DEPARTMENT OF MINES AND ENERGY GEOLOGICAL SURVEY SOUTH AUSTRALIA

REPORT BOOK 92/17

SEISMIC INTERPRETATION OF MT HOPELESS LINE 1

by

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DME 112/77

OCTOBER 1992

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Thirty three kilometres of high resolution seismic was shot in March 1991 on Moolawatana 1:100 000 map sheet, between Lake Crossing Bore and drill hole 588/6, south east of Mt Hopeless.

The project aimed to ascertain the tectonic character of the Blanche Lineament, determine structure and lithologic continuity of the Eromanga Basin sequence, determine the presence or absence of older basin sequences (Cambrian, Permian), examine basement topography and structure, and, if possible, elucidate any structure within the Tertiary sequence.

Geoflex detonating cord provided the seismic energy source. Seismic data aquisition was carried out by VELSEIS Pty Ltd using a Sercel 338-HR 96 tracer recording system. Six hundred percent CDP coverage was obtained using symmetrical spread receiver geometry.

A high quality seismic section was produced, revealing a probable cause for the Blanche Lineament <u>viz.</u> a SW shallow dipping diachronous thrust fault. In addition, the section revealed abundant listric faulting within the Mesozoic shales, the presence of a thick pre-Mesozoic SW dipping sequence, the presence of probable crystalline basement near and south of Mt Hopeless, and deformed Mesozoic/Tertiary strata east and SE of Mt Hopeless.

There is a discrepancy between the drilled depth to 'basement' lithologies and the interpreted position of the basement reflector at the Mt Hopeless end of the line. Furthermore, the ages and lithologies of pre-Mesozoic rocks have not yet been resolved. Two drill holes located at station points 178 and 1685 would resolve these uncertainties.

INTRODUCTION

The Mount Hopeless Seismic Line (#01) was proposed by Regional Geology Branch with significant input from the Geophysics Group within Oil, Gas and Coal Division, as part of CALLABONNA geological mapping (National Geoscience Mapping Accord) and Eromanga Basin data aquisition.

Mount Hopeless is situated 13 km south of the Strzelecki Track and 22 km north of Mt Babbage in the northern Flinders Ranges (Figs 1, 2). The seismic line is 33 km long and runs from 4 km southwest of Mt Hopeless to 3 km northeast of Lake Crossing Bore and approximately 5 km east of Mt Hopeless Outstation. Access is via the Strzelecki Track, Mt Hopeless to Arkaroola Road and the Moomba-Adelaide gas pipeline road.

Topography in the line vicinity ranges from alluvial plains to rolling downs to low hills and At the northern end, salt-bushbreakaways. covered sand flats and channels associated with the floodway between Lakes Blanche and Callabonna occur. These channels are very close to sea level. Between Lake Crossing Bore (11.3 m AHD) and Mt Hopeless Dam, the line crosses gibber clad gentle northerly sloping ground with little or no vegetation. From the Arkaroola Road intersection (31.3 m AHD) to Mt Hopeless (126.3 m AHD) the ground rises firstly as low rounded knolls then into breakaway country with ridges armoured by silcrete. Southwest of Mt Hopeless the ground slopes gently to the south along a drainage divide between westward and eastward gullies to Mt Hopeless and Yerila Creeks. Vegetation is limited to small trees and bushes along creek lines within the hilly portion of the line. Beyond the southern end of the line (77 m AHD), occasional silcrete capped mesas rise above the gently rolling terrain, Mt Yerila being the most prominent, towards the Flinders Ranges.

Objectives of the seismic line were to investigate the:

- 1. Nature of the Blanche Lineament/Fault. This is a major feature trending NW-SE across CALLABONNA passing SW of Lakes Blanche and Callabonna. It forms the hypothetical boundary between the Warburton and Arrowie Basins, and also a major palaeo-faunal boundary. The line was positioned to bisect this feature at ~90°.
- 2. Basement topography, structure and depth.
- 3. Presence or absence of Cambrian deposits (Warburton and/or Arrowie Basin limestones and shales).
- 4. Structure within the Mesozoic sequences (ie faults).
- 5. Structure within the Tertiary sequence (ie. faulting, drag folding, and any major channelling).
- 6. Subsurface geology of the basins to the north of the Flinders Ranges basement outcrop, for incorporation into the geological mapping and tectonic interpretation of the CALLABONNA 1:250 000 and Moolawatana 1:100 000 map areas.

PREVIOUS WORK AND REGIONAL GEOLOGY

A table of stratigraphic units recognised in the Frome Embayment and Callabonna Sub-basin (eastern Lake Eyre Basin) is given in Figure 3. Graphic logs to the region's deep stratigraphic wells are set out in Figure 4.

The line was positioned so as to intersect the Landsat surface trace of the Blanche Lineament

at approximately 90° and to tie into existing drill holes for stratigraphic control. Two drillholes were chosen for line intersection. These were Lake Crossing Bore and hole 588/6. The latter was drilled for Petromin NL et al (1972) on Special Mining Lease (SML) 588 as part of a broad uranium exploration program (Figs 2,5). Additional stratigraphic information was obtained from Montecollina Bore to the north east, Petermorra Bore to the west, and holes 5 to 10 on SML 588.

Only the uranium exploration holes 588/6 to 588/10 intersected rocks with basement characteristics (ie porphyritic quartz monzonite, micro quartz diorite, amphibolite). These rocks are consistent with those outcropping between Mount Babbage and Prospect Hill 20 km to the south of Mt Hopeless.

Table 1 displays the anticipated stratigraphy for the line, and Figure 5 displays the anticipated line section, based on proximal drilling. Summary logs to the strategic drill holes and control drill holes are provided in Tables 2 to 7. The line was extended 3 km beyond each of the stratigraphic control holes in order to provide adequate seismic data at these control points.

TABLE 1 ANTICIPATED STRATIGRAPHY:

(adapated from existing drilling data)

Age Packet	Depth ranges (South- North)	Lithologies and Unit Names
Quarternary	0 ->24 to 33 m	Silts, clays, sands, gravels
Tertiary	24 to 33 -> 60 to 270 m	Clays, sands, some gravel - Eyre Fm
Mesozoic	60 to 270 -> 270 to ~600 m ? -> 510 to 520 m ~400 -> ~730 m	Shales - Oodnadatta Fm, Bulldog Shale (Marree Subgroup) sands - Coorikiana Sandstone sandstone with cemented top - Cadna- Owie Fm
Cambrian	Not present -> ?800* m	Limestones,
Precambrian Basement	~450 ⁺ -> ?100 ⁺ m	qtz porphyry granite, amphibolite

Both Lake Crossing and Montecollina bores were drilled in the late 1890s as government sponsored water supply bores. Neither fully penetrates the basin stratigraphy. Lake Crossing Bore was completed in ?Coorikiana Sandstone and Montecollina Bore was completed in Cadna-Owie Formation (Fig 4). Thirty kilometres to the west of the line is the Santos' Blanchewater Hill CBH #2 stratigraphic hole, which intersected ?Cambrian red-bed mudstone/shale/sandstones at a depth of 602m (Santos, 1981; Preiss and Harris Skeleton #2, drilled 42 km SSE, 1982). intersected granitic basement beneath Mesozoic sediments at a depth of 583.4 m (Callen et al, 1990) (Fig 4). Hole SPH-1 drilled 11 km east of Moolawatana Station Homestead and 15 km west of Skeleton #2, revealed Mesozoic sediments to rest directly on Proterozoic calcsilicate hornfels rocks (BHP Mining, 1983; Tahan and Dunbar, 1983)(Fig 4).

Mount Yerila to the south, exposes Marree Subgroup shales on its lower flanks and ?Coorikiana Sandstone on its northern and eastern mid flanks. The latter unit is unconformably overlain by Tertiary Eyre Fm that has a strongly silcreted upper surface. Mapping around Mt Hopeless has established outcropping Tertiary mudstones, sands and silcretes of the Eyre Fm. Some of these display steeply dipping beds suggesting either localised drag folding or listric block rotation (Sheard and Callen, in prep).

Pre-existing aeromagnetic data maps indicated that the area consisted of 'typical' magnetic basement and that the line would cross a broad magnetic ridge between two highs - to the west and east.

ACCESS ARRANGEMENTS

The line did not intersect any Regional Reserves or National Parks, and the Department of Environment and Planning (DEP) anticipated that there would not be any long term environmental impact provided the following measures were adopted:

- · large shrubs and trees were avoided
- · lower herbs and forbs were not bladed out
- · wind rows and trenches were rehabilitated
- · banks of creeks were not graded for access
- access tracks to the seismic line to be controlled to avoid tourist access.

These requirements were in accord with the <u>Dozer Manual</u> of Nicholls (1988) and the <u>Arid Zone Field Environmental Handbook</u> (Mc Laren et al., 1990).

On the recommendation of the Aboriginal Heritage Unit of DEP with respect to the possible traversing of heritage and/or sacred sites by the proposed line, a site inspection was undertaken with the Flinders Ranges Aboriginal Heritage Consultative Committee (FRAHCC) on the 4th and 5th of March 1991. Representatives from the FRAHCC were Mr G Coulthard (Chairman) and Mr B Coulthard (Community member); and from S.A.D.M.E., M Sheard (Regional Geology) and P Dunne (Geophysics). Three significant but small heritage sites were identified and marked both in the field (pegs and flagging) and on area maps - one of which was

given to the FRAHCC representatives. A site clearance agreement was signed by both parties (Plate 1) to allow work to proceed with avoidance of the three sites. A copy of this agreement is provided in Appendix 1.

The Pipelines Authority of South Australia (PASA) was approached for access to drinking and ablutions water from Compressor Station #2 on the Moomba-Adelaide Gas Pipeline.

Access permission for the seismic work by VELSEIS Pty Ltd to the Mt Hopeless Outstation area was obtained by VELSEIS.

LINE OPERATIONS

A full account of all line operations is set out in the VELSEIS Operations Report in Appendix 2.

On-site personnel and equipment movements are set out in Appendix 3.

A brief summary of the procedures is given below.

Surveying

A contract surveyor set out the line using standard chaining techniques, each geophone spread point was marked with a 'pin flag' which had a plastic coloured tag at the top. These flags were placed at stations 12.5 m apart (100/8 m) and were coloured thus: blue = ordinary point, red = start or end of shot point, and yellow = centre point to shot for detonation (Fig 6).

The line avoided the three Aboriginal Heritage sites previously identified and was layed out well in advance of the seismic work. Line deviation was kept within 7° of a straight line where avoiding obstacles, which also included a silcrete capped ridge (near Mt Hopeless).

Follow-up leveling and survey tie-in to existing Department of Lands benchmark and trig points was made at the completion of line layout work.

A detailed plan of the seismic line is provided in Figure 7, while a list of Permanent Markers along the line appears in Table 8.

Shot Emplacement and Experiments

The seismic energy source consisted of a charge of ICI Red Cord detonating cord (PETN charge - 10 gms/metre), 50 m long and ploughed in to a depth of 0.5 m. The cord was capped with a single electrical detonator at the centre of each 50 m shot (Fig 6). Cord was ploughed in using a Liebherr 731 Bulldozer (equivalent to Caterpillar D-6.5). Attached to the ripper tyne was a copper-lined reinforced cord-feed tube. Above this was a twin cord spool holder and feed assembly (Plates 2, 3).

Experimental shots were carried out at the northern end of the line in order to establish shot length, strength and the signal to noise ratio. Previous work by SADME at Bopeechee near Lake Eyre South, over similar but thinner basin stratigraphy, had established an optimum cord length of 32 m (Cockshell, 1988). Anticipating that similar parameters would work at Mt Hopeless, the line was set out with charge shot points on 100m centres.

Three single strands of Red Cord (25 m, 50 m, 75 m) were ploughed in and fired (Plate 4) to determine optimum charge size. The seismic records indicated that 50 m length provided the best signal. A fourth charge of double strand 50 m long was ploughed in and fired but no additional enhancement to the signal was noticed.

The experimental work accomplished a secondary role in providing an opportunity to further develop the ripper-ploughing technique. Furrow infill/smoothing of the shot point furrows was accomplished simultaneously with the ploughing by towing an improvised set of harrows. Ripping worked well in the sandy to clayey soils but some difficulty was experienced near Mt Hopeless with silcrete. The bouldery edge to a silcrete ridge was pre-ripped three times prior to ploughing in of the Red Cord.

Shot emplacement ripping was achieved without prior line clearing and without putting the Dozer blade to the ground, but rather by just 'Walking' the dozer along the line (Plate 5). No herbs, shrubs or trees were removed and all root stock was left in place where flattened by the dozer tracks. No additional access tracks were prepared. Fences were unhitched and layed flat then re-established following ripping. Shot point-ripping was kept at least two to three kilometres ahead of the recording set up on the

first day. Following that the Dozer kept at least 8 km ahead of the recording crew.

Seismic Recording and Firing

Firing and recording proceeded well with good to excellent records. Only one delay misfire in over 300 shots was observed. Shots were skipped at roads, fences, bores and pipeline crossings with only minimal effect on the final stacked records.

Some time was lost due to problems with the electronic firing system. Additional lost time of two days was due to strong winds that produced unacceptable signal to noise ratios. This problem was solved by shooting the last 4.2 km of line at night when conditions were calm.

DATA PROCESSING

Seismic Processing

Processing was done by Velseis Pty Ltd in Brisbane. A relatively standard processing sequence was used. The high quality of the field data assisted processing and negated the need to apply sophisticated signal enhancement packages. A full account is presented in Appendix 2.

As the line aimed for structural reconnaissance, more emphasis was placed on reflector coherency than true amplitude recovery. Even so, the quality of the data did not necessitate the application of coherency filters. Migration of the data was not deemed necessary, after consideration of the relatively low relief of the reflectors.

Final stack section was presented in film form at a horizontal scale of 1:5000 (8 traces/cm) and a resolution of 1000 dots/inch. A reduced scale version was also prepared as a paper print at 1:10000 with a resolution of 400 dots/inch (Fig 8).

Data Quality

The seismic quality of most of the field data was quite high to excellent. Isolated records were noisy due to windy and possibly poor source tamping. Over most of the line this causes only minor deterioration of section quality. However between stations 340 to 410, section quality is

poor where severe wind conditions caused poor records.

Over much of the section, seismic events near strong reflectors have been substantially attenuated by the application of strong amplitude equalisation over a 400 millisecond window. This makes interpretation more difficult as bland zones can indicate either thick homogeneous rock or mathematically subdued zones.

SEISMIC INTERPRETATION

Geological Control

Geological identification of the seismic profile is based on six drillholes on or near the line. The sequence intersected comprises Quaternary and Tertiary sediments, thickening northeastward, underlain by a relatively uniform Cretaceous sequence (Marree Subgroup and Cadna-Owie Formation). A porphyritic quartz monzonite was intersected in the southwestern-most two holes (588/7 and 588/6) but this may not be representative of basement for the whole area. Details of boreholes and depth intersections are included in Tables 1 to 7, and Figures 2, 4 and 5

Accurate conversion of unit depths to time values on the seismic section is hampered by the absence of measured well velocity data from any of the above boreholes. Interpreted two-way travel times (TWT) are set out in Tables 1 to 7. The nearest bore with such data is Skeleton #2 approximately 40 kilometres southeast of the line (Callen, et al, 1990).

Detailed discussion with Velseis Pty Ltd highlighted the following information on the velocity analyses:

- 1. Original velocity analysis was done on ground level based velocity gathers.
- 2. Four different sets of statics were applied to the data, with the result of time 0.0 seconds on the section representing 0.0 m MSL.
- 3. Velocity analyses were corrected for elevation so that 0 time in the tabulated velocity values represents 0.0 seconds on the section and 0.0 m MSL.

Initial conversion of depths to seismic times used the stacking velocities near each borehole location. These values were then compared to the average velocity values from Skeleton 2 well. The two data sets were found to be reasonably consistent indicating that the computed time picks would reasonably represent the intersected units to within 15% of the MSL value.

Section Interpretation

The processed seismic section is presented in Figure 8 (1) to (5).

(a) Cainozoic

The shallowest and most reliably identified seismic horizon interpreted is the Tertiary-Cretaceous boundary. In Lake Crossing Bore the horizon separates a relatively uniform bland seismic zone, typical of the Marree Subgroup, from an overlying sequence of strong basal Tertiary reflectors. A similar situation is seen at the end of the section closest to Montecollina Bore, where the presence of lignite within the Tertiary sequence would strengthen reflectors. The horizon picks at the northeast end of the line (SP 2653) are shallower than the Montecollina Bore picks, due to anticipated section deepening toward the bore. Southwestward, the Tertiary sequence thins, particularly near SP 1900 and SP 500 where significant onlap events are seen.

Southwest of SP 350 the horizon is interpreted to subcrop at datum. However, interpretation of the 0-0.1 second part of the record is subjective due to lack of data, low fold of stacking and/or selection of recording parameters to target deeper levels.

At its deepest point the Quaternary-Tertiary boundary occurs at 0.055 (ie. not resolvable) at Montecollina Bore and was therefore not interpreted.

(b) Cretaceous

In Lake Crossing Bore, a sandy, brackish water zone which occurs at 404 to 439 m below MSL, corresponds to a relatively consistent reflector mappable along the section. It correlates approximately with similar zones in Montecollina and 588/7 bores. It is suggested that this zone represents the Coorikiana Sandstone. The

presence of thick, uniform and bland seismic sequences above and below this zone (Oodnadatta Formation and Bulldog Shale respectfully) further supports this.

The Marree Subgroup (Oodnadatta Formation/ Sandstone/Bulldog Shale) Coorikiana remarkably uniform in character and thickness along the entire section. This unit has substantial mostly normal listric structuring, internal Such faulting is typical syndepositional movement in thick shale sequences although many faults appear to continue into the basal Tertiary sequence, indicating later or continuing deformation.

A major low angle reverse fault is seen between SP's 1300 and 1500 deforming the underlying sequences and extending at least to the basal Tertiary sequence. The surface trace of the extrapolated fracture closely corresponds to the 'Blanche Lineament'. There are no other features on the section to provide a geological explanation for this lineament. Further seismic work would be required east and west of this line to define more precisely the geometric attitude and extent of this feature. However, a NE-SW compressional regime appears to have promoted the development of this thrust fault.

The Cadna-Owie Formation was intersected in Montecollina and Petermorra Bores beneath Bulldog Shale. Although neither bore lies on the section, a strong, relatively undeformed reflector near this level was interpreted to represent the This unit shows top of this sequence. substantial, generally continuous reflectors. also shows common lensing-out of reflectors with upward and downward terminations, indicating substantial facies variation. This is consistent with an expected marginal marine to fluviatile/deltaic environment of deposition. Over much of the section, this interval is However, in the approximately 100m thick. centre of the section it thins rapidly and may even be absent between SP's 1370 and 1480. of reflectors onto the underlying unconformity in this area indicates that a substantial high existed prior to deposition of the Cadna-Owie Formation in the Early Cretaceous. This is further supported by infilling of erosional and fault related depressions in the underlying surface. The possibility that earlier Mesozoic sediments are preserved in these depressions cannot be discounted because a thickness of 100 metres for the Cadna-owie Fm alone is considered to be anamalous here.

At the southwest quarter of the section, this interval shows consistent thickness even though it is much shallower, particularly southwest of SP 300. Between SP's 300 and 400 is a major zone uplifted to the southwest by reverse faulting and monoclinal flexure. It is interpreted that stable depositional conditions existed in the Early Cretaceous and that deformation occurred in the Late Cretaceous (at earliest) or, more likely, in the Tertiary associated with the Flinders Ranges uplift.

(c) Pre-Mesozoic

The reflector interpreted to represent the base of the Mesozoic section is generally a very strong event, representing a strong unconformity surface. The strength of the event and marked increase in average stacking interval velocities indicates that the underlying rocks are much harder and more indurated than the Mesozoic sequence. This points to rocks of Precambrian to early Palaeozoic age.

The apparent dip of reflectors below this unconformity is 4° to the southwest. This compares to an apparent 3° northeast dip for the regional dip of the overlying Cretaceous sequence.

These reflectors are most observable between SP's 1200 and 2100, down to 1.4 seconds. Below this level they are either absent or are swamped by multiples from the Mesozoic-Cainozoic sequence. Laterally, the occurrence and strength of reflectors diminish quite rapidly probably due to a combination of:

- reduced seismic penetration
- swamping of signal by multiples
- reduced reflectivity caused by facies variations
- major rock-type changes.

The consistency and strength of these reflectors is similar to those from the Cambrian sequences in the Arrowie Basin (to the south) and the Warburton Basin (in the north). However, it is also possible that they represent Adelaidian, Ordovician or even Devonian rocks. Drilling will be required for positive identification.

Southwestward of SP 400 there is a major change of seismic character beneath the unconformity. Here there are no apparent dipping reflectors and very few multiple events. This corresponds to a very high amplitude reflector of the unconformity, indicating the presence of an underlying rock unit with a very high velocity. Although this is not seen in the calculated stacking velocities, velocity analyses in hard rock zones with virtually no reflectors are rarely reliable.

It is therefore postulated that there is a major change of pre-Mesozoic bedrock rock type southwest of SP 400. Such a change may be associated with the zone of reverse faulting and monoclinal flexure between SP 300 and 400.

A major dilema exists regarding identification of bedrock in bores 588/7 and 588/6 (Petromin NL et al, 1972). These 1972 mineral exploration bores were both logged as having intersected porphyritic quartz monzonite at TD. However, transposing of the bore depth data to the seismic section, using existing velocity data, locates these igneous intersections well above the interpreted Cadna-Owie Formation. Even allowing for 15% velocity variation they remain well above this unit.

One possible explanation is that the bores both bottomed in 'lonestones' within the Bulldog Shale. Lonestones, ranging from centimetres to three metres in diameter are common within this unit. They are interpreted as being brought in by ice rafting then dropped into the underlying muds (proto-Bulldog Shale) as isolated erratics (Frakes and Francis, 1988; Sheard, 1990).

Most holes drilled in this mineral exploration series intersected less than 0.5 m of this igneous material at TD. This enhances the possibility that the intersections do not represent pre-Mesozoic bedrock. However, the fact that most holes (8) were logged as intersecting the same material makes the above explanation more difficult. Re-logging of cuttings from the bores will be necessary to verify rock identification.

CONCLUSIONS

The seismic survey has successfully defined the geometry and stratigraphic relationships of the Mesozoic sequences. The configuration of the basal Tertiary sequence has also been stratigraphically defined over much of the line. The base of the Mesozoic section (as interpreted) is clearly shown as a strong unconformity event. A major sequence of pre-Mesozoic rock is observable over much of the section which may be Precambrian to Devonian in age. However, a Cambrian age is thought likely. Crystalline rocks may exist southwest of SP 300.

The survey has been successful in achieving its main aim, identifying the cause of the Blanche Lineament. It has shown the most probable cause of this feature is related to a major low angle reverse fault dipping to the southwest, active in the Tertiary, and possibly more recently.

A seismic unit interpreted to be the main aquifer in the region, the Cadna-Owie Formation, has been delineated. This substantially improves the hydrogeological knowledge of the region.

The postulated occurrence of Precambrian - early Palaeozoic rocks beneath the Mesozoic section may have significance to base metal and hydrocarbon exploration. If the sequence is Cambrian, petroleum prospectivity would be enhanced in terms of generation and reservoir potential. On this particular line, entrapment may be a difficulty, although three mechanisms appear possible:

- 1. Stratigraphic entrapment within shallow dipping early Palaeozoic reservoirs with a weathered or shaly facies near the unconformity separating the reservoir from the Cadna-Owie Formation aquifer.
- 2. Entrapment within the same reservoirs, capped by Bulldog Shale where the Cadna-Owie Formation is absent.
- 3. Entrapment in domal warps within the Cadna-Owie Formation sealed by the Bulldog Shale. However, water flushing would be a major difficulty in this senario.

The good definition of structural features on the section provides new information on the tectonic history of the area and will assist in tectonic reconstruction of the region.

RECOMMENDATIONS

To promote additional exploration in this region, further investigations are recommended:

- 1. Acquisition and interpretation of ground magnetic and gravity data along the line.
- 2. Application of seismic refraction probing at several sites along the traverse.
- 3. Undertake drilling at sites A and B along the line:

Site A

Drill a stratigraphic well near bores 588/6 to 588/7 (Fig. 9) to identify interpreted basement horizons and tie in with the seismic line. NB: No cuttings or samples are available in the Glenside Core Library for these holes.

A shallow hole drilled south of exploration hole 588/6 at Site A (Fig. 9). A saving of some 65 m⁺ in drilling depth may arise if the hole is sited near the seismic line end (ie. SP 75). This results from a topographic advantage and narrower section. Coring only from a depth of 230 m below ground level to basement. Seismic basement interpreted as crystalline rock at a depth of 469 m. Coring to penetrate 5 to 10 m of basement. A seismic velocity well shoot to follow drilling to determine actual seismic unit velocities.

The retrieved core will assist with an assessment of base metal potential for this area of buried basement.

Anticipated unit intersecton depths for drilling proposal A

Unit Depth(m):

Marree
Subgroup 0 to 359

Cadna-Owie
Fm. 359 to 469

Basement 469+

Site B

Identification of the southward dipping interpreted pre-Mesozoic sequence overlying (?) crystalline basement is required. The mid-line dome structure between SP 1350 and 1850 presents the best target area with a cored drill hole optimal at SP 1685 (Fig. 9). At this location advantage is taken of a reasonable twin layer pre-Mesozoic section on a subtle dome structure while avoiding major faults. Organic and inorganic geochemical analyses of retrieved core would assist with an assessment of hydrocarbon and basemetal potential.

It is proposed to drill a stratigraphic well at SP 1685 to a depth of 1200 with selected coring between 450 to 1200 m.

A seismic velocity well shoot at the end of drilling would provide measured unit velocities for the section and further enhance the seismic section data.

Drilling to basement at this location would require a hole at least 1500 m deep.

Anticipated unit intersection depths for Drilling proposal B

Unit	Depth (m):		
Quarternary-Tertiary	0 to 214		
Marree Subgroup	214 to 634		
Cadna-Owie Fm	634 to 654		
Basement (top) Z1 Z2 Z3	654 654 to ~830 ~830 to ~1120 >1500		

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TABLE 2 SUMMARY LOG AND INTERPRETED SEISMIC TWT TIME MONTECOLLINA BORE

LOCATION: 14.9 km NE of SP2656 ELEVATION: Approx. 8.8 m MSL

DEPTH	DEPTH (m MSL)	<u>UNIT</u>	SEISMIC TWT TIME (msec below MSL Datum)
0	9	Quaternary	-14
45	.36	Tertiary sands, clays	55
285	276	Cretaceous Marree Subg	328 roup
743	734	Cadna-Owie Formation sands shales	801
777	768	TD	814
507	498	?Coorikiana	586 Sst
512	503		591

TABLE 3 SUMMARY LOG AND INTERPRETED SEISMIC TWT TIME LAKE CROSSING BORE

LOCATION:

SP 2416

ELEVATION: 11 m MSL

ELEVA'	IION:	II m MSL	SEISMIC TWT TIME
DEPTH (m GL)	DEPTH (m MSL)	UNIT	(msec below MSL Datum)
0	-11	Quaternary	-14
32	21	Tertiary	27
		sands, lignite	
256	245	Cretaceous	279
610	500	Marree - Sub	group - 536
519	508	TD	330
415	404		434
450	439	?Coorikiana S	Sst 470

TABLE 4 SUMMARY LOG AND INTERPRETED TWT TIME PETERMORRA BORE

LOCATION:

7.8 km NW of SP 437

ELEVATION: 55 m MSL

DEPTH DEPTH UNIT

TWT	TIME
(msec	below
MSL	Datum

SEISMIC

(m GL) (m MSL)		L) MS	L Datum)
0	-55	Quaternary	-67
22	-33	Tertiary	-40
57	2	Cretaceous	2
		Marree - subgroup	
367	312	Cadna-Owie Fm	353
379	324	TD	366

TABLE 5 SUMMARY LOG AND INTERPRETED TWT TIME DRILL HOLE 588/5

LOCATION: ELEVATION:

400 m SE of SP 300

Approx 130 m MSL

SEISMIC

 DEPTH
 DEPTH
 UNIT
 (msec below

 (m GL)
 (m MSL)
 MSL Datum)

0	-130	Quaternary	-209
23	-107	Tertiary	-172
		sand, mudstones	
34	-94	Cretaceous	-151
		Marree - subgroup	
88	-42	TD	-68

TABLE 6 SUMMARY LOG AND INTERPRETED TWT TIME DRILL HOLE 588/6

	DIGI	D HODE SO	.,.	
LOCAT	ON:	On SP 178		
ELEVA'		90 m MSL		
	11011.	70 AM 1140-	SEISMIC TWT TIME	
DEPTH	<u>DEPTH</u>	UNIT	(msec below	
	(m MSL)		MSL Datum)	
7				
0	-90	Quaternary	-150	
		Mudstone		
11	-79	Tertiary	-92	
		sandstones		
21	-69	Cretaceous	-81	
		Marree-sub	group	
255	165	Porphyritic	200	
		Quartz	209	
		Monzonite		
255	165	TD	209	
	<u> </u>			
		TABLE 7		
SUMMARY LOG AND INTERPRETED				
TWT TIME DRILL HOLE 588/7				
	DRII	L HOLE 5	88//	
LOCAT	TON:	300 m NW	of SP 100	
ELEVA		Approx 60		
			EISMIC_	
			YT TIME	
DEPTH	DEPTH	UNIT (m	sec below	
	(m MSL		L Datum)	
		_	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	
0	-60	Quaternary	-100	
		Mudstone	07	

Tertiary

sandstones

Cretaceous

Porphyritic

Quartz Monzonite

TD

Marree - subgroup

?Coorikiana Sst

TABLE 8					
LIST O	F PERMAN	NENT MARKERS			
LOCATION	EASTING	NORTHING ELEVATION	1		

(AHD) Northern end of Line *Station 393 585.10 6733 284.40 6.50 m No 2656 Track to Compressor 7.7 m Station No 2. *Station No 2580 Fence (approx *Station No 10.2 m 2460+) Lake Crossing Bore (approx Station No 11.35 m 6731 155.43 391 472.13 2416) *Station No 1991 (approx 5 km SW of Lake Crossing 19.0 m Bore) Track to Mt Hopeless Dam 24.70 m 384.109.03 6723 938.22 Station No 1591 Arkaroola Road 31.32 m 6720 305.93 380 406.04 Station No 1176 Fence west of Road, Station 39.94 m 6718 545.89 378 409.12 No. 963 *Station No 563 (approx 5 km SW of Station No 70.0 m 963) *Station No 280 (old track to Mount 94.5 m Hopeless) Drill Hole 588/6 91.40 m 371 097.63 6712 016.14 Station No 178 *Southern end of line 77.50 m 8710 533.90 369 719.80 Station No 16 * Additional Permanent Markers put in after work completed in order to comply with the marking of seismic lines under the Petroleum Act.

-97

-70

-224

224

-27

-8

-58

-42

197

197

-16

-5

2

18

257

257

44

55

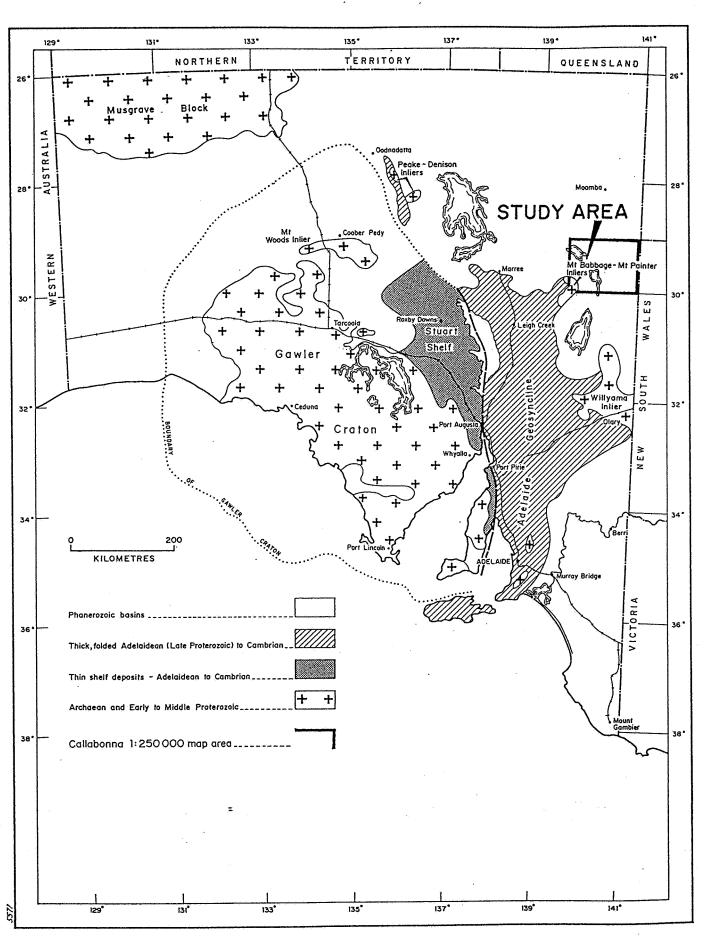


Figure 1. Regional locality plan for Mt Hopeless Line 1 seismic interpretation

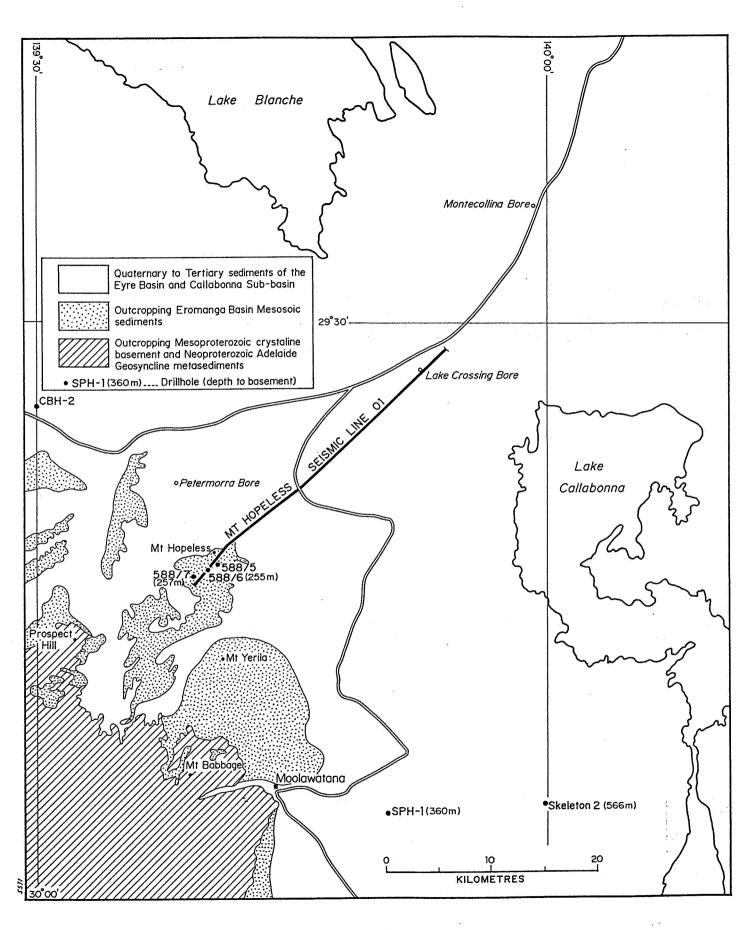
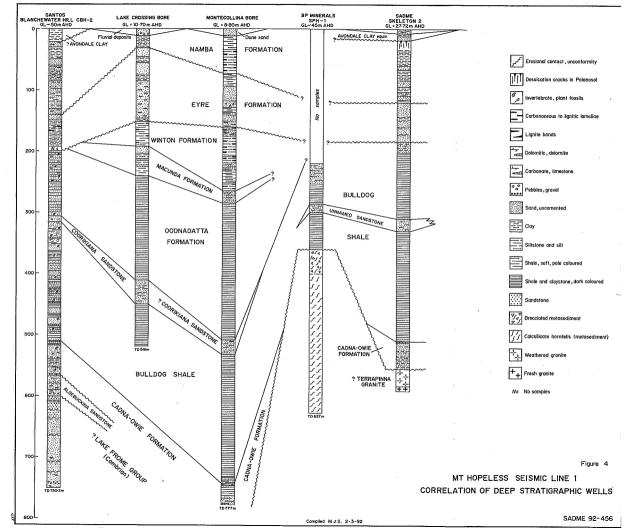


Figure 2. Drillhole and Mt Hopeless Seismic Line 1 locality plan

Mt Hopeless seismic line l, regional stratigraphic units

PF	ROTEROZO	1C	•		PALAEOZOIC	
PALAEO PROTEROZOIC ME	SOPROTEROZO	IC NE	OPROTEROZOIC	CAMB- RIAN	?CAMBRIAN	
Banded siliceous epidote amphibolites near Paraborana Hill and colssilicate horrifells as intersected in drillhole SPH-1 Migmatites, augen gneisses, gneissic granites, colcsilicates, schists, quartzites and meta volcanics	Yerila Granite, Wattleowie Granite, Terrapinna Granite, Mt Neill Granite Porphyry and low grade meta sediments and meta volcanics (te Pepegoana Porphyry)	Intrusive mafic dykes (bosalt, dolerite, gabbro)	Marine mudstones, sandstones and carbonate rocks; glacial sediments Modified by the Delamerian Orogeny	UNCONFORMITY OR NON CONFORMITY Granite, pegnalites	? Lake Frome Group Red bed – mudstones, siltstones, sandstones (as intersected in drillhole CBH+2)	
MT BABBAGE AN	ID MT PAIN	TER	ADELAIDE GEOSYNCLIN	E	ARROWIE BASIN	

JURA- SSIC LATE		MESOZOIC								CAINOZOIC							
		CRETACEOUS						TERTIARY									
				LAT			LATE	ATE	ì								
ļ	NEO	COMIAN	.N		1					·		E O			<u>*</u>	-	
=	<u></u>	≨ :	<u> </u>	BAS	D	Þ			ת ב ב	SE	ALEC	EOCENE		5		MIOCENE	رَ
TITHONIAN	RAI	LAN	175	BARREMIAN	APTIAN	ACBIAN			- TUROMANIAN	SENONIAN	PALEOCENE			OI IGOCENE	1	1	PLIOCENE
N	BERRIASIAN	VALANGINIAN	HALITERIVIAN	Ā	z	Z		1	\$ \$ 2 2	AN	m	m M		η	m A	₹ C	┨''
	2	ž	Z									MIDOLE	LATE		EARLY	MIDOLE	L
•	Algebuckina Sandstone		Cadna—owie Formation (Parabarana Sandstone)	ſ	Unnamed Sand	a Sandstone			Winton Formation			Eyre	Silcrete			Namba Formation	Wildworking Finn (Ayonddie Clay) Sigretii
		L			Marre	ee Subgr	oup				<u>,</u>	KE EYRE BAS	<u> </u>		<u></u>		_1



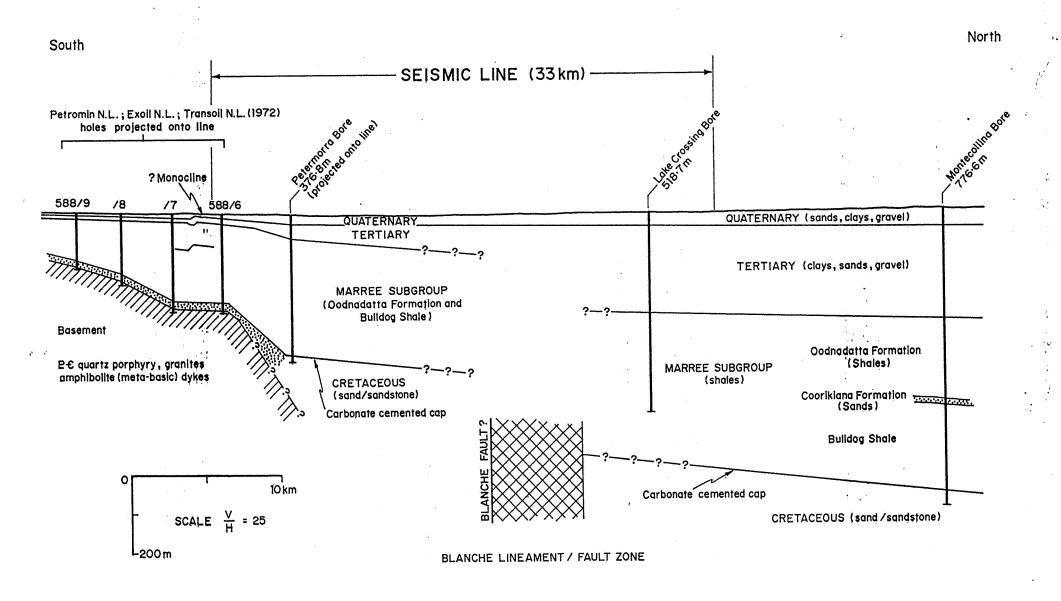
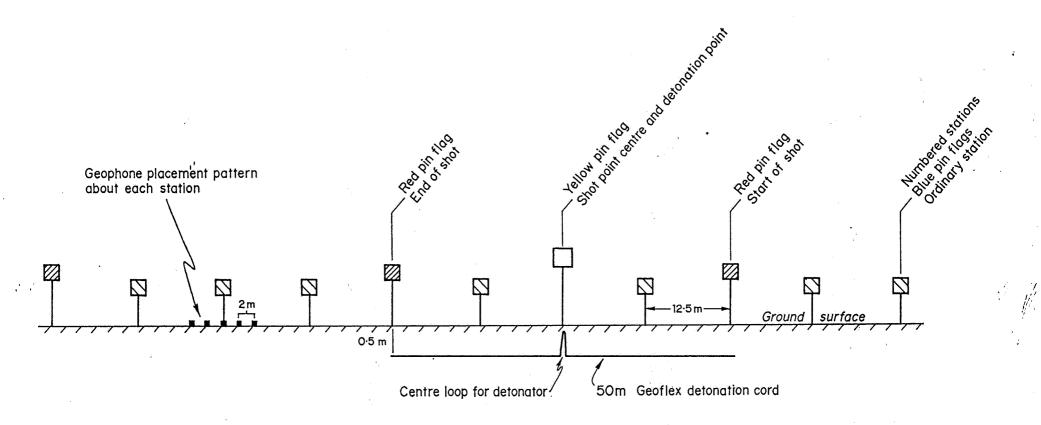
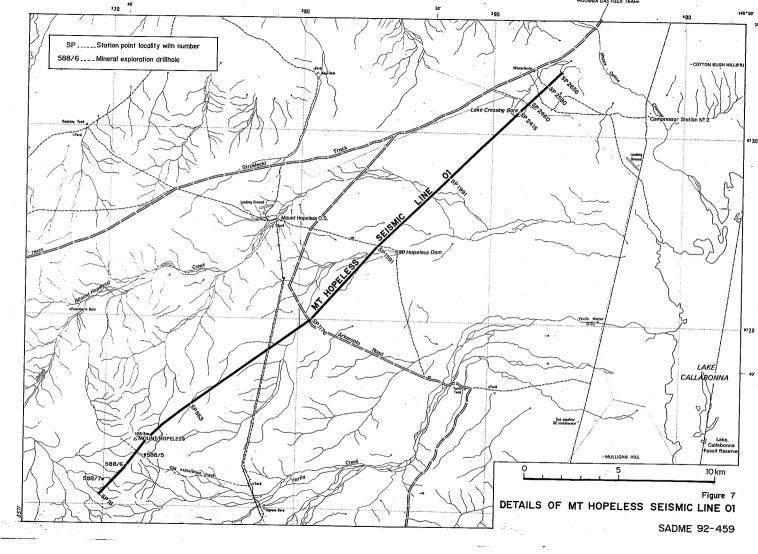


Figure 5. Cross section along Mt Hopeless seismic line, geology adapted from existing drillhole data prior to seismic aquisition



Note: Shot point centres were 100 m apart

Figure 6. Individual shot point layout for seismic interpretation of Mt Hopeless Line 1



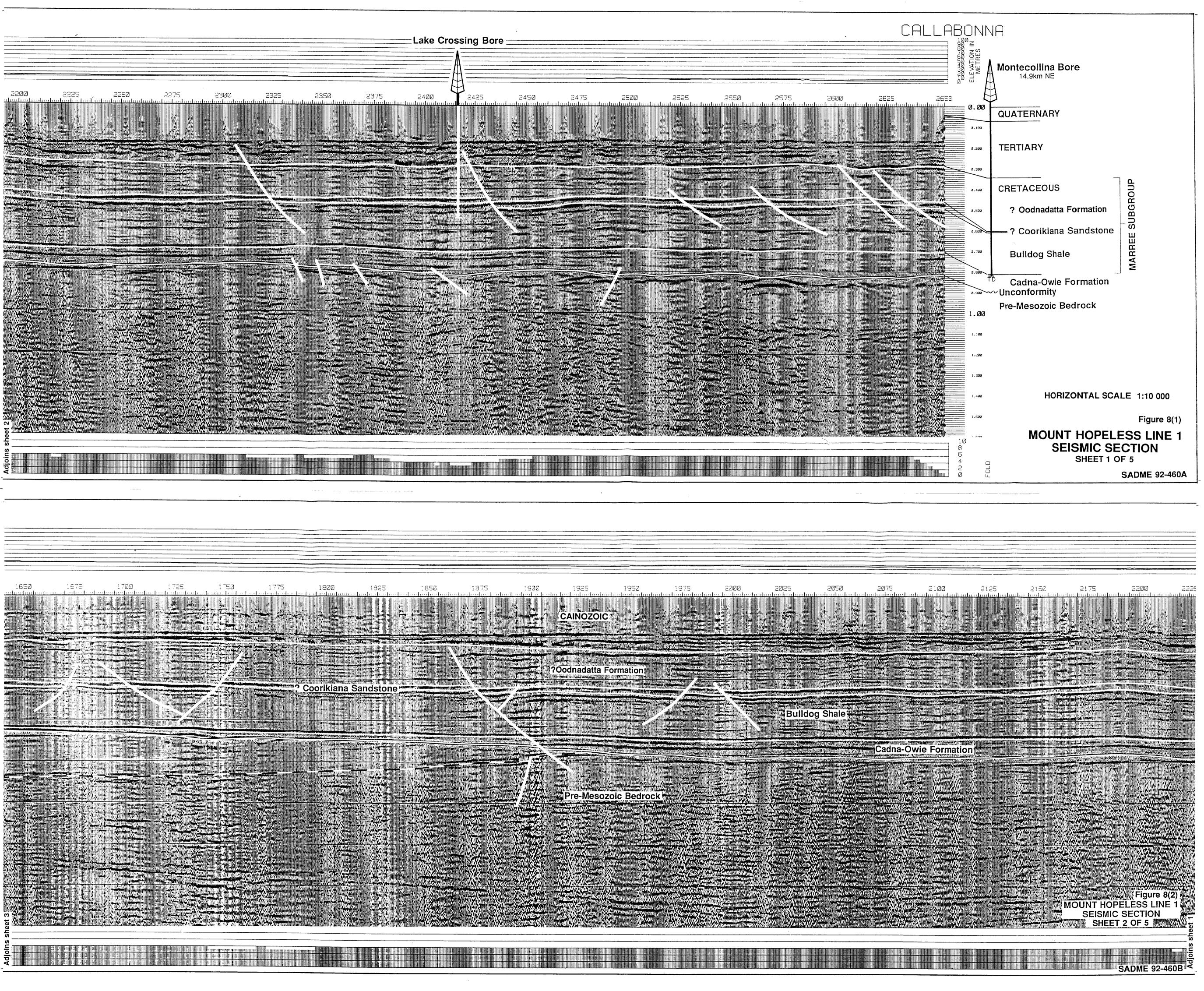


Figure 8(4)
MOUNT HOPELESS LINE 1
SEISMIC SECTION

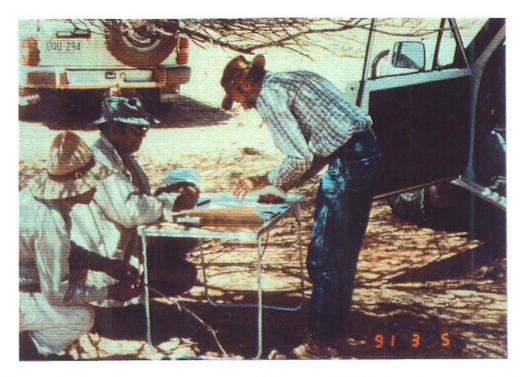


PLATE 1: Signing the Site Clearance Agreement with the Aboriginal Heritage Representatives from the Flinders Ranges Aboriginal Heritage Consultative Committee. L to R: B Coulthard, G Coulthard (Chairman FRAHCC) and M Sheard (SADME).



PLATE 2: Bulldozer with Geoflex cord spool/feeder assembly and hydraulic ripper tyne. The vegetation here is 'old man' salt bush.



PLATE 3: Bulldozer ploughing in the geoflex detonating cord during the experimental work near Moppa Collina Channel. Note that the dozer blade is raised to avoid uprooting the salt bush vegetation.

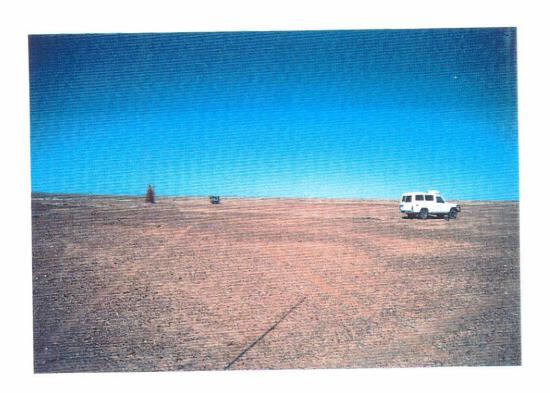


PLATE 4: Firing a shot, the shot man's vehicle (green) near the charge and the recording vehicle (white to the RHS.



PLATE 5: Preloading at the seismic line mid point. Note the dozer blade is raised to minimise ground surface disturbance. Vegetation here was limited to scatterd grass and low herbs.



PLATE 6: View towards Mt Hopeless looking SW along the line which passes to the LHS of Mt Hopeless. A silcrete ridge capping (at centre skyline) was bypassed. Vegetation here is limited to scattered low salt bush, low thorny herbs and along drainage lines are stunted trees.

APPENDIX 1 SITE CLEARANCE AGREEMENT

A SITE CLEARANCE AGREEMENT

BETWEEN

THE SOUTH AUSTRALIAN MINES AND ENERGY DEPARTMENT

AND

COMMUNITY REPRESENTATIVES

ABORIGINAL HERITAGE SITES

Proposed seismic line, Mt Hopeless Tank area, CALLABONNA

We the undersigned acknowledge the receipt of \$220.00 \(\) each for the purpose of inspecting the proposed seismic line operation site situated 3 km SE of Mt Hopeless and running SW of the Strzelecki Track via Lake Crossing Bore and Mt Hopeless Tank.

The actual seismic line and camp site layout are indicated on the attached Plan.

We agree that significant Aboriginal heritage sites have the have been identified but that no* Aboriginal heritage areas lie within the proposed seismic line area. There are indicated on the attacked map and will be avoided.

ABORIGINAL HERITAGE REPRESENTATIVES

18 1 14 1

SIGNED	J. S. Caulhord	DATE
SIGNED	B.L. Carlel	DATE\$-3-91
SADME I	REPRESENTATIVES	
SIGNED	M. J. Shewrol	DATE 5-3-8/

DATE 5 3. 90

(* strike out which ever does not apply).

SIGNED

FROM:

M.J. SHEARD

REGIONAL GEOLOGY

FLINDERS RANGES

ABORIGINAL HERITAGE CONSULTATIVE COMMITTEE

SUBJECT: PROPOSED SEISMIC LINE ON CALLABONNA 1:250 000

TO:

MAP SHEET

PROPOSAL:

33 km of single seismic line on 6838 Moolawatana, CALLABONNA.

CALLABONIN

LOCATION: Between gridpoints 6710.3732 and 6734.3938 passing west of but as close as possible to 'Lake Crossing Bore' and 'Mt

Hopeless Tank'.

ACCESS:

From Strzelecki track and Mt Hopeless Track, See attached

Plan.

OBJECTIVES:

 Nature of the Blance Lineament/Fault. This is a major feature trending NW-SE across CALLABONNA passing SW of Lakes Blanche and Callabonna. It forms the hypothetical boundary between the Warburton and Arowie Basins, and also a major faunal boundary. The proposed line will bisect this feature at ~ 90°

Basement topography, structure, depth.

Presence or absence of Cambrian (Warburton Basin limestones and shales)

Structure within the Mesozoic (ie faults)

Structural disturbance within the Tertiary - faulting, drag folding.

PROPOSED METHODS:

Surveyed line between grid points with pegs at 100 m intervals.

- Single line seismic using buried geoflex exploding cable (depth ~ 0.7 m)
- Cable burial by ploughing in with a D6 Bulldozer.
- Minimal line clearance, Bulldozer will maintain blade well above ground keeping surface disturbance to a minimum.
 Large trees will be gone around and creek disturbance avoided (in keeping with standard practice).
- · Sites of Aboriginal significance avoided.

RESOLUTION:

Geophone spacing 2.5m and recording as a 12 Fold Stack with a 96 geophone array.

TIMING:

VELSEIS of Brisbane ready to proceed 6/3/91 dependent on site

inspections.

DEPARTMENT OF ENVIRONMENT: No objections to proposal, advice on 27/2/91 in writing.

Phone (08) 274 7616

MJS:AM

APPENDIX 2

VELSEIS OPERATIONS REPORT, INCLUDING PROCESSING REPORT

OPERATIONS REPORT

CALLABONNA SEISMIC SURVEY

MOUNT HOPELESS / LAKE CALLABONNA DISTRICT

SOUTH AUSTRALIA

FOR

THE SOUTH AUSTRALIAN DEPARTMENT OF MINES AND ENERGY

MARCH, 1991



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1. INTRODUCTION

1.1 GENERAL

The REGIONAL GEOLOGY BRANCH of the South Australian Department of Mines and Energy, contracted Velseis Pty. Ltd. from Brisbane, to acquire and process data from a single seismic line in the Mount Hopeless/Lake Callabonna area of South Australia, in March, 1991.

The line was recorded using explosive cord. (ICI Redcord)

1.2 LOCATION/ACCESS

The line ran approximately north east, south west with the north eastern end starting just to the south of the Strzlecki Track, between Lake Blanche and Lake Callabonna. The line continued to the south west, past Lake Crossing Bore, Mount Hopeless Tank and passed about one kilometer to the south east of Mount Hopeless.

Access to the line (approximately 33 kilometers long) was gained from the Strzlecki Track and Mount Hopeless Track.

1.3 TERRAIN

There was little elevation change along the line with the exception of a gradual upward slope towards the SW end. Surface conditions varied from gibber type country with some low, weathered ridges, to sandy, salt bush flats.

1.4 WEATHER

The weather was generally fine, with light breezes. However, strong winds towards the end of the survey produced an unacceptable signal to noise ratio (charge sizes would have been increased had the cord plough not left the area) so it was decided to record at night, when the wind had died down.

1.5 LOGISTICS

The crew used a camp which was rented from Wreckair in Adelaide. The camp was established at a creek, about 0.5 kilometers off the Strzlecki Track (on the southern side) near the NE end of the line. The access track to the No. 2 compressor station, for the Gidgealpa/Adelaide Natural Gas Pipeline, was a further eight kilometers NE along the Strzlecki Track. SADME provided two caravans for their own use.

Fuel was collected in drums from Lyndhurst by the crew during mobilisation. One trip was made to Lyndhurst (approx. 180km from camp) to refill the fuel drums before the survey was completed and to purchase supplies.

Water was drawn from the bore at No.2 compressor station.

3. LINE CLEARING AND CORD PLOUGHING

Line Clearing and Cord Ploughing was contracted to Bundara Pastoral Company of Peterborough.

Minimal line clearing was required. The bulldozer was able to scrape salt bush off the line and carry out minor surface smoothing during the cord ploughing operation.

A device was fabricated and fitted to the bulldozer ripper unit to enable a Redcord reel to run freely and supply a continuous length of cord. When the bulldozer reached the shot point flag, the ripper was lifted and cord was capped according to ICI instructions, using only one detonator. The ripper was then lowered so that the primed section was planted to the greatest extent possible, without placing undue strain on the cord. At the beginning of the cord ploughing run, a knot was tied in the end of the cord in order to help prevent the cord from being pulled along the trench.

ICI Redcord was supplied by SADME from their stock. Detonators were purchased by SADME and supplied to Velseis. Cord cutting tools, bell wire, tape etc were supplied by Velseis Pty. Ltd. The ripper attachment for dispensing Redcord was fabricated in Brisbane by Velseis.

4. EQUIPMENT/PERSONNEL

4.1 SURVEY EQUIPMENT

- Nissan Patrol 4x4
- Sokkisha 3FR Semi Total Station
- Survey Chains, Stadia Rods, Compasses etc.
- Survey Pin Markers, Flagging, Star Pickets etc.

4.2 LINE CLEARING/CORD PLOUGHING EQUIPMENT

- Liebherr Bulldozer with Hydraulic Ripper (approximately equivalent to a Caterpillar D-6)
- Ripper Attachment for Redcord dispensing
- Low Loader
- Service Vehicle
- Caravan, Generator and Camp Equipment

4.3 RECORDING CREW VEHICLES

- Toyota Landcruiser 4x4 Recording Vehicle (Air/Cond.)
- 2 Toyota Landcruiser 4x4 Cable/Geophone Vehicles
- John Deere AMT600 All Terrain Vehicle with Trailer

5. RECORDING

5.1 ENERGY SOURCE

A charge of 50 metres of ICI Redcord, 10 grams/metre, (single length) capped with a single detonator in the centre and ploughed to an average depth of 0.5 metres, was used for each shot. Cord ploughing proceeded well ahead of the recording crew and the cord bulldozer was demobilised while recording was in progress.

A reduction in energy was experienced towards the SW end of the line. The signal to noise ratio was further affected by strong winds. The charge size could not be increased because the cord ploughing bulldozer was no longer available, so recording operations were rescheduled at night in order to escape the wind effects.

5.2 SPREAD GEOMETRY

Line Identification : Callabonna Line - 01

Line Direction/Progress : NE ----> SW

Live Geophone Stations : 2,656(NE) to 29(SW))

Shot Points : 2,657(NE) to 16(SW)

Spread Type : 96 trace, symmetrical split

Spread Layout : 662.5-75-0-75-662.5 metres

5.3 RECORDING PARAMETERS

Recording : 96 Trace, IFP, SEG-B Output

Sample Rate/Record Length: 2 milliseconds / 2 seconds

Record Filters : Low Cut - 25Hz, 12db/oct

High Cut - 187.5Hz, 72db/oct

Coverage : 600%

Shot Point Interval : 100 metres

Group Interval : 12.5 metres

Geophone Pattern : Six in line over 12.5 metres

Geophone Frequency : 30 Hertz

6.1 RECORDING SYSTEM cont....

- 8) Four auxiliary channels are available for recording ancillary information (such as confirmation time break and uphole signals).
- 9) Safety interlocks to avoid the recording of corrupted data.

6.2 PRINCIPAL SPECIFICATIONS

- Noise, approx. equal to 0.15uV at 42db fixed gain
- Fixed gain variable between channels, approx. equal to 0.2% (Low cut filters out)
- IFP Linearity 0.05%
- DC Offset 0.2uV
- Distortion < 0.1%</p>
- Dynamic Range > 80db
- Crosstalk > 80db

6.3 VELCOM - INTELLIGENT FIELD CAMERA

This system replaces the conventional camera used in standard seismic data acquisition systems and at the same time has the ability to field demultiplex the seismic data stream.

In principle, the SERCEL SN338 HR acquisition system operates in its designed configuration as far as the buffer output of the A/D converters. At this point in the data flow, Velseis has introduced the interface unit VELCOM, which channels data, data validation, data strobe and status monitor lines from the SERCEL into an IBM 80386 PC based computer system. Lines are also available from the unit to control the operation mode of the SERCEL and other peripherals. This enables full field diagnostic and instrument tests to be analaysed by VELCOM.

The VELCOM system provides a field monitor, data demultiplex on an IBM-PC based screen within five seconds of firing the shot.

Prior to the acquisition cycle, the operator interacts with the computer, via the keyboard, for information regarding spread parameters, ie. position of the shot and position of the geophones. Shot and geophone depths (if applicable) are also integrated onto the PC based seismic database during the recording process, for each individual trace. Line survey and elevation data are also integrated.

7. TIME TABLE OF EVENTS

Survey Crew

26 Feb 91 : On stand-by due to job delay

27/2 to 01/3: Mobilisation to Lake Eyre South

02/3 to 08/3: Working on WMC prospect

09/3 : Mobilise Lake Eyre to Mt. Hopeless

/Surveyor scouting with M. Sheard

10/3 to 16/3: Pegging, Scouting and Surveying

17/3 to 18/3: Demobilisation to Brisbane

19/3 : Survey Calcs in Brisbane office

Recording Crew

27/2 to 01/3: Mobilisation to Lake Eyre South

02/3 to 12/3: Working on WMC prospect

13/3 : Mobilise Lake Eyre South to Mt. Hopeless

14/3 : Bulldozer on site (demobed. 18/3?)

Experimental/Production recording

15/3 to 22/3: Production recording, breakdown, standby

for wind, recorded on night of 22/3.

23/3 to 24/3: Demobilisation via Noccundra to Brisbane

DATA PROCESSING cont....

BANDPASS FREQUENCY FILTER

Band-pass frequency filtering of a seismic trace involves the application of a zero-phase filter. This filter band limits the amplitude spectra without modifying the phase spectrum of the seismic trace.

For this seismic data set, a band-pass filter of 10/20 Hz Locut to 85/95 Hz Hi-cut was implemented.

This filter was applied prior to Deconvolution so to suppress ground roll and high frequency ambient noise that would otherwise contaminate the signal autocorrelation, hence improving the final result of Deconvolution.

DECONVOLUTION

Pre-stack predictive deconvolution is aimed at improving the temporal resolution by collapsing the effective source wavelet contained in the seismic trace to a spike.

By way of autocorrelation algorithms and trials, a predictive lag of 8 milliseconds has been applied to the seismic data.

BANDPASS FREQUENCY FILTER

A band-pass filter of 15/20 Hz Lo-cut to 80/90 Hz Hi-cut was applied after deconvolution so as to minimise the introduced high frequency energy.

AMPLITUDE EQUALIZATION

For this survey a post-deconvolution AGC used a time gate of 300 milliseconds.

VELOCITY ANALYSIS

Normal move-out (NMO) is the basis for determining velocities from seismic data. Computed velocities can in turn be used to correct for NMO so that reflections are aligned in the traces of a Common Depth Point gather before stacking.

Stacking velocities are picked directly from both Constant Velocity Gather (CVG) and Constant Velocity Stack (CVS) panels. The velocity chosen is that which exhibits ideal moveout correction and best stack response respectively.

Velocity Analyses were performed at approximately 450 metre intervals.

DATA PROCESSING cont....

COHERENCY FILTER

A coherency or median filter is applied as a post stack process so to reject anomalous values such as noise bursts.

The median filter is applied horizontally to an array of data seismic samples. These samples are then ordered from small to large values. The median of the series is then substituted for the pre-ordered centre value.

The effect of the median filter may be controlled by altering the horizontal size of the pre-ordered data sample array and also allowing a percentage mix of both pre-median and postmedian values.

For this seismic survey the number of horizontal data samples used for the median calculation were 9 traces and the percentage mix was set to 60% of pre-median and 40% of post-median values.

AMPLITUDE EQUALIZATION

For this survey a post stack AGC used a time gate of 400 milliseconds.

APPENDIX 1

LIST OF SEG-B FIELD TAPES

TAPE NO	0. 01	***************************************				911 240	(EXPERIMENTAL) (PRODUCTION)
TAPE NO	0. 02	******	FILES	241	то	291	-
TAPE NO	0. 03	••••••••	FILES	292	то	342	
TAPE NO	0. 04	•••••••••	FILES	343	TO	391	
TAPE NO	. 05	••••••	FILES	392	то	440	
TAPE NO	. 06	***********	FILES	441	то	490	
TAPE NO	07	***********	FILES	491	то	540	
TAPE NO	. 08	*********	FILES	541	то	589	
TAPE NO	. 09		FILES	590	то	637	
TAPE NO	. 10	•••••	FILES	638	TO	643	

APPENDIX 2

LIST OF PERMANENT MARKERS

LOCATION	EASTING	NORTHING	ELEVATION
Lake Crossing Bore (approx stn no 2416)	391 472.13	6731 155.43	11.35m
Station No. 1591	384 109.03	6723 938.22	24.70m
Station No. 1176	380 406.04	6720 305.93	31.32m
Station No. 963	378 409.12	6718 545.89	39.94m
Drill Hole 588/6 (Past end of line)	371 097.63	6712 016.14	91.40m

APPENDIX 3

SURVEY ORIGINS / LINE LOCATION

The following Trig. Stations were used for survey control:

 $\overline{T1/592}$ AMG Co-ordinates : Easting - 397 407.979

Northing - 6736 406.751

Geographical Co-ords: 29 29 51.2908 south lat.

139 56 29.8299 east long.

Elevation : 38.20m

T1/602 AMG Co-ordinates : Easting - 371 670.181

Northing - 6713 471.039

Geographical Co-ords: 29 42 07.7235 south lat.

139 40 24.4031 east long.

Elevation : 125.80m

Location and survey information for these Trig. Stations was provided by AUSLIG (Australian Surveying and Land Information Group). Both Trig. Stations were established by The South Australian Department of Lands in 1965.

CALLABONNA LINE - 01 LINE END CO-ORDINATES

STATION NO. 2656 - EASTING : 393 585.1

NORTHING: 6733 284.4

STATION NO. 016 - EASTING : 369 719.8

NORTHING: 6710 533.9

CALLABONNA LINE - 01 SUN SHOTS

Three Sun Shots were taken during the survey. One was taken along the traverse from Trig. Station No. T1/592 and two were taken on the line itself.

11 March, 1991 Sun Shot taken at C (between stations 1960

and 1840).

29 35 06 south lat. 139 50 00 east long.

15 March, 1991 Sun Shot taken at Station No. 744.

29 39 55 south lat.

139 44 00 east long.

16 March, 1991 Sun Shot taken approx. 520m SW along traverse

from T1/592 to NE end of line.

29 30 06 south lat. 139 56 22 east long.

HIGH RESOLUTION

SEISMIC REFLECTION SURVEYS

for

DEPARTMENT OF MINES AND ENERGY SOUTH AUSTRALIA

Lake Frome Callabonna area South Australia

Energy Source : Geoflex

SCHEDULE, TERMS AND OPERATING CONDITIONS

December 1990 - March 1991



1. PROVISION OF SERVICES AND SCOPE OF WORK

- A. In respect of the Department of Mines and Energy South Australia, hereinafter known as the Company, seismic program at Lake Frome/Callabonna area, the Contractor agrees to make available personnel and equipment to conduct high resolution seismic reflection survey using geoflex as an energy source under the terms and conditions herein defined and described.
- B. The contractor shall ensure that the equipment is maintained in a serviceable condition.
 All equipment shall remain at the Contractor's risk during transportation, storage and operation.
- C. Programmed lines will be located and surveyed by Company prior to recording. Contractor can provide this service at \$900.00 per day including mobilisation, demobilisation, line clearing supervision, levelling and permanent marker installation. Costs of pegs, tags, marker paint etc are deemed reimbursable expenses.
- D. At the completion of each surveyed area, Contractor shall provide the following;
 - (1) Magnetic tapes of the data recorded
 - (2) A complete and accurate observer's report covering the survey.
 - (3) Copies of field monitors if requested
 - (4) A brief technical report describing equipment and parameters used during survey, together with maps and sketches as required to support the observer's report.
- E. Program changes may be effected upon agreement between the representatives of the Company and Contractor.
- F. Daily, weekly and monthly checking of the equipment recommended by the manufacturers will be diligently carried out.
- G. Crew will work a six (6) day on, one (1) day off schedule. The seventh day is at no charge to the Company and is used for equipment maintenance. All rates apply to a ten (10) hour work day including travel to and from the site to crew accommodation.

2. EQUIPMENT TO BE PROVIDED BY CONTRACTOR

The Contractor shall provide the following equipment:

- One Toyota four wheel drive recording vehicle with mounted, air-conditioned recording cab and independent power system for battery charging and air-conditioning.
- Two toyota four wheel drive cable and geophone vehicles.
- One John Deere 5 wheel All Terrain cable/geophone vehicle.
- One seismic recorder, Sercel Model SN338HR, 96 channel with 2 millisecond sample rate, 187Hz alias filter
- One tape unit
- One VELCOM PC based field monitor and camera system
- One Rota-Long Switch
- 200 geophone arrays Sensor SM-7, 30Hz, 6 per array
- 20 seismic cables, 162 metres, 12 takeouts at 13.5 metres complete with extension cables
- Three radios incorporating shooting system
- All ancillary equipment, radios, jumper cables and necessary spare parts
- Magnetic tapes and recording paper

Any equipment requested by the Company which is not included in the above list and is provided by the Contractor shall be charged at cost plus 5% handling fee.

3. PERSONNEL TO BE PROVIDED BY CONTRACTOR

One Field Supervisor - as deemed necessary by Contractor One Party Manager/Observer One Line Supervisor One Licenced Shotfirer Five Line crew

4. COMPENSATION

Point of origin of Contractor's equipment and personnel shall be from Brisbane, Queensland.

Compensation to the Contractor for services, equipment and personnel to be provided under this agreement shall be as detailed hereunder and includes crew messing and accommodation.

A.(i) Mobilisation/demobilisation charge for Seismic Crew,

\$14,625.00

This charge applies for the establishment on site of the seismic reflection equipment listed above together with the seismic crew personnel.

(ii) Mobilisation/demobilisation charge for One Survey Crew,

\$900.00 per day

This charge applies for the mobilisation and demobilisation of one survey crew consisting of one Surveyor, one Rodman, one four wheel drive vehicle and Survey Instruments.

(iii) Mobilisation/demobilisation of Dozer,

\$2,200.00

This charge applies for the establishment on site of the Dozer (Liebherr type similar to a D6), Operator and includes modifications to a ripper to allow for burial of Geoflex cable.

B. Production Rate; Seismic recording, \$3,600.00 per day Surveying Crew, \$900.00 per day Dozing/Line Clearing, \$800.00 per day

Applies to those days spent on seismic data acquisition, surveying, surveyor on preparation of maps and computations and dozer line clearing.

C. Stand-by Rate

Seismic crew Survey crew \$2,900.00 per day \$540.00 per day

This rate applies to those days lost because of weather or other factors not under the control of the Contractor.

D. Down Time

No charge

Time lost because of equipment breakdown or other factors attributable to the Contractor.

E. Data Processing

Rate applies to computer time on VELSEIS processing system in Brisbane. Charges will be \$18.50 per record for 96 trace line recording at 1200% acquisition. A charge of \$175.00 per metre will be charged for each metre of film used in the production of final film transparency sections. Courier and facsimile charges are also deemed reimbursable expenses.

F. Consulting

\$65.00 per hour

Rate applies to consulting in field program design both in the office and on site during contract. Costs incurred, including airfares, rental vehicles, facsimiles etc, incurred in providing this service are reimbursable.

5. TO BE PROVIDED BY THE COMPANY

The Company shall provide or pay for a representative on site for the duration of the survey. Line clearing, explosives, detonators, bell wire and their shipment and storage are reimbursable expenses.

6. TAXES, LEVIES, ETC.

The Company shall be responsible for payment of all Government levies, duties and taxes relating to provision of the services and equipment herein except payroll tax and taxes on income.

7. METHOD OF PAYMENT

The Company will be invoiced at the end of the survey or at the end of each calendar month, dependent on which is applicable, and payment shall be made within thirty days of receipt of any invoice from the Contractor. Where reimbursement by the Company is "at cost" Contractor shall provide verification of such cost.

8. PERIOD OF AGREEMENT

Agreement shall commence as per attached schedule and continue in effect for a period sufficient for completion of the program, or upon a period of time agreed to by Company and Contractor.

9. FORCE MAJEURE

Neither the Company nor the Contractor shall be liable for failure of or delay in performance of any obligations that result from "force majeure", which term shall include acts of God, strikes, lockouts or other industrial disturbances, wars, blockades, insurrections, riots, landslides, lightning, earthquakes, storms, floods, fire, the elements, the order of any governmental authority having jurisdiction and any other cause, whether of the kind hereinmentioned or otherwise, not within the control of the party and which by exercise of due diligence such party was or is unable to avoid or overcome.

The Contractor will inform the Company by the fastest means possible and confirm by letter when a state of Force Majeure exists and similarly inform the Company when this state ceases to exist and operations can be resumed.

10. COMPLIANCE WITH LAWS AND REGULATIONS

The Contractor shall comply with all statutes, laws, by-laws, regulations and directions of any government, State or Federal or local authority or other entity having jurisdiction in relation to any aspect of the work.

11. INDEMNITIES

- A. Contractor hereby agrees with the Company to indemnify and hold harmless the Company against all liability arising directly or indirectly in connection with this Agreement, and or incidental to loss of or damage to property of, or injury to or death of employees of the Contractor or of its sub-contractors.
- B. The Company hereby agrees with Contractor to indemnify and hold harmless the Contractor and its sub-contractors against liability arising directly or indirectly in connection with this Agreement, for injury to or death of persons employed by the Company, regardless of cause or fault wholly or in part by or of any party so indemnified or held harmless.

12. INSURANCE

The Contractor shall at all times during the currency of this Agreement and at its own expense have in effect the following insurances:

- A. Employers' Liability Insurance in respect of claims by all persons employed by the Contractor in the work.
- B. Comprehensive General Liability in respect of injury to or death of personnel or destruction or damage of property \$5,000,000 any one accident/unlimited in all.
- C. Insurance against loss or damage to the survey equipment for its full insurable value \$425,000.
- D. Comprehensive insurance for automotive equipment subject to Legal Liability Limitation Clause \$5,000,000.

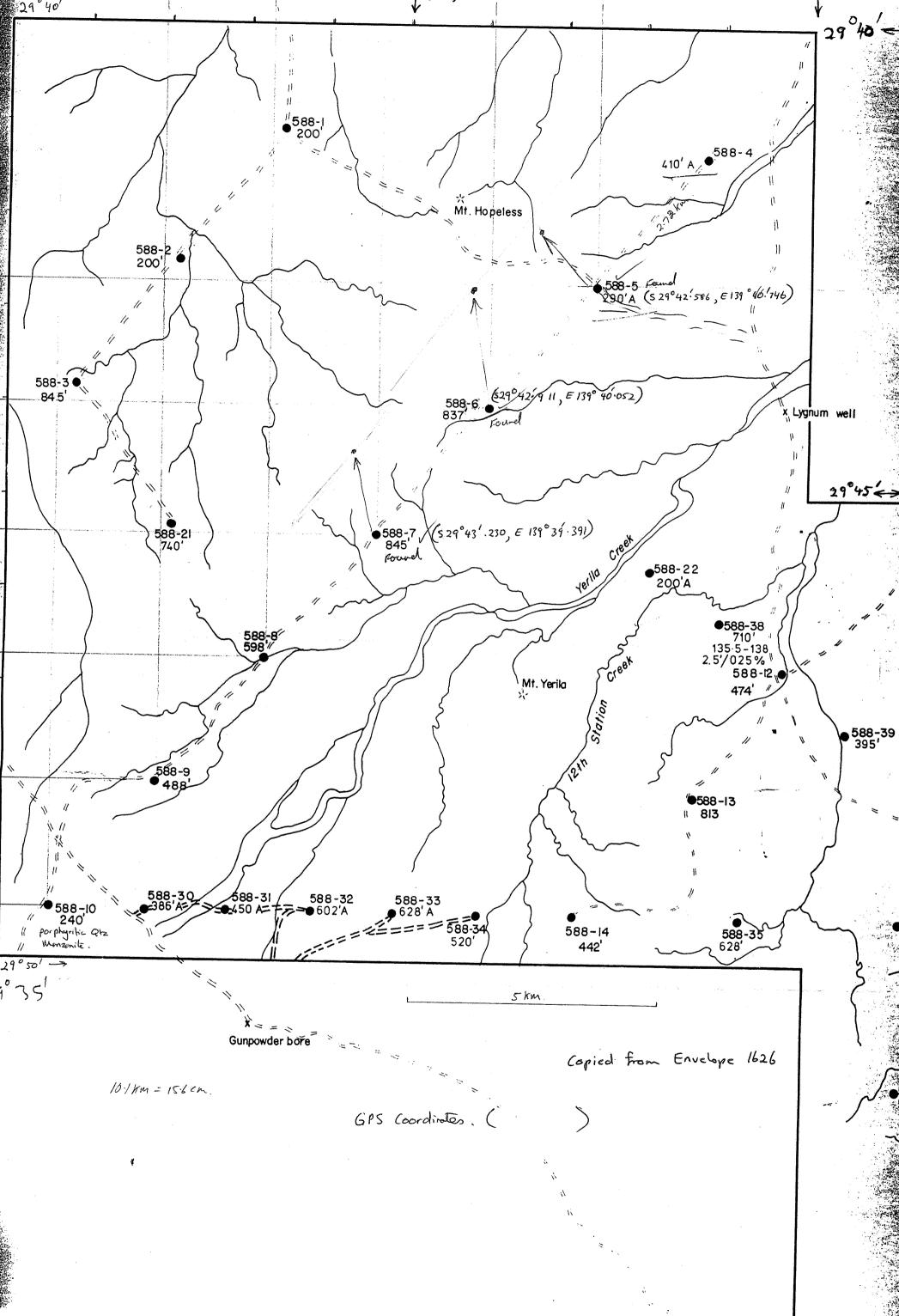
13. INDEPENDENT CONTRACTOR

Contractor shall be an independent contractor, maintaining complete control over Contractor's men and operations at all times.

14. PROFESSIONAL SECRECY

- A. The Contractor acknowledges that it is and that all its employees and sub-contractors are jointly and severally bound by obligations of professional secrecy and agrees that all records, survey books, maps and reports relative to the measurements, their results and their interpretation are and shall remain the exclusive property of the Company.
- B. The Contractor shall not nor shall any of its agents, servants, or employees, or agents, servants or employees of the Company's subcontractors, communicate to a third party nor publish in whole or in part, any such records, survey books, maps or reports, or any information relative to the survey without securing a previous authority in writing from the Company either during the term of the agreement or at any time thereafter.
- C. In a similar way, the Company agrees not to divulge to any person what it may or could learn about the Contractor's own techniques, and to take all necessary precautions to prevent any of its servants, agents or employees from disclosing such information to anyone.

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PROCEDURES TO FOLLOW FOR EXPLOSIVE SOURCED SEISMIC LINE WORK.
Buried defonating cord (red-cord, ICI) source

PRE LINE WORK MUSTS

- 1. Notify Land Holder in writing of proposal so that problems with stock, crops, fences, pipelines, dams, roads etc. can be avoided.
- 2. Notify Environment Department if line likely to cross-or approach Reserves, Parks or sen live areas
- 3. Notify Aboriginal Heritage Branch of D.E.P. for checking by them de traditional owners for sacred sites, burial sites, camps, tool workshops, correborer sites etc. Most of there can usually be avoided by the line.
- 4. Ask Drafting (Bill Mitchell) to go over proposed route using air photos and prepare a strip terrain/vegetation map a hazard zeones(ie: escarpments, main drainage lines, etc), B/W photo enlargements ~1'20,000 useful.
- 5. Check out explosives/blasters permits required, weight limits for explosive trucks a drivers required. ->60 kg powder equivalent 2 drivers needed, >265 kg powder equivalent means vehicle cannot be left unattended or stationing within a builtup area. Uehicle permits to carry explosives (inc. dets) required.
- 6. Check with Depot on availability of drivers, trucks, mogazines, permits etc in addition to rormal year requirements.
- 7. Chase up water availability for camp, drilling etc.
- 8. Find out what special requirements that the Bulldezer may need, and give Dozer Manuel to operator (SANTOS)
- 9. Check with the DME Magazines @ Greenhill Quarries re detrete. already in house.

LINE WORK

- 1. Follow SANTOS/DELHI procedures for line clearing 2 books on Vegetation recognition + arid area procedures,
- 2. Check on all road, fence dam pipeline etc crossed by time and
 their locations with respect to stat points. Some may have to be missed
 or moved to avoid conflict.
- 3. Correct handling of explosives wood aluminium or copper tools NO steel permitted due to sporks. Copper Knives @ Glenside in Science lox

4. When laying det cord watch out for errors in pin flog or peg markers especially around sites where shots have to be moved or dropped out. Errors in pin flog colour sequence can occur human error, see-below Det cord

Det cord

Lift up point

Start of Tonkic of cord end of Station point

blast cord a deforation point

ML Master Science of Cord of Cord of Station point Mt Hopeless Seismic Line Of configuration Station points 12.5 m aport or 8/100m Yields a 6 fold stack. Geophones 2.5 m apart Shot points 100 m contrepoint to contre point. Shet tengths som : , ted flogs every som . 5. Keep a daily Log of progress faults, down time, accidents etc a check against company daily operations sheets. 6. Keep an ege on shots as recorded - can usually view each one in he Dog Box just post firing. Ask for days run of print outs each day to see how reflectors are behaving & if time get a BRUTE Stock done. - A good run @ Mt Hopeless gove 7.2 km/ day line shot orecorded. 7. Allow 1/2 to 3/4 day for experimental work to be carried out - determines ground roll, air blast a other noise characteristics, ground coupling, charge size etc. 8. Obtain copies of Surveyors Mud Maps (made for linemen to avoid obstacles) to get station point locations to pipes; dams, socredistes, rds & fences, These maps are very useful for locating altered a missed shot points. 9. Drive the line at completion of shooting to make sure all unnecessary pickets, pegp, pinflogp, flogging etc are removed and any fences are repaired 10. Check that number tagged star pickets are in place at stort a finish of line, at each track crossing and at 5km intervals in between there.

Taken from Petrolium Act Regulations, 1989.

- (3) A wooden stake, spike, pin or other pointed object must not, in the performance of any geophysical or geological operation, be driven into the carriageway of a road or track.
 - (4) Where a seismic survey is to be carried out in the vicinity of a building or public utility, all reasonable steps must be taken to ensure that the operation does not cause any damage, or inconvenience any person.

Marking seismic lines

113. A permanent marker must be set in place at the intersections of survey lines, at the intersection of a survey line and a road that has been formed or graded, and at intervals on each survey line of not more than five kilometres.

Shot points near buildings and public utilities 114. (1) Unless otherwise approved by the Director, a shot point must

- not be located within-(a) in the case of a shot hole—100m;
- (b) in the case of a vibratory or other surface seismic source—20m, of a well, production facility, pipeline, monument, building or heritage item or site, or public utility.
 - (2) If a seismic line is to cross a pipeline-(a) reasonable notice of the proposed crossing must be given to the owner of the pipeline;
 - (b) the owner must be given a reasonable opportunity to inspect the site and to consider the implications of the proposed crossing; and T
 - (c) if appropriate, an earth ramp must be constructed over the pipeline before earth-moving equipment or heavy vehicles begin crossing the pipeline.

Shot hole temporary plug

115. Unless the Director otherwise approves, when a drilling crew is so far in advance of a firing crew that a shot hole will not be fired immediately after completion of the drilling, a temporary plug or cover must be placed in or over the shot hole until the firing crew is ready to fire the charge.

Permanent shot hole plugs

- 116. (1) Unless the Director otherwise approves, a shot hole must be suitably plugged with consolidated earth after firing, and the disturbed area restored, so far as is practicable, to its original state.
- (2) Any damage caused by the cave-in or collapse of a shot hole must be restored.

Uncontrolled flow of water

the flow.

- 117. (1) If a flow of artesian water is encountered during seismic drilling operations, or is detected at a subsequent time, it must be controlled.
- (2) The Director must be notified of the flow, and the steps taken to control it.
- (3) The Director may require that additional steps be taken to control





Detonating Cord

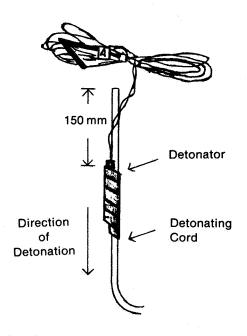
1 Guidelines for Use of Detonating Cords

- 1.1 Select a detonating cord that has the physical and performance characteristics, including explosive core load, consistent with correct blasting techniques and the type of explosives, primers being used.
- 1.2 Handle detonating cords with the same respect as is given to other explosive products.
- 1.3 Handle and use detonating cords with care to avoid damaging or severing the cord prior to firing.
- 1.4 Avoid loops, sharp kinks or angles that direct the cord back towards the oncoming line of detonation.
- 1.5 Detonating cords should always be cut with a sharp knife or an approved cutting tool. Pliers, shears, hand crimpers or similar tools should not be used.
- 1.6 When using detonating cords in wet conditions care should be taken to avoid moisture penetration in the ends of the detonating cord lines.

2. Initiation of Detonating Cords Detonating cords are initiated by an electric or

• Detonating cords are initiated by an electric or No. 8 plain detonator firmly attached with adhesive tape to the side of the cord at least 150 mm from the cut end. The detonator must point along the detonating cord towards the explosive charge and must be firmly fixed so that the base charge of the detonator is in close contact with the side of the detonating cord. The figure illustrates a method of making these connections. Half second or short delay detonators can be used to initiate detonating cords where the technique of delay firing with electric detonators is employed.

They should be attached firmly in the same manner as plain or electric detonators.

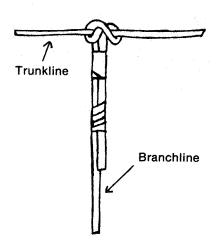


3 Connecting Detonating Cord Lines

 For connecting branch and downlines to trunklines, and connecting lengths of detonating cord, the following methods are recommended.

3.1 Clove Hitch

Connect the branchline or downline to the trunkline using a clove hitch. Pull tight and if desired, tape the end to the branchline to prevent the knot loosening, as illustrated.



MIC	
TO: Mike Crask	FAX: <u>07 393 5457</u>
TELEPHONE: <u>07 893 16</u> 02	
PROM: Jim Stood	PAX: 06 25/6806
TELEPHONE: <u>QG</u> 2525284	No. of PACES: 12 (including this page)
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Warning: Facsimilies on thermal paper can be highly unstable. If the accompanying documents contain authorisations or other important information they should be copied to good quality paper before filing or otherwise storing.

6839/ 1044

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UNCONFI

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Bascon : NONE

Access : 4 UD VEHICLE, 8 HOURS 0 MINUTES CLIMB ON TIME.

Summary : SA 1948 Hu: 44) : 0519: 000PER/245 All 000PER/245

Vert adj : SA LANDS, TRIGHT Photo : NONE

T 1 / 602

6838/ 1128

C Statue : 0 fi04953 Last update 9/85 Frinted 22/ 2/1

Type : TRIG/TRAV STN.

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0 3 VALUES : CLARKE.

ECCE TO MT HOPELESS

Other obs:

Rel info :

visited : 1965 Mark : BRONZE PLAGUE IN CONCRETE AT SURFACE

Beacon : ECCENTRIC CAIRN Access : 4 up VEHICLE, O HOURS O MINUTES CLIME ON TIME. Summery : SA 1965

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Photo Identification:

HAPTONAL LEVELLING ADJUSTMENT OF AUSTRALIA PROGRAM AMENDED 01/02/74 PREPARED FOR THE NATIONAL NAPPING COUNCIL BY C19P0190 28Z16Z76 THE DIVISION OF NATIONAL MAPPING GINEAR ADJUSTMENT RETWEEN PREVIOUSLY ADJUSTED JUNCTION POINTS ,62 A 40 SECTION 58- 62 THIRD DRUEK LEVELLING NUSTRALIAN HEIGHT DATUM 1971 SOUTH ABSTRALIA PRIMARY SECTION BENCHBARKS HEIGHT DIFFERENCES ADJUSTED CURR CAPITUDE GUNGITUDE LOCATION ADJUSTED HT DISTANCE OBSERVED DRINDHETRIC PROM PD IN METRES HETRES 8 A 139 49 PRIERRORRA 33.766 3055 -.0020 29 34 139 51 26,988 -6.7754 -6.7754 ·6.77H7 3456 4.3 3455 22.125 -. 0026 29 32 139 53 -4.8603 -4.8603 -4-11629 3.7 3456 3457 -. 0025 29 31 139 54 -9.9569 -9.9594 -9.9569 3457 3458 3.5 3,277 15,315 -. 0040 29 31 -B. 8843 139 57 3459. -B. H843 -0.0003 3451 -.0032 23 30 12.0414 12.0382 139 58 3460 4.5 17.0414 1459 -. 0033 29 27 139 58 5.600 -9.7121-9.7121 -9.7154 4.7 43460 3461 -. 0030 29 25 139 59 . .3622 4.2 . 3652 .3652 3461 3462 7.575 10.386 -.0028 29 72 139 59 1.6123 1462 1.6151 1.5151 3463 -.0019 29 20 139 59 2.8136 2.8136 2.0117 2.7 3463 3464 *1 66 PE00'-139 59 10.189 -. 1969 -.1935 -. 1935 3465 3464 -.0030 29 16 139 50 10.935 .7453 .7483 .7483 3465 3466 4.2 12.516 -. 0049 24 13 139 59 6.9 1_5862 1.5862 1.5813 3667 34466 -.0028 29 11 1.6687 140 00 14.185 1.6715 1.6715 3467 3468 4.1 -.0030 29 98 140 00 16.223 2.0412 2.0382 2.0412 HABE 3464 1.2 139 59 1.1324 -.0042 29 36 17.355 3470 1.1366 1.1366 3469 5.0 .5541 .5517 -.0024 29 95 139.59 17.407 .5541 16 ላይ 1471 -.0034 29 53 140 00 19.767 .8632 .4632 .8598 3472 4.8 3471 5172 -.0025 _29.01 140 01 19,284 5197 5197 1677 1471 4.2254 4.2254 4.2228 -.0026 29 09 140 03 23.507 3473 3474 3.7 19.074 20.461 -4.4327 -.0040 28 5R 140 04 -4.4287-0.4287 3475 3474 140 06 1.3471 -.0025 28 57 1.3896 1.3896 3476 3.5 3475 140 08 19,981 - 0030 28 56 - 4770 -4770 - 4800 3.476 3477 -.0034 28 54 140 08 23.478 3478 4.B 1.5000 3.5000 3.4966 3477 140 09 19.858 1 blan -3.6161 -3.6144 - 0026 23 52 2679 2470 140 10 1.8466 -.0032 28 50 21.705 3479 3480 4.5 1.8498 1.849# 110 11 22.996 1.2910 -.0035 28 48 ... 1 2945 1 2945 3400 TAUL -. 0033 2B 46 140 12 4.7 2.5442 2.5942 2.5909 3481 3482 140 13 28,330 2.7466 2.7431 -. DD35 28 14... 3402 idili 2. 74ub 58-62

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37 38	·									-	و جوان در دولت مید و خوش و دولت و دولت در این است.	e y die mand appeale o to dat is professe en mandage de la company)3i
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48				······································					mm torr management	e ann han sa manataine à part ann ann a par qu	na manana a si manga samungi samahah sasi segara kanama kanah a pa		41
45	 -				·	· · · · · · · · · · · · · · · · · · ·	gampanatan e er % (anatanatah) erre	***************************************	·····		-	ويها معينتها ومقيدة مادوانية أو منيدة طبية فللمناط المداعية والمحاطية والمحاطية	41 45
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59												in the state of th	52
. 13 15						-company, a c. 10° 10° 1, 14° 60° 60°					Mandagher, film (180), a coloniar mengaputangan ang alimpi		⊹ ਸ਼ ਹ
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59 80		 		·					maamaan gagagaa san a	and a commonwhite of the	en e	62-69	52 5
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DATE: 11/5 9142 PIELD TRAVERSE Remarks Horiz Vert Slope Horiz Hgt of R.L. angle dist dist target Angle -1.67 T00.19 85 2,92 00 00 00 90 08 5 1.06 180000 29 5,50 11.94 1745 14 64 X 2136 10000 2.00 2128 8942 89 49 2120 200.0 .89 52 コリコ 300.0 Zois ous forw. maki Koo-سنا 89 52 5000 2096 89 Si 30 600-0 2088 +1.94 89 51 40 800.21 800 212 180 CG 45 FS 2012 270 08 200 00 0630 -275 BS 2BC 00 00 00 1.04 901150 174 59 50 269 48 15 16.49 × 2072 177 2064 8952 7.00 100.0 89 53 2056 2000 89 SE 320.0 2048 89 53 30 400.0 2040 89.55 ৫ প্ৰটই 2032 600.0 2024 89 55 30 JE0:0 2016 89 55 2.00 800.20 FS 2008 1795425 89 5500 800.20 35954 18 20 0500

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Horiz dist Hat of : Remarks R.L. Horiz Vert angle Slope target Angle RADIO MASI BS Ro. 00 00 00 180 00 05 1177 1:51 38.57 x Ti 592 GUDD RM 57 0240 TI 602 237 02 35 518.80 . 58.82 α 51 1535 90 30 10 237 1525 292950 BS T. 592 00 00 00 89 26 20 2 Ilo 3355 कि २० वहा 176 33.51 X:X 1484.75 1484.515 FS B 9,0120 179 36 25 359 36 15 263 53 35 +25.55 89 a ST BS of 1.04 00 00 00 येष्ठक ह 00 00 or RB 1.69 7.04 2.00 1220.55 1220.55 183 1305 9000 05 E 8 3 1300 200 10 1.01 BS Q0 00·00. 900140 JA 89 II 269: 58: 20 1-61 6.91 1-00 M4 1255 90 0855

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CI	ienti 54	ome .	AREA		LINE		
	******	PIELD TR	3	***************************************			
tation #	Horiz Angle	Vert angle	Slope dist	Horiz dist	Hgt of target	R.L.	Remarks
82 X 3	00 00 00	89 53.10	790-99		+1.60 1.00		
••••••	19 59 56	ॐ गंड		*			
TE.	•				1.67	4-57	(107)
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	32615						
Bs € .	00 00 00	90 13.45		•	-216 101		
· S .	1795950	264 44.35	a 1				
7 6			•		173	603	
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FS: Nov Hohas	2010010	89 57 35		366.96	2.00		
	39 cc 12	360225					
0 1					-0.04 1.67		
B2 4	600000	900100	•		Ma		
χA	180 00 00	369 50 20	 		173	6.04	
A 18							
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	*****	FIELD TRA	*****				
ation #	Horiz Angle	Vert angle	Slope dist	Horiz dist	Hgt of target	R.L.	Remarks
BS RD	KOO GO GU						MAST A PS 2
	निम 45						
26567					1.75	6.04	(182)
2656	ii4 47 30	39 16	55 96	55.96	2.06	,	E.O.L.
2655		४९ ४४	68.5		N., .		11.
2649		89 55	143.5				
2648		89 SC	156.0		i.		· · Windy
2640.		89.55	256:0				
2632		89 55 30	356.0		<u> </u>		
2628		59 55 3c	406.0		h		
2627		395c	418.5		ч,		
స్టాన్ .		395430	44-3-5	•	ъ .		
2624		89 56 30	456.0		4		
2616		895640	226.0		i.		
2613		89 55 20	593.5		in .		and the state of t
2611		89 35	618.5		h		
2610		8158	630.8		4		and a state of the
2608		8956	655.9		i,		d a
2600	<u> </u>	89.56	756.0		*1		
2592	1	8955.	356.0		4		
2584		895420	956.0				
2576		89 53	1056.0		η,		
2515		89 53 15	1068.7		'n		
2574	. •	89 53 45	1081 . 0		~		MIDDIE OF ROAD INTO CS 2
2573		895325	10:93.6				
25C8.		86.23 30	1156.0		L		
FS 2563	111 38 00			1218 -5/16	2.00.		

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	tei <u>(1/3/</u> ¢ Ienti <u>≤</u>		My Hoteles				
Station 0	Horiz Angle	Vert angle	Slope dist	Moriz dist	Hgt of target	R.L.	Remarks
B's A	00 00 G	90620	1218.53		-2.32 1.82		
:	में फड़ें राष्ट्रिक्	209 53 15		•			
x 2563	•		-		i-705	8.27	1.58
2560		89 29	34.5		2.00		
2552		89 Sö	137.5	•	h		11.
2544		89 50	Z37·5		97		
2541		89 50	275.0		'n	•	
25%		89 45	337:5				
2530		89 45 20	412.5		63.		
2529		59 4130	4250		is .		
2528		89 45	431.5	,	n .		
Z52S .		59.46	4750		6		TEACK BOTOMO 2525 - 2524
2524		89.49	487.5		n	-	
2520		89 53 30	537.5		200		
25,7		Sq 51 30	575.0		2.90		
2512		89 52 36	637.5		2.90		
2509		89 54 20	675.6 .	l.	2:00		and the second s
2504	•	895210	731.5		٠,		
FS 2487	179-49.35	8947 25	950-33	950-30	2.00		
	3594930						
						•	1.

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ation 6	Horiz Angle	Vert • angle	Slope dist	Horiz dist	Hgt of target	R.L.	Remarks
Bs 2563.	00 00 00	9e 1300	950.33		-3 62 1.58		
		269 46,50		•			
11th 24th	*	90 40	112.65		2.∞		. • W. 00x
2494		90 54	87.6		9		
2491		91 10	50.1		17.		п.
2483		9130	12.6		2.00		
2487					1715	11.60	(i·c1) :
2+86.		8957	12.3		2.00		
24-80		90 23	.81.3		ìo-		
2498		90 32	112:3.	•	'n	•	
2476		90.37	1318		۳.		
2472		9027	1873		,		_
246h		90 16	262.3		и		
2464		90 14	287:3		'n		
2463	•	90.14	299.8		h		
2+62		9013	323				TRACK MUNIC FRANCE 2462 Centres GATE 2000 SE: TREE
2461	·	90 12	324.8.	1	h		
2456	٠	90 09	357.2		V		2460 Ferra
2454		90 09	42.2		١.		2458 (Pireciae) RODO
2453		90.08.	4247		'n		
2452		.90 07	437.2		ţ,		
2448		900630	487.2		ίς·		
2440		90 05	587.2		1		
2432	. •	90043	687.1		l/s		
2424	i79 38 €	90 04 30	181.1		<u> </u>		
52415	17938 N	1	899.43	899.43	2.00		
		269 58 50		.3.	÷		•

CLIENTI SOOME AREAL LINE Mr HORLICS. FIELD TRAVERSE OBSERVATIONS Hgt of Remarks Horiz R.L. Horiz . Vert Slope angle · angle target dist dist -0.44 00 00 00 90 01.25 899.43 1-07 BS 2487 19 59 45 269 58 60 2.00 25.0 91.00 2417 12.11 11.52 12.13 0.64 00 13.5c 93 5000 essin, B 1.62 1719 11-18 T2415 2.00 917 bursed while ねら 2414 91 05 250 2413 2409 90 20 75:0 31.5 2408 89 S8 100.0. 2000 2401 125.0 90 01 2405 undergrand 0.021 9002 2403 Pupe to 2.781 L 90 of 2400 b) 90 03 287.5 2392 Po 06 30 387.6 2384 2397 487.5 2376 900130 180,00 50 90 04 30 SIS 2368 -062 Fs B 675 575 675.58 2.00 180 28 05 90 0300 29 56 45 که کلا ده 2400 : 1.62 BS 2415 00 00 00 89 57 45 到0 01 30 180005 (1.55) 10-50 N B. 1.18 2.00 2360 156 26. 89 22 13.1 . 62.1 2356 8947 87-6 90:02 2354 2352 89 57 112:2 2350 1311.2 90 01 -:23:+9 -...-1497 Te 60. 23年 +147 90 oi Bario 212 17 2344 176 5S 90 00 2339 90 OC 2747 80 22 287.2 2338 1785210 895505

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tation #	Horiz Angle	tert angle	Slope dist	Moriz dist	Hgt of target	R.L.	Remarks
B= B :	0000	90 05 60	ร์แว่ร '		-0.87 1.55		
		269 53 55		•			
2836		9004	200.0		2.00		
2333	•	9007	1625		h		
2330		9007	250		2:00		п.
⊼ 2320					172	11-10	(i·io)
2312		89 34	100-0		2: vc		
<i>23</i> 04.		89.42	200.4	·	V		
2296		89 47	300.05				CRAVEL RAIN
2288		89 49 30	400.0		i,	<u> </u>	
F5 -2280	1810435	895135	500.07	5ळ.न	2.00		
•	1.04 35		-)	·	·		And the second s
B 2320	00 0e 0e	90 12 15			1.1C		
	iA 59 45	269 47 35					***************************************
×2280					1725	12-15	1.06
2272		89.5+	100.0		2.∞		CRADE. PLOID
2264		8956	200 0		l.		
2256		5952	300 0		j.,		
2248		80.22.	400.0		٨.		
2240		89.55	5000		0		<u> </u>
F52232	1794450	SF 55 30	600:23	6∞:23	2.00		
	389 44 40				,		
		<u> </u>				<u> </u>	
<u> </u>	1.		1	,i	·		

DATE: 11/3/91 42 764 76 · FIELD TRAVERSE Remarks . Hat of Horiz R.L. Horiz Blope target · Angle dist Angle dist. -1.40 00000 600 23 1.06 90 08 10 53 2280 180 00 15 769 SO 10 (1.05) . Buso 17:25 1277 X 2232 1000 2.00 89 43 1224 2216 89 49 2000 B9 53 3000 2208 89 53 337 S 2205 STAY TO WELTER 89 52 380.0 2204 SIDE OF LING h 89 50 373.0 2202 89 49 381.2. 2201 nas 1 2/14 laro 4000 89 50 2200 184 6 Sacco 42.5 89 49 力99 No Book 89 51 298 425.0 U64MGG 89 49 2.184 2197 Én 2202 02 PR 2196 4500 39 49 462.5 2195 2.00 Berso 89 52 05 FS 2192 184 48 05 499.98 499.99. के क ०५ 447 55 -1.78 1.05 BE 2232 00 01 00 90 12 18 269 47 40 180 01 00 171 13 78 1-0C x 2192 2.00 89 54 2184 100.0 2176 89 SG 2000 320.0 2168 89 57 2160 89.55 30 450.0 89 SC 2152 5000 89 56 2144 600.0. 100.185.700 19: 2:00

F5-2136 175 5020 89 55:00

355 50 20 270 0505

My HOPELESS TRAVERSE OBSERVATIONS Hat of Remarks Horiz Vert Slope dist target Angle Angle dist -193 $\alpha \propto \alpha$ 90 08.20 800 is i oi 72 PZ PAT 269 Si 45 GRAVEL 17.59 173 7 200B Ria, 2 100-0 2.00 89.27 2000 1992 89 30 90.0 89 48 3w.0 1984 89 52 1976 400.0 1968 8952 50000 89 SI SS 599.99 F5 1960 599.99 1795305 260815 359 5300 2-00 B<u>& 2008.</u> 90 06 10 ∞ ∞.∞ 25 62 82 74 59 Sc (80.1) 1950 Eno OF × 1960 18.87 1.70 GRAVEL PLAND $2 \cdot \alpha$ 1952 89 50 0.001 1125 1951 89 53 GO OG' 137-5 949 1948 90 18 So e 1945 90 20 187.5 9023 Jes c 1944 · 90 18 225°C 1942 1'57 1939 90 IT 2025 1939 1935 1936 90 13 300.0 1934 325.0. 90 13 30 400.0 1928 9009 1927 90 09 50 412-5 4250 1926 90 11 90 06 · 4715-0 1922. 1921. 80 of 2-875 1920 500.0 90 ot 1912 40530 CO 0 1905 900530 687.5 90 0430 180 08 0.007 1904 -0.67 785905 2003 10 726.865 758.860 2.00 5 C

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tation 6	Horiz Angle	Vert Angle	Slope dist	Horiz dist	Hgt of target	R.L.	Remarks
&s.	1		Solas Hot	@ · C∴			
	.).			•			
•	•	•	•		•	-	
Bs 1960	00 00 00					•	
	228.4350	75 48 10	14 11 50				1724 ".
	228 39 Sc	75 55 05	14 0455				
	228370	T5 59 30	14 00 30				
	228 34 W	7604 40	13 55 20				-9.5
	48535	28404 16	· 14 04 18		•		
•	48 56 35	283 58 40	13 58 40				
•	48 47 40	283 5335	13 5 35				
•	4.8 44 25	283 की 55	4	•	•		1727
FS 1960	180 00 00						
	228 4355	• .	13 59 36				
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		PIELD TRA	***************				
itation 6	Horiz Angle	Vert angle	Slope dist	Horiz dist	Hgt of target	R.L.	Remarks
BS 1960.	00000	જિ ડવ _ા ડ	726.865		1.08		
	Bo oo oo	270 00 50		•			
K C			•		172	17.98	•
	•						
FS D	167 4400	900150	97.915	97-915	2:005		Also STE
	3474400	20 82 pse					
						•	
Bec.	00 00 00	894935		97.913	+0.29 1.7.2		1903 GART OF
•	180 cc cs	270 10 10					Tingce
T D			•	•	1774	17.66	(099) SHOWS BE ARKE
1899	341 54	89 43	69:7		2:00		CRECK 1400
1888	219 28	8 \$ 55	81-3	•			1891 Eno of Tinde
J886		89 52	104.6		h		
(882.		89 56	122.0		5 -5		Pulhos
· 1884		8952	139.0		L		
E781		89 51.30	29.0		i		
1864		895430	380.8 ·		L,		
1856		8955	480.4		4		
1848		89 52	580-2		<u> </u>		
Fs 1840	1970645	89.5040	680.09	€80 · 08	2.003		
	170648	De 09 10					
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tation 6	****	Vert	Slope dist	SERVATION Horis dist	Hgt of target	R.L.	Remarks
BS 1784	00 00 00	900450	70026		1-02		
× 1728	र्शेष्ट्र वृद्धि	29 ८६ ३०			1:75	jq.53	(1.09)
1720		89.29	100.0		2.00	•	
1712		SE PS	200-0		и,		11.
704		.8943	3000		A		
1696		8947	400·\$		<u>ل</u>		GRAVE Paris
1688		89:49	500-1				-
1680		8950	600.2		7°.		,2
后门2	180 00 40	895,05	700-24	70-24	2.00		
	∞ ∞ 32	260855					
				•	-2.57		
BS 1728	00 00 00	901240			-25T 1.09		
	1795950	384731					
X 1672					1772	21 28	(i 10) .
ibbir		89 45	1000		2.00		
1656		89 48	2ක ල .		4		
1448.		89 49	300.1		i.		
1640		8 949 .	400.2		١.		
1632	<u> </u>	89.49.	S20.2		h		
1624		89.4730	6.30.2		A +2.70	•	
FS 1616	1795840		700:31	Jeo: 31	2.00		
	35988 35	218 35					
		<u> </u>	· i				
·	1		:				
<u> </u>	<u> </u>						

CLIENTI SAORE . MT HORELESS. TRAVERSE OBSERVATIONS tation (: Remarks Horiz Vert · angle Slope. Hgt of Horiz R.L. Angle dist target - 3.13 0000 700-21 BS 1672 90 15.55 110 Pg 59 50. 269 44:20 (1.07) in 23-80 T 1616 1000 2.00 1608 8931 8945 2000 8947 2812 1593 ROD TO MY HOROLD TANK 89 49 3000 1892 mag Cidu RM 1591 179 55 15 89 46.55 312 535 3/2 53 2.00 24 70 1584 8947 400 6 Lr. 500.1. 89 52 30 h 1576 600.0 1568 895730 2.00 15:1560 700.07 1795730 895248 700.0] 3595720 2700730 2.00 383.26 892815 383.27 Jary 1040 In 31 35 64 1035 90 35 20 BS 1616 0000 1795950 DES 2420 (1:08) 1.72 27.07 T'X 90.0305 150 03 50 2.0074 FS BY 330 03 40 969 56 50 908.63 30g. 62 1.08 BS X 89 89 35 60 co co 1959 45. Il 00 35 26:15 1.785 1.10) x 4.

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EINE MY HOPELEST ... CLIENT! SAOME. FIELD TRAVERSE OBSERVATIONS Vert angle Slope Horiz dist Hgt of Remarks Horiz R.L. Angle target -2.65 BS 1616: 100 00 00 To .005 90 0955 1.07 119 59 45 294945 (1.08) 1.76 25.09 560 750 1554 9,16 200 (rect. 91 28 81-5 1553 4 91 49 1582 100.0 1545 9,47 i55i m-5 1530 1550 9147 125:0 CECEK 1549 9128 1375 90 59 1625 1547 90 53 1750 1546 h 187:5 1545 91 11 90 47 1544 200.0 153% 90 25 300.0 90 21 400.0 1528 1520 500.0 9014 90 0830 1512 600.0 1504 90 04 40 0.00 179946 90 03 40 1496 900.0 1488 90:0130 0.00 O h 2000 1480 1000.0 1472 89 59 45 1700:0 'n 89 58 55 1464 1200-0 2.0043 79 4445 89 58 45 F5 1456 1300.18 1300-18 39.4140 260100

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DATE: (2 3/9)

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	******	PIELD TRA	VERSE OB	SERVATION	3 *****	•	*************			
tation 0	Horiz Angle	Vert Angle	Blope dist	Horiz dist	Hgt of target	R.L.	Remarks	•		
BS 1560	O0 00 00	90 02.56	1300-18		-1.06					
:		26957 15		•						
X 145C	•		-	•	176	25.3]	1.08. · 00.1	PEHNC		
1448		89.46	100.0		200	·		•		
1440		89 47	200.0		ъ.			11.		
1432		89 43	30 0.0		٨.					
1424		89 42	400.0		۲,	-				
1416.		89 43	Socie		5			• •		
1408		89 44	600-2		h.			_/_		
1400		89 4530	700.2	•	ч		: <u> </u>			
1392		89 45 30	8062		in .		YRAG PA			
1384.		89 44 55	900.3		n ·		PN	<u>. </u>		
1376		89 4500	1000.3							
1368		89 4525	1100.3		.,					
1360		89 4600	1200.3		نی					
1352					2					
FS 1344	79 4350	89 47'5	1400.59.	1400 57	2. 00 5.21			/		
•	359-4350	2101250						/		
,										
BS 14-56	00 00 00	90 15 25	•		1.08					
	180 cm co	29,44.20						1		
7 1344					175	30 69	((05)			
13.3°C		89 45	wo e		2.00			-		
1328		89 50	200.0.		٤.					
1320		89.52	300.0		۲.			• ,		
1312		89:52	1400.0		h					
1304		89 53 40	5000:	؞	٠ <i>،</i>		• •			
1296		89 SS	600		h .		agramatica de la compania de la com La compania de la co			
1288		89 53 30 89 53 30	700.0		₩	•				
1280 151272	180 06 8	84 53 So	900·18	900.18	200	•				
1-1-1-	00 06 10	270 0605	•	•				•		

VELSEIS!

CLIENTI JAJME MT HOPELESS: Remarks Horiz Horiz Hgt of Vert Slope target Angle · Angle dist dist -2:36 00 00 00 900 B BS 1349 1.03 2010 of 22 PR PT 2695105 32.23 (110) 171 X 1272 200 9006 100:0 1264 90 28 1256 2000 300.0 90 17 1248 90 11 30 400.0 1240 500:0 90 08 45 1232 60.0 % ob 30 1224 903 45 O. 00 1216 50000 9002 15 1208 900.20 900.26 ودعا E 1200 2∞ 1794625 9002 50 35946 15 289 57 15 +10.17 60 00 00 89 57 30 BE 12712 200.45 180 00 05 (i e4-) 171 31.33 X 1200 200 1192 89.48 100.0 1184 89 56 200.0 ARKAGELA 31.32 MAIN ROATO 2.00 895C.45. 300-02 300 02 PM 1176 183 15 Sc 1175 3025 39 59 4000 1168 go of 6 500.0 1160 89 58 5 895730 600.0 1152 700.0 1144 8956 15 Zer 143 89 38 89 56 725 1142 895530 750 1140 1136 **ξ**9 5€. 100.0

h +196

1100.17 2.00

1123

1120

FS 1112 183 0410

30400

89 SS 45

89 53 50

2700605

Z9 SS

0.00P.

1000 0

81.0011

VELSEIS

C	ienti <u>SA</u> C	ME	MT	MT HORELGE			
tation 6	Horix Angle	Yert Angle	Slope dist	SERVATION Horiz dist	Hgt of target	R.L.	Remarks
85 1200 !	00000	90 08 40	1100 18		-2.60 1.04		
:	180 00 15	16 Si 55		•			
X 1112	44		-		172	38.13	((10)
1104		89 45°	ico o		2.06		•
1096		89 44	200.0		.9		Α,
1088		89 29	300.0		4		
1080		89 28	400.0		h		: Snave.
1072		89 28	5a:0_		h		Pun
1064		39 30 20	·600-0		ñ-,		
1056		8932	700.00		м.		
1048		89 33	·800 0				
joyo.		893215	900;0				_
1032		89 30 15	10000.0		•		
1024		892340	0-0011		h		
后1016	180 20 25	892105	1200.20	1200-13	£ 13.57 2.∞		
	ca 20 25	2763850				,	
•				•			
BS 1112	000000	90 40 SS			-14.24 10		
,	180.00.00	29 19 20				·	
T 1016			•		1.75	46.57	1.04
1008		.91.45	100.0		2.00		
1003		9,37	1625		u,*		
éwi		91.15	200.0		14		
996		9108	280.0.		h		
992		9109	3000		فر		
984.		9104	400-0		λ,		
976	1.	90 09	2600.		V1	لــنــا	

VELSEIS.

		AOME		Coi - Ann	∾ <u>Á</u> Line	J. M.	HOPELESS
CL	******		VERSE OB	•			MARCO CONTRACTOR
tation #	Horiz Angle	Vert Angle	Slope dist	Horiz dist	Hgt of target	R.L.	Remarks
972	/	90 41.	550 00 .		<u> </u>		
drs :		90313	6 00 0	·,	ι,		
M 963	180 44-25	90 33 10	662.30	6(2.27	200	39.94	ON FENEC .
960		90 28 45	7000		Ù.		
952		902030	800.0		ч.		11.
944		90 1220	୍ର ଫୁ		ls:		
936		90 06 50	1000.0		<u>ل</u>		
428 .		90 0130	inod io		· 10		
9De		8955 20	12000		h*.		
912		895140	1300.0	•	N		and the second s
904		894820	1460.0		и.		
F8:896 .	180 39 40	89 43 25	1500.13	1500-11	2:00		
	∞ 34 30	201655					
							SPANG
BS_1016	00 00 00	90.18.30			1.04		N ₇ th
•	73 9 59 55	269.41.20					Nags
₹ 896					1765	53.79	(1.06)
888 .		90 7	1000		2.00		
.880		90 06	200-0		41		ang ing ing ing ing ing ing ing ing ing i
872		39.55.	300 -0		١,		
864		89.50	4000		is,		1
827		89 41	487.5		, ,		
826		89 43 20	5 553 € €		200		
848		89 52 +5	600.0		2.90		
846		8953	6250		3.20		
840 ·		89:415	700-0		2.03		
<u>ডিপ্র</u> ১	1794710	89 36 20		799.98	2.00.		

VELSEIS!

VELSEIS

	TE: 15/3	NET -		100 AUABO		Mr	blaces
Station 6	Horiz Angle	Vert	Slope dist	SERVATION Horiz dist	Hgt of target	R.L.	Remarks
BS 896.	100 00 00	902600	799.98		1.06	:	
:	119 59 55	269 34-10					
T 832	, ,				i73_	59.10	(1.85) . •
824		9008	voc. c		20		
800		9020	No.0		t _j		11.
ଷାଧ		89 47	2000		и		
808		89 47	3000		ju .		
800.		89.49	400.0		h.		
792		89 45 36	500 O		h.		
784		89 42	6000		4		
776		59 42 20	7000		k .		
768 .		39 43 20	800.00		и .		
760		89 44	2000		Ŋ		
752		89 44 40	1000.0				
FS 744	179 48 55	89年15	1100-23	ij∞.22	200		
	359 48 50	•				,	
			•				A STATE OF THE STA
BS 832	00000	901350			1.8543		
	180,00,05	•					
× 744					175	63:29	1.06
736		89,46	00:00		2.00		1
728		90 13	2∞ €		on .		
7ાંજે		9025	325.0	· -	6		
717		9028	337.5	• • • • • • • • • • • • • • • • • • • •	h		
TIC:		90.28	350.0		lq.		
715 ·		90 23	3¢2.5		h		

4000

90 14

712

VE SEIS

C1	ient: Sa	orie ·	AREA	CALLABON	<u>Vá</u> Line	Mr H	06.65
	*****	FIELD TRA	VERSE OB	SERVATION	3 *****		******
Station 6	Horiz Angle	Vert Angle	Slope dist	Horiz dist	Hgt of target	R.L.	Remarks
Tout !	4	90 12.	5 ₀₀ 0		2:00	:	
To:	.3.	9e 12	5315	٠.	h		
696	•	90 18	60000		i		
694		9020	625.0		200		
i92		901820	650.0		2.90		GRAVE ".
(38)		901520	700.0		2.0		Ro
680		%0520	800.0		2400	•	Wiry
F3 672.	1795210	90 Oct 30	TO-00P	To:00P	2.00		- Sra
	359 5200	209 5530					
			•			·	:
55 744	00 00 20	89 58 ie	3		106.		
	180 00 20	270015c		•	•	_ : .	
x 672					175	61.99	(106)
42		89 49	[co: ⊕		200		
656		89 59	J& .@		b		
648		89 89	300-0		٧٦		
645		9006	337.5 .		h.		
Gift.	•	90 90	320.0		V.	•	
Gato		39 Si .	400.0		i.		
(32:		89.42	50.0				
624.		89 35 3°	Covio		λj		<i>j</i> ·
616		89 3i	700.0	•	^ *	,	
608		89 27 30	800.0		ħ		
5 600	150 0405	89 2740		900-16	2°00°	-	
	00 0400	26320				•	
			:				
				,			•
,	****		حدمه به پاکورسید	- 			

VESEIF

DATE: 15/3/91 CLIENT' SAGNE AREA, COLLABONING LINE MT HORLESS PIELD TRAVERSE OBSERVATIONS : Remarks . . tation # Horiz Horiz Hgt of R.L. Slope Angle angle dist dist target 000000 \$5672 ··· 90 34E 106 900.20 20 00 081 292515 1-755 70.30 T 600. (1.06) 100.0 592 9021 2.00 584 9017 JA 200.0 576 90 14 300.0 h TO 0P 548 400 · C 90 00 500:0 560 552 89 51 600.0 89 56 30 544 700.00 2+103 806.30 FS 536 18037 55 89 55 40 300 30 200430 0031 45 100 00 00 00 900730 BS 600 180 oc 15 295245 (i 06) 71.22 170 R 536 528 89 35 2.00 0 00) 520 89 48 .o. 52C 516 89 51 2500 bet ox 800 **SiS** . 89 22 2625 513 89,46 287.5 512 3000 5945 505 8945 2.188 504 89 49 450 6 496 89 45 30 500.0 6000 488 89 41 700.0 488 8936.20 472 89 33 8cb.2 8932.30 .900.21 900.18 200 F3 464 179 53 15

270 2730

38 53.12

VELSEIS

, DI	TE. 15/3/9						
CI	ient: S	aong.	AREA		LINE	MT H	offices
	****	PIELD TRA	VERSE OB	SERVATION	3 *****		
tation #	Horiz Angle	Vert • Angle	Blope dist	Horiz dist	Hgt of target	R.L.	Remarks
Bs 536	00 0030	90 29 SS	900-31		-7.79 1.06		
:	180 00 20	Jed 30, 25.		,			
X 464	•				1745	78 23	(i 06) •
456		89.32	100.0		2.00		
448		89 31	2000		ч.		11.
440		·89 37	3.00 ·e		Ù		
432		8929	400.0		ú		• • • • • • • • • • • • • • • • • • • •
424		89.19	260 €0.		ų ,		
FS 420	1793105	891310	549.88	549.835	3:00		
	359 31 05	2704656	•	•			
•		•					
85.464.	₹\$958	90 5015			-802 106		_
	119 59 40	259 10 00					
× 420					176	85-50	(101)
419		9157	12.5		2.00		
415		95.26	62.5		٧.		
414		9522	75.0		J		
41	•	94,35	112.5		·v		
406		93 31	175.1				
403		9256.	212.6		i,		
400		.92,44	250 i		u		/ .
394		92.23	325-1		bą ,		
393.		92 20	337.6	•	* i y		94.00GK 93-94 - 90-91
391		9209	362. C		h		
390		9202	3 15 j				
389 .	1	91:57	387.6		ls.		
388		92.00	400-1		h o		MAIN CR BY



PO Box 118 Darra Old Australia 4076

Telephone (07) 376 5544

Fax (07) 376 6939

CLIENT: SADME

AREA : CALLABONNA

LINE : Mr HOPELESS

	SURVEY ELEVATIONS								
Station	R.L.	Station	R.L.	Station	R.L.				
1480	24.7	1500		1520	22.8				
1481		1501		1521					
1482		1502		1522					
1483		1503		1523					
1484		1504	24.0	1524					
1485		1505		1525					
1486		1506		1526					
1487		1507		1527					
1488	24.5	1508		1528	22.4				
1489		1509		1529					
1490		1510		1530					
1491		1510		(531					
14 92		1512	23.4	1532					
14 93		15 13		1533					
1494		1514		1534					
1495		15 15		1535					
1496	24.1	1516		1536	227				
1497		1517		1537					
1498		15 18		1538					
1499		15 19		1539.					



AREA: CALLABONNA

LINE : MT HOPELESS

			<u> </u>		
Station	R.L.	Station	R.L.	Station	R.L.
1420		1440	25.9	1460	
1421		(441		1461	
1422		1442		1462	
14 23		14 43		14 63	
1424	27.2	1444		1464	25.3
1425	•	14 45		14 65	
1426		1446		1466	
1424		14 47		1467	
1428		1448	25.5	14 68	
1429		1449		1469	
1430		14 50		1470	
1431)	1451		1471	
1432	26.6	1452		14 72	25.0
14 33		14 53		14 73	
1434		14 54		1474	
14 35		14 55		1475	
1436		1456	25.4	1476	
14 37		1457		1477	
14 38		1458		1478	
1439		1459		14 79	



AREA : CALLABONNA

LINE : MT HOPGIESS

		SURVET ELE			
Station	R.L.	Station	R.L.	Station	R.L.
1360	30.2	1380		1400	28.7
1361		1381		1401	
1362		13 82		1402	
13 63		13 83		1403	
1364		1384	29.2	1404	
1365		1385		1405	
1366		1386		1406	
1367		1387		1407	
13 68	30.0	13 88		1408	28.0
1369		1389		1409	
1370		13 90	,	1410	
1371		1391		1411	
13 72		1392	28.6	1412	
13 73		13 93		1413.	
13 74		1394	- Andrews	1414	
13 75		1395		1415	
13 76	29.7	1396		1416	27.6
13 77		13 97		1417	
1378		1398		14 18	
13 79		1399		14 19	



AREA: CALLABONNA

LINE : MT HOPELESS

Station	R.L.	Station	R.L.	Station	R.L.
(3ec	·	1320	31.1	1340	
1301		1321		13 41	
1302		1322		1342	
1303		(323		1343	
1304	31.4	1324		1344	30.7
1305		13 25		13 45	
1306		(3.26		1346	
1307		13 27		1347	
1308		1328	31.0	13 48	
1309		1329		1349	
i310		1330	·	13 50	
1311		1331		13 <i>5 i</i>	
1312	31.4	(332		1352	
13 13		1333		13 53	
1314		1334		13 54	
13 15		13 35		1355	
1316		1336	30.9	13.56	
1317		1337		1357	
1318		1338		13 58	
13 19		13.39		1359	



AREA : CALLABONNA

LINE : MT HOPELESS

Station	R.L.	Station	R.L.	Station	R.L.
1240	30.6	1260		1280	32. (
1241		1261		1281	
1242		1262		1282	
1243		1263		1283	
1244		1264	31.8	1284	
1245		1265		1285	
1246		1266		1286	
1247		1267		1287	
1248	30.5	1268		1288	31.9
1249		1269		1289	
1250		1270		1290	
1251		1271	·	12 91	
1252		1272	32.2	12 92	
1253		1273		1293	
1254		12 74		1294	V.
1255		12 75		1295	
1256	36.3	1276		1296	31.4
1257	· ·	1277		1297	
1258		1278		1298	
1259		1279		1299	



CLIENT : SADME

AREA : CALLABONNA

LINE : MT HORLESS

		SURVEI ELLEV			
Station	R.L.	Station	R.L.	Station	R.L.
1180		1200	3i·3	1220	
1181		1201		1221	
1182		1202		1222	
1183		1203		1223	
1184	31.3	1204		1224	30.9
1185		1205		1225	
1186		1206		1226	
(187		1207		1227	
1188		1208	31.5	1228	
1189		1209		12 29	
1190		1210		1230	
1191		1211		12 31	
1192	31.4	1212		1232	30.7
1193		12,13		12 33	
1194		1214		12 34	
1195		1215		1235	
1196		1216	31.3	12.36	
1197		1217		12.37	
1198		12.18		1238	
1199		1219		1239	:
			-,	•	



CLIENT:

SAOME

AREA : CALLABONNA

LINE : MT HOPELESS

		SURVET ELEV	11110110		·
Station	R.L.	Station	R.L.	Station	R.L.
1120	32.6	1140	32.1	1160	31.3
1121		1141		1161	
1122		1142	31.9	(162	
1123		1143	31.5	1163	
1124		11 44	31.8	1164	
1125		1145		1165	
1126		1146		1166	
1,27		1147		1167	
1728	32:3	11 48		1168	31.0
1129		11.49		1169	
1130		1150		1170	
1131		1151		1171	
1132		1152	31.5	1172	×
11 33		11 53		11 73	
1134		11 54		1174	
1135		1155		1175	31.1
1136	32.1	1156		1176	31.3
1137		1157		1177	
1138		1158		11.78	
1139		1159		1179	



CLIENT :

SAOME

AREA : CALLABONNA

LINE : MY HOPELESS

		SURVEY ELEV	ALTONO		
Station	R.L.	Station	R.L.	Station	R.L.
1060		1080	36.6	1100	
1061		1081		1101	
1062		1082		1102	
1063		1083		1103	
1064	38.1	1084		1104	33.3
1065		1085		1105	
1066		1086		1106	
1067		1087		1107	
1068		1088	35.6	1108	
1019		1089		1109	,
1070		1090		1110	
				(111	
	37.5			1112	33.1
				1113	
				1114	
		1095		1115	
		1096	33.8	11.16	
		1		1117	
				1118	
				1119	
1071 1072 1073 1074 1075 1076 1077 1078	37.5	1091 1092 1093 1094	33.8	1111 1112 1113 1114 1115 1116 1117	33



CLIENT:

SAOHE

AREA: CALLABONNA

LINE : MT HOPELESS

SURVEY ELEVATIONS							
Station	R.L.	Station	R.L.	Station	R.L.		
1000	42.0	1020		1040	40.2		
1001		1021		1041			
1002		1022		1042			
1003	41.7	1023		1043			
1004		1024	44.6	1044			
1005		1025		1045			
1006		1026		1046			
i∞7		1027		1047			
1008	43.3	1028		1048	39.2		
1009		.1029		1049			
1010		1030		1050			
1011		1031		1051			
1012		10 32	41.6	1052	•		
1013		10 33		1053			
1014		1034		1054			
1015		10 35		1055			
1016	46.6	1036		1056	38.6		
1017		1037		1057			
1018		1038		1058			
1019		1039		1059			
	1				1		



CLIENT : SADME

AREA : CALLABONNA

LINE : M- HOPELESS

SURVEY ELEVATIONS								
Station	R.L.	Station	R.L.	Station	R.L.			
94°		960	40.5	980				
941		961		931				
942		962		982				
943		963		983				
944	43-1	964		984	38.9			
945		965		985				
946		966		986				
947		967		987				
948		968	39.8	୧୧୧				
949		969		959				
	- 	970		990				
950		971		991				
951	41.6	972	39.8	942	40.3			
952 953		973		993				
954		914		994				
955		975		995				
956		976	39.2	996	41.4			
957		971		997				
		978		998				
953		979		999				
959								



AREA : CALLABONNA

LINE : MT HOPELESS

SURVEY ELF-ATIONS					
R.L.	Station	R.L.	Station	R.L.	
53-2-	900		920	48·i	
	901		921		
			922		
			923		
		51.2	924		
, , , , , , , , , , , , , , , , , , , 			925		
· · · · · · · · · · · · · · · · · · ·		w.	926		
			927		
53.2			928	46.0	
			929		
			930		
			931		
		49.6	932		
	913		933		
			934		
			935		
53.8	916		936	44.4	
			937		
			938		
			939		
	8.L. 53.2. 53.2.	53.2 900 901 902 903 904 905 906 907 53.2 908 909 910 911 912 913 914 915	53.2. 900 901 902 903 904 51.2 905 906 907 53.2 908 909 909 910 911 912 49.6 913 914 915 53.8 916	53.2 900 920 901 921 902 922 903 923 904 51.2 924 905 925 907 927 908 928 909 929 910 930 911 931 912 49.6 932 913 933 914 935 935 538 916 937 918 938	



AREA : CALLABONDA

LINE : MT HOPELESS

SURVEY ELEVATIONS								
Station	R.L.	Station	R.L.	Station	R.L.			
830	58.0	840	57.5	<u> </u> ଟ୍ରେ				
821		541		361				
802		342		862				
823		£43		863				
824	58.6	844		864	54.7			
825		845		865				
876		846	537	866				
827		847		867				
828		848	53.9	<i>8</i> €8				
		849		569				
829		850		870				
830		851		871				
831	59.1	852		812	54.0			
832 833		853		813				
		854		874				
\$34. 835		855		\$15				
		856	56.0	876	•			
836		857	563	877				
837		858		878	,			
838		859		879				
839		7.60						

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CLIENT: SAOME AREA: LINE

ion s	Moriz Angle	Vert Angle	Slope dist	Horiz dist	Hgt of target	R.L.	Remarks
	1	91 49	412:5		2.00		
(c)		9,45	425.0	•	7		
+		91 35	·45e.0		h		
19		91 17	512.5		٩		
13		90 46	587-5		b .		11.
1		90 ga 30	612.5		N.		
8		90 46.30			is		
3		90 25 30	712:5		le .		
ر م		9011	800.0		lr.		
9		901145	887.5	•	h		
-Co		90 15 10	925.0		2000		
tit.		90715	-950.00		3.64		
3		90 17 00	962.5		3.90 ^	-	Lagy CK BLO
H		901310	987.5		3.64		
35		9006	i062-3		2.00		Rowy of clase.
34		90310	10/15·80	1074.80	}-		
316	180 43 15	89 51 50		1299.66	2.00		
•		河0835					
	•						
•				•	,		
	•						
•							
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VELSEIS

CI	ienti Sac	sme	AREAL	CALLASS.	<u> 기타</u> FINE	MT	Hopeiss
ation #	Horiz Angle	Yert	Slope dist	SERVATION Horiz dist	Hgt of target	R.L.	Remarks
s 420	\$ \$ \$ \$	90 1030		1299.4	-3.94 1-07		
:	130 00 05	269 49 40		•			
33 ₊		91.01	224.895	224.86	200	·	•
33.5		9101	205		ŀn	•	be official
32B		9.39	1500		'n		11.
319		90 48	37-5		2000		
3K				•	175	88:59	/1-165) :
314		9022	32 -9		200		
3:2		9155	·&·6		١.		
311		92 26	625.	•	Ъ.		
310		9138	78.0		ty .		
<i>3</i> 508 .		9132	100.0	•	h •		
306 ·		9039	125.0		١,		
304		9013	150.0		U.		
296		8937	2500		4,		(300 ASSO STE DSM E
294		89 49	275.0		lin.		1293. 296 cheest provide
291		89 42	312.5.	1	h		
290		89 43	352.0		N.		Str. pur cx Bcp "
<i>:</i> 288		89 33	350.0		1.		
287		8933.	3625		h		
283		.89 12	412.5		h		1.
s 282	180 18 45	891120	424.65	424.61	2.00		Bans - 00 Accor
	00 18 yo	26 48 35			,		TEACK.
				,			
		•	:				
							•

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VELSELE

CLIENTI SADME MT HOPELESS ... PIELD TRAVERSE OBSERVATIONS Hgt of target Remarks Vert angle Slope dist Horiz Horiz R.L. dist Angle -6.42 1.105 63 316: 100 00 00 424.65. 90 5200 TASA ST 08 80 PDC 9437 MA 282 2.00 584 85 T1602 278 333 8458 IS 98 33 20 भेड वर ठव 25.0 280 89 02 200 90 47 272 DS-0 M 9051 225.0 264 90 SO 2625 احالت 90 42 352.6 256 387-5 251 90 48 425 6 348 90 39 525-0 240 90 23 45 23.2 13∞ 40 624.83 624.805 901745 FS 232 353 oo 30 269 4215 35 282 93 00 30 581-65 586.835 00 00 00 2659 40 190 00 00 125.88 r' TRIG 125.20 170 Si Piris 2594625 TO 592 FI Pirc 100 12:45

VEISEIS

	TE: 15 3 4	1 28 3 2.3.4					
D).	ienti <u>sa</u>	orie		19.19.21.2	LINE		
	*****	FIELD TRA	VERSE OB		7	******	***********
ation \$	Horiz Angle	Vert Angle	Slope dist	Horiz dist	Hgt of target	R.L.	Remarks
s 282.	00 00 00	894135	624.82		+3.34 174		
	•	Je 18:20		•			
232	•				1.76	ع) ۹. وا	(ros) . •
200		9,19	75.6		2.00		Forc - DOWN SOME
224		90 55	iQe · c		Ь		и.
218		90 08	1750	:	N		
216		90 13	200.0	•	4		
212.		9034	250.0	,		 	
201		90.36	312.5		h.		
203		90 14	362 <i>5</i>		4	<u> </u>	
200		90 18	400.0		Ь.		
195 .		90 10	462.3		is :	<u> </u>	
191		89 49	512.5		N 100 100		
કે 188	1795710	89 44 30	549.66	549.66	2.00		
		A 15 30					
		• .					
BS 232	00 00 0s	90 18:20			1.08		
	1800005	269 41 45				<u> </u>	
۲٬188		•			172	23.22	1.05
184		90 25.	20.0		200		
3H 588 6	1785325		125-15	125.135	2.∞	91.06	OPENTAL 178
176		9050	0.081	,	ų '		
171		9040	212.5		'h		
164		90 53	3cc.		'n	· .	
160	1	90:49	0.0KE		~~		
156		90 Set	400.0		h		
150	1	90 37	475.0		h .:		
E 118:	.180 0130	902010	814.83	शंप है।	2.00		ا در
	,00010	269 40 03			-5-10	• •	

VELSEI5

- D)	78 15 3	MARIE .					
Cl	ienti <u>s</u>	PIELD TRA	VERSE OR	SERVATION	S AAAAA	PIT	loperest.
ation #	Horiz Angle	Vert Angle	Slope dist	Moriz dist	Hgt of target	R.L.	Remarks
35 188	00 0025	89 42.50	/ 4 43		1.02		
:	1800015	ये० ग्य		,			
149	•	90 30	387-4		2.00		•
146		90 36	3.20-6		И		
143		9053	312.5		V ₁ .		11.
136		9103	225.0		h		
132		9058	US:0		~		
130 .		9106	0.0Sj				
129		9120	ાકા-ડ		hr.		
128		9111	N20.	•	S		
121		9017	37:5		200		
c *118 .					1.75	27.48	(1.61)
9		89 49	25.0		2:00		
110		9,54	0.80		ij		
161		92 03	B7.5		h		
105		9201	162.5		l _i		
104		9209	1750.		И		
103	•	9,58	187.5		ц	·	
.96		9106.	2750		5		
95.		TO 56.	287.5		e _j		, , , , , , , , , , , , , , , , , , , ,
88 .		.90 38	375.0		J		<u> </u>
ଞ୍ଚ		90 35	400.0		(ı '		
79:		900630	487.5	•	'Vi		
, r T	186 18 10		52 13		2.00		
•	ळ.गुड़ा	269 5505	·			•	
			:				
				.3	÷		•

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VELSEIS

FIELD Horiz Vert Angle Slope dist Remarks Horiz Hgt of R.L. Angle target dist 1-61 00 00 00 B 118 ... 89 54,20 20 05 55 179 59 50 1.70 77 12.5 76 90 44 2-00 73 9416 50.0 Rossing 93 50 70 81.5 GRAVES 93 35 69 100.0 92.24 1625 64 63 92 12 175-0 G 9134 26 262.5 48 9006 362.5 en up 381.2, 240 45 9101 400.0 9055 40 462.5 32 90 49 5624 90.4710 662.4 24 ۸ 20 90 47 30 712-B Rivorbed 904845 19 7249 90 46 .18 737.4 90.4205 M9 43 20 EOL \$ 16 762.40 762.34 2.00



AREA : CALLABONISA

LINE : MT Holciess

Station	R.L.	Station	R.L.	Station	R.L.
2620		2640	62	2660	·
2621		2641		2661	
2622		264-2		2662	
2623		2643		2663	
2624	63	2644		2664	
2625	6.5	2645		2665	
2626		2646		2666	
2627	6.3	2647		2667	
2628	6.3	2648	6.0	24%	
5629		2649	6.0	2469	
2630		2650		290	
2631		2651	,	2671	
2632	6.3	2652		2672	
2633		2653		2673	
2634		2654		24	
2635		2655	5.8	2612	
5636		3656 Eo.	6.5	এ বে८	
2637	·	2657		2677	
2638		2658		2678	
2639		2659		2619	



AREA : CALLABONNA

LINE : MT. HOPELESS

		DOKANTANDAY			
Station	R.L.	Station	R.L.	Station	R.L.
2560	8.3	<u> 2</u> 580		. 2600	6.7
2561		<u> </u> 258 (2601	
2562		2582		2602	
2563	8.3	2573		2603	
2564		2584	7.5	2604	
2565		2585		2605	
2566		2584		2606	
2567		2587		2607	
2568	82	2588		2608	6.6
1569		2589		2609	
2570		2590		2610	6.2
2571		2591	,	2611	6.7
2572		2592	7.1	2612	
2573	8.0	5 263		2613	6.6
2574	7.9	2594		2614	
2575	8.0	2595		2615	
2576	8.1	1596		2616	6.3
ברפב	,	2597		2617	
2578		2598		2618	
2579		2599		2619.	



AREA : CALLA BODDA

LINE : MT HORELESS

	SOKARI ETIPAKITORO								
Station	R.L.	Station	R.L.	Station	R.L.				
2500		2520	9.0	2540					
2501		2521		254-1	88				
2502		2522		2542					
2503		2523		2543					
2504	9.8	2524-	9.6	2544	8.7				
2505		2525	9.9	2545					
2506		2526		2546					
2507		2527		2547					
2508		2528	9.9	2548					
2509	9.2	2529	10.3	2549					
2510		2530	9.7	2550					
2511		2 53 (<i>;</i>	2551					
2512	8.5	2532		2552	8.4				
253		2533		2553	•				
2514		2534		2554					
2515		2535		2555					
2516		2536	9.5	2556					
2517	8.5	2537		2557					
2518		2538		2558					
2519		2539		2559.					



AREA : CALLABONNA

LINE : Mr HOPELESS

SURVEY ELEVATIONS								
R.L.	Station	R.L.	Station	R.L.				
i0·5	2460		2480	107				
,	2461	10.2	2481					
	2462	10-1	2482					
	2463	10.1	2483					
	2464	10-2	2484					
	2465		2 485					
	2466	10-1	2486	11.3				
	2467		2487	11.6				
10.4	2468		2488	11.0				
	2469		2489					
	2470		2490					
	2471	<i>;</i>	2491	10.3				
10.4		9.8	2492					
10.3	2473		2493					
10.3	2474		2494	9.9				
•			2495					
10.3		9.93	2496	10-0				
				,				
	•	10.3	•					
	2479		2499					
	R.L. 10.5	R.L. Station io. 5 2460 2461 2462 2463 2464 2465 2466 2467 2469 2470 2471 io. 4 2472 io. 3 2474 2475 10. 3 2474 2476 2478	R.L. Station R.L. 10.5 2460 2461 10.2 2462 10.1 2463 10.1 2464 10.2 2465 2466 10.1 2467 10.4 2468 2469 2470 2471 10.4 2472 9.8 10.3 2474 2475 10.3 2476 9.8 2477 2478 10.3	R.L. Station R.L. Station 10.5 2460 2480 2461 10.2 2481 2462 10.1 2482 2463 10.1 2483 2464 10.2 2484 2465 2485 2466 10.1 2486 2467 2487 10.4 2468 2488 2469 2488 2470 2470 10.4 2472 9.8 2492 10.3 2474 2495 10.3 2476 9.8 2496 2477 2498				



AREA : CALLABONNA

LINE : MT HORLESS

Station	R.L.	Station	R.L.	Station	R.L.
2380		2000	8·0í	2420	·
2391		2001	,	2421	
2382		24.62	· · . · . · . · . · . · . · . · . ·	2422	
2382		2063	10.9	24 23	
21,84	10.9	2666		21,24	10-4
23 85		alos	10-9	2425	
2386		2006		2426	
2380		2.401	11.0	2427	
23 88		2408	11.0	2428	
23.89		24.09	10-5	2429	
2390		2410		2430	
2391		25 11		2431	
2397	10:7	26.12	· .	永4.32	10.4
2343		26 13	10-5	2433	
2394		24 14	10-7	2434	
2395		2415	11-2	24.35	
2396		2416 Appr	ov L.C. Boli	24.36	
2397		2417	10.5	2437	
2398		2418		2438	
23.99		24 19		2439	



AREA : CALLABONNA

LINE : Mr HORLESS

				<u>and the second control of the second contro</u>	
Station	R.L.	Station	R.L.	Station	R.L.
2320	11.1	,9240		2360	10.4
2221		2341		2361	1
じょっち		2547		2362	
22,23		2343		2363	
2224		125 W.A.	10.3	2266	
2325		2345		2365	
೩९३७		2346		23 66	
27.27		2341	10.2	2267	
23.28		2348		2368	10.3
2529		23,49	10.3	2369	
2330	10.6	2350	10.2	2370	
- 2331		d351	,	. 2371	
2232		23,52	10.4	2372 -	
2333	10.5	23.53	·	2373	
2234		2354	10.2	2374	
23 35		2355		2375	
2336	10.6	23.56	10.5	2.376	10.9
2337		2357		2377	
2338	107	2358		2378	
23.34	10.3	2359		2379	



AREA : CALLABONNA

LINE : MT HOPELESS

		Station	R.L.	Station	R.L.
2260		2280	12.2	~30c	
2261		27.21		2301	
2262		7187		2302	
2263		2283		2303	
2264 12.	1	2284		2204	11.9
2265		2285		23.05	
2266		2286		2306	
2267		2287		236)	
22 68		2288	12.1	.230%	
2269		22 89		2309	
2270		22 90	-	,0,3,10	• .
2271		23 91	,	. 2311	
2272 12.		2292		2312	11.6
2273		22 93		23 13	
2776		2294		23 14	
2275		2295		7312 ·	
2276		2296	12.0	2316	
2277	•	22 91		23 17	
2278		22 98		2318	
22.79		22 99		2319.	



AREA: CALLAGONNA

LINE : Mr HOPELESS

SURVEY, ELEVATIONS									
Station	R.L.	Station	R.L.	Station	R.L.				
2200	13:7	22,20		J2 lin	12.7				
2201	13.8	2221		<u> </u>					
2202	13.6	2222	·) <u>}</u> = 2					
2203		22 23		2 به لالم 1 به الالم					
ジガ C に	13.3	2224	13-∞	ر) بر تبرن					
2205	13.2	2225		7445					
2266		22 26		2266					
22 C7		2227		9467					
2268	13.1	77 28		22 48	12.6				
7209		22 29		2249					
4210		22.30		22.50					
22.11		22 31		2251					
2212		2232	12.8	2252					
22 13		-22 33		2253					
32 14		2284		2250	~				
2215		22/35		2255					
2216	13.1	2236		2256	12.6				
.22 m		2237		2257					
22 18		2238		2258					
22 19	÷	2239		2259.					



AREA : CALLABONDA

LINE : MT HOPELESS

Station	R.L.	Station	R.L.	Station	R.L.
2140		2160	14-1	2130	·
2141		2161		े 	
2142		2162		2: 32	
2143		2163		2 33	
2144	14.3	2164		2) 34	13-7
2145		2165		3:35	
2146		2166		3 86	
2147		2167		3187	
2148		2168	13.8	2188	
2149		21/2		2189	
2150		2170		2190	
2151		2171		. 2, 911	
2152	14.2	2172		2192	13-8
2153		2173		2193	
2154		2174		2194	
2155		2.75		21 95	14-1
2156		2176	13.7	2196	13.9
2157		2177		2197	14.0
2158		2178		2198	i3·7
2159		2179		2199	13.89



AREA : CALLABONNA

LINE : HT HOPELESS

		DORVER, ELECTR	r Control	<u> </u>	
Station	R.L.	Station	R.L.	Station	R.L.
2080		2100		2120	15.0
2081		2101		2121	
2082		2102		2122	
2083		2163		2123	
2084		2104	15.3	2124	
2085		2105		2125	
2086		2106		2126	
2087		2107		2127	
2088	15.9	2108		2128	4.9
2089		21.09		2129	
2090		2110		2130	
2091	·	2111	<i>;</i>	2131	
2692		2112	15.1	2132 .	
2093		2113		2133	
2694		2114		2134	
2095		2115		2135	
2096	15.6	2116		2136	14.6
2097		217		2137	
2098		Z118		1138	
2099		2119		2139	



AREA : CALLABONNA

LINE : MT HOPELESS

SURVET ELECANTIONS						
Station	R.L.	Station	R.L.	Station	R.L.	
2020	`•	2040	U·1	2060		
2021		2041		2061		
2022		204-2		2062		
2023	to exercise the second	2043		2063		
2024	17.1	2044	· · · · · · · · · · · · · · · · · · ·	2064	16.5	
2025		2045		2065		
2026		2046		2066		
2027		2047		2067		
2028		2048	167	2068		
2029		2049		2069		
2030		2050		2070		
2031		2051	,	. 2071		
2032	17.1	2052		2072	16-5	
2033		2053		2013		
2034		2054		2074		
2035		2055		2075		
2036		2056	16.7	2076		
2037		2057		2077		
2038		2058		2678		
2039		2059		2079		



AREA : CALLABONNA

LINE : Mr HOPELESS

				
R.L.	Station	R.L.	Station	R.L.
18.9	1980		2000	18-3
	1981		2001	
	1982		2002	
	1983		2003	
	1984	18.4	2004	
	1985		2005	
	1986		2006	
	1987		7,000	
18.5	1988		2∞8	П.6
	19.89		2009	
	1990		2010	
	1991		2011	
	1992	19.1	2012	
	1993		2013	
	1994		2014	
	1995		2015	
18.3	1996		2010	17.4
	1997			
•	1998		2018	
			2019	
	18.9	1980 1981 1982 1983 1984 1985 1986 1987 1988 1990 1991 1992 1993 1994 1995 1995 1996 1997 1998 1997 1998	18.9 1980 1981 1982 1983 1984 18.4 1985 1986 1987 1988 1990 1991 1992 19.1 1992 19.1 1995 1995 1996 1997 1998 1998 1997 1998	18.9 1980 2000 1981 2001 1982 2002 1983 2003 1984 18.4 204 1985 2005 1986 2006 1987 2007 18.5 1988 2008 1990 2010 1991 2012 1992 19.1 2012 1994 2014 1995 2015 18.3 1996 2016 1998 2018



AREA : CALLABONNA

LINE : MT HOPDESS

Station	R.L.	Station	R.L.	Station	R.L.
1900		1920	17.6	1940	
1901		1921	п.5	1941	
1902.		1922	17-8	1942	17.4
1903		1923		1943	·
1904	17.7	1924		1944	17.2.
1905	17.5	1925		1945	17.5
1906		1926	17.2	1946	
1907		1927	กร	1947	
1908		1928	17.5	1948	17.8
1909		1929		1949	18.3
1910		1930		1950	
1911		1931	,	1951	18.8
1912	17.7	1932		1952	18.9
1913		1933		1953	:
1914		1934	17.3	1954	
1915		1935		1955	
1916		1936	17.4	1956	
1917		1937		1957	
1918		1938		1958	•
1919		1939	17.3	1959	



CLIENT: SADME

AREA: CALLABONNA

LINE : MT HOPELESS

Station	R.L.	Station	R.L.	Station	R.L.
1840	19.3	1860		1880	·
1841		1861		1881	
1840,		1862		1882	
1843		1863		1883	
1844		1864	18.1	1884	17.7
1845		1865		1885	17.5
1846		1866		1886	17.6
1847		1867		1887	
1848	18.8	1868		1888	п.5
1849		1869		1889	
1850		1870		1890	·
1851		1871		1891	/
1852		1872		1892 .	
1823		1873	18.1	1893	
1854		1874		1894	
1855		1875		1895	
1856	18.1	1876		1896	
1857		1877		1897	
1858		1878		1898	
1859		1879		1899	7-7



AREA : CALLABONNA

LINE : MT HOPELESS

Station	R.L.	Station	R.L.	Station	R.L.
1780		1800	19-6	1820	
1781		1801		1821	
1782		1802		1822	
1783		1803		1823	
1784	19.5	1804		1824	19.7
1785		1805		1825	
1786		1806		1826	
1787		7081		7281	
1788		1808	19.6	1878	
1789		1809		1829	
1790		1810		1830	
1791		ଧଥା	,	, চিত্ৰ	
1792	19.6	1812		1832	19.4
1793		1813		1833	
1794		1814		1834	
1795		1815		1835	
1796		1816	19.5	1836	
1797		1817		1837	
1798		1818		1838	
1799		1819		1839	



AREA : CALLABONNA

LINE : MT HOPELESS

Station	R.L.	Station	R.L.	Station	R.L.
1720	20.2	1740		1760	19.8
1721		1741		1761	
1722		1742		1762	
1723		1743		1763	
1724		1744	19.6	1764	
1725		1745		1765	
1726		1746	•	1766	
1727		1747		1767	
1728	19.5	1748		1768	19.6
1729		1749		1769	
1730		1750		1770	
1731		1751	,	177(
1732		1752	20.0	1772	
1733		1753		1773	
1734		1754		1774	
1735		1755		1775	
1736	19.3	1756		1776	19.5
1737		1757		1777	
1738		1758		1778	
1739		1759		1779	



AREA : CALLAGONNA

LINE : Mr HORGESS

Station	R.L.	Station	R.L.	Station	R.L.
1660		1680	21-1	1700	
1661		1681		1701	
1662		1682		1702	
1663		ાવ્ક3		1703	
1664	21.4	1684		1704	20.8
1665		1685		1705	
1666		1686		1706	
1667		1687		1707	
1668		1688	20.9	1708	
1669		1689		1709	
1670		1690		1710	
1671		1691	,	1711	
1672	21.3	1692		1712	20.6
1673		1693		1713	
1674		1694		1714	
1675		1695		1715	
1676		1696	20.8	1716	
1677		1697		1717	
1678		1698		1718	
1679		1699		1719	



AREA: CALLABOUNA

LINE : Mr HORIESS

				<u> </u>	
Station	R.L.	Station	R.L.	Station	R.L.
1600	24.4	1620		1640	22.3
1601		1621		1641	
1602		1622	And the second control of the second control	1642	
1603		1623		1643	
1604		1624	23.3	1644	
1605		1625		1645	
1606		1626		1646	
1607		1627		1647	·
1608	24.4	1628		1648	22.0
1609		1629		1649	
1610		1630		1650	
1611		1631	,	1651	
1612		1632	22.7	1652	
1613		1633	, -, -, -, -, -, -, -, -, -, -, -, -, -,	1453	
1614		1634		1654	
1615		1635		1655	
1616	23.8	1636		1656	21.7
1617	•	1637		1657	
1618		1638		1628	
1619		1639		1659	



AREA : CALLABONDA

LINE : Mr Hopeless

Station	R.L.	Station	R.L.	Station	R.L.
1540		1560	25.1	1580	
1541		1561		1281	
1542		1562	<u></u>	1582	
1543		1563		1583	
1544	22.1	1564		1584	25.1
1545	21.0	1565		1585	
1546	22.2	1566		1586	
1547	22.1	1567		1587	
1548		1568	24.0	1588	
1549	21.3	1569		1589	
1550	21.0	1570		1590	
1551	21.4	1571		1591	24.7
1552	21.7	1572		1592	24.5
1553	22.6	1573		1593	24.6
1554	23.2	1574		1594	
1222		1575		1595	
1556		1576	24.6	1596	
1557		1577		1597	
1558		1578		1598	
1559		1579		1599	



CLIENT :

SAOME

AREA : CALLABONNA

LINE : Mr HOPELESS

		SURVEY ELEV	ATTONS		
Station	R.L.	Station	R.L.	Station	R.L.
760	63.2	780		Sco	60.1
761		781		801	
762		782		Sc2_	
763		793		803	
764		784	62.1	804	
765		785		805	
766		786		806	
767		787		807	
768	62.8	783		§0§	60.0
769		789		809	
		750		810	
770		791		311	
771		792	61.0	812	
773		793		813	
774		794		814	
775		795		812	
776	62.6	796		816	59.6
777		797		817	
		798		કાક .	
778		799		819	
779	1		 		



CLIENT: SADME

AREA : CALLABONNA

LINE : MT HOPELESS

		SURVET ELLEV			
S tation	R.L.	Station	R.L.	Station	R.L.
700		720		740	
701	61.2	721		741	
702		722		742	
7e3		723		74-3	
7c4	61.3	724		744	63.3
7cS		725		745	
706		726		746	
707		727		747	
708		728	62.3	748	
		729		749	
709		730	·	750	
710		731		751	
711	61.4	732		752	63.5
7.3	1 917	733		75:3	
714		734		754	
715	60.6	735		755	
716	60.2	736	63.5	756	•
	60.3	731		757	
7:7		738		758	
718	60.7	739		759	•
719		121			



client : Saom

AREA: CALLASONNA

LINE : MT HORELESS

Station	R.L.	Station	R.L.	Station	R.L.
640	62.8	660		(30	61.9
641		661		(8)	
642		662		682	
643		43		ধ্যে	
644	61.8	664	62-1	(34	
645	61.2	665		682	
646		CLL		686	
47		457		687	
648	61.8	668		683	60.0
649		669		୯୫୧	
650		670		690	
451		671		691	
652		672	62.0	692	58.8
653		6 13		693	
654		614		694	59.5
655		675		695	
656	64.8	616		696	60.0
657		677		697	,
628		678		698	
659		(ଗବ		699	



AREA: CALLABONNA

LINE : MT HOPELESS

Station	R.L.	Station	R.L.	Station	R.L.
5%		600	70.3	620	
581		601		621	
582		602		612	
583		603		623	
584	69.1	604		624	66.1
585		605		625	
586		606		626	
<i>5</i> 87		ରେ		627	:
588		608	69.4	628	
589		609		629	
590		610		630	·
591		611		631	
592	69.4	612		632	64.4
593	1	613		633	
594		614		634	
595		615		435	
596		616	67.7	(36	
597	·	લી		437	
598		618		638	
599		619		639	



AREA : CALLAGONOA

LINE : MT HOPELESS

, .	SURVEY ELEVATIONS					
Station	R.L.	Station	R.L.	Station	R.L.	
520	71.6	540		560	70-1	
521		541		561		
522		542		562		
523		543		543	,	
524		544	70.9	564		
525		545		545		
526		546		566		
527		54-7		567		
528	71.7	548		5୯୫	69.3	
529		549		<i>5</i> લ		
530		550		570		
531		551		571		
532		552	70.7	512		
533		553		573		
534		554		574		
535		<i>\$</i> 55		575		
536	71.2	556		576	L8.8	
537		557		577		
538		558		518		
539		559		. 519		



CLIENT :

SAOME

AREA: CALLABONNA

LINE : MT HOPELESS

i	SURVEY ELEVATIONS					
Station	R.L.	Station	R.L.	Station	R.L.	
460		480	75.8	500		
461		481		501		
462		482		502		
463		433		503		
464	78.2	484	·	504	72.2	
445		485		565	72:6	
466		486		506		
467		487		557		
468		488	74.3	568		
469		489		509		
470		490		510		
471		491		511		
472	77.3	492		512	72.2	
473		493		53	72.1	
474		494		514		
475		495		515	71.3	
476		496	73.1	516	71.6	
477		497		รก		
478		498		518		
47A		499		5:0		
			1			



CLIENT:

SAOME

AREA : CALLABONNA

LINE : Mr HOPGLESS

Station	R.L.	Station	R.L.	Station	R.L.
400	73.3	420	85-5	440	80·0
401		421		441	
402		422		442	
403	74.4	423		443	
404		424	84.0	444	
405		425		445	
406	74.5	426		446	
407		427		447	
408		428		448	79.7
409		429		449	
410		430		450	
411	76.3	431		451	
412		432	81.6	452	% /
413		433		453	
414	78.3	434		454	
415	79.3	435		455	
416		436		456	78.8
417		437		457	
418		438		458	
419	84.8	439		459	



AREA : CALLASONNA

LINE : MT HOPELESS

Station	R.L.	Station	R.L.	Station	R.L.
340		360		380	
341	79.9	361		381	
342		362		381	
343	78.7	343	801	383	
344	78.9	364		354	72.8
345		365		385	
346	81.3	366		386	72.3
347		367		387	72.2.
3 48		368	76.5	388	71:3
349	82.3	369		389	72.1
350		310		390	72.0
35i		371	78.1	391	71.7
352		372		392	
353		313	77.4	<i>3</i> 93	71.5
354		374		394	71.7
355		375		395	
356	82.8	376		396	
357		377		397	
35'8		378		398	
359		379	73.8	399	



AREA : CALLASONNA

LINE : MT HOPELESS

Station	R.L.	Station	R.L.	Station	R.L.
280	94.5	300		320	
281		301		32i	
282.	94.4	302		322.	
253	94.1	303		323	
284		304	87.8	324	
285		305		325	
236		306	86.9	326	
257	91.2	307		327	
288	91.1	308	85.7	328	84-0
2 ≤ 9		309		329	
290	90.0	310	86.2	330	
291	90.0	30	85.7	331	
292		312	86.7	332	
293		313		333	84.6
294	89.2	314	88.2	334	84.4
295		315		335	83.5
296	90.0	316	88.6	336	
297		317		337	
298		318		338	
299		319	87.8	339	



AREA : CALLABONNA

LINE : MT HOPELESS

Station	R.L.	Station	R.L.	Station	R.L.
220		240	90.5	260	
221		241		261	90.3
222		242		262	
223		243		263	
224	89-1	244		264	90.8
225		245		265	
226	89-0	246		266	
227		247		267	
228		248	89.3	268	
229		249		269	
230		250.		270	
231		25 i	88.7	271	
232	91.0	252		272	92.4
233		253		273	
234		254		274	
235		255		275	
236		256	90.2	276	
237		257		277	
238		258		278	
239		259		279	



AREA : CALLABOTONA

LINE : MT HOPELESS

Station	R.L.	Station	R.L.	Station	R.L.
160	88.0	180		200	88:7
161		181		201	
162		182		262	
163		183		203	89.3
164	88·3	184	92.6	204	
165		185		205	
166		186		206	
167		187		207	87.5
168	:	188	93.2	208	
169		୲୫ବ		209	
170		190		210	
171	90-5	191	92.4	211	
172		192	\	212	88.3
173		193		213	
174		194		214	
175		195	89.4	215	
176	90.8	196	· ·	216	90-0
177		197		217	
178	-	198		218	90-3
179		199		219	



SAME

AREA : CALLABONNA

LINE : MT HORELESS

SURVEY ELEVATIONS

Station	R.L.	Station	R.L.	Station	R.L.
ico		120		140	
101		121	87.5	141	
102		122		142	
103	81.3	123		143	82.9
104	81.2	124		144	
105	82.0	125	•	145	
106		126		146	84.1
107	82.8	127		14-7	
103		128	85.2	148	
109		129	84-5	149	81.5
110	84.4	130	84.9	150	87.8
111		13i		151	
112		132	84.8	152	
113		i33		153	
114-		134		154	
115		135		155	
116	87.8	136	83.6	156	86-7
117		137		157	
118	88.0	138		128	
119		139		159	

ELEVATIONS

77.8

76-5

76-9

71.5

20

19

18

16

LIENT: SAOME	ANEA: CALLA BONNA	Line:	Mr	HOPELESS
Stations	R.L.			
96	82.5			
95	83.1			
ଟିଖ	83.6			
86	83.7			
79	86.9			
77	87.0			
76	86.6			
73	83.0			
70	30 .9			
69	80.5			
64	79.9			
63	৪০.০			
56	79.5			
48	79.8			
46	80-0		•	
45	79.6			
40	79.3			
32	78.8			
24.	77.7			
•	• •			



SADME

AREA: CALLABONNA

LINE NO! MT HOPELESS

Station	Easting	Northing	R.L.
Ti \$592	397 407 - 979	673 6406.751	
., oʻ	397 019 45	6736 063 12	
β	395 914 52 .	6735 072 19	
K	394 961.77	6734 309 72	
.€	394 397 30	28.527 EEL9	
6	393 985·11	6733 397 33	
А	393 626.62	6733 321.70	
2543	392 764 29	6732 461.17	
2487	392 093 82	6731 788-01	
24-15	391 463 30	6731 146.87	
В	390 985 77	6730 669.19	

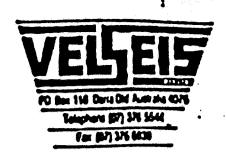


CLIENT: SADME

AREA: CALLABONNA

LINE NO! MT HOPELESS

Station	Easting	Northing	R.L.
.2320	390 631.26	6739 300.28	
., 22 80	390 278·14	6729 946.35	
2232	389 856.17 .	6729 519 67	
ज्य १२,	389 476·18	6729 194 89	
. :2136	388 978 58	6728 702 : 51	
2012	388 408.82	6728 140.88	
2008	387 839·98	6727 578 . 32	
1960	387 414 32	6727 155.66	
C	386 907.81	6726 634 . 57	3
D	386 856.05	6726 551 48	
1840	386 342 63	6726 105.71	



SAPME

AREA: CALLABONNA

LINE NO! MY HOTELESS

Station	Easting	Northing	R.L.
1784	385 840 25	6725 618 24	
"∏ 2 8	385 331·63	6725 130·88	
IE72	384-834-92	6724 643 64	
1616	384 332 34	6724 156.16	
·1560	383 830 28	6723 668-50	
1456	382 902.62	6722 757 91	
1344	381 907.94	6721 772·34	
1272	381 267.48	6721 140.05	
1200	380 629 47	6720 505 19	
1112	379 809 37	6719 772 19	
1016	378 910.05	6718 977.90	•



SAOME CLIENT:

AREA: CALLABOINDA

LINE NOW MY HOPELESS

station	Easting	Northing	R.L.
. 896	377 774 55	6717, 998 11	
	मध्य अनु		
.832	377 170-97	61n 413·38	
T44-	376 343·16 ·	6716 749.02	
612	375 467 32	6716 154 88	
·.600	374 990.87	6715 561·28	
536	374 383·69	6715 040 19	
464	373 701.95	6714 452.66	
420	373 288 63	6714 090.24	
316	372 300.95	6713 245 92	
282	371 976.78	G12 971.83	
TI 602	371 668.85	6713.471.23	

371 670.181 6713 471.039

SUNSHOT 11/3/91 @ C

LabS 29 35 06 Long 139 50 00

Mean obs V 13 59 36 -ref 3 53

Mean H 228 43 55

13 55 43

Mean Ro 00 00 00

UT of 085 756 11/3/91

Dec = S 3 52 32

 $\cos Az = \sin Dec - \sin V \sin Lab$ $\cos V \cos Lab$

 $= \frac{-0.0615 - (0.2401 \times -0.4937)}{0.9706 \times 0.8696} = \frac{0.0513}{0.8445} = 0.0608$

Az = 360 - 86 30 55

= 273 29 05 = 228 43 55

Az Ro = 44 45 10

conV = -3433

Geo Az = 44 10 37 C -> 1960

44 11 43

SAOME

SONSHOT 15/3/91 @ SP 744

lat S 29 39 43 long 139 44 15. CM 144°

Mean obs V = 29 57 53 141

Mean H 24 48 46

= 29 56 12

Mean Ro 00 00 32

Ur of 085 23 04 14/3/91

Dec = S 2 26 13

cos Az = sin Dec - sin V sin hab cos V cos Lab

 $= -0.0425 - (0.4990 \times -0.4949) = 0.2044$ 0.8666×0.8699 0.7530

Az = 74 14 47

H = 24 48 14

49 26 33 Az Ro

- 37 29 Conv

GRO AZ

SAOME.

SUNSHOT 16/3/91 @ d

Lat. S 29 30 06 Long. 139 56 22°5

Mean dos V = 265202- ref = - 154 = 265008

Mean H = 27 03 40

Mean Ro 00 00 00

OT of 085 22 49 (15/3/91)

Dec = S 20245

 $\cos Az$, $= \frac{\sin \Omega_{ec} - \sin V \sin Lab}{\cos V \cos lab}$

$$= \frac{-0.0357 - (0.4514 \times -0.4924)}{0.8921 \times 0.8703} = \frac{0.1866}{0.7764} = 0.2404$$

Az = 76 05 34

-H = -27 03 40.

Az Ro = 49 01 54

-and = -3120

GROAZ = 48 30 34



AREA : CALLAGOISINA

LINE : MT. HOPCLESS

Traverse Computations

Station	Horiz angle	Bearing	Adjusted Bearing	Horiz Dist
Ti/602				
		48 1741	48 17 41	
Ti / 592.	00 12 52			
		228 30 33	228 3032	518.80
٠ ح	T19 36 17			
		228 06 50	228 06 48	14-84 · 515
β	183 13 02			
		231 19 52	231 19 49	1220.55
8 .	174 12 52		and the second s	
		225 32 44	225 32 39	790,99
ϵ	: 183 26 20			
		228 59 04	<u> </u>	546.42
∠ ∠	209 06 17			
		258 05 24	258 65 14	366.46
A	146 58 22			
		225 03 43	225 03 35	1218 515
2563	179 49 35			_
		224 53 18	224 53 08	950-30
2487	179 38 10			
		224 31 28	224 31 17	899.43
24.15		1	1	

.34) 463.30 6131 146.87

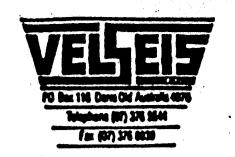


AREA : CALLABOANA

LINE : MT. HOPELESS

Traverse Computations

Station	Horiz angle	Bearing	Adjusted Bearing	Horiz Dist
2487				
	•	224 31 28	224 31 17	
2415	190 28 12			1
		224 59 40	224 59 28	675.58
В	178 52 05		5 31	511.75
		223 51 45	203 51 31	
2320	181 04 35	224 56 20	224 56 05	500·07
2280	179 44 52			
2250		224 41 12	224 40 56	600.23
2232	184 47 52			
		229 29 04	229 28 47	499.98
2192	175 49 20			
		225 18 24	225 18 06	700.19
2136	130 06 38			
•		225 25 02	225 24 42	800.51
2072	179 54 25			622.20
•		225 927	225 19 06	800.20
2008	179 53 05	200 12 22	2 225 12 10	599.99
		225 12.32	- 20 12 18	



AREA : CALLABOANA

LINE : MT HORLESS

Traverse Computations

Charles	Horiz angle	Bearing	Adjusted Bearing	Horiz Dist
Station	not 12 aug 16			
2008				
	•	225 12 32	225 12 10	
1960	178 59 05	•		
7 100		224 11 37	224 11 13	726.86
C	167 44 00	·		
	181 91	211 55 37	211 55 16	97.914
D	197 06.42		·	
		229 02 19	229 02 02	680 08
1840 5 6 6 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	£ 176 49 42			
1040:,2000		225 52 01	225 51 47	700.16
1784	180 0108			
110-1		215 53 B	225 52 59	700-26
1728	180 00 40			
1120	100 00 110	225 53 53	225 53 42	700-24
1672	Π9 58 42			
1612	111 30 72	225 52 35	225 52 28	700-31
1/-1/	179 57 30			*
1616		225 50 05	225 50 01	700.07
1560	179 41 50			
1300		225 32 00	225 31 55	1300.18
1456				(722757.91



AREA : CALLABOANA

LINE: MY HOPELESS

Traverse Computations

Station	Horiz angle	Bearing	Adjusted Bearing	Horiz Dist
1560		:		
		225 32 ∞	205 3155	
1456	179 43 50			
		225 15 50	225 IS 49	1400.57
1344	180 06 12			
		225 22 02	225 22 04	900·18
1272	179 46:22			
		225 08 24	225 08 30	900.26
1200	183 04 02	-	· · · · · · · · · · · · · · · · · · ·	
		228 12 26	228 12 35	11:0011
1112	180 20 17	1943		
		228 32 43	228 32 56	1200-13
1016	180 39 35			
•		229 12 18	229 12 36	1500-11
896	П9 47 12	2		
•		228 59 30	228 50 50	799.96
832	179 48 55			
		228 48 25	228 48 48	1100-22
744	179 52 02	18	. 39	
		228 40 27	228 40 50	900.07
672				

575 (67.30 Cm. 154.89



AREA: CALLABONNA

LINE : MT HORELESS

Traverse Computations

Station	Horiz angle	Bearing	Adjusted Bearing	Horiz Dist
744				
		228 40 18	228 40 So	
672	180 03 42		. 09	
		228 44 00	228 44 32	900.16
600	180 37 48		21 5	
		229 21 48	229 22 20	800·30
536	T19 53 68		4 41	
		229 14-56	229 15 28	900.18
464	179 30 40		45 17	
		228 45 36	228 46 08	549.835
420	180 43 27		8 28	
		229 29 03	229 29 35	1299.66
316	180 18 40		7 02-	
	F	229 47 43	229 48 15	424.61
282	Z18 33 28		20 30	
•		328 21 11	328 21 43	586.84
TRIG TI 602				

371.668-22

-85

6713 472 . 26



AREA : CALLABOINNA

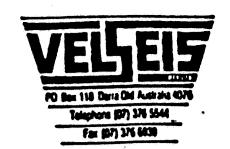
LINE : MT HORLESS

Traverse Computations

Station	Horiz angle	Bearing	Adjusted Bearing	Horiz Dist
316				
		229 47 02	229 47 02	
282,	173 00 38	•	•	
		222 41 40	222 47 32	624.805
232.	179 57 08	<u> </u>		
		222 44 48	222 44 35	549.66
188	180 01 18		·	
		202 46 06	222, 45, 46	814.81
118	180 17 42			50.12
		273 03 48	223 03 15	512 · 13
77	179 43 20		202 (6.06	762.34
		222 47 08	222 46 26	1100
16				
· •				

Co-oros AMG

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AREA: CALLABOUNA

LINE NO: MT HOPELESS

PERMANENT MARKER LIST

Station	Easting	Northing	R.L.
Bore Bore	391 472:13	6131 155 43	11.35
 Pm 1591	384 109:03	6123 938 · 22	24.70
PM 1176	380 406 04	6720 305 93	31.32
PM 963	378 409 12	6718 545 89	39.94
Ри ОН 588 6	371 097 63	6712 016-14	91.40
			~
		·	
		•	



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AREA: CALLABONNA

LINE NO MY HOPELESS

Station	Easting	Northing	R.L.
2656	393, 585 · 1	6733, 284 4	
.2563	392 764 .5	6732 461-1	
2487	392 094.1	6731 788.0	
:2415	391 463.6	6731 146.8	
2216	200 844 4	6130 511.3	
2344	390 844.4	1 100 311.3	
2320	390 631.6	6130 300.2	
			~
2280	390 278.5	6729 946.3	
2232	389 856 6	6729 519 7	
2200	389 55S·O	6729 257.0	
2192	389 476 6	67.29 · 194.8	



SADME

AREA: CALLAGONNA

LINE HO! MT HOPELESS

Station	Easting	Northing	R.L.
2136	398 979.0	6728, 702.5	
.,2512	388 409:3	6728 140.8	
2008	387 840.5 .	6727 578.3	
1960	387 414.8	6727 155-6	
: 1040			
1840	386 343 2	6726 105.6	
i784-	385 840·8	6725 618-2	
1728	365 336 3	6725 130.8	
1672	384-835·L	6724 643.6	
1616	384 333.0	6724 156.1	
1560	383 831.0	6723 668.4	
1456	382 903 4	6722: 757.8	•



SAOME

AREA: CALLABONNA

LINE NO! MY HOPELESS

Station	Easting	Northing	R.L.
.1344	381 908·8	6721, 772.2	
.1212	381 268.3	6721 1399	
1200	380 630.4 .	6720 505-1	
4.0	270 000	(7.0.27	
1112	379 810.3	6719 772.1	
·1016	378 911.0	6718 9778	
		6110 1118	
896	317 745.6	6117 998 0	
832	377 172.0	6717 473.2	
			`
744	376 344.3	6716 748.9	
<i></i>			
612	375 68.4	6716 154-6	
600	374 000 0	(7-5/1)	
4 00	374 992.0	6715 561.1	
536	374-384-9	6715 040.0	•



SAOME

AREA: CALLABOINDA

LINE HO! MT. HORELESS

Station	Easting	Northing	R.L.
.464	373 703·i	6714, 452.5	
. 420	313 289.9	6714 MO-1	
316	372 302 2 .	6713 245.7	
282_	371 978 . 1	6712971.6	
232	371 553 7	G12 513.2	
188	371 180.8	6712109.6	
1(8	370 586 9	6711 467.5	
77	370 231 4	6711 093 4	
16	369 719.8	6710 533.9	

SURVEY TYPE	eveción	AREA	PROSPECT	-=	
DAY/DATE 13.3.51 STN. INT. (m		1) 12,	5	CONTI	RACT # 160
PRODUCTION SUMMARY					
LINE	SHOT POINT/RAM SE START	EGMENT/G	EOPHONE FINISH		TOTAL METRES
					
					
CREW					
				taki , in in Jung wayangan	
TIMES Start	Finish		<u></u>	Tota	al Hours
TIME CIMMARY			Çeleşleri, in az anınlını medine		
TIME SUMMARY TRAVEL to: from			 	T	WEATHER
PRODUCTION					
NAME OF THE OWNER O			Total		
STANDBY					
			Total		FIELD CONDITIONS
DOWNTIME					
			Total		
COMMENTS MARILY	SE LAW	EF	FYRE	So	57H-13
AL HOSEL	ECS				ωH-1°
				A Commence	againea de la Sala de Casa de C Casa de Casa d

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SURVEY TYPE		ang ayar da ayar gara - garar ar	ADEA/	PROSPECT		
C080	ex Ler	recoja	Ancayi	HOSFEUI	MT.	HOPELES
DAY/DATE 14-3.31 STN. INT. (n			n) Q-≤	`	CONT	RACT # 160
PRODUCTION SUM	MARY					
LINE		SHOT POINT/RAM S	SEGMENT/G	EOPHONE FINISH		TOTAL METRES
0 1	26	56	2	520		1677m
						
		andra desperan		· · · · · · · · · · · · · · · · · · ·	 	
Por		Petile,	Miek	. Jan		<u> </u>
TIMES Start	30am.	Finish 18	8.00.	pm.	Tot	tal Hours 10.5
TIME SUMMARY	*			,		
TRAVEL to: . 2	from:	-25		.5	-	WEATHER Time, Sight Beege
PRODUCTION	PRODUCTION 4.25			Total 45	25	ine, son one
STANDBY EX	2TKS		- (1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	5		·
				Total		FIELD CONDITIONS SANT ROSH
DOWNTIME		.45				FLATS
				Total		
COMMENTS C	muerce	d 000	erne	Jals	on	Easten
E2) of	Line,	CHANGE	りつ	10 2	SEZ	Skoess.
Doer	Commen	a bu	e la	dang.		Decarding
		0 - 1		$ \langle -\rangle \langle$	11	\sim - (V)

Client Representative M.J. Signed: Observer



CLIENT)37/1/C			·	PIV LTD
SURVEY TYPE	PADEX PEREGIO	AREA/	PROSPECT	TT. +	topeless
DAY/DATE 15.3	STN. INT. (m		5	CONTR	ACT # 160
PRODUCTION SUMM	IARY				
LINE	SHOT POINT/RAM SE Start	EGMENT/G	EOPHONE FINISH		TOTAL METRES
01	2520	\mathcal{Q}	1240		3500
		· · · · · · · · · · · · · · · · · · ·			
			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		
CREW	sear Jamia	D USS	ell Ar	192	Don.
TIMES Start 6.36 am Finish 16.30 pm Total Hours 1 opm					
TIME SUMMARY	17	·			
TRAVEL to: .5	from:		1	V	NEATHER SY OO
PRODUCTION	PRODUCTION S				true, Shill
STANDBY	ンに				
			Total		FIELD CONDITIONS SOLV ROOK into
DOWNTIME \.			1	<	spen Gibber
			Total		
COMMENTS	a Dahlans	<u> </u>	L dan	1 V	4
ENCODER	/DEDER	Mist	ned-	1/0	ioninally,
Qual	a to get i	1 05	pario	nal	J
Shul	down for re	pan),)		
W.T.H		#W			
Signed: Observer		Clier	it Representativ	ve///	1. J. Sheard
	\bigcirc				/

CLIENT SASME



CLIENT	72VIE		PTY LTD.
SURVEY TYPE	2012 DEVILECTION	AREA/PROSPECT	MTHOPKLESS
DAY/DATE A	. 3.91 STN. INT. (m	1 12.5	CONTRACT #
PRODUCTION SUMM	IARY		
LINE	SHOT POINT/RAM SI Start	EGMENT/GEOPHONE FINISH	TOTAL METRES
01	2240	19<0	2600
	2240	1137	- 3000 m
		<u></u>	
		·	
CDEW			O =0
CREW	Jame, Garad	, Ady	on, fossell
TIMES Start 7.	45am Finish 16	,.00	Total Hours 84
TIME SUMMARY			hargeable 6.0 hes.
TRAVEL to: .5	from:		WEATHER
PRODUCTION	5	Total	Free, Stall
STANDBY	Ní	ig and the similar in	
endergere, it is to be be an incommon and an animal an		Total	FIELD CONDITIONS
DOWNTIME	2.25	2.25	open gisher
	<u></u>	Total	
COMMENTS	Alla Carr	THE PL	ME CALS PRISBANE.
			. 🗘
			JANY Mishins
			JABRE TO HAKE
Dros	DER ENODER T	FIDE. (werest or 9. ppm)
Micke	Tomuy Comple litis Del	ved Som	when TODAY.
(145	lits Diel)		,
_			10/6

CLIENT SADME



SURVEY TYPE COLDEX	DENECTION	AREA/PROSPECT	PELESS	
DAY/DATE	3.31 STN. INT. (m		NTRACT # 160	
PRODUCTION SUMM	IARY			
LINE	SHOT POINT/RAM S Start	EGMENT/GEOPHONE FINISH	TOTAL METRES	
0\	1952	1712	3000m	
CREW	Jame Roser	J. Ady, D	on, Dissell Phil	
TIMES Start 7.	Dan Finish	7.30	Total Hours 10.5	
TIME SUMMARY		CHARC	EARLE 45 hrs.	
TRAVEL to: .) S PRODUCTION STANDBY	from: 4.75	Total	WEATHER The, Breeze	
DOWNTIME	NiL Li:5	Total (4, 5	FIELD CONDITIONS	
	ER FRONT FOR			
	ish wint In	the state of the s		
MISFIRED INTERMITATING ALL AFRERVERN, DORE COMPLETED LINE THIS AFRERVERN,				
Observer _		Client Representative		

SADME



SURVEY TYPE			AREA/PROSPECT HOPELESS			
DAY/DATE 18.3.31 STN. INT. (m)						
PRODUCTION SUMM	ARY	2000 D. (1000) 2000 D. (1000)				
LINE	SH Sta	DT POINT/RAM SEG RT	MENT/GEOPHONE FINISH	TOTAL METRES		
01	7710		1136	7250m		
CREW	Agni	· C.	ed, Ad	. Phil Dan		
D.	منهولا		, ///), 1/01, 1/01		
TIMES Start	60	Finish \	.30	Total Hours 10.5		
TIME SUMMARY						
PRODUCTION	- from:	.4	8-	WEATHER The Hot		
STANDBY	9.7		Total 9.	Fre, Hot Recery		
	Nu		Total	FIELD CONDITIONS		
DOWNTIME NO.			- OPEN CIBBER			
			Total			
COMMENTS N	s Per	shlens	Au T	AT.		
Himor	5 Nov	nowl c	of Ri	AT. ASTRE MISHRES.		
		energia de la propriazione de la p	o o o o o o o o o o o o o o o o o o o			

Signed: Observer _______

Client Representative M. A. Sheml



SURVEY TYPE	ROW PERROOM	AREA/PROSPECT	MTHOPRESS
DAY/DATE (" Q.5	CONTRACT # \60
PRODUCTION SUMM	IARY		
LINE		EGMENT/GEOPHONE	TOTAL METRES
	START	FINISH	MEINES
01	1136	656	6000m.
·			· , · , · , · , · , · , · , · , · , ·
		1.	
CREW	BILL	D0.0	
7,7	anie, Cesad,	they, m	as were dusters
	,		
TIMES Start	Finish C	J. 0D	Total Hours \\ \(\frac{1}{\infty} \cdot \)
TIME SUMMARY	water the state of		
TRAVEL to:	from: . S		WEATHER
PRODUCTION			Fre Gusky
, i nobovick	4	Total	- Lousin
STANDBY	Ni		Werenson
			<u> </u>
		Total	FIELD CONDITIONS Cyber Didges.
DOWNTIME	Ni		July alogu.
	ndy vije men a gang aljer je in var a na a na a ' je je je je sa na a gang a na a na gang a na a na gang a na a		
		Total	
COMMENTS	**		
COMMENTS	Johans L	Day	
Wind	Came on	stone	this afterior.
		3	7,
			Control of the Contro

Client Representative M. J. Sheard

CI	LIENT		\leq	B	M	\subseteq



SURVEY TYPE COLDEX	Dene	Serion.	AREA/PROSPECT	Mr. Hoperess
DAY/DATE 20.	હે.91	STN. INT. (m)	12.5	CONTRACT#
PRODUCTION SUMMA	RY			
LINE		SHOT POINT/RAM SE Tart	GMENT/GEOPHONE FINISH	TOTAL METRES
CREW	كوهم	, Asy	Phil,	janie, Don, Durol
TIMES Start	·	Finish		Total Hours \O -O
TIME SUMMARY				antini di mangantini di mantini d
PRODUCTION	from:		Total	Tre, Very Wis
STANDBY				
			Total	FIELD CONDITIONS
DOWNTIME	10	0,0	0	
			Total	
COMMENTS	nob	1, 45	H Wins	

Signed:

Observer .





CLIENI WAY ST	D1116		i i garan ka ang ang ang ang ang ang ang ang ang an	77117
SURVEY TYPE CORDER DE	herion	AREA/	PROSPECT M	THOPELESS
DAY/DATE 21.3.91	STN. INT. (m	1/12.	l co	NTRACT # 160
PRODUCTION SUMMARY				
LINE	SHOT POINT/RAM SE Start	EGMENT/G	EOPHONE FINISH	TOTAL METRES
01 65	56		352_	3800m
			Agentalia Barana da Agentalia da Agentalia Barana da Agentalia	
			mannen mannen annen annen erren serien anteres annen erren erren erren erren erren erren erren erren erren err	· · · · · · · · · · · · · · · · · · ·
CREW CREATER) Jame	٢, ٦	A Desc	ny In Dessel
TIMES Start & ODa	Finish (2,OC	Sp.	Total Hours ()
TIME SUMMARY				
TRAVEL to: 75 from:	.75	***************************************	1.5	WEATHER Wing Exect,
PRODUCTION	4.0		Total 4	Word Energy
STANDBY				
45			Total 4:5	FIELD CONDITIONS
DOWNTIME 2				open gisser
			Total	Slopes.
COMMENTS LEST L	junsy 1	5as	THIN	(This
Moesing.	QJ.ET	الاي) Dow	m howetherings
So ATTEMP	TED PRE	D7.	na.	
DROPDS Au	M CHAC	ARC	jmr J	DUE SUPRIT
LOW ENERGY	405/	s Q	Wins.	
Signed: Observer	2 '	Clier	nt Representative	M. J. Sheorel

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SURVEY TYPE CO			AREA/	PROSPECT	Mr.	Hopeless	
DEVILERON STN. INT. (m)							
PRODUCTION SUMMA	ARY						
LINE	SI ST/	IOT POINT/RAM SE RT	GMENT/G	EOPHONE FINISH		TOTAL METRES	
01	35%	2		16	· · · · · · · · · · · · · · · · · · ·	4200m	
			aragman nel cel cel cel c e				
CREW ,		<u> </u>				000	
Tim, do	aute ()	2,195	lan), /h.	الح (Do Lissell	
TIMES Start		Finish			Tot	al Hours 10 has PeoDuchan	
TIME SUMMARY				+ 101		TOGUATO	
TRAVEL to: 75	from:	•75		1.5	-	WEATHER Whiley, Jaytime	
PRODUCTION	9.25			Total			
STANDBY	00		· · · · · · · · · · · · · · · · · · ·	0		Shel as night	
10hrs.				Total	(FIELD CONDITIONS	
DOWNTIME • 7	5			<i>:</i> 75		des sietre	
BLASTER	Mighie	>		Total			
COMMENTS				. To train a chart a train a	 		
COMMENTS Vera	y Www	of ALL	JA1	· AR	fow.	DROW	
				•		SET OUT	
6.15		. 3		•	_	cian UP	
	E 3-1			22.3.9	•		
			,,.,				

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SURVEY TYPE		AREA/PROSPECT	AREA/PROSPECT			
DAY/DATE 22.3.51	STN. INT. (1	m)	CONTRACT #			
RODUCTION SUMMARY		· · · · · · · · · · · · · · · · · · ·				
LINE		SEGMENT/GEOPHONE	TOTAL METRES			
	START	FINISH				
	managan aga aga an aga an anga ta aga da aga da aga aga aga aga aga aga 					
	war and a state of the state of					
·	i, t		- The state of the			
			1			
CREW Jan James	Carad	7 l.l)	My Don Just			
TIMES Start	Finish	· · · · · · · · · · · · · · · · · · ·	Total Hours			
TIME SUMMARY						
TRAVEL to: from	anderson en		WEATHER			
PRODUCTION		Total				
STANDBY	and the second s	Total				
	a est any amin'ny desira desira desira des		FIFE D. COMPLETIONS			
		Total	FIELD CONDITIONS			
DOWNTIME						
enger som en	lationi suomati sa tee teeta suote	Total				
 		1.0.01				
COMMENTS PLANE	MY Car	THO DIS 131				
No cons		Hopera				
Nocous	ska '	1 JSCHD	OD (AND FELS.			
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	()					
gned: Observer	(Client Representa	tive			

APPENDIX 3

Project Personnel and Equipment Movements (March 1991)

The surveyor arrived on site on the 9th with an inspection of benchmarks and key geographical features done the same day. Line layout work commenced on the 10th. Camp buildings and messtent arrived on the 11th and were set up ready to use. The camp cook and water tanker arrived on the 12th. All crews (SADME, VELSEIS and BULLDOZER) arrived late on the 13th ready to commence next day.

Experiments were carried out on the 14th and line pre loading commenced late morning. Line surveying was completed and permanent markers installed by the 16th. Preloading of the line was completed by the 18th. Seismic work continued to early morning of the 23rd and included 2 days lost as down time due to electronics failure and 2 days standby time lost due to strong winds.