#### DEPARTMENT OF MINES AND ENERGY

#### GEOLOGICAL SÜRVEY

SOUTH AUSTRALIA

**REPORT BOOK 95/5** 

PROPOSED MARINA AT KINGSTON HYDROGEOLOGY AND ASSESSMENT OF THE IMPACT ON LOCAL GROUND WATER RESOURCES

by

N L Watkins Groundwater and Environmental Services Division

FEBRUARY 1995 DME 152/95

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### DEPARTMENT OF MINES AND ENERGY GEOLOGICAL SURVEY SOUTH AUSTRALIA

REPORT BOOK 95/5 DME 152/95

## Proposed Marina at Kingston. Hydrogeology and Assessment of the Impact on Local Groundwater Resources

N L WATKINS

The Lacepede District Council is considering a proposal for the construction of a marina and associated infrastructure in Maria Creek, Kingston. The proposal includes two options, A and B, with Option A closest to existing town amenities. Option B involves excavating the marina further to the north near the outlet of Maria Creek. The proposal has been forwarded to MESA for an assessment of the hydrogeology of the site and possible effects of the marina on groundwater quality in nearby private and council water supply bores.

An assessment of groundwater monitoring data indicates that there is unlikely to be any adverse impact on the local groundwater resources from Option B. The worst case scenario for Option A could result in a 50 m lateral shift away from Maria Creek of the existing salinity profiles in the Bridgewater Formation aquifer. A further program of monitoring is recommended which includes intensive groundwater monitoring during periods of peak high tides to assess the tidal efficiencies of both aquifers, continued monitoring to assess the impacts of surface water flows in Maria Creek and a small trial excavation with associated monitoring. It may also be possible to mitigate any such impacts of Option A through the use of stormwater recharge trenches located just inland of the proposed marina.

#### INTRODUCTION

The Lacepede District Council has forwarded a proposal for a marina in Maria Creek, Kingston to MESA for an assessment of the hydrogeology of the site and possible effects of the marina on groundwater quality in nearby private and council water supply bores.

Two proposed layouts for the marina have been considered. Option A comprises a two stage basin excavation adjacent to the Maria Creek bird sanctuary with parking, launching and future commercial areas to the south on existing low-lying areas which are currently subject to inundation with salt water during winter high tides. Option B involves

excavating the marina further to the north. The proposed basin excavations are shown on Figure 1.

#### **HYDROGEOLOGY**

The area contains Holocene age surface deposits of the St. Kilda Formation. These sediments include dune sands of the Semaphore Sands member overlying fossiliferous clayey sands and clays with some seaweed deposits. The St. Kilda Formation overlies variably cemented siliceous calcarenites of the Bridgewater Formation. The subsurface geology is shown on Figure 2. The deposits contain groundwater of highly variable

salinity depending on distance from the coast and from the low lying saline swamp areas adjacent to Maria Creek which is the main drainage channel for inland farm areas. Winter tides at Kingston cause sea water to intrude up Maria Creek and inundate the adjacent swamp areas.

Shallow groundwater supply bores are usually completed in the Bridgewater Formation with the upper loose and unstable sands cased off.

### MONITORING OF GROUNDWATER LEVELS AND SALINITY

#### General

Measurements of groundwater salinity, water levels and tidal heights at Kingston were taken over the period March 1994 to January 1995. Volumes and salinity of surface water flow in Maria Creek were not measured as the creek did not flow due to the dry weather conditions. The monitoring network included thirteen private and council water supply bores at distances of up to 700 m from Maria Creek and a line of dual completion observation bores installed by the District Council of Lacepede between the Lions Pioneer Park bore (site 1450) and Maria Creek. These were installed at approximate distances of 20 m (site 1/1a), 50 m (site 2/2a), 90 m (site 3/3a) and 140 m (site 4/4a) from the creek. A 10 cm graduated survey pole installed in Maria Creek was used to relate all bores and water levels to a reference datum of local mean sea level. The locations of the bores are shown on the attached site plan (Figure 1) and well details are contained construction Appendix A.

#### **Groundwater Levels**

Groundwater levels in both the St. Kilda Formation and Bridgewater Formation aquifers show a seasonal fluctuation with maximum water levels recorded during winter. For comparative purposes, potentiometric levels in the Bridgewater Formation at the end of summer and winter are shown on Figures 3 and 4. Hydraulic gradients are very flat at the

end of summer so contours are not shown. The paired piezometers, sites 1/1a to 4/4a, generally indicate a downward hydraulic gradient exists from the St. Kilda Formation to the Bridgewater Formation as shown on the cross section, Figure 2. It is likely that vertical recharge following tidal inundation during winter causes the water level rises measured at these locations. However, the tidal efficiencies of the aguifers should be determined through intensive monitoring over a one month period to investigate the extent of lateral intrusion of sea water into the aquifers. Seasonal water level changes away from the creek in piezometers 1140 and 1747 are probably due to vertical infiltration of rainfall. There was no surface water flow in Maria Creek during the period of monitoring so further measurements during periods of flow is required to assess the effect of this flow on groundwater levels.

Hydrographs for tide heights and all piezometers are included in Appendix B.

#### **Groundwater Salinity**

Monitoring of groundwater salinity in both aquifers below the low lying areas adjacent to Maria Creek (piezometer sites 1/1a, 2/2a and 3/3a) show an increasing trend from early winter into summer. This is interpreted to be due to initial recharge to the aquifers following inundation with sea water during the high tide period, followed by evaporation and lateral drainage of this water. This seasonal salinity increase is indicated by the salinity contours at the end of summer and winter shown on Figures 2a and 2b. A slight rise in salinity at site 4/4a, adjacent to this area was measured. It is not considered likely that lateral influx of seawater into the aquifers is the major recharge mechanism to the aquifers, however further monitoring is required to confirm this. The Lions Pioneer Park bore and other private bores in the area show a decrease in salinity during late winter to early spring which is interpreted to be due to vertical recharge by rainfall infiltration and/or roof runoff being directed into the bores. Measurements of groundwater salinity in April and September are shown on Figures 5 and 6 for comparative

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purposes.

An interface between high salinity groundwater and relatively fresh groundwater extends between piezometer sites 3/3a and 4/4a (Figure 2). This interface should not migrate inland unless a considerable increase in discharge is experienced from the fresh groundwater zone through either evaporation during particularly dry seasons or pumping.

Graphs of salinity against time for all piezometers are included in Appendix B.

#### IMPACT OF MARINA

#### **Basin Excavation**

#### Option A

Option A includes excavation of the basin up to 50 m from the edge of Maria Creek towards Lions Pioneer Park. In the extreme worst case, this could cause a lateral shift of 50 m away from Maria Creek of the salinity profiles shown on Figure 2. This would result in large (> 1 000 mg/L) increases in groundwater salinity in the Bridgewater Formation aquifer within 125 m of the basin, decreasing to no salinity increase at about 300 m from the basin. However, this scenario assumes a rapid lateral transmission of seawater into the aquifers but further monitoring to determine the tidal efficiencies of the aquifers is required to confirm this. A small trial excavation with associated monitoring is also recommended if Option A becomes the preferred option.

#### Option B

There is unlikely to be any adverse impact on the local groundwater resources due to the proposed basin excavation.

#### **Associated Works**

Both Option A and Option B include the filling of existing low lying areas adjacent to Maria Creek for construction of parking, boat compound and commercial areas which will necessitate the filling of this area to prevent

inundation during high tide periods. This will stop the vertical recharge of seawater to the aquifers in these areas which is interpreted to cause the observed water level and salinity fluctuations. The groundwater mound which is evident from monitoring in this area, would not be sustained and locally the groundwater would flow in a northeasterly direction towards Maria Creek throughout the year. The result will be an increase in throughflow of relatively fresh groundwater and a general freshening of the groundwater below these areas.

### CONCLUSIONS AND RECOMMENDATIONS

The District Council of Lacepede is considering the construction of a marina in Maria Creek at Kingston. Two proposed options exist for the marina; option A includes a basin excavation near Lions Pioneer Park whereas the basin for option B is to be excavated further to the north along Maria Creek and closer to the coast. Both options also include the filling of low lying areas between the Lions Pioneer Park and Maria Creek for use as parking, boat compound and future commercial areas. Some concerns exist as to the impact of this project on the local groundwater resources. As a consequence, a tide height, groundwater level and groundwater salinity monitoring program commenced in February 1994. This program uses existing council and private water supply bores, as well as dual completion piezometers installed between Maria Creek and Lions Pioneer Park.

An assessment of this monitoring data concludes that;

- for option B, there is unlikely to be any adverse impact on the local groundwater resources due to the proposed basin excavation
- for option A, the worst case scenario could result in a 50 m lateral shift away from Maria Creek of the existing salinity profiles. This would cause a salinity increase in excess of 1000 mg/L in the Bridgewater Formation aquifer within 125 m of the

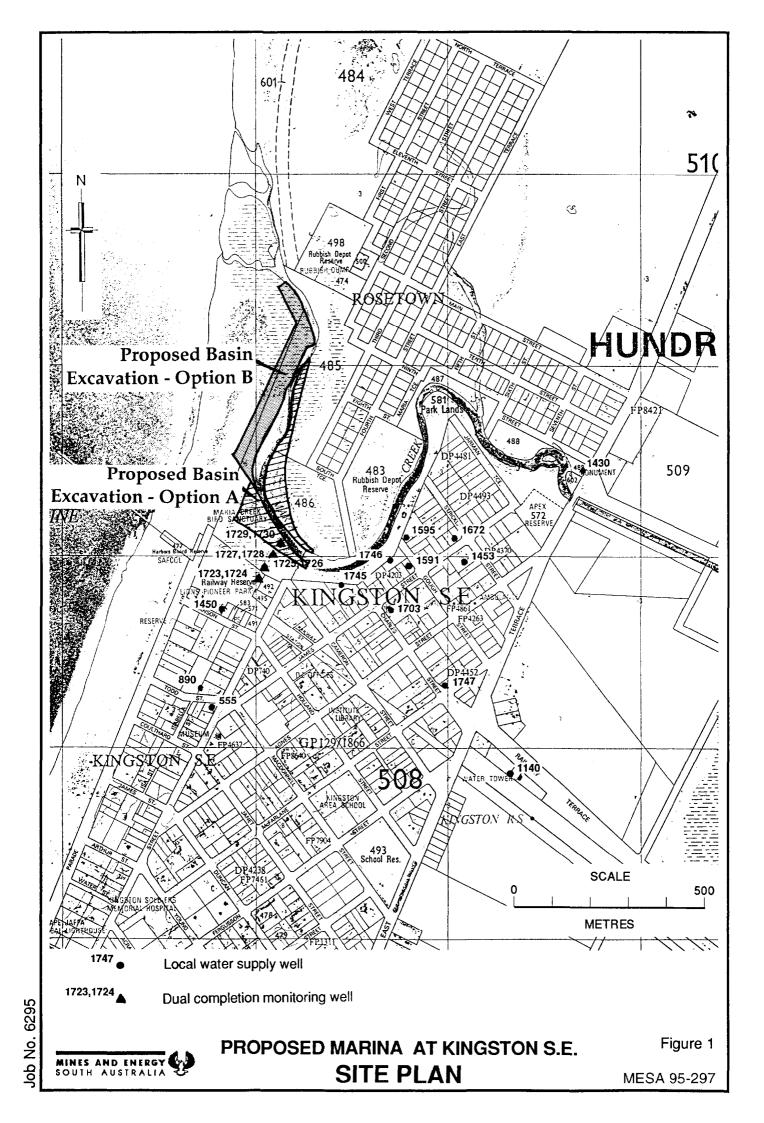
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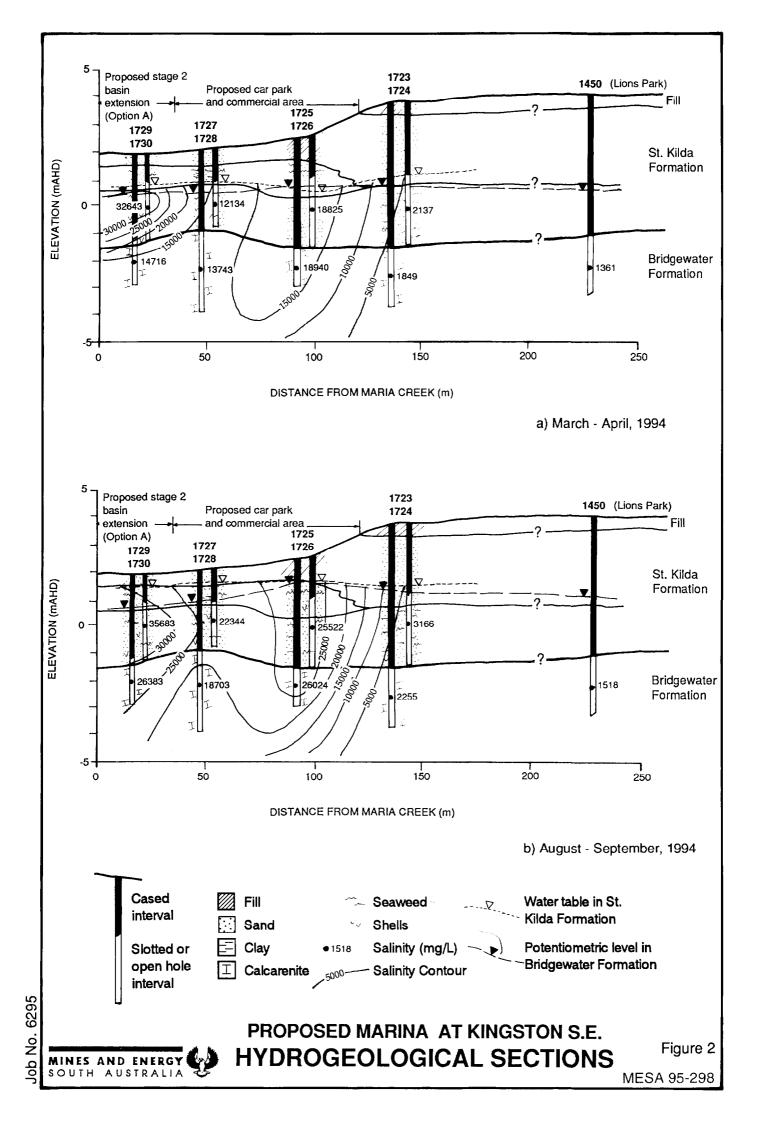
proposed basin, decreasing to no impact at about 300 m from the basin. This scenario assumes a rapid lateral transmission of sea water through the aquifer but the existing monitoring data have been insufficient to fully assess this impact. It may be possible to mitigate any such impacts by the use of stormwater recharge trenches located just inland of the proposed marina.

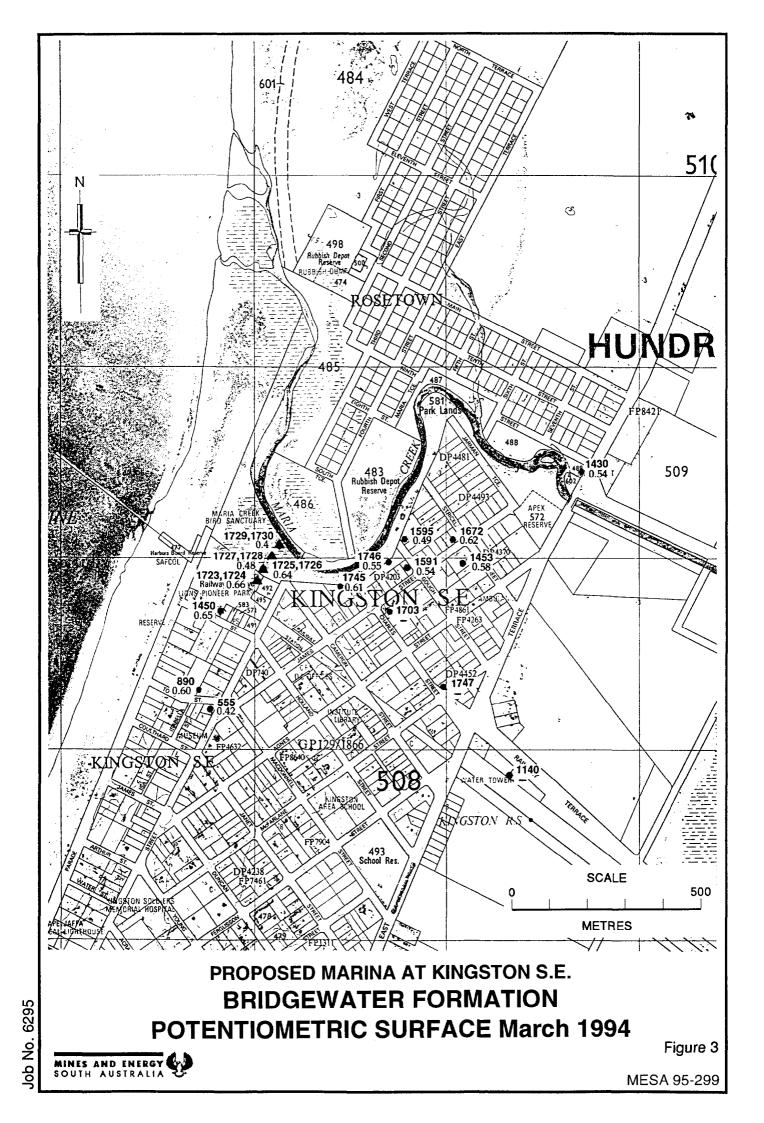
A further program of monitoring is recommended to fully assess the impacts of option A and this should include;

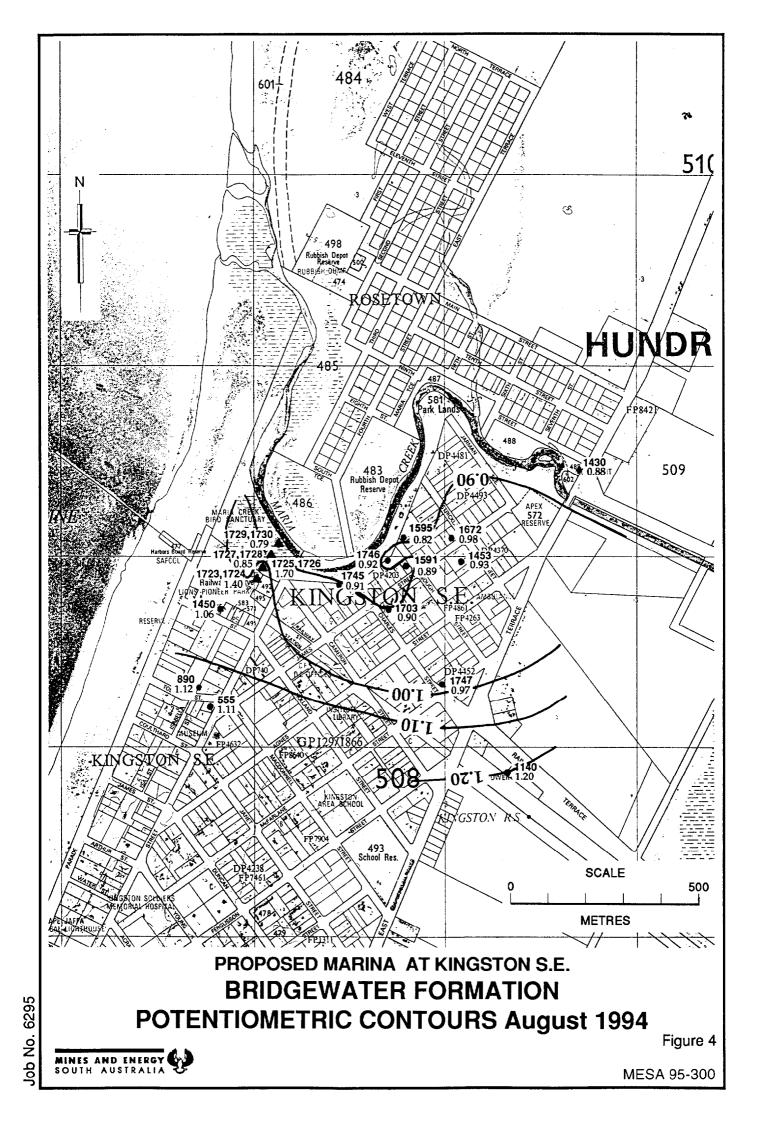
- intensive groundwater monitoring during periods of peak high tides to assess the tidal efficiencies of both aquifers
- continued monitoring to assess the impacts of surface water flows in Maria Creek
- a small trial excavation with associated monitoring.

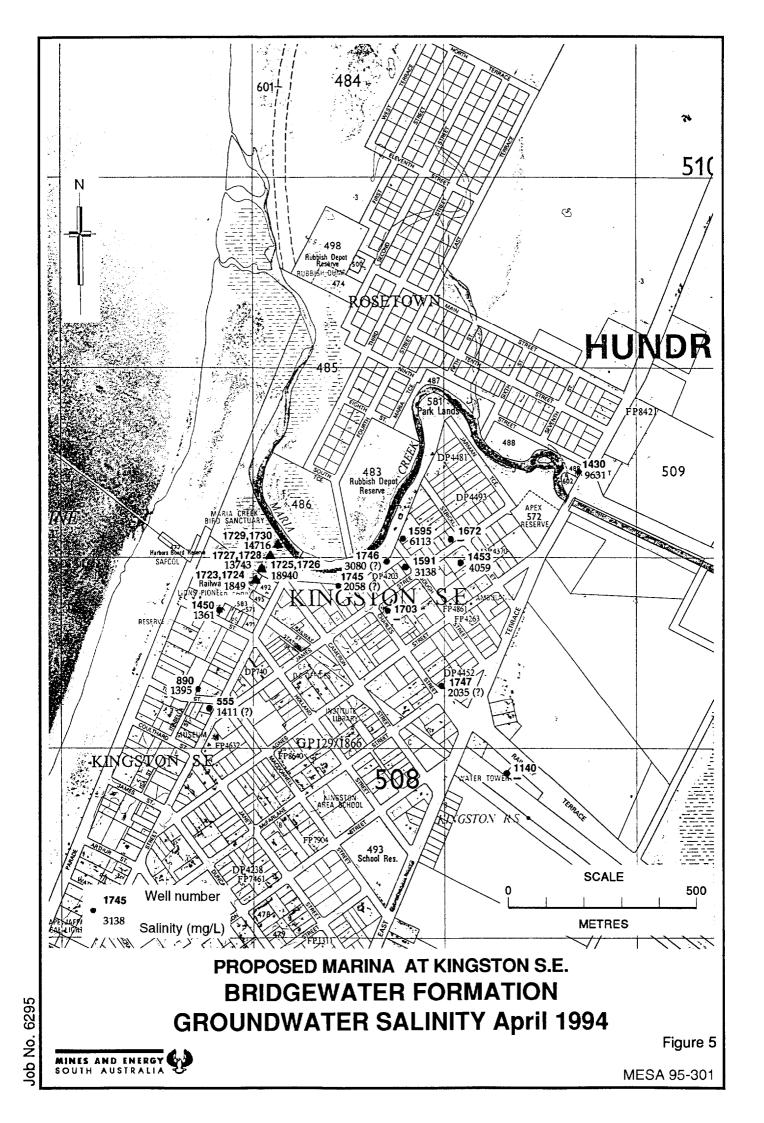
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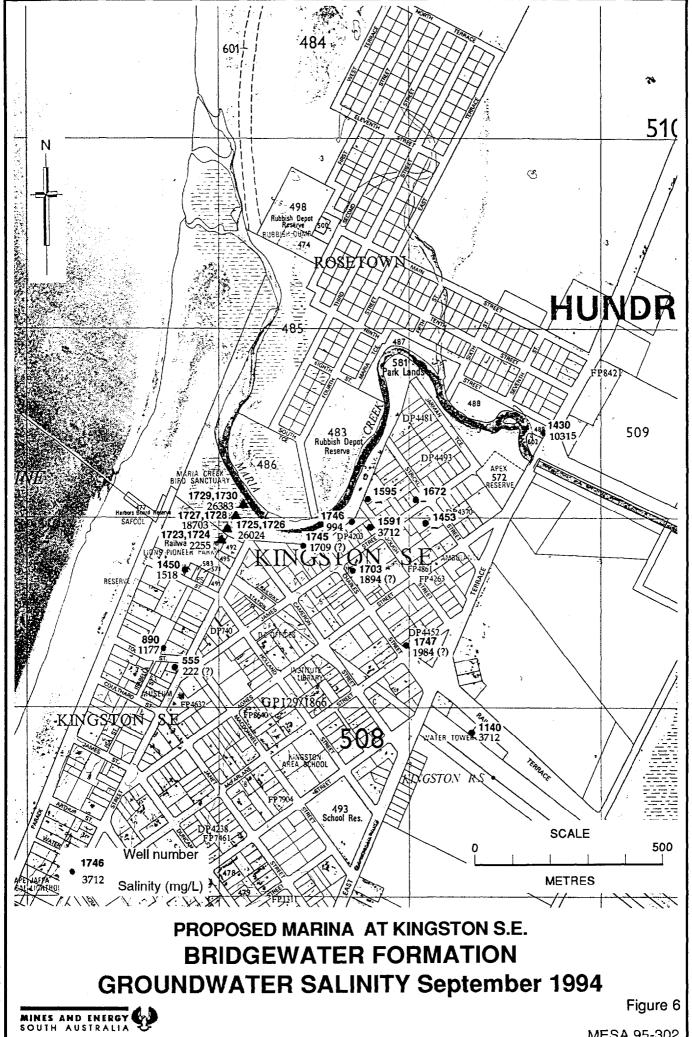












MESA 95-302

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## Appendix A Well Construction Details

TABLE A1: PROPOSED MARINA AT KINGSTON WELL CONSTRUCTION DETAILS

| Unit No.<br>6824- | Depth (m) | S.W.L. <sup>(1)</sup> (m) | Casing<br>Diameter<br>(mm) | Casing<br>Depth (m) | Open or Slotted<br>Interval (m) | Aquifer <sup>(2)</sup> |  |  |
|-------------------|-----------|---------------------------|----------------------------|---------------------|---------------------------------|------------------------|--|--|
| 1729 (1)          | 5.32      | 1.30                      | 152                        | 3.30                | 3.30 - 5.32                     | BWF                    |  |  |
| 1730 (1a)         | 3.75      | 1.30                      | 76                         | 3.40                | 1.10 - 3.30                     | SKF                    |  |  |
| 1727 (2)          | 4.95      | 1.30                      | 152                        | 3.00                | 3.00 - 4.95                     | BWF                    |  |  |
| 1728 (2a)         | 3.41      | 1.08                      | 76                         | 3.00                | 1.10 - 3.00                     | SKF                    |  |  |
| 1725 (3)          | 5.10      | 1.64                      | 152                        | 4.10                | 4.10 - 5.10                     | BWF                    |  |  |
| 1726 (3a)         | 4.00      | 1.64                      | 76                         | 4.00                | 1.50 - 4.00                     | SKF                    |  |  |
| 1723 (4)          | 7.50      | 2.90                      | 152                        | 5.30                | 5.30 - 7.50                     | BWF                    |  |  |
| 1724 (4a)         | 5.14      | 2.52                      | 76                         | 5.20                | 2.40 - 5.10                     | SKF                    |  |  |
| 1595              | 7.00      | 3.56                      | 152                        | 5.00                | 5.00 - 7.00                     | BWF                    |  |  |
| 1591              | 7.14      | 3.81                      | 152                        | 5.50                | 5.50 - 7.14                     | BWF                    |  |  |
| 1672              | 4.37      | 2.20                      | 860                        | _ :                 | _                               | BWF                    |  |  |
| 1453              | 4.85      | 2.44                      | 152                        | 4.40                | 4.40 - 4.85                     | BWF                    |  |  |
| 1140              | 5.50      | 2.14                      | 127                        | 3.60                | 3.60 - 5.50                     | BWF                    |  |  |
| 1450 (5)          | 7.30      | 2.60                      | 203                        | 5.00                | 5.00 - 7.30                     | BWF                    |  |  |
| 555               | 9.75      | 2.00                      | 203                        | <b>-</b> .          | -                               | BWF                    |  |  |
| 890               | 6.20      | 2.30                      | 127                        | 5.20                | 5.20 - 6.20                     | BWF                    |  |  |
| 1430              | 5.20      | 1.50                      | 152                        | 3.30                | 3.30 - 5.20                     | BWF                    |  |  |
| 1745              | 5.30      | 2.30                      | 127                        | -                   | -                               | BWF                    |  |  |
| 1746              |           | 3.42                      | 102                        | -                   | -                               | BWF                    |  |  |
| 1703              | 5.55      | 3.00                      | 102                        | -                   | -                               | BWF                    |  |  |
| 1747              | 4.35      | 1.95                      | 102                        | -                   | -                               | BWF                    |  |  |

NOTES:

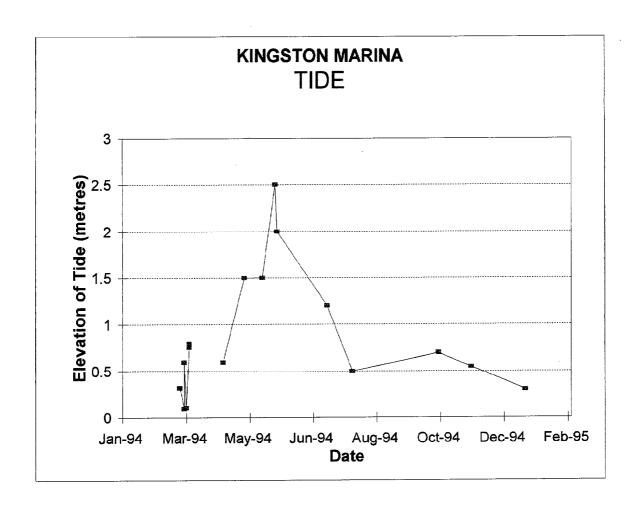
Guide only as fluctuates seasonally.
 BWF - Bridgewater Formation SKF - St. Kilda Formation

# Appendix B Groundwater Monitoring Data and Groundwater Level and Salinity Graphs

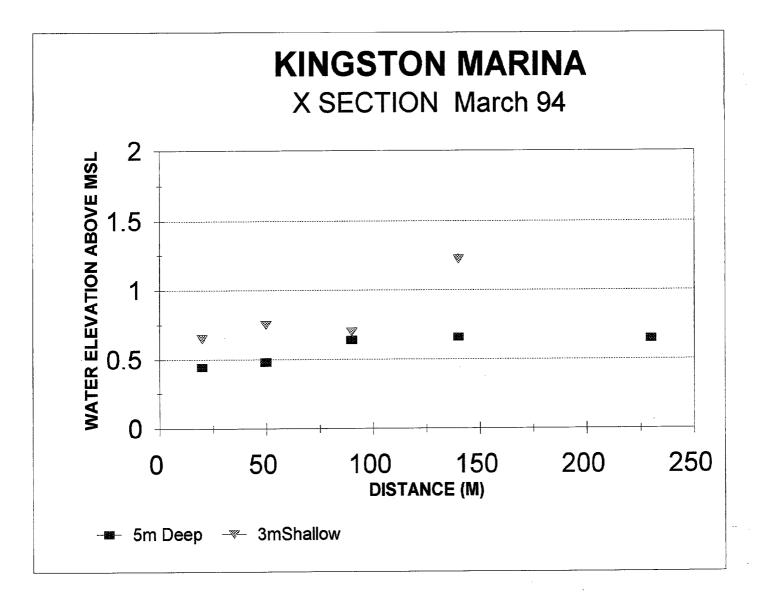
#### KINGSTON MARINA PROJECT

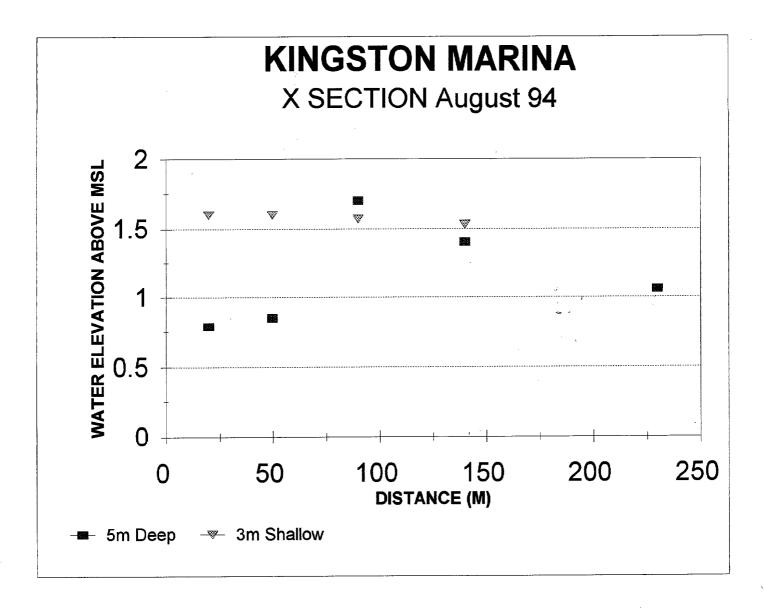
#### WATER LEVEL MONITORING DATA

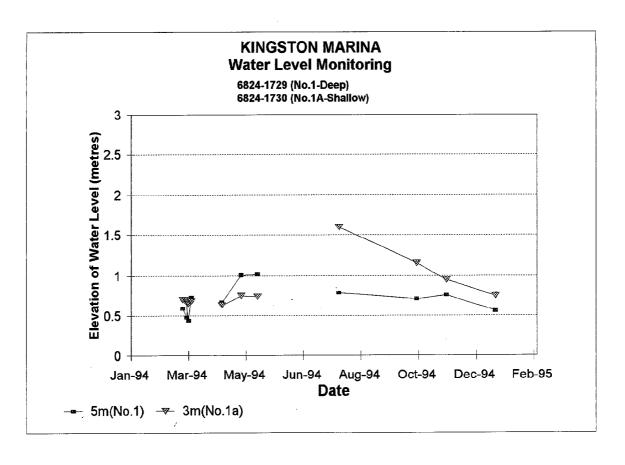
| STAFF EL   | EVATION   |   | 2.22  | 2.1   | 2.16  | 2.14  | 2.62   | 2.48  | 3.95  | 3.74  | 4.08  | 3.15  | 4.45   | 4.58   | 4.82   | 3.42  | 3.26   | 2.9   | 2.34   | 3.53  | 3.91  | 2.81  | 3.25  |                       |
|--|---|---|---|---|---|---|--|---|---|---|---|---|--|--|--|---|--|---|--|---|---|---|---|-----------------------|
| DATE<br>24/02/94<br>28/02/94<br>28/02/94<br>02/03/94<br>05/03/94   | UNIT NO.<br>TIME<br>AM 10.30<br>AM 10.10<br>PM 4.00<br>AM.9.30<br>PM 6.00<br>PM 7.00                          | 6824<br>TIDE<br>0.32<br>0.1<br>0.6<br>0.11<br>0.76<br>0.8         | 1729<br>1<br>0.59<br>0.48<br>0.68<br>0.44<br>0.73               | 1730<br>1A<br>0.7<br>0.67<br>0.7<br>0.65<br>0.68    | 1727<br>2<br>0.63<br>0.5<br>0.68<br>0.48<br>0.72                | 1728<br>2A<br>0.84<br>0.84<br>0.83<br>0.75<br>0.82  | 1725<br>3<br>0.74<br>0.67<br>0.72<br>0.64<br>0.72        | 1726<br>3A<br>0.8<br>0.72<br>0.78<br>0.7<br>0.76            | 1723<br>4<br>0.75<br>0.69<br>0.75<br>0.66<br>0.75         | 1724<br>4A<br>1.26<br>1.25<br>1.24<br>1.22<br>1.25          | 1450<br>5<br>0.64<br>0.64<br>0.65<br>0.72                           | 1745<br>PINK<br>0.72<br>0.6<br>0.85<br>0.61<br>0.86     | 1746<br>KER<br>0.7<br>0.57<br>0.8<br>0.55<br>0.85                | 1595<br>PETERS<br>0.67<br>0.51<br>0.72<br>0.49<br>0.84   | 1591<br>STARLING<br>0.69<br>0.57<br>0.8<br>0.54<br>0.84        | 1453<br>RAD<br>0.72<br>0.6<br>0.58<br>0.82                        | 1672<br>RASH<br>0.7<br>0.69<br>0.62<br>0.78                      | 1430<br>APEX<br>0.55<br>0.55<br>0.54<br>0.7<br>0.75                 | 555<br>TOD<br>0.46<br>0.46<br>0.42<br>0.68                         | 890<br>WHITE<br>0.41<br>0.41<br>0.6<br>0.7                        | 1703<br>THORPE  | 1747<br>LAMPIT  | 1140<br>BAKER   | <b>WEIR</b> 0.85 0.54 |
| WEIR REI<br>06/04/94<br>26/04/94<br>13/05/94<br>25/05/94<br>27/05/94<br>13/07/94<br>66/08/94<br>26/11/94<br>16/01/95 | PM 12.30<br>PM 12.45<br>PM 2.00<br>PM 2.00<br>PM 3.00<br>PM 1.45<br>AM 9.15<br>PM 1.30<br>AM 11.00<br>PM 1.00 | 0.6<br>1.5<br>1.5<br>2.5<br>2<br>1.2<br>0.5<br>0.7<br>0.55<br>0.3 | 0.67<br>1.01<br>1.02<br>FLOODED<br>0.79<br>0.71<br>0.76<br>0.56 | 0.63<br>0.75<br>0.74<br>1.6<br>1.15<br>0.95<br>0.75 | 0.66<br>0.99<br>0.98<br>FLOODED<br>0.85<br>0.85<br>0.78<br>0.52 | 0.72<br>0.89<br>0.88<br>1.6<br>1.25<br>1.08<br>0.83 | 0.72<br>0.87<br>0.8<br>1.3<br>1.7<br>0.92<br>0.87<br>0.7 | 0.73<br>0.87<br>0.8<br>1.38<br>1.57<br>1.29<br>1.11<br>0.85 | 0.77<br>0.9<br>0.97<br>1.18<br>1.4<br>0.96<br>0.9<br>0.75 | 1.2<br>1.35<br>1.26<br>1.28<br>1.53<br>1.32<br>1.25<br>0.98 | 0.72<br>0.89<br>0.81<br>1.11<br>1.21<br>1.06<br>0.95<br>0.89<br>0.7 | 0.8<br>1.06<br>1<br>1.27<br>1.3<br>0.91<br>0.95<br>0.89 | 0.83<br>1.08<br>1.04<br>1.3<br>1.29<br>0.92<br>1<br>0.86<br>0.71 | 0.8<br>1<br>0.97<br>1.29<br>1.31<br>0.82<br>0.91<br>0.83 | 0.8<br>1.03<br>1<br>1.28<br>1.3<br>0.89<br>0.94<br>0.85<br>0.7 | 0.83<br>1.05<br>1<br>1.28<br>1.31<br>0.93<br>0.96<br>0.87<br>0.71 | 0.75<br>0.9<br>0.82<br>1.1<br>1.2<br>0.98<br>0.98<br>0.9<br>0.75 | 0.7<br>0.87<br>0.83<br>1.12<br>1.15<br>0.88<br>0.84<br>0.85<br>0.75 | 0.7<br>0.77<br>0.72<br>1.1<br>1.19<br>1.11<br>0.99<br>0.92<br>0.74 | 0.7<br>0.79<br>0.75<br>1.2<br>1.2<br>1.12<br>0.92<br>0.93<br>0.74 | 0.98<br>0.98<br>1.21<br>1.31<br>0.9<br>0.85<br>0.73<br>0.62 | 0.85<br>0.9<br>1.12<br>1.22<br>0.97<br>0.93<br>0.81<br>0.72 | 0.77<br>0.8<br>1.2<br>1.25<br>1.2<br>1.05<br>0.91<br>0.79 |                       |
| WATER SALINITY MONITORING  |   |   |   |   |   |   |  |   |   |   |   |   |  |  |  |   |  |   |  |   |   |   |   |                       |
| WELLS  | 1 -   | 1A  | 2   | 2A  | 3   | 3A  | 4  | <b>4A</b>   | 5   | PINK  | KER   | PETERS  | STARLING   | RAD  | RASH   | APEX  | TOD  | WHITE   | THORPE   | LAMPIT  | BAKER   | WEIR  |   |                       |
| 06/04/94 06/106/94 01/09/94 26/10/94 26/11/94 16/01/95   | 14716<br>26383<br>22204<br>19995<br>17599   | 32643<br>35683<br>36399<br>36399<br>32643                         | 13743<br>18703<br>16492<br>15502<br>17559                       | 12134<br>22344<br>23184<br>23254<br>24596           | 18940<br>24596<br>26024<br>27105<br>26239<br>24241              | 18825<br>25165<br>25522<br>28195<br>26024<br>24171  | 1849<br>1804<br>2255<br>1956<br>2086<br>2080             | 2137<br>2636<br>3166<br>2624<br>2539<br>2767                | 1361<br>1602<br>1518<br>1305<br>1350<br>1434              | 2058<br>1832<br>1709<br>1928<br>1883<br>1860                | 3080<br>2783<br>994<br>2273<br>2278<br>2312                         | 6113<br>4933<br>3482<br>3367                            | 3138<br>4407<br>3712<br>2795                                     | 3943<br>3568<br>3724                                     | 3166<br>1984<br>2001<br>1501<br>1753                           | 9631<br>8708<br>10315<br>4757<br>5344<br>5876                     | 1411<br>1227<br>222<br>871<br>1077<br>1316                       | 1395<br>1384<br>1177<br>1021<br>1077<br>1272                        | 971<br>1894<br>1860<br>1021<br>2041                                | 2035<br>2001<br>1984<br>2041<br>2080<br>2069                      | 3857<br>3712<br>4030<br>4233<br>3955                        | 36399<br>26744  |   |                       |

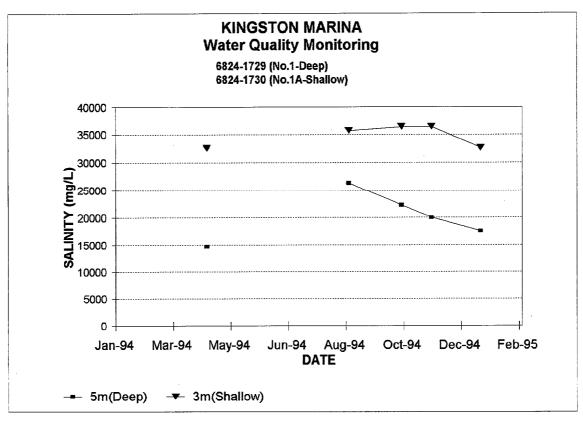


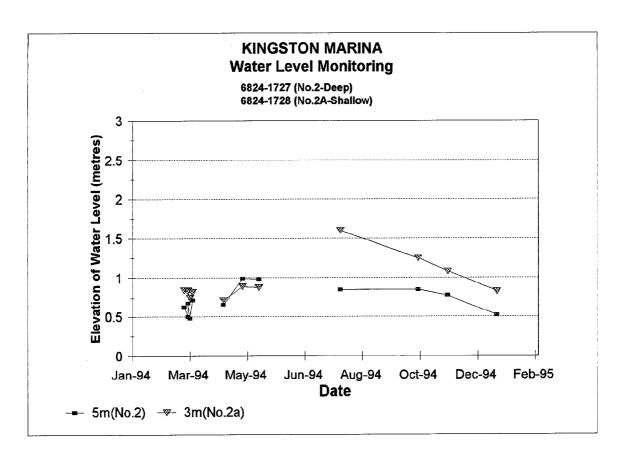


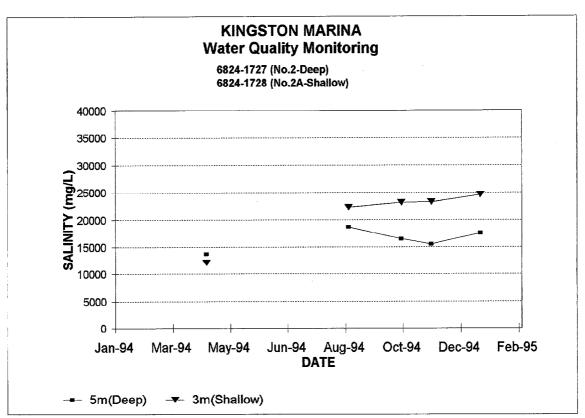


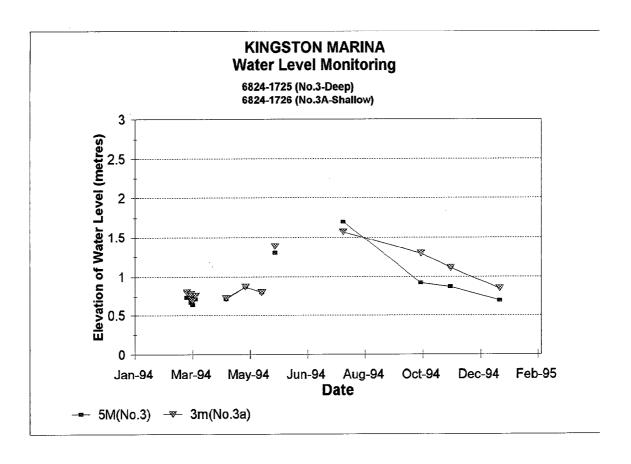


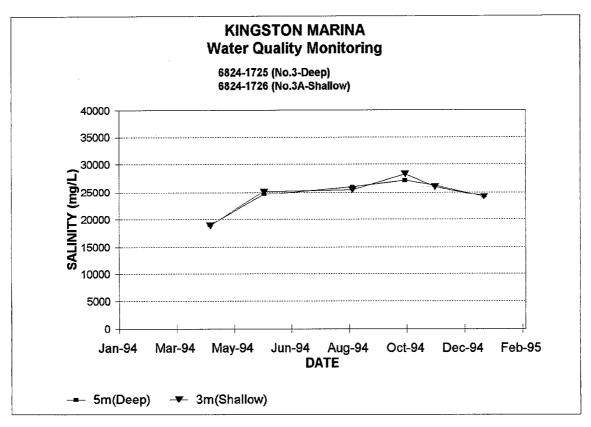


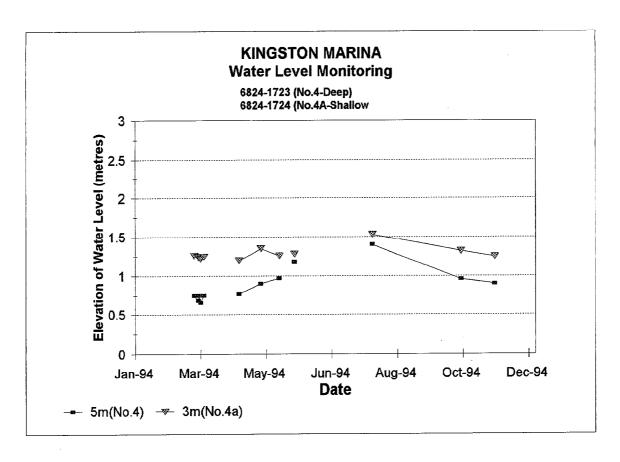


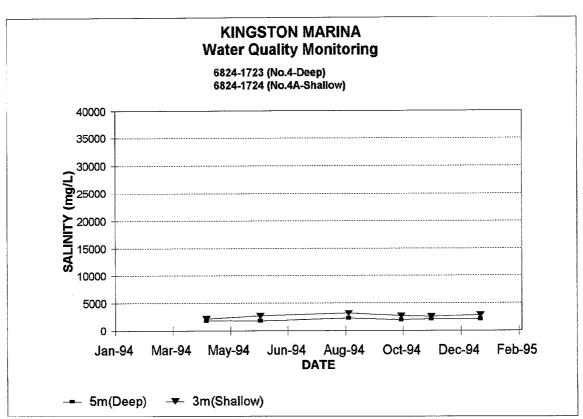


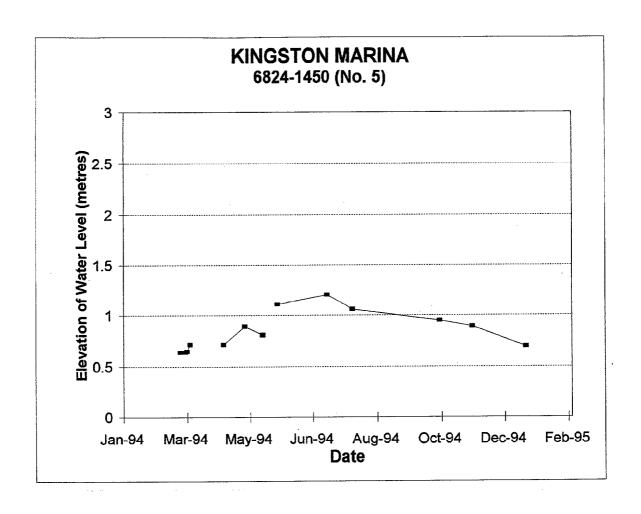


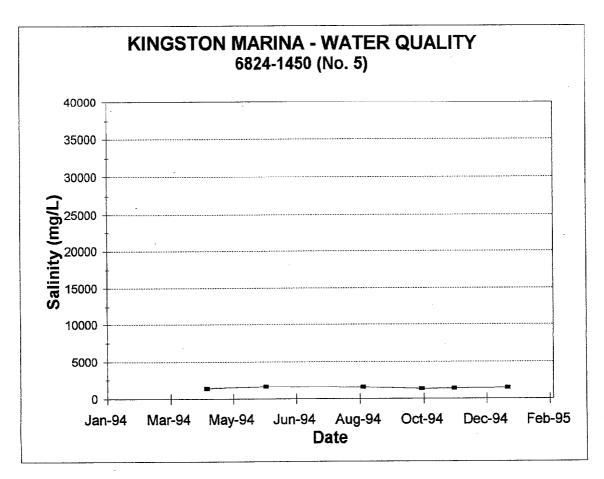


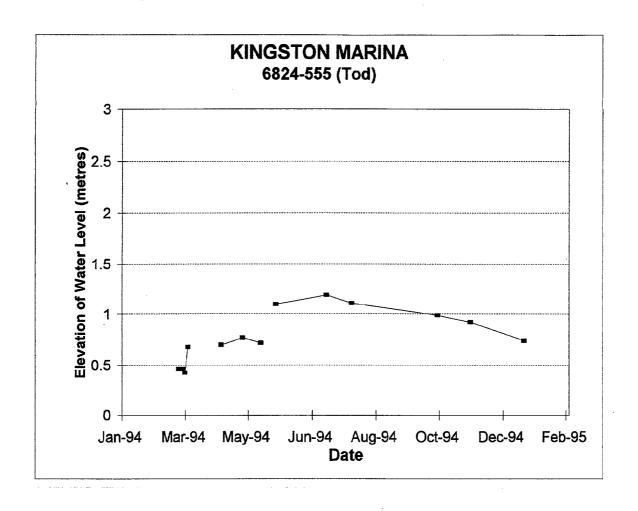


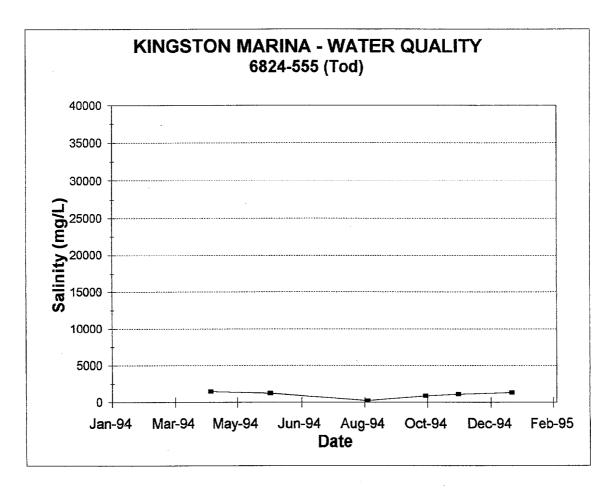


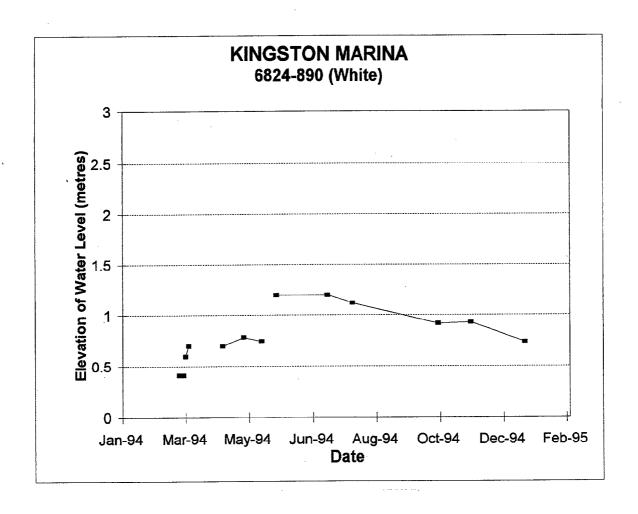


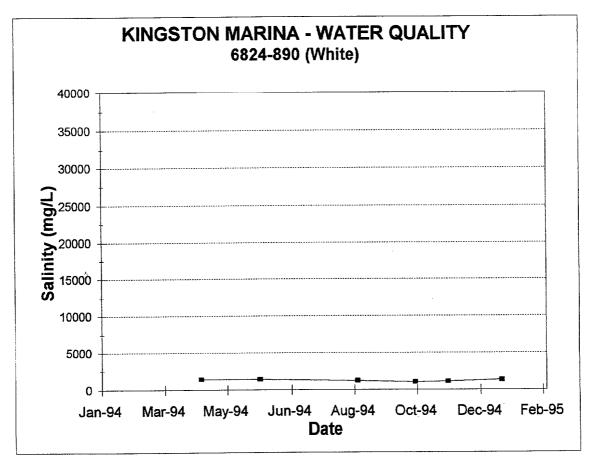


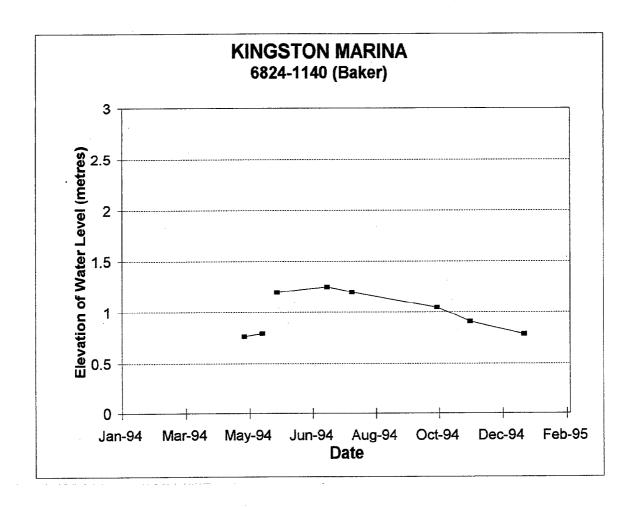


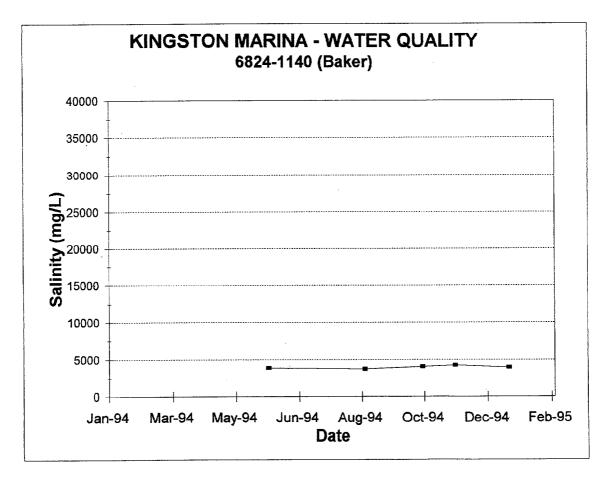


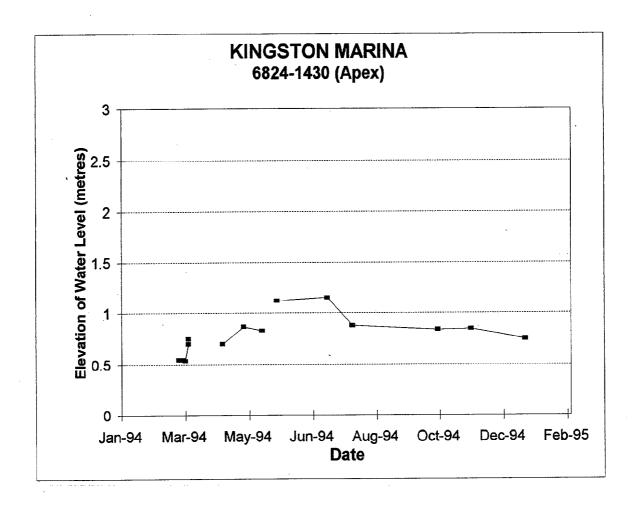


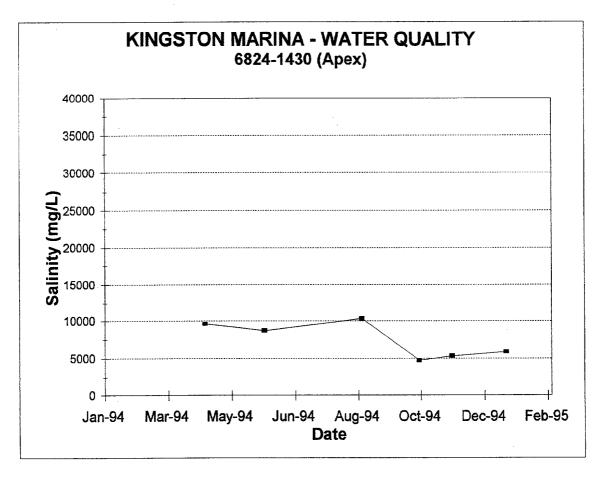


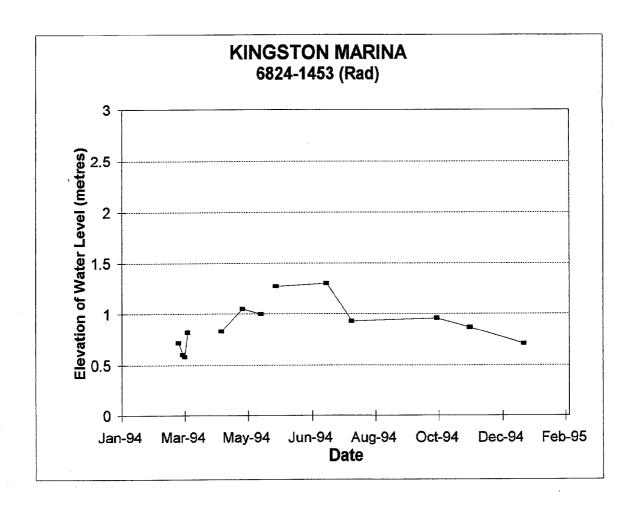


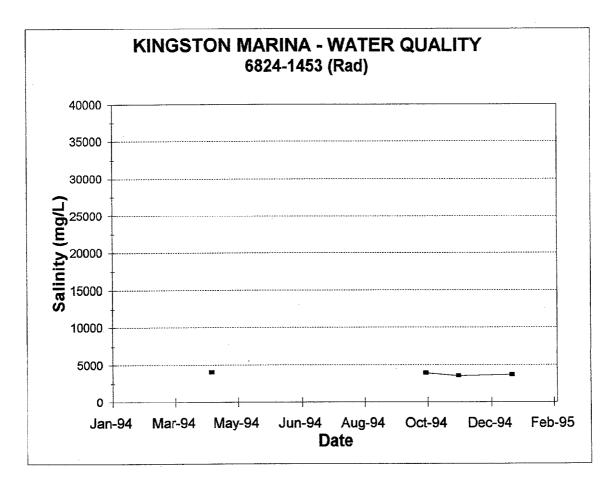


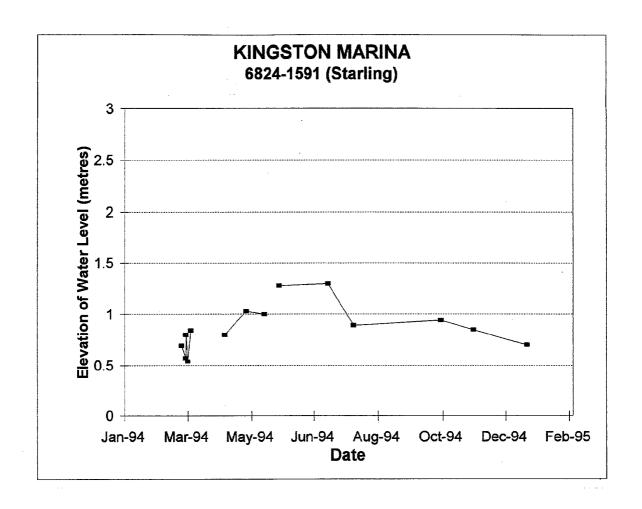


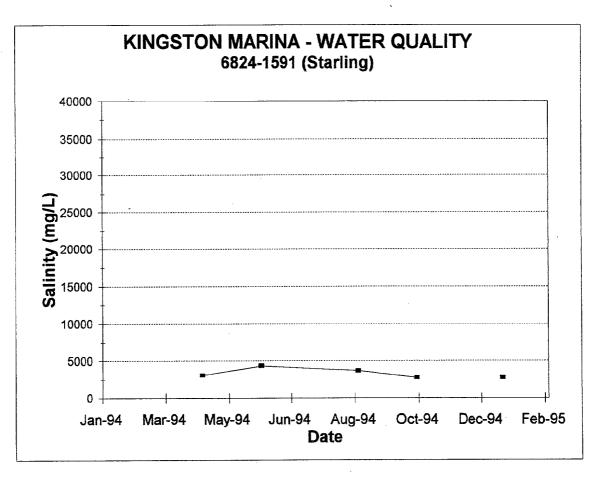


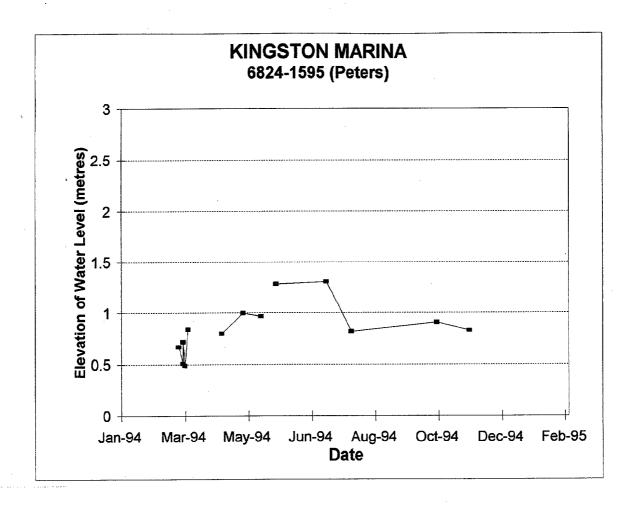


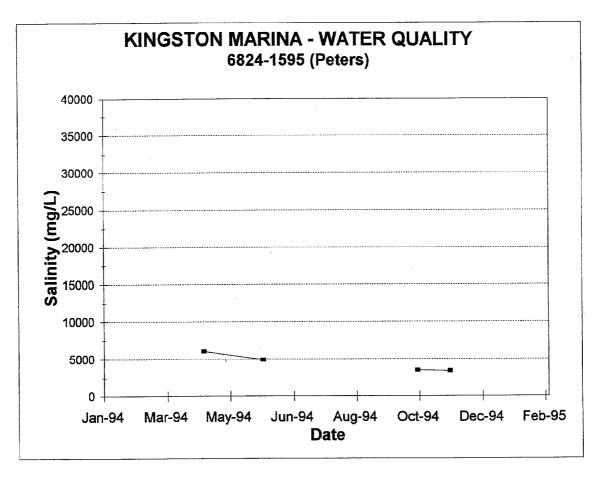


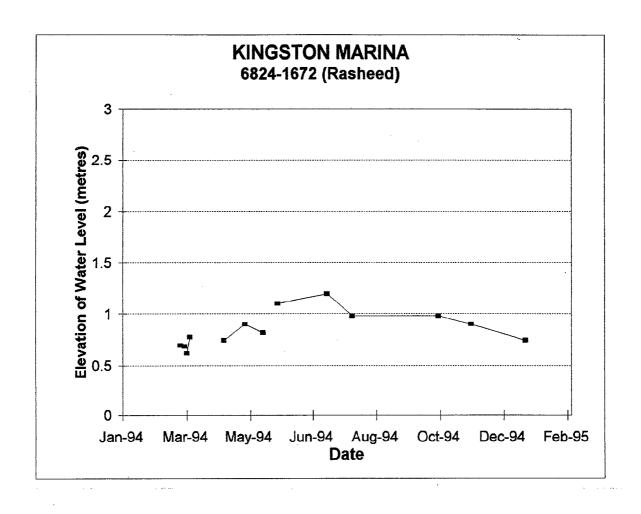


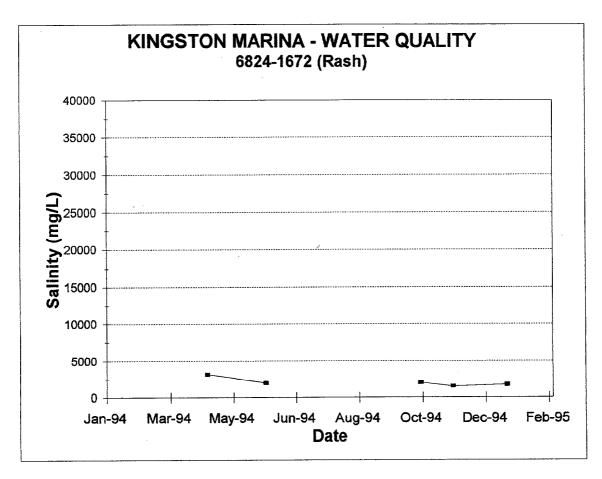


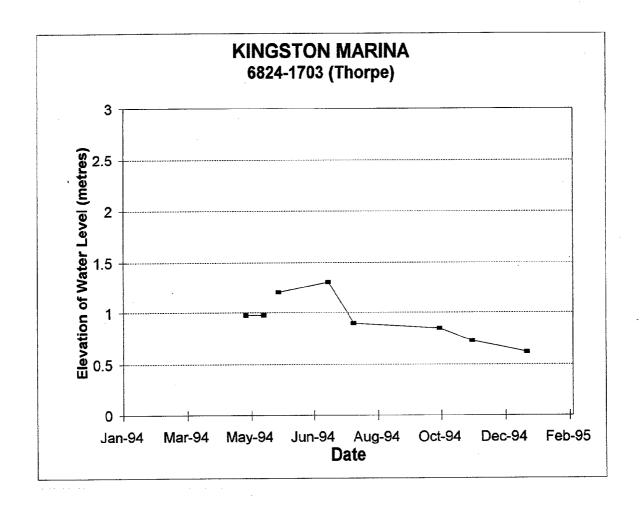


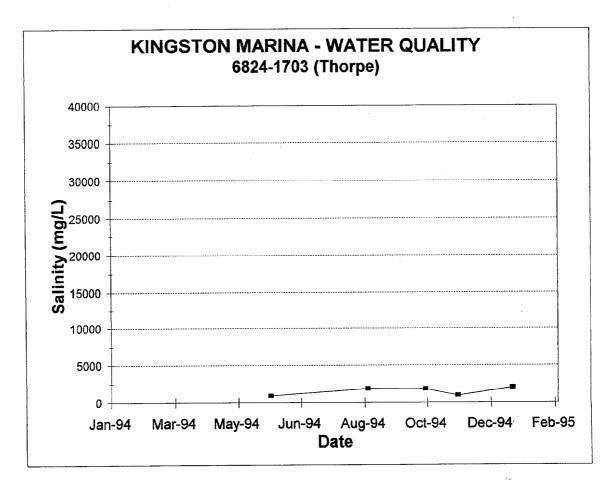


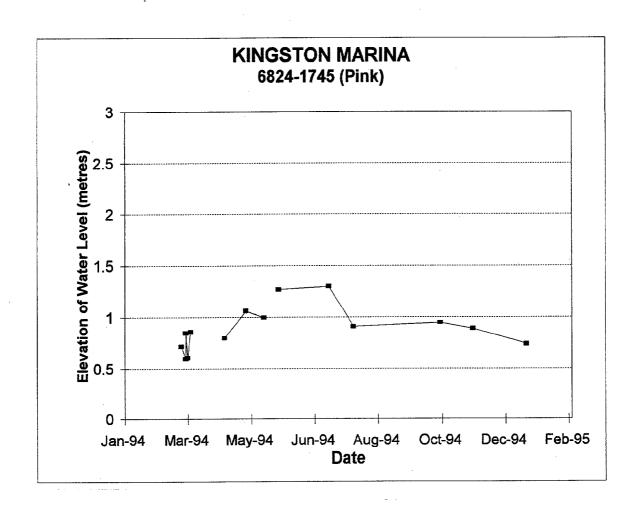


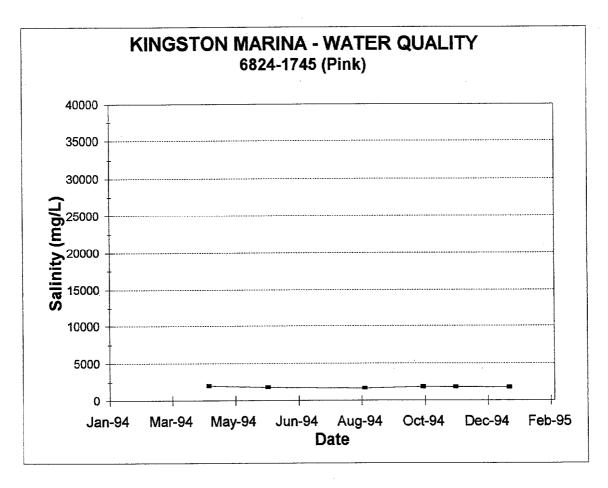


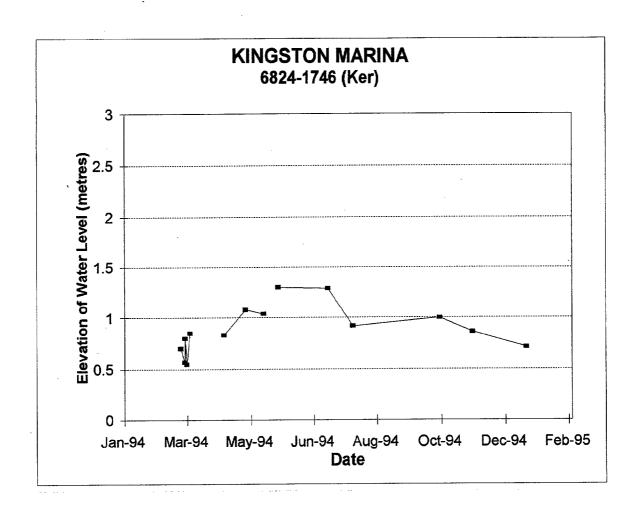


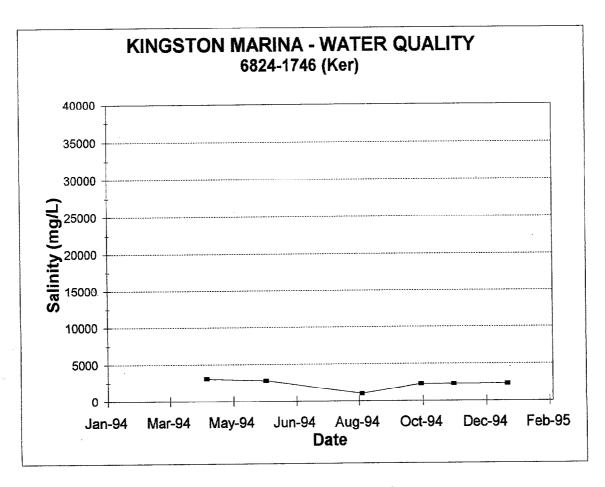


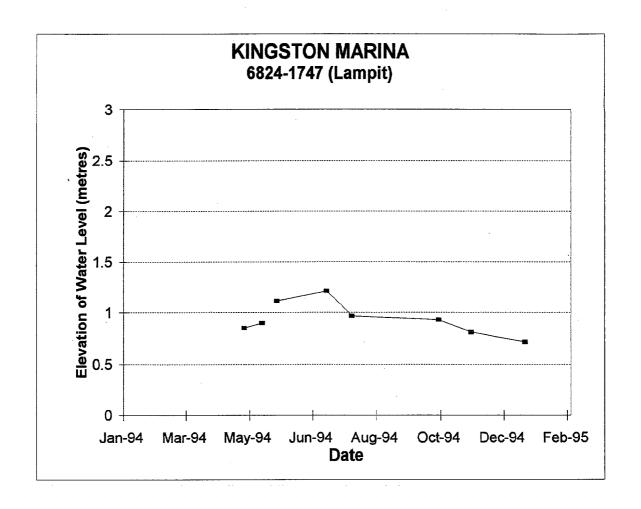


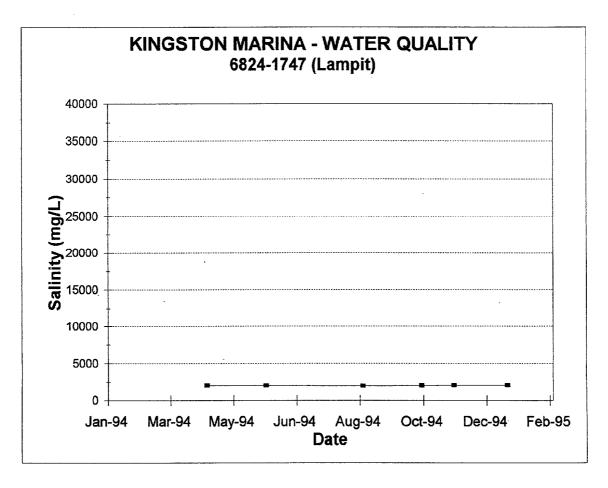


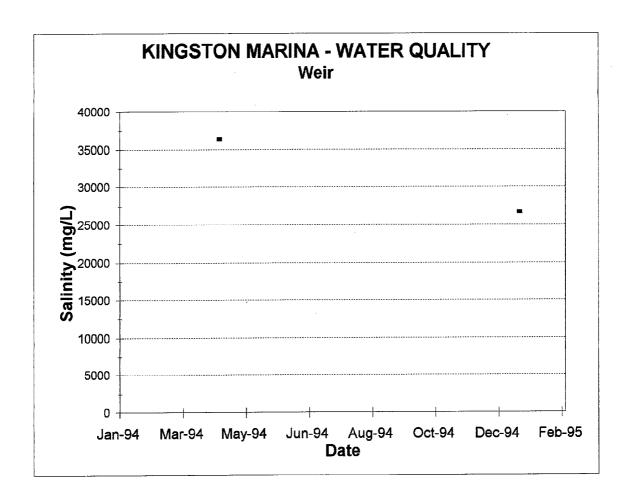












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