Open File Envelope No. 7528/2

PEL 5 AND PEL 6; PATCHAWARRA EAST BLOCK EROMANGA BASIN AND COOPER BASIN

PENNIE 1 TEST REPORTS

Submitted by

Santos Ltd 1996

© 10/12/97

This report was supplied as part of the requirement to hold a mineral or petroleum exploration tenement in the State of South Australia. PIRSA accepts no responsibility for statements made, or conclusions drawn, in the report or for the quality of text or drawings. This report is subject to copyright. Apart from fair dealing for the purposes of study, research, criticism or review as permitted under the Copyright Act, no part may be reproduced without written permission of the Chief Executive of Primary Industries and Resources South Australia, GPO Box 1671, Adelaide, SA 5001.

Enquiries: Customer Services

Ground Floor

101 Grenfell Street, Adelaide 5000

Telephone: (08) 8463 3000 Facsimile: (08) 8204 1880



Santos Ltd A.C.N. 007 550 923 39 Grenfell Street Adelaide SA 5000 GPO Box 2319 Adelaide SA 5001 Telephone: (08) 218 5111 Facsimile: (08) 212 5476

Ref: PED: 1322/96

Mr N Taylor Joint Interests Manager Delhi Petroleum Pty Ltd c/- Esso Australia Ltd 12 Riverside Quay SOUTHBANK VIC 3000

Dr Chris Longman General Manager Crusader Limited 27th Floor 12 Creek Street BRISBANE QLD 4000 Santos

28 October 1996

Dr M Clegg Engineering Manager Boral Energy Resources 60 Hindmarsh Square ADELAIDE SA 5000

Mr T Aust Mines and Energy SA PO Box 151 EASTWOOD SA 5063

Gentlemen,

Re: Pennie 1 DST 1 - PEDSA No. 032/96

Please find attached an interpretation of the above DST.

DST 1 (9338' - 9400' KB-L, Epsilon 93-5 & 93-7) the tool was opened for a 10 minute pre-flow at 10:42 to a closed chamber, a flow rate of approximately 16 MMscf/d was calculated. Following a 49 minute initial build-up, the tool was opened to a 0.5 inch choke with the pressure building dramatically (to 1903 psig) when a leak in the flare line appeared. The tool was closed at 11:56 to repair the flare line. At 12:17 the tool was opened to a 0.75 inch choke for the main (third) flow and a mean stabilised rate of approximately 18.9 MMscf/d (1600 psig) was calculated using the choke equation. The fluid recovery was lost due to the drill string being filled with mud to allow reverse circulation. Radial flow was identified from the main shut-in period with reservoir flow capacity of 3509 md.ft (163 md) and an apparent skin factor of +1.5 being interpreted. A barrier to flow was interpreted from the late time data at a distance of approximately 110 ft. from the wellbore. Alternatively, the character of the radial derivative may indicate a very high permeability streak resulting in frac-like behaviour. A reservoir pressure of 4150 psia, at a depth of 9350 ft.KB, was determined from the main build-up. No depletion was apparent during the test.

If you have any queries about the above results please contact Richard Leslie on (08) 8224 7898.

Yours faithfully,



G. GUGLIELMO Manager - Petroleum Engineering

cc. R.D. Leslie / G.J. Schumacher
JS Evanochko w/o attachments
PA Min w/o attachments
Well file



Report File:

PEN1_1.PAN

Pennie 1 DST 1 December 1995

Well Test Analysis Report

Analyst name C.J. Thompson
Company Santos Limited

Field Pennie
Well 1
Date 7/12/95

Formation Epsilon 93-5 & 93-7 sands

Test DST₁ Depth Reference - MSL 182 ft.ASL Panex Gauge Type 1273 Gauge Number Gauge Depth - Measured 9350 ft.KB Gauge Depth - Vertical -9168 ft.SS Test Interval Top 9338 ft.KB 9400 ft.KB Test Interval Bottom

Remarks: The well was opened for a 10 minute pre-flow at 10:42 to a closed chamber, a flow rate of approximately 16 MMscf/d was calculated. Following a 49 minute initial shut-in, the tool was opened to a 0.5 inch choke with pressure increasing dramatically (to 1903 psig) when a leak in the flare line appeared. The tool was closed at 11:56 to repair the flare line. At 12:17 the tool was opened to a 0.75 inch choke for the main (third) flow and a mean stabilised rate of approximately 18.9 MMscf/d (1600 psig) was calculated using the choke equation. The tool was closed at 13:26 for a 127 minute final shut-in. The liquid recovery was lost due to the drill string being filled with mud to allow reverse circulation.

The test overview indicates rapid pressure build-up during shut-in periods and that the well unloaded the cushion approximately 15 minutes into the final flow.

From the radial derivative (Log-Log plot) a period of radial flow was identified in the early time data of the main build-up and wellbore storage is not observable. Following this initial period of radial flow is a transition to a second period of radial flow. This is interpreted to represent the influence of a single barrier to flow. Alternatively, the character of the radial derivative could also indicate the influence of a very high permeability streak resulting in Frac-like behaviour. Analysis of the main flow was not conduted as the well was still cleaning up and the flow was not completely stable.

Extrapolation of the initial period of radial flow (main build-up) on the Horner plot indicates a reservoir flow capacity of approximately 3509 md.ft (163 md) with an apparent skin factor of 1.5. This is in agreeance with the initial build-up which indicated a flow capacity of 3507 with an apparent skin factor of 1.

Extrapolation of the second radial flow regime (main build-up) on the Horner plot suggests a likely distance of approximately 110 ft. to the permeability barrier. The development of this flow regime during the initial build-up is apparent but not certain.

A reservoir pressure of 4150 psia, at the gauge depth (9350 ft.KB), was determined, from the main build-up, by extrapolation of the single fault radial flow regime on the Horner plot. Depletion following the main flow is not evident.

Report File:

PEN1_1.PAN

Pennie 1 DST 1 December 1995

Well Test Analysis Report

Reservoir Description

Fluid type : Gas

Well orientation : Vertical Number of wells : 1 Number of layers : 1

Layer Parameters Data

| | Layer 1 |
|------------------------------|-----------------|
| Formation thickness | 21.50 ft |
| Average formation porosity | 0.131 |
| Water saturation | 0.256 |
| Gas saturation | 0.744 |
| Formation compressibility | 4.3468e-6 psi-1 |
| Total system compressibility | 1.2099e-4 psi-1 |
| Layer pressure | 4150.0239 psia |
| Temperature | 268.0000 deg F |

Well Parameters Data

| | Well 1 |
|--|--------------|
| Well radius | 0.354 ft |
| Distance from observation to active well | 0.0000 ft |
| Wellbore storage coefficient | 0.00 bbl/psi |
| Well offset - x direction | 0.00 ft |
| Well offset - y direction | 0.00 ft |

Fluid Parameters Data

| | Layer 1 |
|-------------------------------|-------------------|
| Gas gravity | 0.9230 sp grav |
| Water-Gas ratio | 0.0000 STB/MMscf |
| Water salinity | 0.0000 ppm |
| Check Pressure | 4150.0000 psia |
| Check Temperature | 268.0000 deg F |
| Gas density | 15.6632 lb/ft3 |
| Initial gas viscosity | 0.026694 cp |
| Gas formation volume factor | 4.4999e-3 ft3/scf |
| Water density | 58.701 lb/ft3 |
| Water viscosity | 0.18512 cp |
| Water formation volume factor | 1.06244 RB/STB |
| Initial Z-factor | 0.90551 |
| Initial Gas compressibility | 1.5555e-4 psi-1 |
| Water compressibility | 3.5677e-6 psi-1 |

Layer 1 Correlations

Ug Correlation : Carr et al

Layer Boundaries Data

Layer 1 Boundary Type : Single fault

L1 Boundary: No-flow

| | Layer 1 |
|--------------------|--------------|
| L1 | 106.2946 ft |
| L2 | 0.0000 ft |
| L3 | 0.0000 ft |
| L4 | 0.0000 ft |
| Drainage area | 0.0000 acres |
| Dietz shape factor | 0.0000 |

Report File:

PEN1_1.PAN

Pennie 1 DST 1 December 1995

Well Test Analysis Report

Layer 1 Model Data

Layer 1 Model Type : Radial homogeneous

| | Layer 1 |
|-------------------------------------|---------------------|
| Permeability | 163.2032 md |
| Skin factor (Well 1) | 1.5323 |
| Rate dependent skin coefficient (D) | 0.0000 1/(Mscf/day) |

Layer 1 P/U/Z Table

| Di Initial gas vissosity. 7i | | | |
|------------------------------|------------|--------------------------|--|
| Pi | | Initial gas viscosity Zi | |
| psia | ср | | |
| 0.0000 | 0.0126452 | 1.000 | |
| 200.0000 | 0.01278956 | 0.9752 | |
| 400.0000 | 0.01311214 | 0.95107 | |
| 600.0000 | 0.01351041 | 0.92788 | |
| 800.0000 | 0.01389447 | 0.90595 | |
| 1000.0000 | 0.01441568 | 0.88567 | |
| 1200.0000 | 0.01500523 | 0.86747 | |
| 1400.0000 | 0.01568053 | 0.85175 | |
| 1600.0000 | 0.01635141 | 0.8389 | |
| 1800.0000 | 0.0170223 | 0.82917 | |
| 2000.0000 | 0.01771112 | 0.8227 | |
| 2200.0000 | 0.01853585 | 0.81944 | |
| 2400.0000 | 0.01936058 | 0.81924 | |
| 2600.0000 | 0.02018531 | 0.82184 | |
| 2800.0000 | 0.02103093 | 0.82693 | |
| 3000.0000 | 0.02188108 | 0.8342 | |
| 3200.0000 | 0.02273124 | 0.84337 | |
| 3400.0000 | 0.02358139 | 0.85417 | |
| 3600.0000 | 0.02443154 | 0.86636 | |
| 3800.0000 | 0.02528169 | 0.87974 | |
| 4000.0000 | 0.02611396 | 0.89414 | |
| 4200.0000 | 0.02688739 | 0.9094 | |
| 4400.0000 | 0.02766082 | 0.92542 | |
| 4600.0000 | 0.02843426 | 0.94206 | |
| 4800.0000 | 0.02920769 | 0.95926 | |
| 5000.0000 | 0.02998113 | 0.97692 | |

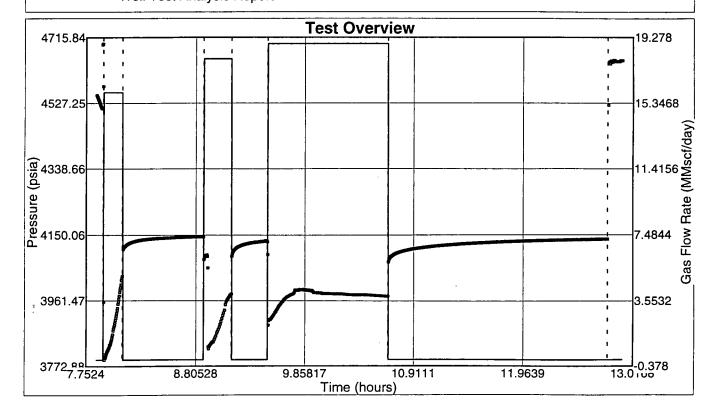
Rate Change Data

| | , | |
|----------|-----------|-----------|
| Time | Pressure | Rate |
| Hours | psia | MMscf/day |
| 7.91614 | 4576.5498 | 0.0000 |
| 8.09945 | 4033.0100 | 16.0000 |
| 8.87854 | 4145.1401 | 0.0000 |
| 9.14935 | 3982.3701 | 18.0000 |
| 9.49514 | 4131.8999 | 0.0000 |
| 10.66167 | 3976.2100 | 18.9000 |
| 12.77393 | 4137.6602 | 0.0000 |

Santos Limited
Pennie 1 DST 1 December 1995

Report File: PEN1_1.PAN

Well Test Analysis Report

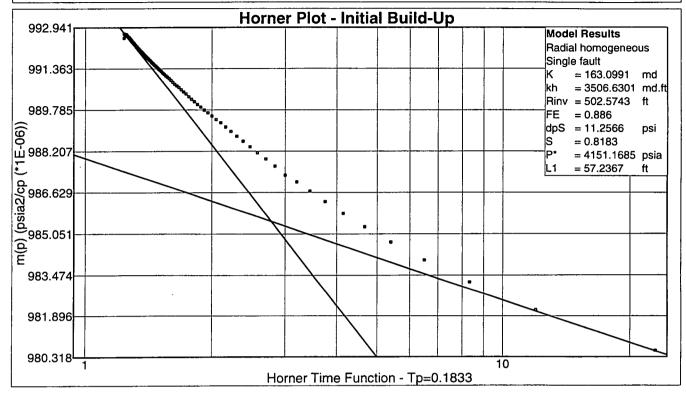


Report File:

PEN1_1.PAN

Pennie 1 DST 1 December 1995

Well Test Analysis Report



Horner Plot - Initial Build-Up Model Results

Radial homogeneous Single fault

| | Value |
|---------------------------|-----------------|
| Permeability | 163.0991 md |
| Permeability-thickness | 3506.6301 md.ft |
| Radius of investigation | 502.5743 ft |
| Flow efficiency | 0.8860 |
| dP skin (constant rate) | 11.2566 psi |
| Skin factor | 0.8183 |
| Extrapolated pressure | 4151.1685 psia |
| Distance to nearest fault | 57.2367 ft |

Horner Plot - Initial Build-Up Line Details

Line type: Radial flow Slope: -5.43372 Intercept: 987.937

Coefficient of Determination: Not Used

| | Radial flow |
|-------------------------|----------------------------|
| Extrapolated m(p) | 987.9367 psia2/cp (*1E-06) |
| Extrapolated pressure | 4131.7505 psia |
| m(p) at $dt = 1$ hr | 987.5395 psia2/cp (*1E-06) |
| Pressure at dt = 1 hour | 4130.5928 psia |

Line type: Single fault radial flow

Slope: -20.4409 Intercept: 994.599

Coefficient of Determination: Not Used

| | Single fault radial flow |
|-------------------------|----------------------------|
| Extrapolated m(p) | 994.5987 psia2/cp (*1E-06) |
| Extrapolated pressure | 4151.1685 psia |
| m(p) at $dt = 1$ hr | 993.1045 psia2/cp (*1E-06) |
| Pressure at dt = 1 hour | 4146.8135 psia |

Report File:

PEN1_1.PAN

Pennie 1 DST 1 December 1995

Well Test Analysis Report

Number of Intersections = 1

Intersection 1

First Line: Radial flow

Second Line: Single fault radial flow

Intersection time: 0.06596

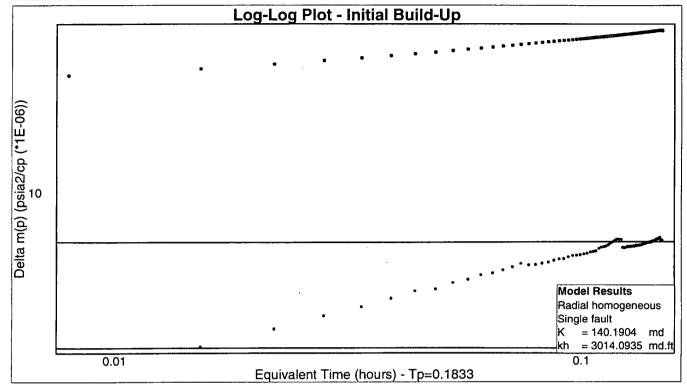
Distance to nearest fault: 57.2367 ft

Report File:

PEN1_1.PAN

Pennie 1 DST 1 December 1995

Well Test Analysis Report



Log-Log Plot - Initial Build-Up Model Results

Radial homogeneous

Single fault

| | Value |
|------------------------|-----------------|
| Permeability | 140.1904 md |
| Permeability-thickness | 3014.0935 md.ft |

Log-Log Plot - Initial Build-Up Line Details

Line type: Radial flow

Slope: 0

Intercept: 2.74546

Coefficient of Determination: Not Used

Line type: Single fault radial flow

Slope: 0

Intercept: 6.63847

Coefficient of Determination: Not Used

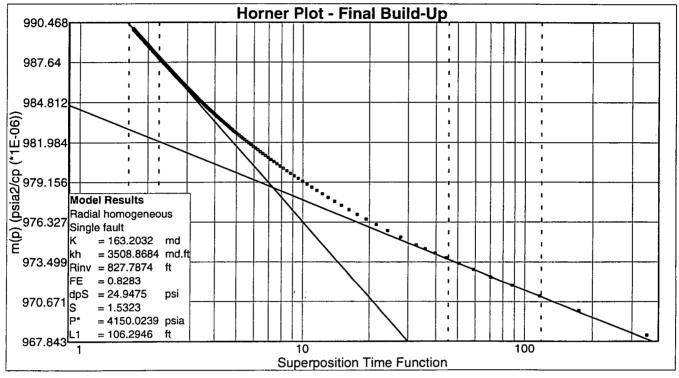
Number of Intersections = 0

Report File:

PEN1_1.PAN

Pennie 1 DST 1 December 1995

Well Test Analysis Report



Horner Plot - Final Build-Up Model Results

Radial homogeneous Single fault

| | Value |
|---------------------------|-----------------|
| Permeability | 163.2032 md |
| Permeability-thickness | 3508.8684 md.ft |
| Radius of investigation | 827.7874 ft |
| Flow efficiency | 0.8283 |
| dP skin (constant rate) | 24.9475 psi |
| Skin factor | 1.5323 |
| Extrapolated pressure | 4150.0239 psia |
| Distance to nearest fault | 106.2946 ft |

Horner Plot - Final Build-Up Line Details

Line type: Radial flow Slope: -6.41448 Intercept: 984.321

Coefficient of Determination: 0.999553

| | Radial flow |
|-------------------------|----------------------------|
| Extrapolated m(p) | 984.3215 psia2/cp (*1E-06) |
| Extrapolated pressure | 4121.2129 psia |
| m(p) at $dt = 1$ hr | 981.8287 psia2/cp (*1E-06) |
| Pressure at dt = 1 hour | 4113.9468 psia |

Line type: Single fault radial flow

Slope : -17.8511 Intercept : 994.206

Coefficient of Determination: 0.999774

| | Single fault radial flow |
|-------------------------|----------------------------|
| Extrapolated m(p) | 994.2060 psia2/cp (*1E-06) |
| Extrapolated pressure | 4150.0239 psia |
| m(p) at $dt = 1$ hr | 987.2688 psia2/cp (*1E-06) |
| Pressure at dt = 1 hour | 4129.8037 psia |

Report File:

PEN1_1.PAN

Pennie 1 DST 1 December 1995

Well Test Analysis Report

Number of Intersections = 1

Intersection 1

First Line: Radial flow

Second Line: Single fault radial flow

Intersection time: 0.19776

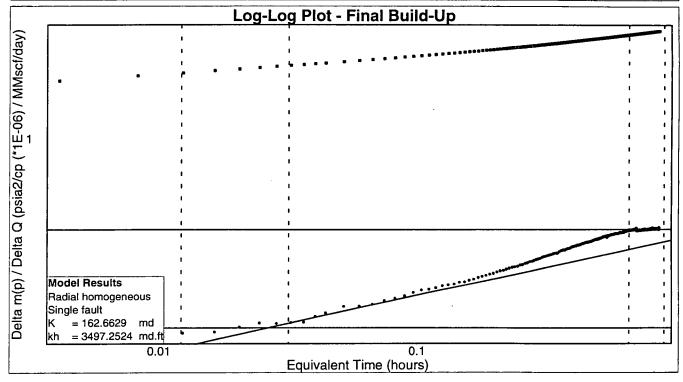
Distance to nearest fault: 106.295 ft

Report File:

PEN1_1.PAN

Pennie 1 DST 1 December 1995

Well Test Analysis Report



Log-Log Plot - Final Build-Up Model Results

Radial homogeneous

Single fault

| | Value |
|------------------------|-----------------|
| Permeability | 162.6629 md |
| Permeability-thickness | 3497.2524 md.ft |

Log-Log Plot - Final Build-Up Line Details

Line type: Radial flow

Slope: 0

Intercept: 0.147885

Coefficient of Determination : Not Used

Line type: Free model line

Slope: 0.25

Intercept: 0.366526

Coefficient of Determination: Not Used

Line type: Single fault radial flow

Slope: 0

Intercept: 0.40266

Coefficient of Determination : Not Used

Number of Intersections = 0