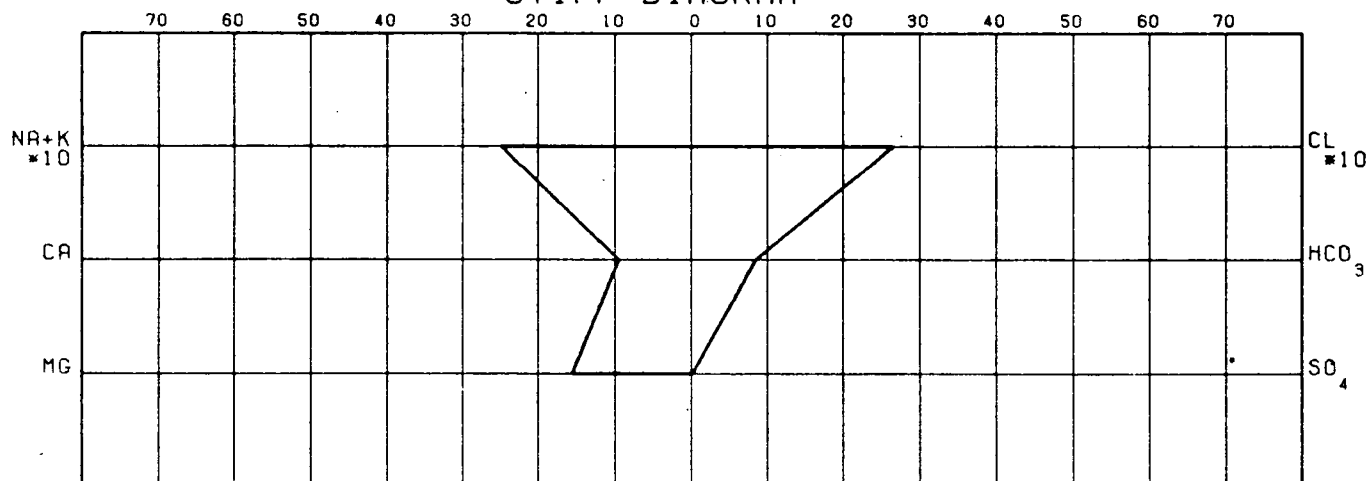
SODIUM TO TOTAL CATION RATIO: 90.7 %

PH: 6.3

SODIUM CHLORIDE EQUIVALENT: 15650.

EQUIVALENT RW AT 75 F: 0.39

STIFF DIAGRAM



00082

SANTOS EXPLORATION DATA BASE

WATER ANALYSIS

WELL: BIG LAKE

4

LAB: AMDEL

TEST: PROD

DATE: 27/10/1986

SAMPLE: .

DEPTH: -

FT (KB)

FT (SUBSEA)

FORMATION:

COMMENT: LET 26-27/10/86: G=2.342MMSCFD, W=139.68PD, WGR=59.61; TOOL/DARAL

CATIONS	MG/L	MEQ/L	ANIONS	MG/L	MEQ/L
SODIUM	5300.0	230.4	CHLORIDE	8880.0	250.1
POTASSIUM	87.0	2.2	BICARBONATE	589.0	9.7
CALCIUM	180.0	9.0	CARBONATE		
MAGNESIUM	60.0	4.9	SULPHATE	22.0	0.5
IRON			NITRATE	4.0	0.1
			HYDROXIDE		
TOTAL CATIONS	5627.0	246.6	TOTAL ANIONS	9495.0	260.3

ION BALANCE: -2.7 %

TOTAL DISSOLVED SOLIDS: 14800.0 MG/L

MEASURED RESISTIVITY: 0.408 OHM-M AT TEMP 77. F 25. C

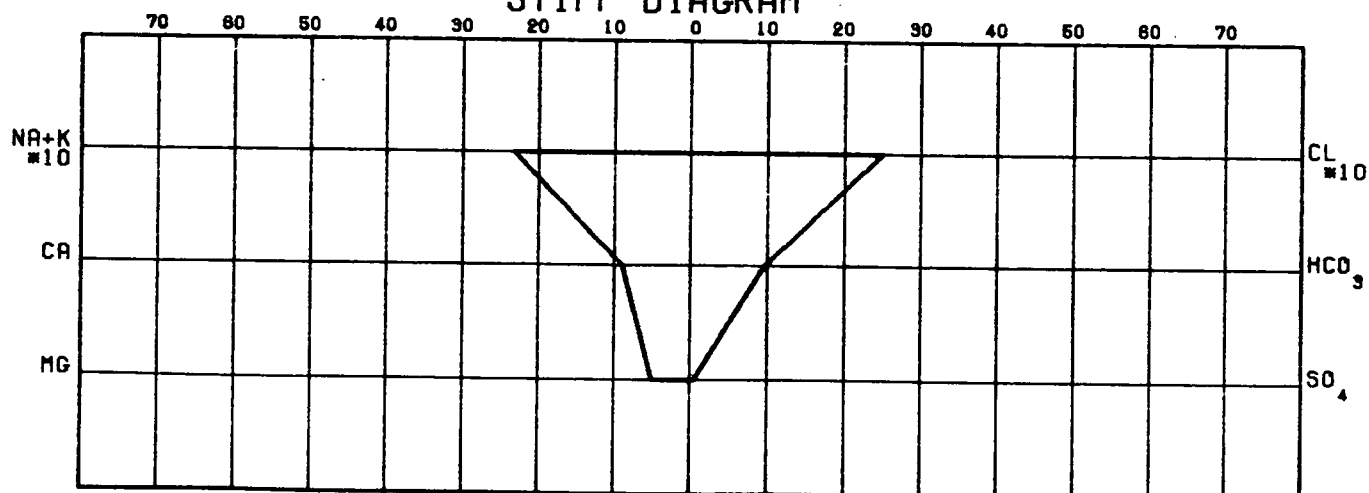
SODIUM TO TOTAL CATION RATIO: 93.5 %

PH: 6.6

SODIUM CHLORIDE EQUIVALENT: 14640.

EQUIVALENT RW AT 75 F: 0.41

STIFF DIAGRAM



00083

SANTOS EXPLORATION DATA BASE

WATER ANALYSIS

WELL: BIG LAKE

4

LAB: AMDEL

TEST: PROD

DATE: 18/02/1987

SAMPLE: .

DEPTH: - FT (KB)

- FT (SUBSEA)

FORMATION:

COMMENT: LET 4-6/2/87; G07.03MMSCFD. H/CONIL. W0214.37BPD; WGR=30.5BPD; IMBAL DUE TO NH3

CATIONS	MG/L	MEQ/L	ANIONS	MG/L	MEQ/L
SODIUM	4910.0	213.5	CHLORIDE	8680.0	244.5
POTASSIUM	66.0	1.7	BICARBONATE	513.6	8.4
CALCIUM	103.0	5.1	CARBONATE		
MAGNESIUM	52.0	4.3	SULPHATE	6.0	0.1
IRON			NITRATE	0.1	0.0
			HYDROXIDE		
TOTAL CATIONS	5131.0	224.6	TOTAL ANIONS	9199.7	253.1

ION BALANCE: -6.0 %

TOTAL DISSOLVED SOLIDS: 14074.0 MG/L

MEASURED RESISTIVITY: 0.370 OHM-M AT TEMP 77. F 25. C

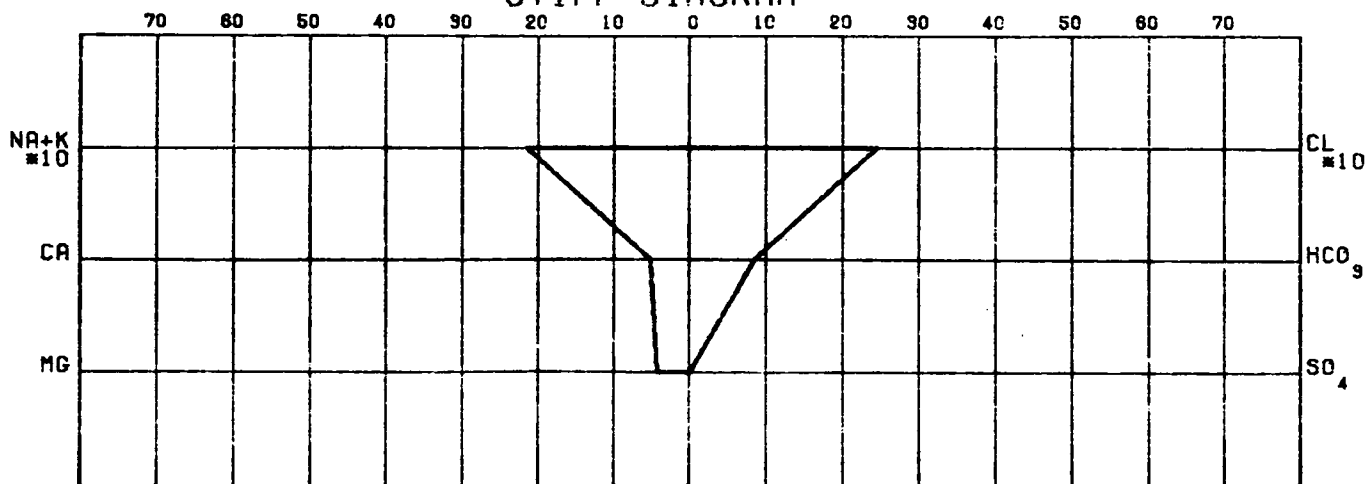
SODIUM TO TOTAL CATION RATIO: 95.1 %

PH: 5.8

SODIUM CHLORIDE EQUIVALENT: 13932.

EQUIVALENT RW AT 75 F: 0.43

STIFF DIAGRAM



00084

SANTOS EXPLORATION DATA BASE

WATER ANALYSIS

WELL: BIG LAKE

4

LAB: AMDEL

TEST: PROD

DATE: 15/06/1987

SAMPLE: .

DEPTH: - FT (KB)

- FT (SUBSEA)

FORMATION:

COMMENT: LET 15/6/87: G01.37MMSCFD. H/C01.05BPD. W04.38BPD. WGR=3.2: NH3&B: TOOL/DARAL

CATIONS	MG/L	MEQ/L	ANIONS	MG/L	MEQ/L
SODIUM	84.0	3.7	CHLORIDE	192.0	5.4
POTASSIUM	100.0	2.6	BICARBONATE	128.7	2.1
CALCIUM	7.9	0.4	CARBONATE		
MAGNESIUM	3.4	0.3	SULPHATE	50.0	1.0
IRON			NITRATE	0.1	0.0
			HYDROXIDE		
TOTAL CATIONS	195.3	6.9	TOTAL ANIONS	370.8	8.6

ION BALANCE: -10.9 Z

TOTAL DISSOLVED SOLIDS: 501.0 MG/L

MEASURED RESISTIVITY: 10.000 OHM-M AT TEMP 77. F 25. C

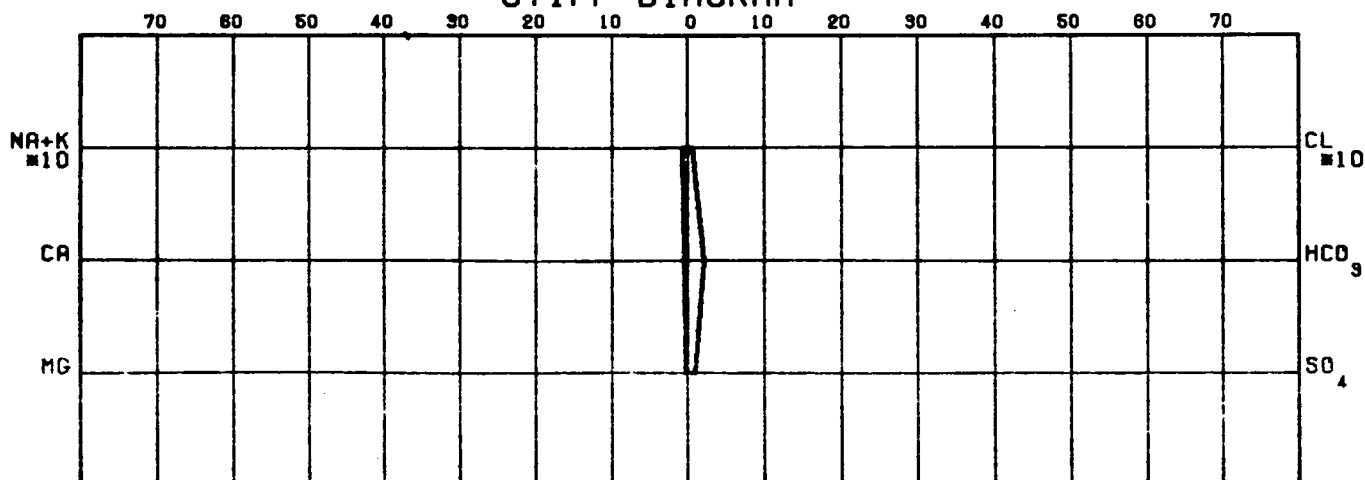
SODIUM TO TOTAL CATION RATIO: 53.1 Z

PH: 5.3

SODIUM CHLORIDE EQUIVALENT: 465.

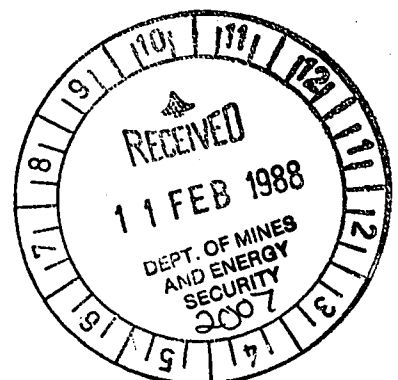
EQUIVALENT RW AT 75 F: 10.77

STIFF DIAGRAM



SANTOS LIMITED
RESERVOIR ENGINEERING DEPARTMENT
BIG LAKE #4
PRODUCTION LOGGING SURVEY 6/2/87

Report No: RE:077/87
Author: C.L. Pidcock
Date: January, 1988



1. INTRODUCTION

Big Lake #4 is located in the south-western portion of the Big Lake field. The well was drilled and completed in 1972 in the Toolachee and Daralingie sands. In 1984 the well was producing approximately 5 MMscfd prior to the shut-in of the Big Lake field. Subsequent to this the well was brought back on line at rates below 1 MMscfd. The well was loading up with water and could not produce when the Big Lake compressors were off line.

A PLT (Production Logging Tool) survey was run on the 6th February 1987 to determine the relative flow contribution from each sand under dynamic conditions and to try and locate from which sand the water was being produced. A shut-in survey was also performed to check for cross flow between sands under static conditions.

2. SUMMARY

The well was logged at a maximum flow rate and under shut-in conditions. Slugging of liquids causing a continually changing flow regime made the data very difficult to analyse. The following results were derived using the data available and engineering judgement.

SAND	<u>WELL FLOWING</u>		<u>WELL SHUT-IN</u>	
	Q (MMscfd)	% of Total	Q (MMscfd)	
	<u>Ptf = 472 psia</u>		<u>Pts = 1302 psia</u>	
Toolachee:				
Lower Unit B:-	74-5	0.25	3.5	0
	75-3	0	0	-0.68
Unit C	75-5	0.24	3.4	0.35
	76-0	<u>2.57</u>	<u>36.0</u>	<u>-0.36</u>
Sub Total Toolachee		3.06	42.9	-0.69
Upper Daralingie	76-7	0	0	0
Lower Daralingie	77-3	<u>4.07</u>	<u>57.1</u>	<u>0.69</u>
TOTAL		7.13	100.0	0
		=====	=====	=====

The survey also found approximately 550 BWPD was being produced from below the bottom perforations. The probable source of this water is a leak in the casing at 8200'KB which corresponds to the base of the Epsilon sands.

3. CONCLUSIONS & RECOMMENDATIONS

1. The Lower Daralingie sand (77-3) is the major gas producer under normal operating conditions.
2. During the survey, approximately 550 BWPD was being produced from below the bottom perforations in the Lower Daralingie Beds. As recommended by this study, a bridge plug was set above the Epsilon Formation in March 1987. During the June 1987 LET Test, Big Lake 4 was producing only 5 BWPD and 1.4 MMscfd of gas at a FWHP of 600 psia.
3. There is crossflow from the Daralingie Beds into the Toolachee Unit 'C' and Unit 'B' sands when the well is shut-in.

4. TOOL CONFIGURATION

The PLT tool string was composed of the following:

1. Gamma Ray - For depth control and detection of sands producing significant volumes of water.
2. Thermometer - To locate zones of gas entry and to obtain downhole temperatures for the calculation of $1/B_g$.
3. Strain Gauge - To measure down hole pressures for $1/B_g$ calculation.
4. Gradiomanometer - To measure fluid densities to determine gas/water entry points.
5. Full Bore Spinner - To measure fluid velocities in the wellbore.

5. DISCUSSION

5.1 Survey Method

Prior to the test commencing the well was flowed on a 40"/64" choke for 12 hours. The well was choked back to 10/64" as the PLT tool was run in the hole, returned to the initial choke setting and flowed for an additional two hours. It was found that the well was slugging and consequently there was a poor gradiomanometer and spinner response. The well was subsequently opened to 64/64" choke where it stabilized at a tubing head pressure of 472 psi. The well was still found to be slugging liquid, however, the gradiomanometer and spinner response had improved. The flow rate measured through the separator was 7.13 MMscfd with an associated liquid rate of 201 BWPd.

The test was conducted at this flow rate over the interval 7576' - 8000'KB, with the tool making 8 passes (4 up and 4 down). The well was then shut-in and allowed to build-up until the pressure had stabilized. An additional 8 passes (4 up and 4 down) were then made while the well was shut-in. Static tests were also done at specified depths subsequent to the flow and shut-in passes.

5.2 Interpretation

There are some large discrepancies in the data from the survey due to the inability of the well to obtain a constant flow regime. Readings of spinner speed vs logging speed were taken at locations above and below each set of perforations and are shown in Tables 1 and 2. This data was used to construct the lines shown in Figures 1 and 2. Due to the large variation in results these data show considerable scatter and the plots were therefore constructed using engineering judgement.

Velocities were calculated for each corresponding depth. The results indicate flow originating from below the bottom perforations and as a result the flow response line was unable to be constructed. The threshold velocity for the spinner was estimated at 17 ft/min and the spinner response at 0.13 RPS/ft/min. These values concur with those estimated by Schlumberger.

The Bg values were calculated using pressure and temperature data from the PLT logs. The overall flow rate was calculated at 7.34 MMscfd. This is comparable with the rate of 7.14 MMscfd measured through the separator. The 7.34 MMscfd represents both gas and water production as the well was continually producing with slug flow. It was decided to use 7.14 MMscfd as the actual gas rate because it gave a better representation of gas production from each sand. Flow was apportioned to each sand weighted on the corresponding velocity. This is shown in Figure 3. The flow from below the bottom perforations was determined to be water at an approximate rate of 550 BWPD calculated from the response measured at 7950'KB in Figure 1. It should be noted that water at a rate of 210 BPD was measured through the separator and this lower rate may be due to the slug flow regime.

The results from the PLT survey while the well was shut in indicate that there is crossflow between the sands. Gas flowed from the Lower Daralingie Bed (77-3) into the Toolachee Unit 'C' 75-5 and 76-0 sands at a rate of 0.69 MMscfd. There also appeared to be some crossflow from the 75-5 sand into the 75-3 sand at a rate of 0.68 MMscfd. Down hole crossflow would therefore occur from the Lower Daralingie Formation into the Toolachee Formation if the well is shut-in. This is shown in Figure 3. This crossflow is typical of the south western Big Lake wells as reported in PLT's run on Big Lake #7 (ref:RE:188/84) and Big Lake #24 (ref: RE-IN:033/83). The crossflow in Big Lake #4 shows that the Lower Daralingie formation continues to deplete slower than the Toolachee formation.

The PLT test also tried to locate the origin of the water being produced below the bottom perforations. Two possibilities were:

- (i) water was being produced from the Epsilon Formation through a leak in the casing.

(ii) water was coming through the bridge plug from the Patchawarra Formation which had previously been fracture stimulated.

The tool was only run to 8600'KB since it was not possible to proceed any further due to the temperature approaching 410°F (the tool's limit). A kick in the spinner response and some anomalies in the temperature and pressure gradients were recorded at 8200'KB. This depth corresponds to the bottom of the Epsilon formation and therefore makes the first of the two possibilities the more plausible.

TABLE I
FLOW METER DATA
BIG LAKE #4

RATE = 7.13 MMscfd @ Ptf = 472 psia
SPINNER SPEED (revolutions per second)

CABLE VELOCITY (ft/min)	DEPTH (ft KB)									
	7576	7619	7656	7667	7687	7718	7736	7802	7874	7950

Logging Down:

32	63.0	57.3	56.4	56.0	54.9	54.8	44.4	33.0	34.9	4.6
68	74.0	61.6	62.0	61.2	60.1	60.0	49.6	36.9	39.8	7.8
82	78.8	65.6	65.3	62.6	61.9	62.2	52.2	40.2	41.5	9.9
112	80.4	72.8	70.4	68.0	67.0	66.2	56.0	41.4	43.5	12.3

Logging Up:

32	54.8	52.8	51.2	48.8	54.4	50.8	43.3	29.2	30.8	1.6
46	48.1	50.2	51.7	51.6	47.6	46.8	38.4	30.9	24.8	4.9
77	46.6	52.8	44.3	47.6	45.8	45.8	37.2	29.2	27.8	7.1
116	43.9	46.0	46.8	47.6	43.6	42.4	33.2	20.9	23.4	11.6

WP:5033N(11)

CLP/jbf

18/6/87

TABLE 2
FLOW METER DATA
BIG LAKE #4

SHUT-IN SURVEY @ Pts = 1302 psia
SPINNER SPEED (revolutions per second)

CABLE VELOCITY (ft/min)	DEPTH (ft KB)									
	7576	7619	7656	7667	7687	7718	7736	7802	7874	7950
Logging Down:										
113	11.0	11.0	13.0	11.0	13.0	13.0	12.8	14.6	13.2	12.2
80	8.0	8.0	9.7	8.0	10.0	10.1	9.8	11.8	10.2	9.0
66	6.1	6.1	7.5	6.1	8.4	8.7	8.3	10.0	8.1	8.0
33	0.5	0.0	3.0	0.0	1.5	3.8	3.6	6.2	2.2	3.7
Logging Up:										
33	0.0	0.0	+2.3	0.0	0.0	0.0	0.0	+1.0	+1.5	-2.0
56	-4.0	-4.2	-2.3	-4.5	-2.2	-2.2	-2.2	-1.2	-1.2	-4.0
84	-7.8	-8.0	-4.0	-8.0	-5.8	-5.8	-5.3	-3.5	-3.5	-8.0
100	-10.0	-10.0	-6.0	-10.0	-8.0	-8.0	-7.8	-6.0	-6.0	-10.0

4P:5033N(12)

CLP/jbf

18/6/87

TABLE 3
B_g V. Q.
GAS PRODUCTION

DEPTH (ft)	RATE: -- 7.13 MMscfd			WELL SHUT-IN		
	1/B _g (scf/ft ³)	VELOCITY (ft/min)	FLOW (MMscfd)	1/B _g (scf/ft ³)	VELOCITY (ft/min)	FLOW (MMscfd)
7576	53.2	447.8	7.13	81.0	0.0	0.0
7619	53.4	432.4	6.88	81.1	0.0	0.0
7656	53.5	432.4	6.88	81.1	27.0	0.68
7667	53.6	424.7	6.76	81.1	0.0	0.0
7687	53.6	417.0	6.64	81.2	13.0	0.33
7718	53.7	417.0	6.64	81.3	13.0	0.33
7736	53.8	324.7	5.17	81.3	15.5	0.39
7802	54.0	255.5	4.07	81.8	27.0	0.69
7874	54.0	255.5	4.07	82.6	27.0	0.69

WP:5033N(13)

CLP/jbf

18/6/87

TABLE 4
SAND FLOW SUMMARY

SAND	PERFORATED INTERVAL (ft.KB)	WELL FLOWING		WELL SHUT-IN	
		Ptf = 472 psia		Pts = 1302 psia	
		Q (MMscfd)	% of Total	Q (MMscfd)	
TOOLACHEE:					
Lower Unit B	74-5	7586-7591	0.25	3.5	0
	75-3	7646-7651	0	0	-0.68
Unit C	75-5	(7661-7666	0.12	1.7	0.68
		(7668-7675	0.12	1.7	-0.33
		(7698-7713	0	0	0
	76-0	(7722-7734	1.47	20.6	-0.06
		(7737-7773	1.10	15.4	-0.30
TOOLACHEE TOTAL					
DARALINGIE:					
	76-7	7831-7839	0	0	0
LOWER DARALINGIE:					
	77-3	7908-7914	4.07	57.1	0.69
TOTAL			7.13	100.0	0.00
			=====	=====	=====

NOTE: There was a flow of approx. 550 BWPD measured at 7950 ft.

WP:5033N(14)

CLP/jbf

18/6/87

FIGURE 1
BIG LAKE #4
PLT SURVEY

(225)

SPINNER SPEEDS

FLOW RATE = 7.1 MMSCFD

STATION DEPTH
(AKB)
7576'

7681, 7718'

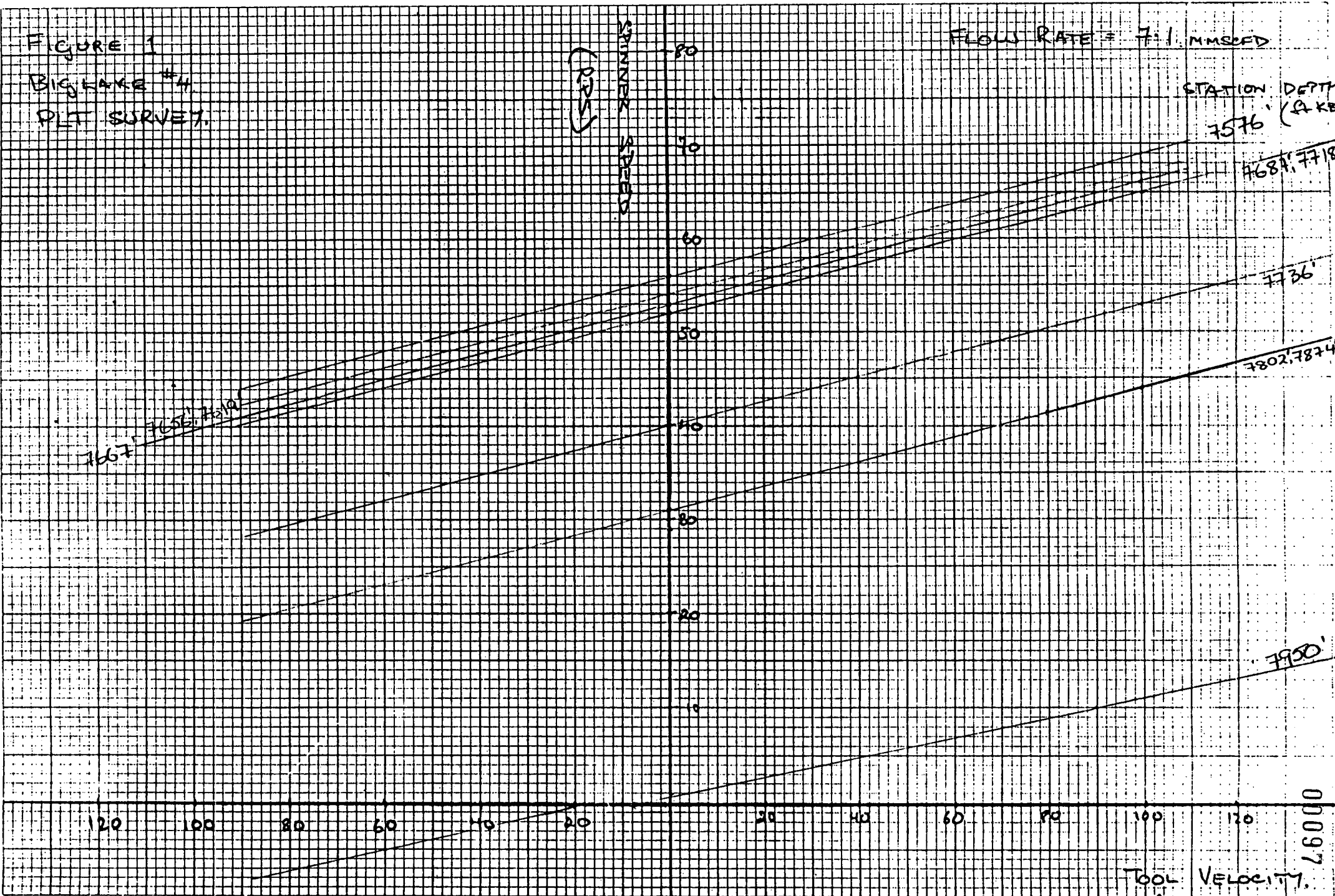
7736'

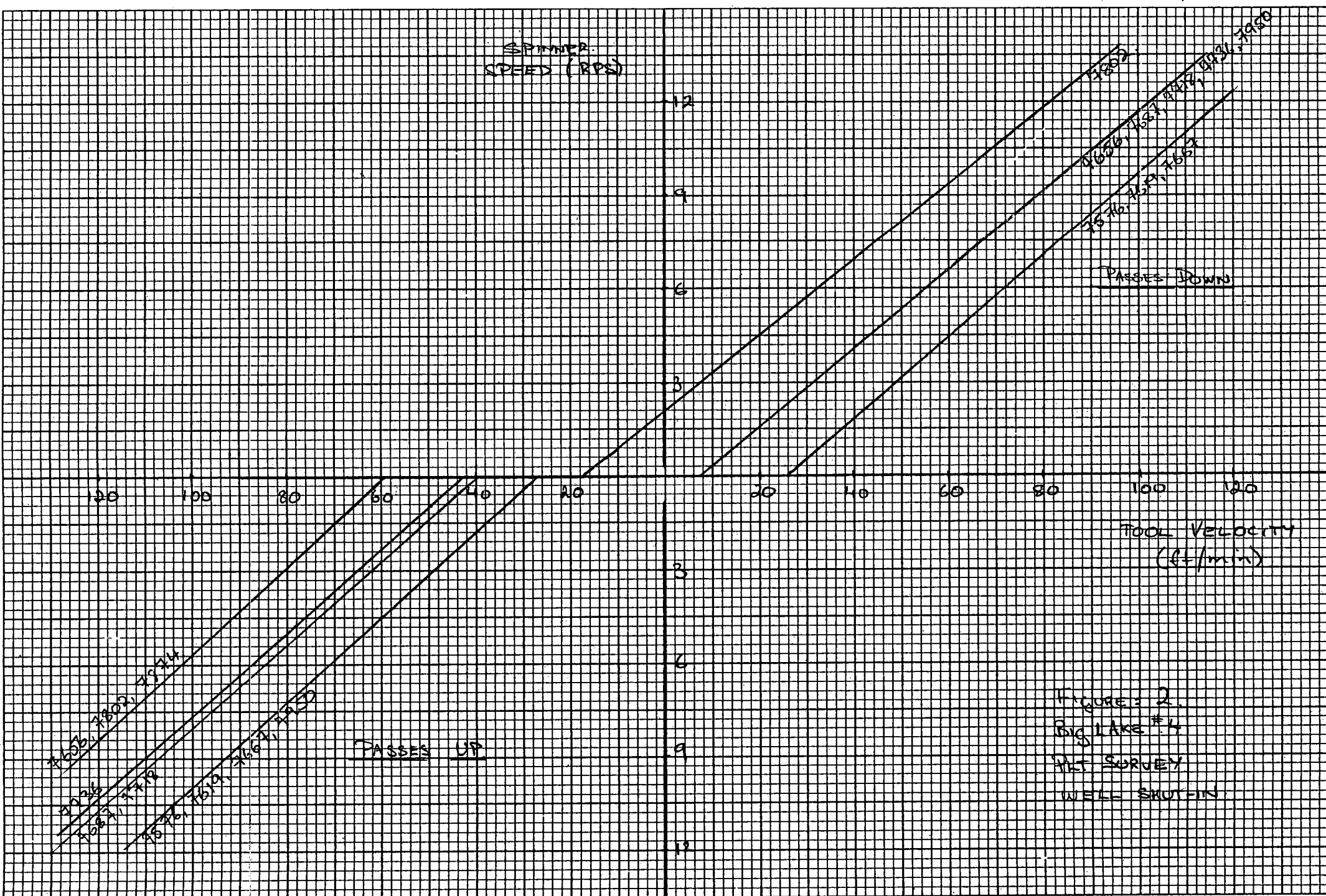
7802, 7824'

7900'

00097

TOOL VELOCITY
(FT/MIN)



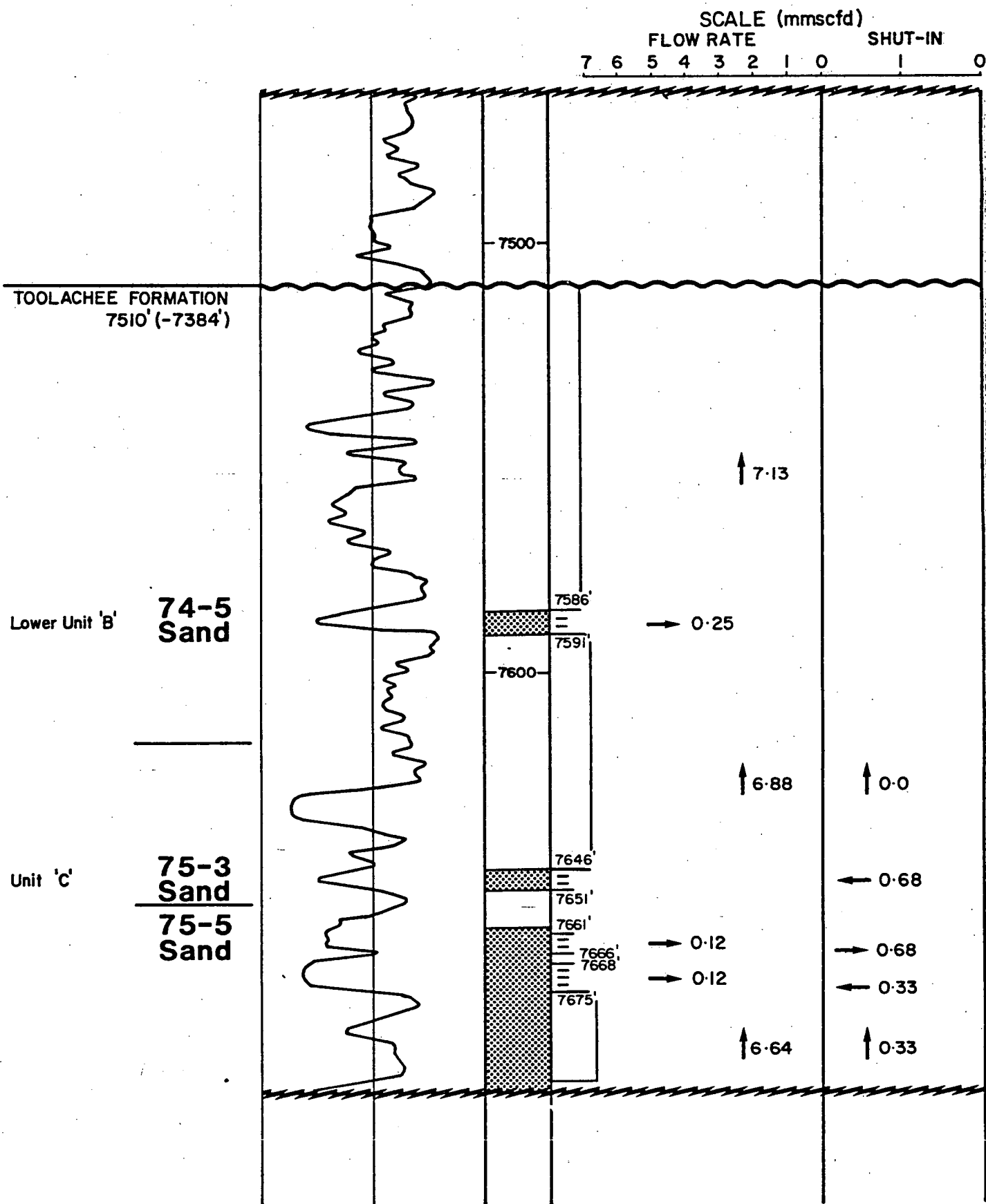


BIG LAKE 4 PLT SURVEY

GAMMA RAY OVERLAY AND FLOW DIAGRAM

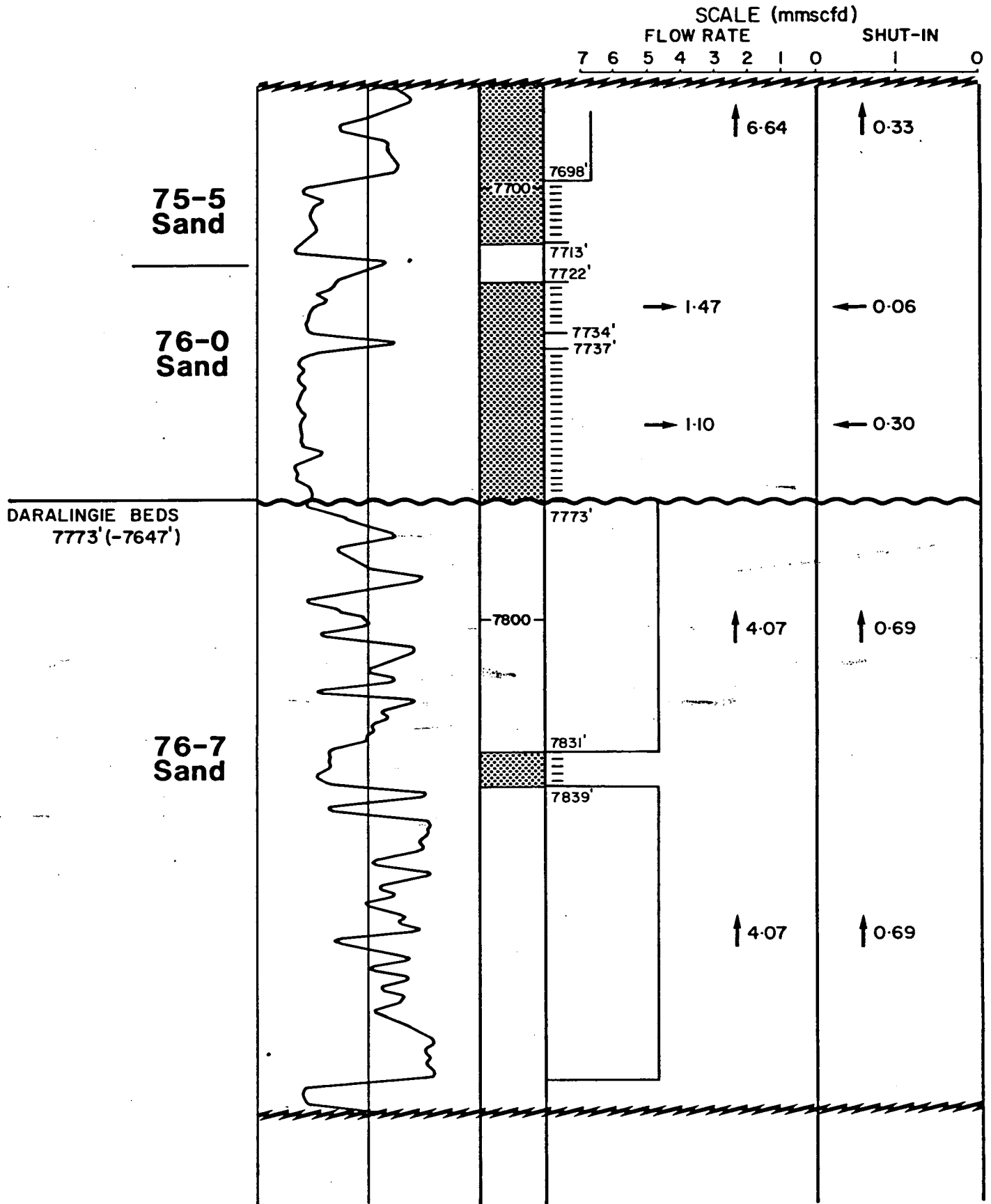
FIGURE 3

00099



GAMMA RAY OVERLAY AND FLOW DIAGRAM

00100



00101



ROLLING BOTTOMHOLE PRESSURE SURVEY GAS CALCULATION SHEET

WELL: Big Lake # 4 Pf = 5100 kPa ✓
 ORIFICE SIZE: 44.450 mm 1.750 " ✓ T = 56 °C ✓
 LINE SIZE: 87.325 mm 3.438 " ✓ Diff = 9.7 kPa ✓

Cumulative Production to end of August = 1263.596 m³ x 10⁶ ✓

Number of hours online in August = 708 ✓

Production in August = 1.601 m³ x 10⁶ ✓

• • Average flow rate in August = (1.601 / 708) x 24 = 0.054 m³ x 10⁶/d ✓

Number of days online in August after Shut In 1600 hrs 30/ 8 /87
 = NL

• • Production up to 1600 hrs 30/ 8 /87 = 1.601 m³ x 10⁶

Total cumulative production =
 = 1263.596 m³ x 10⁶
 = 44850.076 mmscf ✓

Flow rate just prior to Shut In = 0.084 m³ x 10⁶ ✓
 = 2.988 mmscf/d ✓

2007

4 NOV 87

SANTOS LTD
39 GRENFELL ST
ADELAIDE

SUB-SURFACE PRESSURE SURVEY

CO. SANTOS		RUN 01 FIELD BIG LAKE	WELL 04
EFF DEPTH		WELL STAT	TOOL HUNG 7738'
CASING 7"	-	CASING PRESS	ON BOTTOM 1303 30/8
LINER	-	TUBING PRESS	OFF BOTTOM 0600 4/9
DATE 870826		ELEMENT RANGE 0 - 3107	ZERO POINT
ELEVATION		ZONE	SHUT-IN 1600 30/8
MAX TEMP		PICK-UP	ON-PROD
PERF 7586'-7914'		CAL SER NO. 56429	MPP 7750'
TUBING 2-3/8"	-		
UNITS ENGLISH		PURPOSE BUILD-UP	

SURVEY DATA

CO. SANTOS				RUN 01 FIELD BIG LAKE				WELL 04			
TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME
16:00	1285.2	0.0	0.0	18:25	1527.1	241.9	2.4				
16:03	1347.8	62.7	.1	18:58	1525.2	240.0	3.0				
16:05	1420.8	135.6	.1	20:28	1523.4	238.2	4.5				
16:09	1487.1	201.9	.2	0:08	1522.2	237.0	8.1				
16:12	1511.1	225.9	.2	4:45	1522.4	237.2	12.7				
16:12	1523.5	238.3	.2	12:13	1522.5	237.3	20.2				
16:15	1526.3	241.1	.3	20:42	1522.9	237.7	28.7				
16:20	1529.5	244.3	.3	5:25	1522.7	237.5	37.4				
16:31	1530.7	245.5	.5	13:06	1522.7	237.5	45.1				
16:37	1532.9	247.7	.6	1:11	1522.2	237.0	57.2				
16:47	1537.4	252.2	.8	15:29	1520.9	235.7	71.5				
17:02	1540.7	255.5	1.0	3:56	1519.4	234.2	83.9				
17:19	1539.7	254.5	1.3	19:57	1519.2	234.0	99.9				
17:34	1535.7	250.5	1.6	6:01	1519.3	234.1	110.0				
17:56	1530.5	245.3	1.9	0:00	0.0	0.0	0.0				

LUB IN DWT = 790 PSI / OUT = 1257 PSI
LUB IN AMERADA = 781 PSI / OUT = 1262 PSI

SANTOS LTD
39 GRENFELL ST
ADELAIDE

SUB-SURFACE PRESSURE SURVEY

CO. SANTOS		RUN 02 FIELD BIG LAKE	WELL 04
EFF DEPTH		WELL STAT	TOOL HUNG 7744'
CASING 7"	-	CASING PRESS	ON BOTTOM 1303 30/8
LINER	-	TUBING PRESS	OFF BOTTOM 0600 4/9
DATE 870826		ELEMENT RANGE 0 - 3121	ZERO POINT
ELEVATION		ZONE	SHUT-IN 1600 30/8
MAX TEMP		PICK-UP	ON-PROD
PERF 7586' - 7914'		CAL SER NO. 28515	MPP 7750'
TUBING 2-3/8"	-		
UNITS ENGLISH		PURPOSE BUILD-UP	

SURVEY DATA

CO. SANTOS			RUN 02 FIELD BIG LAKE			WELL 04		
TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME	
16:00	1286.5	0.0	0.0	18:20	1524.2	237.6	2.3	
16:02	1342.0	55.5	.0	19:17	1523.9	237.3	3.3	
16:04	1407.6	121.1	.1	20:50	1523.2	236.6	5.0	
16:06	1467.4	180.9	.1	23:17	1522.4	235.9	7.3	
16:09	1513.5	226.9	.2	3:19	1521.7	235.2	11.3	
16:13	1528.4	241.9	.2	7:35	1521.5	234.9	15.6	
16:21	1530.7	244.2	.3	16:40	1522.2	235.6	24.7	
16:32	1534.2	247.7	.5	1:00	1522.3	235.7	33.0	
16:41	1539.9	253.4	.7	11:04	1520.6	234.1	43.1	
16:53	1539.9	253.3	.9	22:58	1520.4	233.9	55.0	
17:05	1536.9	250.3	1.1	10:53	1519.7	233.2	66.9	
17:16	1533.1	246.5	1.3	1:21	1517.9	231.3	81.3	
17:28	1531.0	244.4	1.5	18:14	1516.1	229.5	98.2	
17:52	1526.7	240.1	1.9	6:00	1517.3	230.7	110.0	

LUB IN DWT = 790 PSI / OUT = 1257 PSI
LUB IN AMERADA = 786 PSI / OUT = 1267 PSI

Well: BIG LAKE # 4.

Date: 30.8.87

Lubricator Data:

- ① 781
- ② 786

1262
1267

Pressure with D.W.T. IN 40 ps

OUT 1257 psi

Time Pressured.....1:45

Time Depressured.....0715

Time Run in Hole.....1245

Time off Bottom.....0600

Bomb No. 1 Data

Bomb No. 2 Data

Element No. and Range	56429 x 3000 psi	28515 x 3000 psi
Recorder No.	14628 x 15 TUS	13027 x 15 TUS
Clock and Lead Screw Data	K 15306 x 120 HR	K 15309 x 120 HR
Engage Stylus	Date: 30.8.87 Time: 1129	Date: 30.8.87 Time: 1129
Disengage	Date: 4.9.87 Time: 0732	Date: 4.9.87 Time: 0732

Remarks: TEMP ELE RAN - 22945 x 184° - 439°; 14621 x 157°; F8243 x 120°
WELL FLOWING ON 24/64

Max S/BH Temp = 297.8°F

Well-Head Data for Final Build-up

[illegible]

WELL: BIG LAKE #4TYPE OF TEST: BHP

SANTOS LTD.

WELL TEST DATA SHEET

DATE: 30.8.87PAGE No: ONE

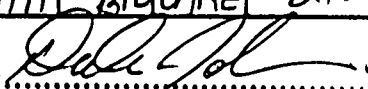
DATE TIME	WELLHEAD					GAS FLOW DATA				OIL/CONDENSATE PRODUCTION			WATER PRODUCTION		WELL TEST RESULTS				
	CASING PSI	TUBING PSI	TEMP. °F	CHOKE SIZE INS.	B.S.W. %	PI PSI	HW INS. H ₂ O	TEMP. °F	ORIFICE SIZE INS.	TANK DIP INS.	TANK PROD BBLs	API GRAVITY @60 °F	TANK DIP INS.	TANK PROD BBLs	GAS FLOW RATE MMSCFD	OIL FLOW RATE BBLs/ DAY	WATER FLOW RATE BBLs/ DAY	TOTAL LIQUID FLOW RATE BBLs/ DAY	G.O.R. SCF/BBL
30.8.87.																			
1000	ARRIVE ON LOCATION.																		
1030	S.W.1. RIG UP SWAB VALVE AND W/L UNIT																		
1045	0	1253	-	16/64		OPEN WELL TO FLARE													
1100	0	885	-	22/64		OPENED CHOKE TO DROP WELL HEAD PRESSURE													
1115	0	845	-	24/64		OPENED CHOKE TO DROP WELL HEAD PRESSURE													
1145	0	750	84	24/64		ELEMENTS IN LUB PRESSURE LUB.													
1245	0	790	84	24/64		RIH WITH ELEMENTS.													
1303	0	775	84	24/64		ELEMENTS HANGING @ 7750' KB AS PER PROGRAM.													
1330	0	769	87	24/64															
1400	0	780	84	24/64															
1430	0	785	96	24/64															
1500	0	785	86	24/64															
1530	0	787	80	24/64															
1600	0	787	80	24/64		SHUT WELL IN FOR 110 HR BUILD UP.													
1615	0	1267																	
1630	0	1280																	
1645	0	1284																	
1700	0	1280																	

OPERATOR:

00106

WELL: <u>BIG LAKE #A</u>						 SANTOS LTD. WELL TEST DATA SHEET										DATE: <u>30.8.87</u>				
TYPE OF TEST: <u>BHP</u>						PAGE No: <u>TWO</u>														
DATE TIME	WELLHEAD					GAS FLOW DATA				OIL/CONDENSATE PRODUCTION			WATER PRODUCTION		WELL TEST RESULTS					
	CASING PSI	TUBING PSI	TEMP. °F	CHOKE SIZE INS.	B.S.W. %	PI PSI	HW INS. H ₂ O	TEMP. °F	ORIFICE SIZE INS.	TANK DIP INS.	TANK PROD BBLs	API GRAVITY @ 60 °F	TANK DIP INS.	TANK PROD BBLs	GAS FLOW RATE MMSCFD	OIL FLOW RATE BBLs/DAY	WATER FLOW RATE BBLs/DAY	TOTAL LIQUID FLOW RATE BBLs/DAY	G.O.R. SCF/BBL	
30.8.87			CONTINUE BUILD UP																	
1715	0	1275																		
1730	↑	1274																		
1745		1270																		
1800		1270																		
1815		1266																		
1830		1266																		
1845		1266																		
1900		1266																		
1915		1266																		
1930		1265																		
1945		1265																		
2000	↓	1265																		
2400	0	1265																		
31.8.87																				
0400	0	1264																		
0800	↑	1264																		
1200		1264																		
1600	↓	1263																		
1800	0	1263				BUILD UP READING CHANGED TO FIT IN WITH BIG LAKE #21.														

OPERATOR



00107

WELL: <u>BIG LAKE #4</u>						 SANTOS LTD. WELL TEST DATA SHEET										DATE: <u>31.8.87</u>				
TYPE OF TEST: <u>BHP</u>						PAGE No: <u>3</u>														
DATE TIME	WELLHEAD					GAS FLOW DATA				OIL/CONDENSATE PRODUCTION			WATER PRODUCTION		WELL TEST RESULTS					
	CASING PSI	TUBING PSI	TEMP. °F	CHOKE SIZE INS.	B.S.W. %	PI PSI	HW INS. H ₂ O	TEMP. °F	ORIFICE SIZE INS.	TANK DIP INS.	TANK PROD BBLs	API GRAVITY @ 60 °F	TANK DIP INS.	TANK PROD BBLs	GAS FLOW RATE MMSCFD	OIL FLOW RATE BBLs/ DAY	WATER FLOW RATE BBLs/ DAY	TOTAL LIQUID FLOW RATE BBLs/ DAY	G.O.R. SCF/BBL	
31.8.87						CONTINUE				BUILD UP										
2200	0	1263																		
1.9.87																				
0300	0	1262																		
0600	0	1262																		
1000	0	1262																		
1400	0	1262																		
1800	0	1262																		
2200	0	1262																		
2.9.87																				
0200	0	1262																		
0600	0	1262																		
1000	0	1262																		
1400	0	1262																		
1800	0	1261																		
2200	0	1260																		
3.9.87																				
0200	0	1260																		
0600	0	1260																		

OPERATOR: *Dale Jol*

00108

WELL: <u>BIG LAKE #4</u>						SANTOS LTD.										DATE: <u>3.9.87</u>				
TYPE OF TEST: <u>BHP</u>						WELL TEST DATA SHEET										PAGE No: <u>FOUR</u>				
DATE TIME	WELLHEAD					GAS FLOW DATA				OIL/CONDENSATE PRODUCTION			WATER PRODUCTION		WELL TEST RESULTS					
	CASING PSI	TUBING PSI	TEMP. °F	CHOKE SIZE INS.	B.S.W. %	PI PSI	HW INS. H ₂ O	TEMP. °F	ORIFICE SIZE INS.	TANK DIP INS.	TANK PROD BBLs	API GRAVITY °60 °F	TANK DIP INS.	TANK PROD BBLs	FLOW RATE MMSCFD	FLOW RATE BBLs/ DAY	FLOW RATE BBLs/ DAY	TOTAL LIQUID FLOW RATE BBLs/ DAY	G.O.R. SCF/BBL	
<u>3.9.87</u>						<u>CONTINUE BUILD UP.</u>														
<u>1000</u>	<u>0</u>	<u>1260</u>																		
<u>1400</u>	<u>0</u>	<u>1260</u>																		
<u>1800</u>	<u>0</u>	<u>1259</u>																		
<u>2200</u>	<u>0</u>	<u>1259</u>																		
<u>4.9.87</u>																				
<u>0200</u>	<u>0</u>	<u>1257</u>																		
<u>0600</u>	<u>0</u>	<u>1257</u>				<u>PULL BOMBS - END OF TEST</u>														
<u>0615</u>	<u>0</u>	<u>1257</u>				<u>IN LUB</u>														
<u>0715</u>	<u>0</u>	<u>1257</u>				<u>DEPRESSURE LUB - GOOD CHARTS</u>														
<u>0758</u>	<u>0</u>	<u>1257</u>				<u>PRESS LUB - PREPARE TO RUN STATIC GRADIENT</u>														
<u>0813</u>	<u>0</u>	<u>1257</u>				<u>RIH.</u>														
<u>0925</u>	<u>0</u>	<u>1257</u>				<u>POOH FROM MPP</u>														
<u>0940</u>	<u>0</u>	<u>1257</u>				<u>LUB</u>														
<u>0950</u>	<u>0</u>	<u>1257</u>				<u>DEPRESSURE - REMOVE BOMBS GOOD CHARTS</u>														
<u>1000</u>						<u>END OF TEST HAND WELL OVER TO PRODUCTION.</u>														

OPERATOR: Dal R

00109



WIRELINE REPORT

00110

WELL: BIG LAKE # A.

DATE: 29.8.87

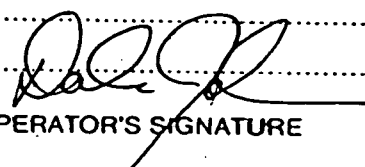
PROGRAM: BIG LAKE BHP SURVEYS

PURPOSE OF WORK: TAG PBTD

REPORT OF WORK PERFORMED:

1400 ARRIVE ON LOCATION AWAIT FIELD OPERATOR
1425 S.W.I RIG UP W/L UNIT
1445 RIH WITH 1.75" B/BOX
1505 TAG PBTD @ 7994' W/L POOH.
1525 IN LUB.
1535 RIG OUT W/L UNIT
1600 HAND WELL OVER TO PRODUCTION.

XNB & GIN POLE NOT SECURE NEEDS TOP BRACKET.


OPERATOR'S SIGNATURE

WORK PERFORMED BY: DALE JOHNS OF EXPERTEST

WELL DATA:

Tubing Size: 2 3/8 FWHP: — SIWHP: —

Sub Surface S.V./Landing Nipple @ S.S.D. @:

"X" Nipple @ "N"/"XN" Nipple @ other

Min I.D. @ Packer @ 7487

Perforated Interval: 7576' — 7914'

Forward to: Petroleum Engineering — Adelaide
Production Department — Moomba



WIRELINE REPORT

00111

WELL: BIG LAKE #4

DATE: 30.8.87

PROGRAM: BHP SURVEYS

PURPOSE OF WORK: RUN ELEMENTS AS PER PROGRAM

REPORT OF WORK PERFORMED:

30/8 1000 ARRIVE ON LOCATION - AWAIT PRODUCTION OPERATOR
1030 SWI RIG UP SWAB VALVE + W/L UNIT.
1045 OPEN WELL TO FLARE - PREPARE GAUGES.
1145 PRESSURE LUB - ELEMENTS IN LUB.
1245 RIH WITH ELEMENTS.
1303 ELEMENTS HANGING @ 7750' KB (MPP)
1600 SHUT WELL. START 110HC BUILD UP.
1/9 0600 PULL ELEM.
0615 ELEMENTS AT SURFACE
0715 DEPRESSURE LUB - GOOD CHARTS.
0803 RIH WITH ELEMENTS FOR STATIC GRADIENT
0950 ELEMENTS AT SURFACE - GOOD CHARTS - RIG DOWN
1000 HAND WELL BACK TO PRODUCTION

OPERATOR'S SIGNATURE

WORK PERFORMED BY: D. JOHNS OF EXPERTS

WELL DATA:

Tubing Size: 2 3/8 FWHP: SIWHP: 1257 ps.

Sub Surface S.V./Landing Nipple @ S.S.D. @:

"X" Nipple @ "N"/"XN" Nipple @ 7497 other

Min LD. 1.791 @ 7497 Packer @ 7470

Perforated Interval: 7594 - 8229

Forward to: Petroleum Engineering - Adelaide
Production Department - Moomba



**** BIG LAKE # 4 ****

STATIC PRESSURE GRADIENT

TEST DATE: 4/9/87

TOP PRESSURE ELEMENT 56429/3000				BOTTOM PRESSURE ELEMENT 28515/3000		
DEPTH (FT.)	DEFLECTION (INCHES)	PRESSURE (PSIG)	GRADIENT (PSI/FT)	DEFLECTION (INCHES)	PRESSURE (PSIG)	GRADIENT (PSI/FT)
LUB	0.8140	1258.4	----	0.8120	1256.9	----
1000	0.8380	1295.6	0.0373	0.8350	1292.7	0.0358
2000	0.8610	1331.3	0.0357	0.8550	1328.6	0.0358
3000	0.8820	1363.9	0.0326	0.8795	1362.1	0.0335
4000	0.9030	1396.5	0.0326	0.8995	1393.2	0.0312
5000	0.9235	1428.4	0.0318	0.9200	1425.2	0.0319
6000	0.9450	1461.8	0.0334	0.9390	1453.2	0.0281
7000	0.9650	1492.8	0.0311	0.9585	1485.2	0.0319
7750	0.9800	1516.1	0.0311	0.9730	1507.8	0.0301
LUB	0.8150	1259.9	----	0.8140	1260.0	----

GENERAL REMARKS:

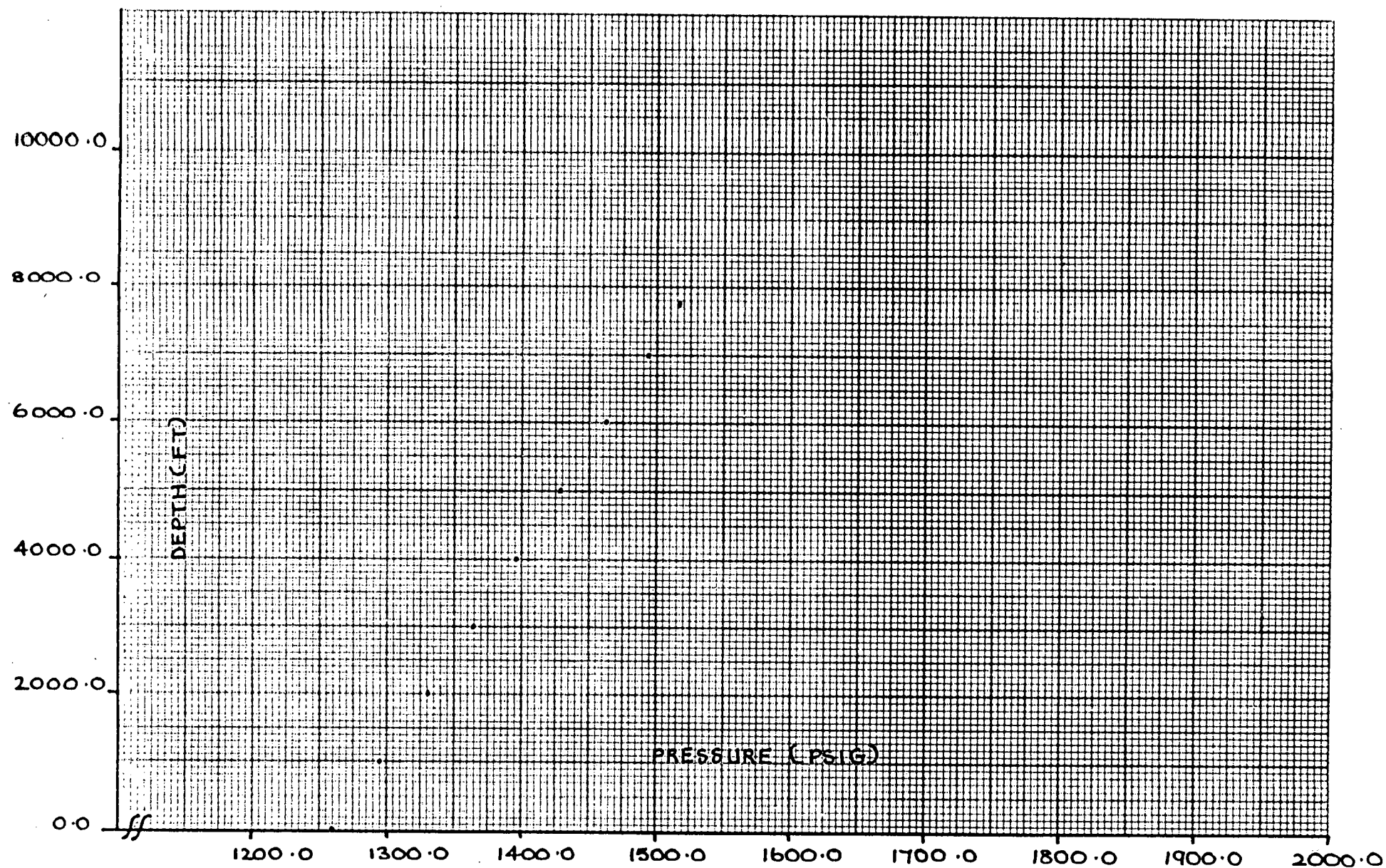
TEMP ELE USED

DWT IN: 1257
DWT OUT: 1257
MAX BHT: TEMP ELE USED 291.7°F

ELEMENT 56429/3000 CALIBRATED 26-8-87
ELEMENT 28515/3000 CALIBRATED 26-8-87

BIG LAKE # 4 - STATIC PRESSURE GRADIENT - 4/9/87

ELEMENT # 56429/3000 (TOP)



STATIC GRADIENT SURVEY

CLIENT SANTOS

WELL BIG LAKE # 4

OPERATOR DALE JOHNS

DATE 4.9.87

[illegible]

GENERAL REMARKS: TEMP FUE USED $\div$ 22945 x 1841 - 439°F.
14621 x 1575.
2395 x 342

CALIBRATED 26.8.87 @ 290°F.
TOP LOCK BACKED OFF WHILE IN HOLE

ROLLING BOTTOMHOLE PRESSURE SURVEY GAS CALCULATION SHEET

WELL: Big Lake #4 Pf = 4700 kPa
 ORIFICE SIZE: 34.000 mm 1.339 " T = 58 °C
 LINE SIZE: 87.325 mm 3.438 " Diff = 16.7 kPa

Cumulative Production to end of August = $1296.357 \text{ m}^3 \times 10^6$

Number of hours online in August = 744

Production in August = $1.679 \text{ m}^3 \times 10^6$

.. Average flow rate in August = $(1.679/744) \times 24 = 0.054 \text{ m}^3 \times 10^6/\text{d}$

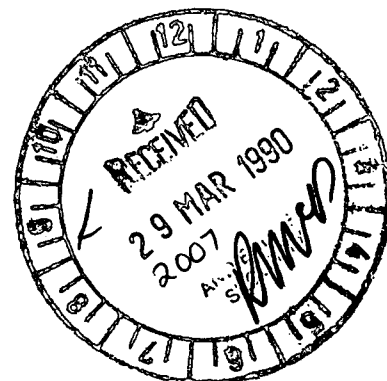
Number of days online in Sep before Shut In 0800 hrs 3 / 9 / 89
 = 2.292

.. Production up to 0800hrs 3 / 9 / 89 = $0.054 \times 2.292 = 0.124 \text{ m}^3 \times 10^6$

Total cumulative production = $1296.357 + 0.124$
 = $1296.481 \text{ m}^3 \times 10^6$
 = 46017.288 mmscf ✓

Flow rate just prior to Shut In = $0.060 \text{ m}^3 \times 10^6$
 = 2.128 mmscf/d ✓

2007



SUB-SURFACE PRESSURE SURVEY

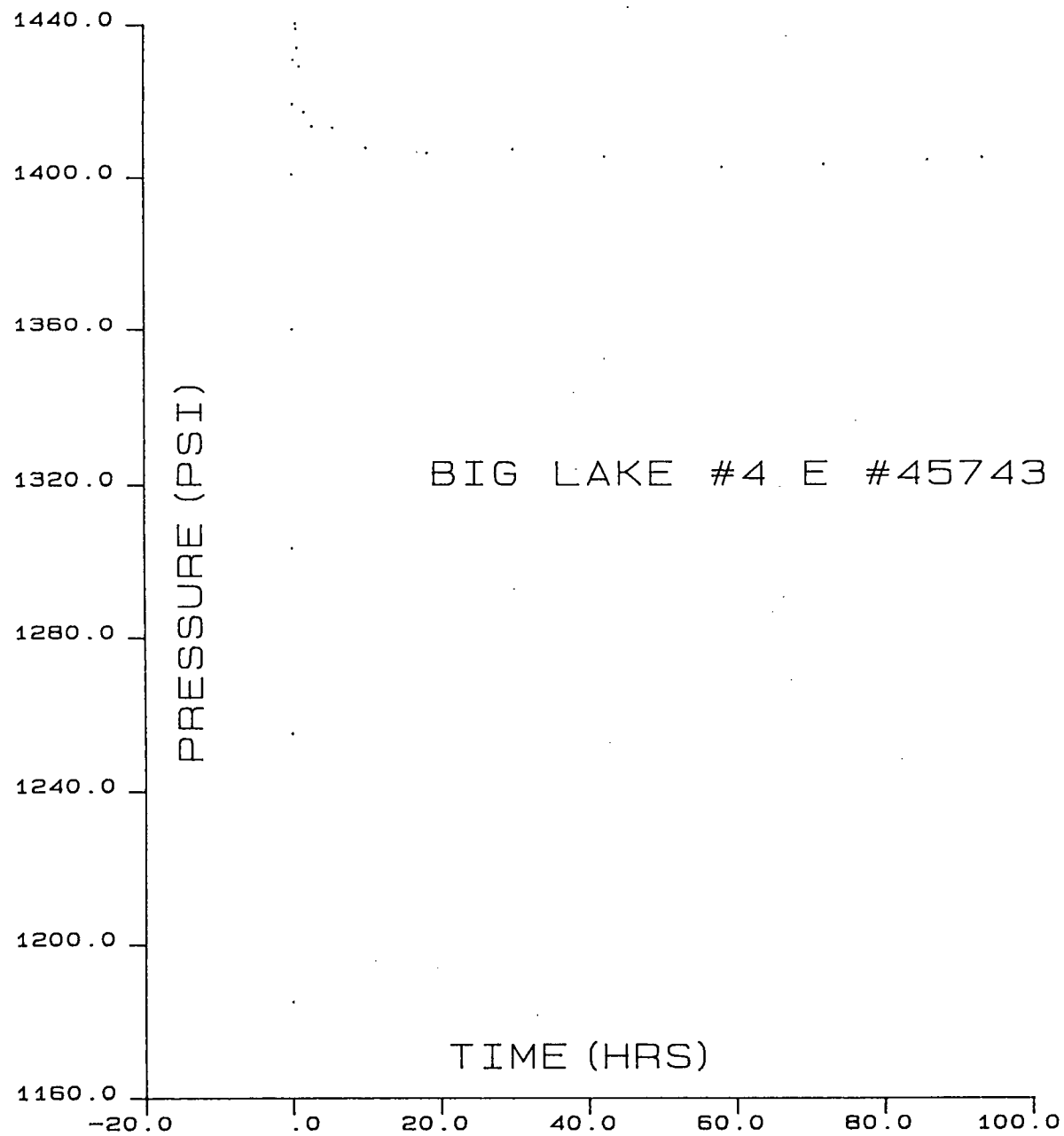
CO.		RUN 01 FIELD BIG LAKE	WELL 04
EFF DEPTH		WELL STAT	TOOL HUNG 7744'
CASING	-	CASING PRESS	ON BOTTOM 1400 2/9
LINER	-	TUBING PRESS	OFF BOTTOM 0800 7/9
DATE	890902	ELEMENT RANGE 0 - 4082	ZERO POINT
ELEVATION		ZONE	SHUT-IN 0800 3/9
MAX TEMP		PICK-UP	ON-PROD
PERF	-	CAL SER NO. 45743	MPP
TUBING	-		
UNITS	ENGLISH	PURPOSE	BUILD-UP

SURVEY DATA

CO.	TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME
	8:00	1185.1	1185.1	.0	9:48	1417.0	1417.0	1.8
	8:01	1255.1	1255.1	.0	10:51	1413.4	1413.4	2.9
	8:03	1303.4	1303.4	.0	13:43	1412.9	1412.9	5.7
	8:05	1360.2	1360.2	.1	18:10	1407.6	1407.6	10.2
	8:08	1400.8	1400.8	.1	2:28	1406.2	1406.2	18.5
	8:13	1419.1	1419.1	.2	14:02	1407.2	1407.2	30.0
	8:22	1430.7	1430.7	.4	2:24	1405.1	1405.1	42.4
	8:38	1440.3	1440.3	.6	18:20	1402.3	1402.3	58.3
	8:44	1438.8	1438.8	.7	8:07	1403.2	1403.2	72.1
	8:54	1434.1	1434.1	.9	22:07	1404.3	1404.3	86.1
	9:11	1429.0	1429.0	1.2	5:31	1404.8	1404.8	93.5

LUB IN DWT = 712 PSI / OUT = 1186 PSI
 LUB IN DWT = 713 PSI / OUT = 1178 PSI

NOTE; CLOCKS RAN OUT.



00117

SUB-SURFACE PRESSURE SURVEY

CO.		RUN 02 FIELD BIG LAKE	WELL 04
EFF DEPTH		WELL STAT	TOOL HUNG 7750'
CASING	-	CASING PRESS	ON BOTTOM 1400 2/9
LINER	-	TUBING PRESS	OFF BOTTOM 0800 7/9
DATE	890902	ELEMENT RANGE 0 - 4067	ZERO POINT
ELEVATION		ZONE	SHUT-IN 0800 3/9
MAX TEMP		PICK-UP	ON-PROD
PERF	-	CAL SER NO. 45735	MPP
TUBING	-		
UNITS	ENGLISH	PURPOSE	BUILD-UP

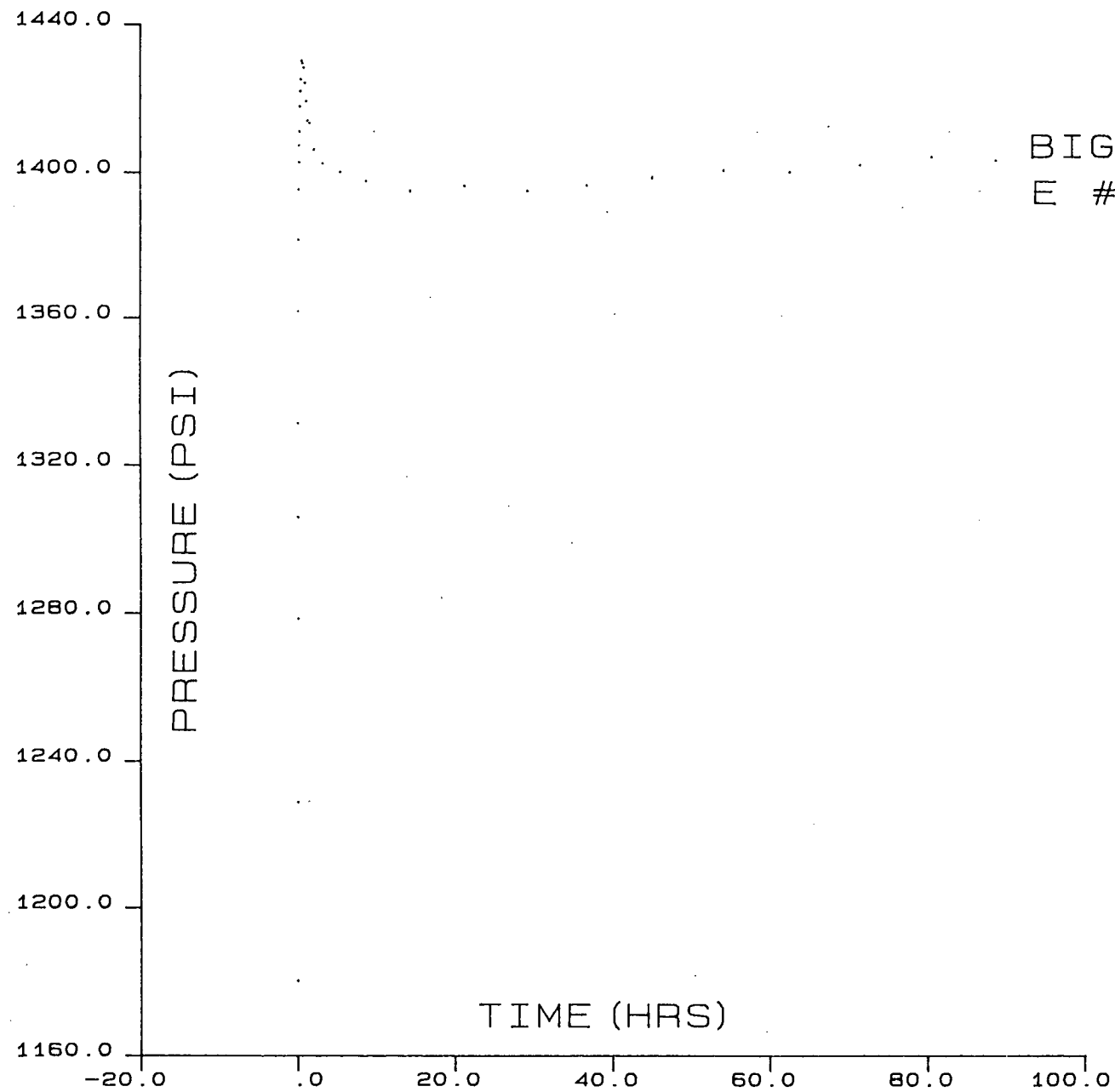
SURVEY DATA

CO.	TIME	P-T	DP-DT	DTIME	TIME	P-T	DP-DT	DTIME
	8:00	1180.4	1180.4	.0	9:11	1419.3	1419.3	1.2
	8:02	1228.8	1228.8	.0	9:21	1414.0	1414.0	1.3
	8:04	1278.5	1278.5	.1	9:36	1413.3	1413.3	1.6
	8:05	1306.0	1306.0	.1	10:09	1406.1	1406.1	2.1
	8:06	1331.3	1331.3	.1	11:14	1402.5	1402.5	3.2
	8:07	1361.7	1361.7	.1	13:27	1400.0	1400.0	5.5
	8:09	1381.6	1381.6	.1	16:45	1397.6	1397.6	8.8
	8:11	1395.3	1395.3	.2	22:23	1394.8	1394.8	14.4
	8:13	1402.8	1402.8	.2	5:18	1396.4	1396.4	21.3
	8:15	1407.3	1407.3	.3	13:18	1394.9	1394.9	29.3
	8:18	1411.2	1411.2	.3	20:48	1396.6	1396.6	36.8
	8:21	1417.8	1417.8	.3	5:08	1398.6	1398.6	45.1
	8:27	1421.9	1421.9	.5	14:12	1400.7	1400.7	54.2
	8:31	1425.2	1425.2	.5	22:37	1400.1	1400.1	62.6
	8:38	1430.1	1430.1	.6	7:32	1402.2	1402.2	71.5
	8:44	1429.3	1429.3	.7	16:37	1404.3	1404.3	80.6
	8:52	1428.1	1428.1	.9	0:47	1403.2	1403.2	88.8
	9:02	1424.1	1424.1	1.0	5:27	1404.3	1404.3	93.5

LUB IN DWT = 712 PSI / OUT = 1186 PSI

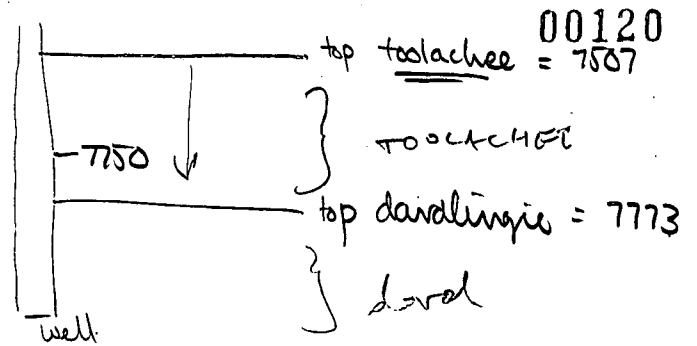
LUB IN AMERADA = 709 PSI / OUT = 1174 PSI

NOTE ; CLOCKS RAN OUT.



BIG LAKE #4
E #45735

00119



EXPERTEST PTM Ltd

WIRELINE & WELL TESTING SERVICE

PO BOX 354 COWANDILLA 5033

Tested Thursday, 7th September 1989.

PH. (08) 354 0488 TELEX AA87183

FAX (08) 43 7408

138 RICHMOND ROAD MARLESTON
SOUTH AUSTRALIA 5033

CLIENT	LOCATION	FORMATION
Santos Ltd.	Big Lake # 4	0

STATIC PRESSURE GRADIENT REPORT

PRESSURE ELEMENT DATA			
POSITION	SERIAL NO.	RANGE	CALIBRATED
Top	45743	4000	30/ 7/89
Bottom	45735	4000	30/ 7/89

WELL DATA	
PARAMETER	VALUE
DWT In	1185 PSI
DWT Out	1181 PSI
Max BHT	274 F

DEPTH FT KE	TOP ELEMENT			BOTTOM ELEMENT		
	DEFLECTION INCHES	PRESSURE PSIG	GRADIENT PSI/FT	DEFLECTION INCHES	PRESSURE PSIG	GRADIENT PSI/FT
LUB.	0.4360	889.8	-----	0.5760	1170.9	-----
1000	0.5930	1209.7	0.320	0.5930	1205.4	0.035
2000	0.6090	1242.3	0.033	0.6090	1237.8	0.032
3000	0.6240	1272.9	0.031	0.6230	1266.2	0.028
4000	0.6390	1303.4	0.031	0.6390	1298.6	0.032
5000	0.6530	1332.0	0.029	0.6520	1324.9	0.026
5500	0.6600	1346.2	0.029	0.6590	1339.1	0.028
6000	0.6670	1360.5	0.029	0.6660	1353.3	0.028
6500	0.6720	1370.7	0.020	0.6730	1367.5	0.028
7000	0.6790	1384.9	0.029	0.6800	1381.6	0.028
7750	0.6900	1407.4	0.030	0.6890	1399.9	0.024
LUB.	0.4820	983.6	-----	0.5750	1168.9	-----

GENERAL REMARKS

M B H T 274 F

BIG LAKE # 4 - STATIC PRESSURE GRADIENT - 7/9/89
ELEMENT # 45735/4000 (BOT)

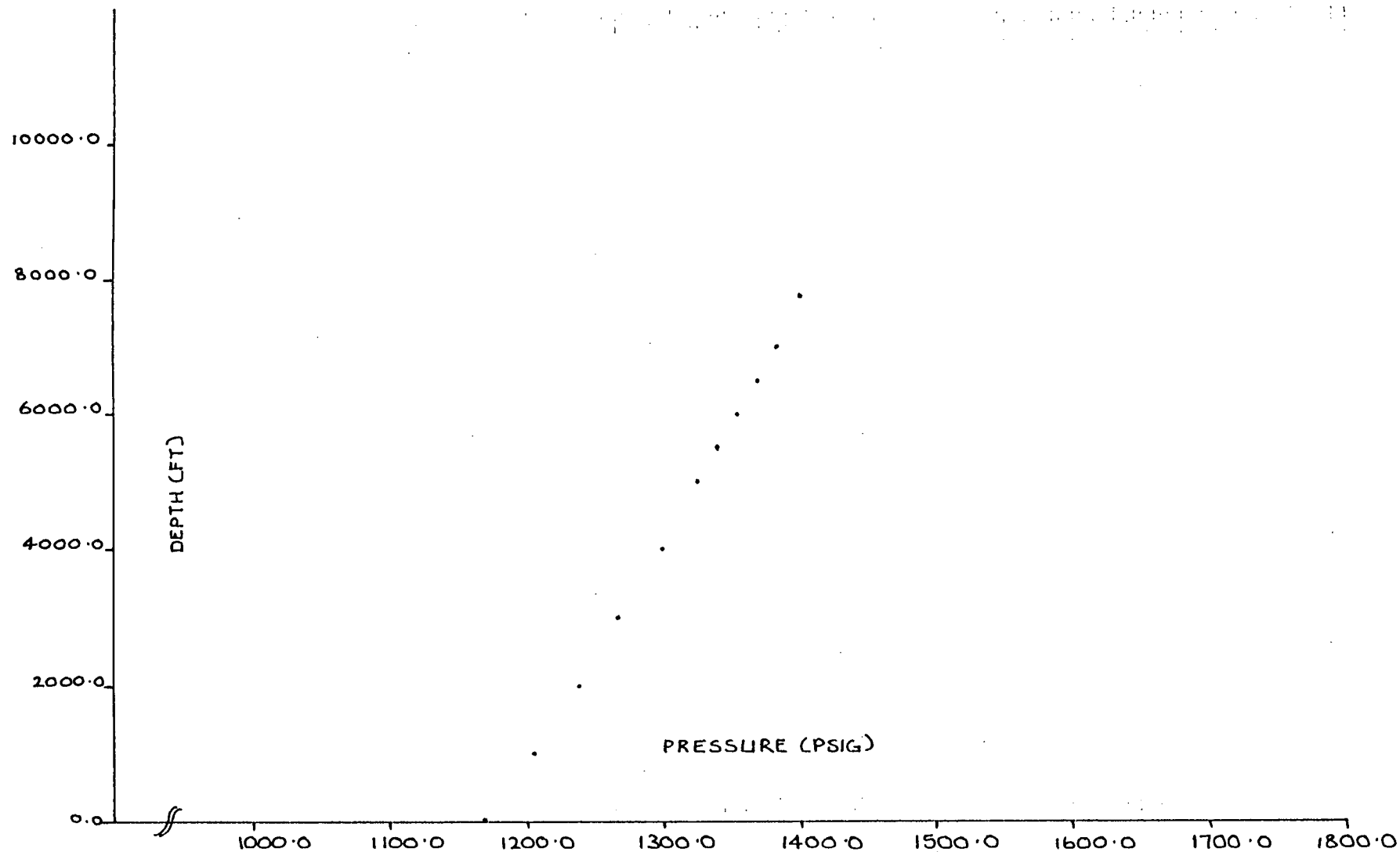


FIG 5030



WIRELINE REPORT

CLIENT SANTOS WELL BIG LAKE #4

DATE 1.9.89

PROGRAMME BOTTOM HOLE PRESSURE SURVEY

PURPOSE OF WORK BLIND BOX RUN: TO ENSURE TUBING IS CLEAR OF OBSTRUCTIONS PRIOR TO RUNNING AMERADAS

REPORT OF WORK PERFORMED

14.30 SWI RIG UP SWAB VALVE AND W/L UNIT
 15.00 RUN IN HOLE WITH 1.75" BLIND BOX
 15.35 TAG AN OBSTRUCTION @ 7495^{KB}
 JAR DOWN 4 TIMES, UNABLE TO PASS
 THROUGH OBSTRUCTION
 15.45 P.O.O.H
 16.20 @ SURFACE, DEP. LUBRICATOR
 WELL ON LINE, SECURE LEASE O/NIGHT

[Signature]
 Operator's Signature

WORKED PERFORMED BY P. DOUGLAS / W. BOND OF EXPERTEST

WELL DATA:

Tubing Size 2 3/8" FWHP 4875 SIWHP 8302

Subsurface S.V./Landing Nipple @ S.S.D. @

'X' Nipple @ 'N'/XN' Nipple @ Other @

Min. I.D. 1.990" @ 7487.00' Packer @ 7487.00'

Perforated Interval: 7586' - 7914'



WIRELINE REPORT

CLIENT SANTOS WELL BIG LAKE # 4 DATE 2.9.89
 PROGRAMME BOTTOM HOLE PRESSURE SURVEY
 PURPOSE OF WORK CLEAR OBSTRUCTION IN TUBING

REPORT OF WORK PERFORMED

07:00 STANDBY ON INSTRUCTIONS FROM P.E. OFFICE.
 Do PAPERWORK & READ CHARTS FROM BIG LAKE #22
 08:30 TRAVEL TO LOCATION WITH MEDIUM SIZE WIRE LINE
 UNIT #53 & REAMING TOOLS
 09:20 STANDBY ON FIELD OPS TO SHUT WELL IN.
 09:40 R.I.H. WITH 1.5" TOOL STRING. ENCOUNTER OBSTRUCTION
 @ 7495 KB ; JAR DOWN 6-7 TIMES ON
 OBSTRUCTION & CLEAR
 RUN UP & DOWN THROUGH SEVERAL TIMES
 - ALL CLEAR
 10:00 R.I.H. & TAG P.B.T.D. @ 7459' KB
 10:20 P.O.O.H.
 10:40 @ SURFACE ; DEP LUB ; RIG UP TANDEM PRESSURE
 ELEMENTS & HANG IN LUB FOR B.H.P SURVEY
 11:00 STANDBY FOR FIELD OPS TO PUT WELL ON LINE
 11:25 PUT WELL ON LINE
 11:30 PRESSURE LUBRICATOR & HANG IN LUB FOR 2HRS
 13:30 R.I.H. WITH TANDEM PRESSURE ELEMENTS
 14:00 HANG GAUGES @ 7750' KB

Operator's Signature

WORKED PERFORMED BY P. DOUGLAS / W. BOND OF EXPERTEST

WELL DATA:

Tubing Size 2 3/8" FWHP 4909 SIWHP 8302
 Subsurface S.V./Landing Nipple @ S.S.D. @
 'X' Nipple @ 'N'/'XN' Nipple @ Other @
 Min. I.D. 1.990" @ 7487' Packer @ 7487'
 Perforated Interval: 7586 - 7914



CLIENT SANTOS

STATIC GRADIENT SURVEY

WELL BIG LAKE #4

OPERATOR N. HAY

DATE 7-9-89

BOMB No. 1 DATA						BOMB No 2 DATA				DWT IN 8177 KPA DWT OUT 8149 KPA	
ELEMENT No. <u>D-45743</u>		ELEMENT RANGE <u>4000 PSI</u>				ELEMENT No. <u>D-45735</u>		ELEMENT RANGE <u>4000 PSI</u>			
RECORDER No <u>55338</u>		CLOCK DATA <u>2431 X 3HR 15TL5</u>				RECORDER No <u>55337</u>		CLOCK DATA <u>2509 X 3HR 15TL5</u>			
ENGAGE STYLUS <u>10:40</u>		DISENGAGE <u>13:00</u>				ENGAGE STYLUS <u>10:40</u>		DISENGAGE <u>13:00</u>			
PRESSURE LUBRICATOR <u>10:50</u>						BLEED LUBRICATOR <u>12:56</u>					
DATE	TIME	DEPTH'	DEFLEC-TION	PRESSURE TEMP.	GRADIENT psi/ft	DEPTH'	DEFLEC-TION	PRESSURE TEMP.	GRADIENT psi/ft	REMARKS	
7-9-89		LUB	.436			LUB	.576			HANG 15 MIN	
	11:05									R.I.H	
	11:08	1000	.593			1000	.593			HANG 5	
	11:15	2000	.609			2000	.609				
	11:22	3000	.624			3000	.623				
	11:29	4000	.638			4000	.639				
	11:36	5000	.653			5000	.652				
	11:42	5500	.660			5500	.659				
	11:48	6000	.667			6000	.666				
	11:54	6500	.672			6500	.673				
	12:00	7000	.679			7000	.680				
	12:07	7750	.690			7750	.689				
	12:22									P.O.D.H	
	12:41	LUB	.482			LUB	.575			HANG 15 MIN	
										M.B.H.T 274°F	

GENERAL REMARKS:



Well: BIG LAKE #4 Date: 2ND SEPTEMBER 1989

Lubricator Data: ① 713 / 1178 Operator W. BOND
 ② 709 / 1174

Pressure with D.W.T. In 4909 kPa (112 psi) Out 8177 kPa (1186 psi)

Time Pressured 11:30 2.9.89 Time Depressured 10:20

Time Run in Hole 13:30 2.9.89 Time off Bottom 08:00

Bomb No. 1 Data

Bomb No. 2 Data

Element No. and Range	D-45743 x 4000 Psi	D-45735	x 4000 Psi
Recorder No.	55338 x 15 TLS	55337	x 15 TLS
Clock and Lead Screw Data	F15308 x 120 HRS	F1530A	x 120 HRS
Engage Stylus	Date: 2.9.89 Time: 10:43	Date: 2.9.89	Time: 10:43
Disengage	Date: 7.9.89 Time: 10:31	Date: 7.9.89	Time: 10:31

Remarks: MAXIMUM BOTTOMHOLE THERMOMETER RUN

Clocks Ran Out.

Well-Head Data for Final Build-up

Date	Time	Hours shut-in Time	Wellhead KPa	Casing KPa	Wellhead Temp. °C	Remarks
2ND	SEPTEMBER 1989					
	11:30		4909	∅	41	PRESSURE LUB
	13:30		4944	↑	59	RUN IN HOLE
	14:00		4985		59	HANG GAUGES @ 7750
	16:00		5040		59	
	20:00		4992		60	
	24:00		4937		60	
3RD	SEPTEMBER 1989					
	04:00		4930		60	
	06:00		4930		60	
	06:30		4930		60	
	07:00		4923		61	
	07:30		4930		61	
	08:00		4944		61	SHUT WELL IN
	08:05		7847			COMMENCE 96 HOUR
	08:10		8184			BUILD-UP
	08:15		8253			
	08:30		8357			
	08:45		8357			
	09:00	1 HOUR	8322			
	09:15		8281			
	09:30		8246	↓		
	09:45		8226	∅		



Well: BIG LAKE # 4 Date: 3RD SEPTEMBER 1989

Lubricator Data: Operator W. BOND

Pressure with D.W.T. In 4909 kPa 2-9-89 Out 8177 MPa 7-9-89

Time Pressured 11:30 2-9-89 Time Depressed 10:20

Time Run in Hole 13:30 2-9-89 Time off Bottom 08:00

Bomb No. 1 Data

Bomb No. 2 Data

Element No. and Range	D-45743 x 4000 Psi	D-45735 x 4000 Psi
Recorder No.	55338 x 15 TLS	55337 x 15 TLS
Clock and Lead Screw Data	F15308 x 120 HRS	F15309 x 120 HRS
Engage Stylus	Date: 2-9-89 Time: 10:43	Date: 2-9-89 Time: 10:43
Disengage	Date: 7-9-89 Time: 10:31	Date: 7-9-89 Time: 10:31

Remarks: MAXIMUM BOTTOM HOLE THERMOMETER RUN

Well-Head Data for Final Build-up

Date	Time	Hours shut-in Time	Wellhead KPa	Casing KPa	Wellhead Temp.	Remarks
3RD	SEPTEMBER 1989					CONTINUE BUILD-UP
	10:00	2 HOURS	8226	φ		
	10:15		8219	Λ		
	10:30		8205			
	10:45		8205			
	11:00	3 HOURS	8205			
	11:15		8205			
	11:30		8205			
	11:45		8205			
	12:00	4 HOURS	8205			COMMENCE 4 HOURLY READINGS
	14:00	6	8184			
	18:00	10	8157			
	22:00	14	8136			
4TH	SEPTEMBER 1989					
	02:00	18 HOURS	8115			
	06:00	22	8102			
	10:00	26	8129			
	14:00	30	8157			
	18:00	34	8143			
	22:00	38	8129			
5TH	SEPTEMBER 1989					
	02:00	42	8122	V		
	06:00	46	8122	φ		



Time off Bottom..... 28:00 - 11 -

Bomb No. 2 Data

Remarks: MAXIMUM BOTTOM HOLE THERMOMETER RUN

Remarks: Maximum Bottom Hole Thermometer Run

Wellhead Data for Final Build Up						
Date	Time	Hours shut-in Time	Wellhead Kpa	Casing Kpa	Wellhead Temp.	Remarks
5TH	SEPTEMBER	1989				
	10:00	50 HOURS	8136	Ø		CONTINUE TO MONITOR
	14:00	54	8150	Ø		BUILD-UP
	18:00	58	8150	Ø		TAKEN FROM W.H. CHART
	22:00	62	8143	Ø		
6TH	SEPTEMBER	1989				
	02:00	66	8122	Ø		
	06:00	70	8122	Ø		
	10:00	74	8129	Ø		
	14:00	78	8150	Ø		
	18:00	82	8150	Ø		
	22:00	86	8136	Ø		
7TH	SEPTEMBER	1989				
	02:00	90	8129	Ø		
	06:00	94	8129	Ø		
	08:00					OFF BOTTOM
	08:30					ARRIVE IN LINE
						M.B.H.T. 276°F

● CLOSE-UP PHOTOGRAPH.

DELHI. BIG LAKE. # 4

9790'—9798'9"

CORE. 1

9792

9791

9790

9795

9794

9793

9798

9797

9796

12"

50 cm.

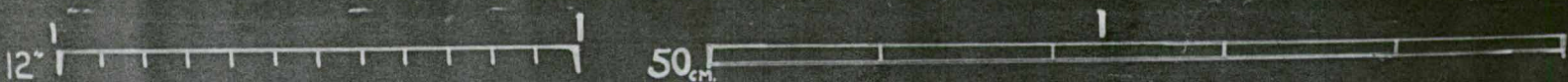
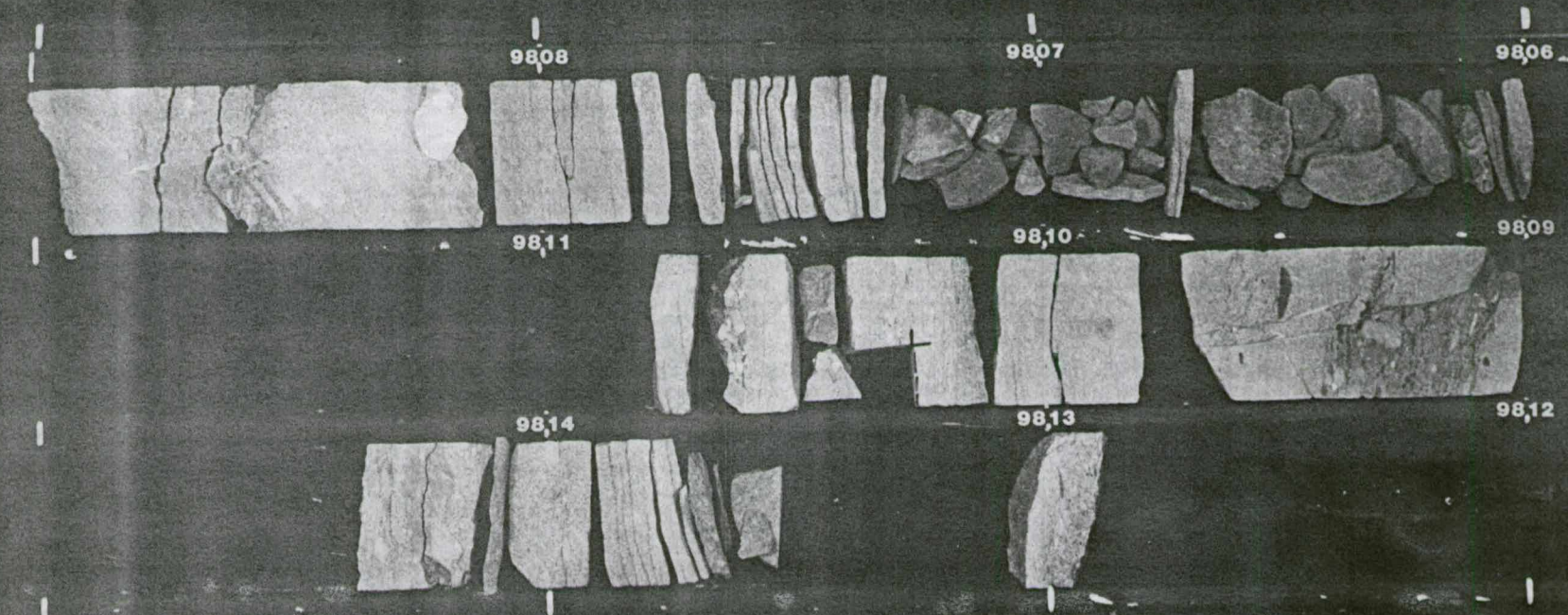
00128

● CLOSE-UP PHOTOGRAPH.

DELHI. BIG LAKE. # 4

CORE. 2

9806'—9814' 4"



00129