DEPARTMENT OF MINES SOUTH AUSTRALIA

GEOLOGICAL SURVEY ENGINEERING DIVISION

MONARTO NEW TOWN - PARAGUM STRATIGRAPHIC BORE : COMPLETION REPORT

Hd. Monarto: Sec. 266

- Monarto Development Commission -

bу

J.SELBY

SENIOR GEOLOGIST

Rept.Bk. No. 75/41 D.M. No. 1119-74 G.S. No. 5579 Eng:Geol.No. 1972/17

12th March, 1975

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DEPARTMENT OF MINES SOUTH AUSTRALIA

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STRATIGRAPHIC BORE : COMPLETION REPORT

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INTRODUCTION

A stratigraphic bore has been completed to a depth of 48.0m at Paragum Station, Monarto South (Fig. 1) by request of Messrs. Kinnaird Hill, de Rohan and Young, Consulting Engineers engaged by the Monarto Development Commission.

Drilling was carried out using a cable tool rig to obtain continuous drive tube samples according to the procedure outlined in Appendix II. Work commenced on 10th December 1974 and was completed by 17th December 1974 at a total cost of \$2250.

Purpose of the bore was to investigate groundwater conditions and the existence of possible aquifers in connection with the Regional Hydrological Survey. It has also served to indicate foundation conditions beneath the proposed Sewage Treatment Works.

A detailed geological log is given in Appendix I.

PREVIOUS WORK

A seismic refraction survey was carried out in May 1974 (Ref. 1) in an attempt to predict depth to Kanmantoo Group bedrock to ensure that drilling did not take place over a bedrock high. Location of the seismic spreads is shown in Fig. 1.

Spread 1 showed a major high speed refractor at a depth of around 30 m which has proved to be the Mannum Limestone. Seismic refraction penetration below this horizon would be difficult due to the velocity inversion provided by the underlying Compton Conglomerate. The shallow velocity change at about 3 m suggesting the start of the hard Blanchetown Clay Member has not been confirmed accurately by the log.

It is interesting to note that results from the other seismic spreads indicate a slight northward dip of the Mannum Limestone in this area.

FOUNDATION CONDITIONS

A comparison between the engineering properties of the Hindmarsh clay and the Blanchetown Clay has been made by Stapledon (Ref.2). Foundation conditions in this area may be expected to resemble those in the Adelaide City area. Briefly this will imply shrink-swell movement of the clay which has a high bearing capacity, with the possibility of groundwater seepage at shallow depth through fissures. There is also some indication of gilgai "puff" structures in Section 264.

EXTRACTIVE MINERALS

Sieve analyses carried out on the sand member of the Blanchetown Clay Formation show that the material falls between the limits set by Australian Standard A.77 (Appendix I for results), and would therefore be suitable for concrete aggregate. Its depth however probably precludes economic development.

The overlying clay member is probably not suitable for brick construction due to its highly plastic nature.

Near Murray Bridge the Mannum formation is quarried as a source of limestone aggregate but would be too deep on this site for feasible development.

GROUNDWATER

Only one minor water seepage was struck at 36 m within the Mannum Limestone, rising slightly in the hole.

The water was saline giving an Approximate Total Solids reading of 25 000 mg/l.

The 5m thick Sand member which was struck at 14.5m below ground, was completely dry. This may be due to the confining effect of the overlying Blanchetown Clay. The sand layer would be suitable as a drainage aquifer although its permeability cannot be estimated reliably without test pumping.

SENIOR GEOLOGIST

REFERENCES

Wightman W.E., Seismic Refraction Survey at Monarto. S.A.D.M.

Rept.Bk. 74/100 (unpubl.)

Stapledon D.H., Changes and Structural Defects developed in some South Australian clays, and their Engineering Consequences. C.E. Trans. Inst. Engineers Aust.

Vol. C.E9 No.1

APPENDIX I

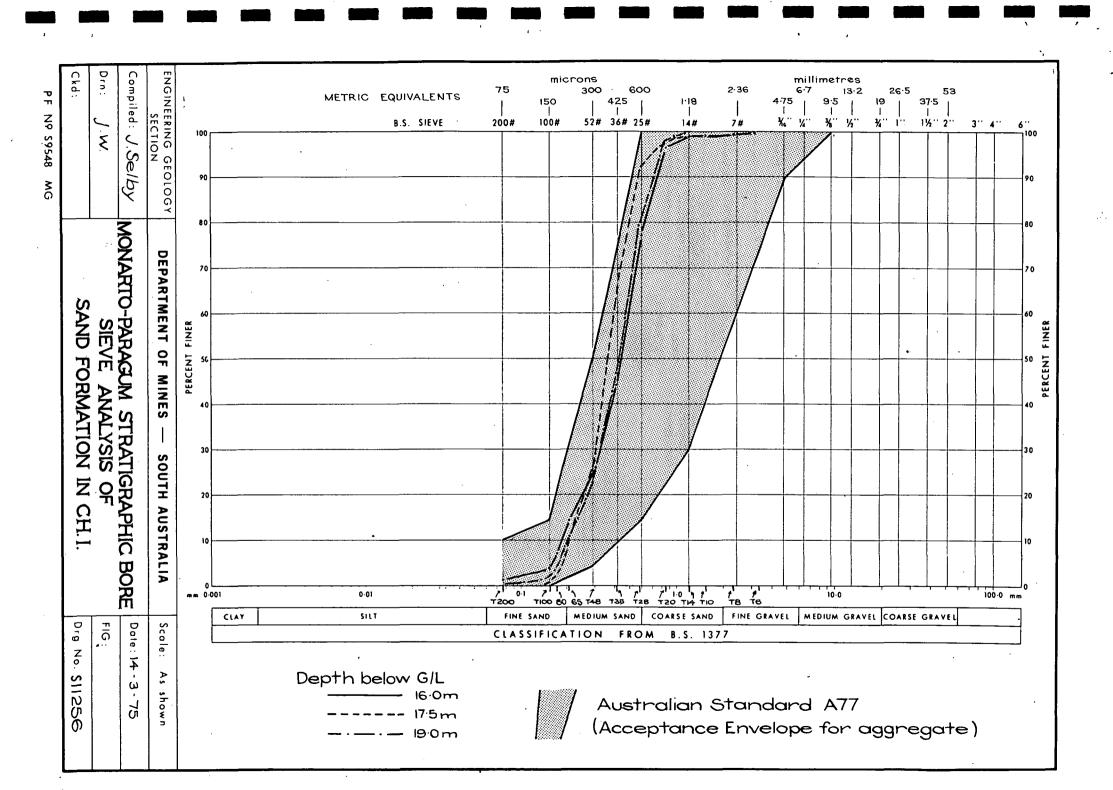
Geological log & Sieve
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APPENDIX II

Cable Tool Drilling Proceedure and Descriptive Terms.

NOTES ON CABLE TOOL DRILLING PROCEDURES

Equipment

Drilling is carried out with a cable tool drilling plant using sampling tubes with special cutting shoes attached, through a vacuum head, to the sampling tools.

Continuous samples for logging purposes are taken with a heavy duty galvanised steel "S" tube (ID 106.5 mm). Sealed samples for laboratory testing are obtained with a special "L" type thin walled, cadmium plated steel tube and cutting shoe (ID 101.6 mm or 4 ins.) designed to reduce sample disturbance to a minimum.

Continuous Sampling Procedure

The "S" tube assembly, fitted with an "A" type cutting shoe (ID 103.2 mm), is lowered to the bottom of the hole and the tube is driven exactly 30 cm. The number of blows required for the 30 cm penetration is recorded.

Sample, or core, is extracted from the "S" tube using a hydraulic ram. This extracted core is sealed in a labelled plastic bag and stored in a core box.

The hole is reamed with a "D" shoe (ID belled out to 124.5 mm) and then the next sample is taken, using the same procudure as above. Thus the hole proceeds by alternate sampling, reaming and (where required) casing operations and the samples form a nearly continuous record of the materials penetrated.

In loose saturated material such as wet sand, a copper "basket" is inserted in the "S" tube above the cutting shoe to help retain the sample.

Sealed Tube Sampling Procedure

Before the sample is taken the hole is cleaned out to the depth specified. The hole is not reamed or cased for at least 30 cm from the bottom however, because these operations can cause considerable disturbance in the soil below. The sampling assembly is lowered carefully to the bottom of the hole, the sampling tube driven exactly 30 cm, and the number of blows recorded.

The sample is sealed in the tube by inserting in each end plastic seals with rubber sealing rings, and the tube is then labelled and stored in a Laboratory Sample Box.

The copper "basket" is never used during sampling for sealed tubes because of its marked disturbing effect on the sample.

Standard Penetration Test (SPT)

The Standard Penetration Test (Terzaghi and Peck 1967) is used to test the in-situ density of sands and to give an indication of the consistency of clays, and compactness of silts. However the test results can be affected by several geological factors such

as degree of cementation, and size and shape of grains. In loose saturated ground the test underestimates the consistency of the material due to piping effects, and under these conditions the drillers are instructed to stabilise the water level before testing. These factors should be taken into account in interpretation of results.

Equipment consists of a 5.1 cm (2 in.) diameter sampling tube and a hammer having a standard weight of 64 kg (140 lbs). The hammer is allowed to fall on the drill rods until the sampling shoe has penetrated 15 cm into the soil. The standard Penetration Number (N) is the number of blows required to produce the next 30 cm of penetration.

NOTES ON CABLE TOOL DRILL LOG SHEETS

During logging, soils are classified and described according to the Unified Soil Classification (USBR, 1966) which assigns letter symbols to each soil group.

Consistency, compactness and relative density of the soil is assessed from the results of the continuous blow count and SPT'S. This information is plotted in the form of a continuous histogram in the Field Test Data Column which also distinguishes various types of sample with a hatching code shown at the bottom of the log sheet.

In the column at the far right of the log sheet, readings of unconfined compressive strength (qu) made with a Soiltest Penetrometer, are recorded. The readings are plotted as a histogram. The Soiltest Penetrometer only gives true values of qu when used in clays in which $\emptyset = 0$.

(January, 1974)

REFERENCES

TERZAGHI, K. and PECK, R.B., 1967. Soil Mechanics in Engineering Practice, (2nd Edition). John Wiley and Sons.

UNITED STATES DEPARTMENT OF THE INTERIOR, BUREAU OF RECLAMATION, 1966. Earth Manual, (2nd Edition).

DESCRIPTIVE TERMS

1. CLAY SOILS

CONSISTENCY

CONSISTENCY	SYMBOL	UNCONFINED COMPRESSIVE STRENGTH (kg/sq. cm)	FIELD TEST	N
Very soft	V.S.	Less than 0.25	Easily penetrated several centimetres by fist.	2
Soft	S.	0.25 to 0.5	Easily penetrated several centi- metres by thumb	2 to 4
Firm	F	0.5 to 1.0	Can be penetrated several centimetres by thumb with moderate effort.	4 to 8
Stiff	St	1.0 to 2.0	Readily indented by the thumb but penetrated only with great effort.	8 to 15
Very Stiff	V.St.	2.0 to 4.0	Readily indented by thumb nail.	15 to 30
Hard (Extremely stiff)	Н	over 4.0	Indented with difficulty by thumb nail.	30 and over

Based partly on Terzaghi, K. and Peck, R.B., 1966. Soil Mechanics in Engineering Practice, Wiley - New York.

MOISTURE CONTENT

ABBREVIATION	MEANING
MC = LL	Moisture content near liquid limit.
MC < LL	" less than liquid limit.
MC > PL	" greater than plastic limit.
MC ≃ PL	" " near plastic limit.
MC < PL	" less or equal to plastic limit.
MC < PL	" less than plastic limit
MC << PL	" much less than plastic limit.

2. SILT SOILS

SYMBOL	N
Ls	0 to 8
· MC	8 to 15
C	15 to 30
VC	greater than 30
	Ls MC C

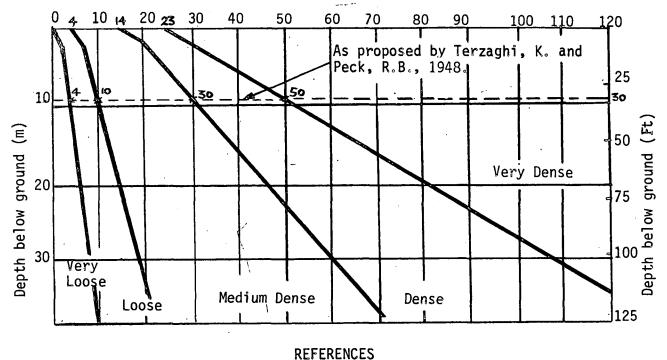
3. SANDS

CLASSIFICATION OF SANDS BY STANDARD PENETRATION TEST

The relative density of granular soils has been judged from the results of Standard Penetration Tests carried out by the procedure described by Terzaghi and Peck (1948) bearing in mind the limitations of the method as discussed by Gibbs and Holtz (1957). At all times the water in the drill hole was kept at the level of surrounding ground-water.

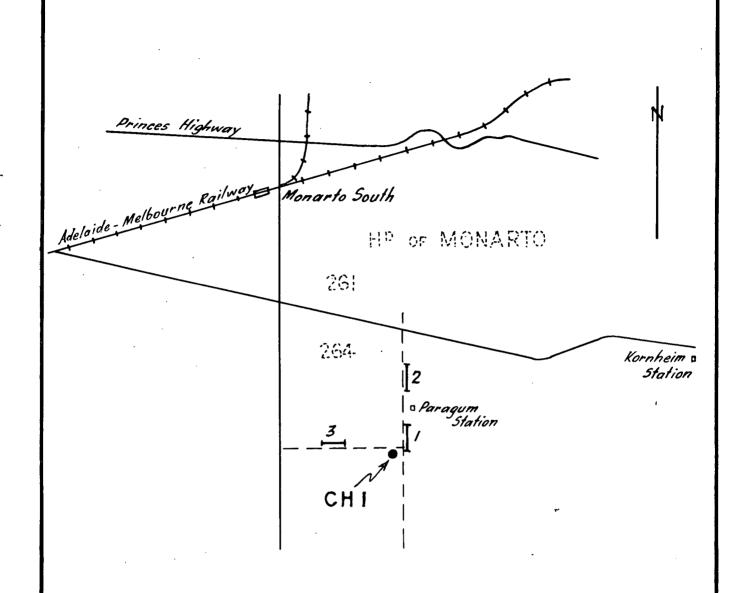
EFFECT OF OVERBURDEN PRESSURE ON STANDARD PENETRATION TEST

Standard Penetration Test (N) Blow/30 cm



Terzaghi, K. and Peck, 1948. "Soil Mechanics in Engineering Practice". Wiley, New York.

Gibbs, H.T. and Holtz, W.G., 1957. Research on Determining the Density of Sands by Spoon Penetration Testing. Proc. 4th Inter. Conf. SM & FE, London, Vol. 9.



Seismic refraction spreads shown .

Refer Report Book 74/100 by W. E. Wightman.

Exd.

Fig. 1

5ketch

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	Exd.	STRATIGRAPHIC BORE

DEPARTMENT OF MINES

11257

SOUTH AUSTRALIA

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