

ENG. GEOLOGY SECTION

DEPARTMENT OF MINES SOUTH AUSTRALIA



GEOLOGICAL SURVEY
ENGINEERING DIVISION

FERRY BERTH - CAPE JERVIS

Marine Res. Hd. Waitpinga

- Department of Marine and Harbors -

by

W.R.P. BOUCAUT
SUPERVISING GEOLOGIST
ENGINEERING DIVISION

Rept. BknNo. 71/12

28th January, 1971.

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DEPARTMENT OF MINES
SOUTH AUSTRALIA

FERRY BERTH - CAPE JERVIS

Marine Res. Hd. Waitpinga

REPORT ON GEOLOGICAL INVESTIGATIONS

Client: Department of Marine and Harbors

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1	Ferry Berth - Cape Jervis Location of Drill Holes.	71-57

Rept. Bk. No. 71/12
G.S. No. 4593
D.M. No. 999/79

DEPARTMENT OF MINES
SOUTH AUSTRALIA

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G.S. No. 4593
D.M. No. 999/70

FERRY BERTH - CAPE JERVIS

Marine Res. Hd. Waitpinga

REPORT ON GEOLOGICAL INVESTIGATIONS

Client: Department of Marine and Harbors

SUMMARY AND CONCLUSIONS

Foundation conditions for a proposed ferry berth in a small inlet of the sea at Cape Jervis were investigated by 3 diamond drill holes to 50 ft., deep, put down into the sea bed from an existing jetty. These holes showed the floor of the inlet to be composed of sediments of Permian age and it is likely that the inlet was formed by glacial action in Permian times. Rocky outcrops of fresh, very strong greywacke of the Kammantoo Group of Cambrian Age forms the sides of the inlet.

The Permian sediments typically consist of beds, often lenticular, of gravels, sands, and silts of varying strength, and it would be difficult to locate a strong horizon thick enough, and continuous enough to form a foundation for driven piles.

* Terms underlined are defined in Table 1.

An exploration programme to prove the thickness and nature of the Permian sediments and the strength of the underlying greywacke is proposed, as it is considered that the greywacke would provide the best foundation material.

INTRODUCTION

It is proposed to construct a berth for a ferry in the small inlet of the sea at Cape Jarvis. The berth would replace the existing jetty. A request to drill 3 drill holes to investigate foundation conditions was received in a letter from the Acting Chief Engineer, dated 17th August, 1970. Initially cable tool holes put down from a floating barge were proposed, but this was later changed to three cored diamond drill holes (D.H. 1, H.H. 2 and D.H. 3) put down to a depth of about 50 ft., from the existing jetty (Fig.1.). Logs of these diamond drill holes are included in Appendix A.

SITE GEOLOGY

Much of the shore line near Cape Jarvis is composed of steep rocky cliffs. In a few places small inlets lead to sandy beaches. The existing jetty at Cape Jarvis is located in an inlet approximately 300 ft., wide. Both sides of the inlet are composed of rock outcrops, but the floor of the inlet appears to be mainly beach sand and loose rock of Recent age (Fig.1.).

The rocky outcrops in the area are mainly of fresh very strong greywacke of the Kammantoo Group of Cambrian age. However outcrops of sediments of the Cape Jarvis Beds of Permian Age occur near the shore about 1/2 mile north of Cape Jarvis. These sediments are, at this location,

about 100 ft., thick and consist of beds of clay, clayey shale, sandstone and gravel up to 30 ft., thick. These deposits were formed following the glaciation of Permian times, and generally fill old glacial valleys (L.W. Parkin (Ed.) 1969). Similar sediments were recovered during the drilling from the jetty, and is also exposed in batters of recent earthworks for parking areas at the back of the inlet. Details of the materials recovered during drilling are shown in the drill logs. (Appendix A).

DISCUSSION

The drilling results and surface exposures indicate that the inlet was formed during Permian times as a glacial valley and was then infilled with sediments. However, there is no indication as to the depth of the sediments or the condition of the underlying greywacke.

Experience in similar sediments elsewhere suggests that they are often lenticular and variable in nature from coarse gravel horizons, through dense sands to weak silts and clays, and it is common for the weaker horizons to be intermingled with the stronger layers. The various horizons would be expected to be generally flat lying although local dips of up to 35° have been recorded.

Due to the lenticular nature and the marked variation in strength of the various horizons it would be difficult to locate particular horizons on which driven piles could be founded, and results so far suggest that piles could be safely founded only on the underlying greywacke.

It is recommended that an investigation programme be undertaken to determine the thickness of the Permian sediments beneath the proposed berth, and also the strength of the underlying greywacke.

This could be carried out in 2 stages.

- (1) Seismic refraction traverses across the inlet to indicate depth to high velocity material. A suggested location of the traverses is shown on Fig. 1.
- (2) One and possibly two push-tube/diamond drill holes to prove the nature and thickness of the Permian sediments as indicated by the seismic traverses, and to prove the nature of the underlying material,

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WRPB:JTS
28.1.71

REFERENCES

PARKIN, L.W. (Ed.) 1969. Handbook of South Australian Geology. Government Printer. Adelaide.

TABLE 1
CLASSIFICATION OF ROCK CONDITIONS AND STRENGTH OF ROCK SUBSTANCE

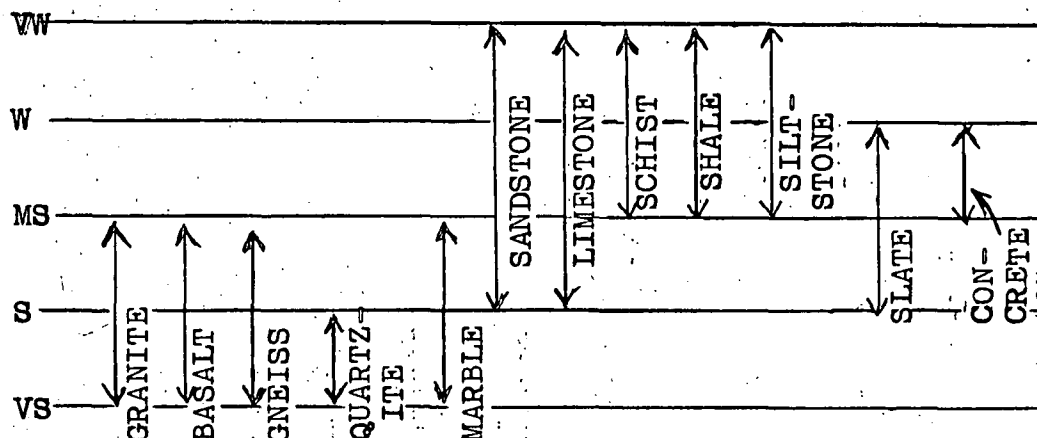
1. ROCK CONDITION TERMS

TERM	ABBRN	DEFINITION
Fresh	(F)	Substance shows no effects of chemical decomposition.
Chemically Decomposed	(D)	Substance is affected by chemical decomposition, but the exact process is not obvious.
Chemically Weathered	(W)	Substance shows effects of chemical decomposition processes which have occurred due to surface and near-surface agencies such as air and groundwater.
Chemically Altered	(A)	Substance shows effects of chemical decomposition processes which have occurred due to plutonic or volcanic fluids.
Extremely {Decomposed Weathered Altered}	{(XD) (XW) (XA)}	Substance has been reduced to material which shows fabric of original rock, but which can be remoulded, i.e. soil substance. (Classified by Unified System).

2. CLASSIFICATION OF ROCK SUBSTANCES BY UNCONFINED COMPRESSIVE STRENGTH

TERM	ABBRN	UNCONFINED COMPRESSIVE STRENGTH (Kg/sq.cm)	(lb/sq.in)
Very weak	VW	<70	≤ 1000
Weak	W	70 - 200	1000 - 3000
Medium strong	MS	200 - 700	3000 - 10,000
Strong	S	700 - 1800	10,000 - 25,000
Very strong	VS	>1800	>25,000

**RANGE OF STRENGTHS OF SOME COMMON
ROCK SUBSTANCES IN THE FRESH STATE***



*Samples of fresh rock tested to Australian Standard, For rocks showing planar anisotropy the long axis of the sample is normal to fabric planes.

3. EXAMPLES OF USE OF CLASSIFICATION

<u>Geological Name</u>	<u>Rock Condition Term</u>	<u>Strength Term</u>
Granite	Fresh	Strong
Granite	Weathered	Medium Strong
Schist	Fresh	Weak
Schist	Altered	Very Weak

APPENDIX A

Logs of diamond drill holes and explanation notes

APPENDIX A

LOGS OF DIAMOND DRILL HOLES AND EXPLANATORY NOTES

NOTES ON DRILLING PROCEDURES

Equipment

The core sizes are as follows:-

<u>Symbol</u>	<u>Nominal Diameter of Cores (inches)</u>
NXC (NX casing)	2.8
NMLC	2.0
BMLC	1.4

The NMLC and BMLC cores were obtained with "M" type stationery inner tube core barrels fitted with bottom discharge bits. The inner tubes were of the split type, ensuring minimum disturbance of the core during removal from the barrel.

Storing and marking of core

Cores are stored in wooden boxes, each compartment of which is designed to contain five feet of core. The internal length for each compartment is actually five feet one inch, to allow for 100 per cent core recovery. Roughness of the ends of the core, and small inaccuracies in measurement when breaking it to fit the box, make it difficult to fit five feet of core in a compartment of exactly that length. The boxes are marked with consecutive compartment numbers at one end, and the drilled depths from the surface in feet at the other.

The core was boxed in this manner at the drill site, the core being placed in its appropriate place in the box as soon as it was extracted from the core barrel. The bottom of each lift was marked with paint or indelible ink immediately it was placed in the box, and a corresponding mark made on the side of the core box. The measured depth of the hole in feet from the surface was painted on the side of the core box and on the core. Timber blocks cut to the correct length indicate core not recovered (red blocks), and core removed for testing (white blocks).

The core has been stored at the Department of Mines, Drilling and Mechanical Branch, Dalglish Street, Thebarton, South Australia.

NOTES ON DIAMOND DRILL LOG SHEETS

The logs are plotted on a vertical scale of one inch = 10 feet (1:120) or one inch = five feet (1:60). In the column headed "Log", places where core was obtained are shown by stippling. Places where core was lost are shown by blank spaces.

The descriptions given on the log sheet refer only to materials recovered as core. Core is lost by the material being

ground or washed away during the drilling process; it may usually be inferred that such material is relatively weak. The weakness may arise from weathering or else from sheared, crushed, or closely jointed rock. It cannot always be assumed that the material not recovered is weak, since even solid rock core may be ground away and lost during drilling operations.

To the left of the graphic log is a geological description of the materials sampled. This includes:-

... Geological age)	
... Rock unit name)	Printed vertically
... Type of material)	
... Mineral composition		
... Cementation		
... Physical description of core		

Classification of the rock substance in terms of its strength and its condition (eg. weathering, alteration) is shown graphically in the column "Strength Term". The terms used in the classification are defined in Table 1. Where the substance has soil properties this is shown graphically in the column, and immediately to the left of the column under "Group Symbol", the symbol representing the remoulded sample as classified under the Unified Soils Classification (USBR 1966) is given.

The "Fracture Log" to the right of the graphic log column shows the degree of fracturing of the core by means of a histogram-type plot. Degree of fracturing means the degree to which the rock has mechanically broken up along geological defects such as joints, cleavage planes, foliation planes, bedding planes or seams. Fresh fractures across the fabric of the rock, not along the existing planar geological defects, are not included. In sections in which no core was recovered, the fracture log column is left blank.

In the column marked "Structures" the angles shown on joints, bedding, or other geological structures are the angles which they make with the plane at 90° to the axis of the core, unless otherwise stated.

Percentage loss of drilling water as recorded by the driller is shown graphically in the column "Drill Water Loss %".

REFERENCE

1. UNITED STATES BUREAU OF RECLAMATION 1966, Earth Manual
2nd Edition.

DEPARTMENT OF MINES SOUTH AUSTRALIA						HOLE NO. 1		
PROJECT. FERRY BERTH			LOG OF DIAMOND DRILL HOLE			SERIAL No. 659/71		
FEATURE. FOUNDATIONS			SECTION MARINE RES. HUNDRED WAITPINGA			R. L. Surface . FT.		
LOCATION From existing jetty			CO-ORDINATES			R. L. Collar . FT.		
			ANGLE FROM HORIZ. 90°			DIRECTION		
DESCRIPTION OF CORE			GROUP SYMBOL		STRENGTH TERM		CORE SIZE DEPTH	
			LOG		FRACTURE LOG		STRUCTURES	
			LOG		LOG		JOINTS, VEINS, SEAMS, SHEARED ZONES, CRUSHED ZONES	
			LOG		LOG		LIFT CORE LOSS %	
			LOG		LOG		WATER LEVEL	
			LOG		LOG		CASING	
			LOG		LOG		DRILL LOSS %	
			LOG		LOG		WATER PRESSURE TESTS	
			LOG		LOG		LUGGONS	
			LOG		LOG		0.5 5 10 50	
			10		20		30	
			40		50		60	
			70		80		90	
			100		110		120	
			130		140		150	
			160		170		180	
			190		200		210	
			220		230		240	
			250		260		270	
			280		290		300	
			310		320		330	
			340		350		360	
			370		380		390	
			400		410		420	
			430		440		450	
			460		470		480	
			490		500		510	
			520		530		540	
			550		560		570	
			580		590		600	
			610		620		630	
			640		650		660	
			670		680		690	
			700		710		720	
			730		740		750	
			760		770		780	
			790		800		810	
			820		830		840	
			850		860		870	
			880		890		900	
			910		920		930	
			940		950		960	
			970		980		990	
			1000		1010		1020	
			1030		1040		1050	
			1060		1070		1080	
			1090		1100		1110	
			1120		1130		1140	
			1150		1160		1170	
			1180		1190		1200	
			1210		1220		1230	
			1240		1250		1260	
			1270		1280		1290	
			1300		1310		1320	
			1330		1340		1350	
			1360		1370		1380	
			1390		1400		1410	
			1420		1430		1440	
			1450		1460		1470	
			1480		1490		1500	
			1510		1520		1530	
			1540		1550		1560	
			1570		1580		1590	
			1600		1610		1620	
			1630		1640		1650	
			1660		1670		1680	
			1690		1700		1710	
			1720		1730		1740	
			1750		1760		1770	
			1780		1790		1800	
			1810		1820		1830	
			1840		1850		1860	
			1870		1880		1890	
			1900		1910		1920	
			1930		1940		1950	
			1960		1970		1980	
			1990		2000		2010	
			2020		2030		2040	
			2050		2060		2070	
			2080		2090		2100	
			2110		2120		2130	
			2140		2150		2160	
			2170		2180		2190	
			2200		2210		2220	
			2230		2240		2250	
			2260		2270		2280	
			2290		2300		2310	
			2320		2330		2340	
			2350		2360		2370	
			2380		2390		2400	
			2410		2420		2430	
			2440		2450		2460	
			2470		2480		2490	
			2500		2510		2520	
			2530		2540		2550	
			2560		2570		2580	
			2590		2600		2610	
			2620		2630		2640	
			2650		2660		2670	
			2680		2690		2700	
			2710		2720		2730	
			2740		2750		2760	
			2770		2780		2790	
			2800		2810		2820	
			2830		2840		2850	
			2860		2870		2880	
			2890		2900		2910	
			2920		2930		2940	
			2950		2960		2970	
			2980		2990		3000	
			3010		3020		3030	
			3040		3050		3060	
			3070		3080		3090	
			3100		3110		3120	
			3130		3140		3150	
			3160		3170		3180	
			3190		3200		3210	
			3220		3230		3240	
			3250		3260		3270	
			3280		3290		3300	
			3310		3320		3330	
			3340		3350		3360	
			3370		3380		3390	
			3400		3410		3420	
			3430		3440		3450	
			3460		3470		3480	
			3490		3500		3510	
			3520		3530		3540	
			3550		3560		3570	
			3580		3590		3600	
			3610		3620		3630	
			3640		3650		3660	
			3670		3680		3690	
			3700		3710		3720	
			3730		3740		3750	
			3760		3770		3780	
			3790		3800		3810	
			3820		3830		3840	
			3850		3860		3870	
			3880		3890		3900	
			3910		3920		3930	
			3940		3950		3960	
			3970		3980			

WATER PRESSURE TESTS LUGEONS

SC/CL

END OF HOLE 46.9 ft.

NOT TESTED

- SHEET 1 OF 1 DRG. No. S9149 HCII

P.F. N° S5027D MB

DEPARTMENT OF MINES SOUTH AUSTRALIA										HOLE NO. 3	
LOG OF DIAMOND DRILL HOLE										SERIAL No. 662/71	
PROJECT. FERRY BERTH			SECTION MARINE HUNDRED WAITPINGA			R. L. Surface. FT.			R. L. Collar FT.		
FEATURE. FOUNDATION			CO-ORDINATES			ANGLE FROM HORIZ. 90°			DIRECTION -		
LOCATION From existing jetty			DATE			Datum			WATER PRESSURE TESTS LUGEONS		
DESCRIPTION OF CORE	GROUP SYMBOL	STRENGTH TERM	CORE SIZE DEPTH LOG	FRACTURE LOG	STRUCTURES JOINTS, VEINS, SEAMS, SHEARED ZONES, CRUSHED ZONES	LIFT CORE LOSS%	WATER LEVEL	CASING	DRILL WATER LOSS%	WATER PRESSURE TESTS LUGEONS	
<div style="display: flex; justify-content: space-between;"> 10 20 30 40 50 </div>											
DRILLED THROUGH SEAWATER. <i>Sea Floor</i>											
sticks have some dry strength as noted. sandy portions are weaker than shales. All sticks loose strength when saturated.						No structures apparent. Mainly broken across near horizontal planes - no joints. Weathered seam? structures mainly indeterminate - few joints apparent. dip 35° Weathered seam?					
PERMIAN - CAPE JERVIS BEDS SHALE, clayey, grey grading to SANDSTONE in parts. Sand is mainly quartz up to 0.7mm size, in clay matrix.						END OF HOLE 50.5 ft.					

1 STRENGTH TERM

VS-Very Strong
S-Strong
MS-Medium Strong
W-Weak
VW-Very Weak
SO-Soil properties

2 CONDITION TERM

Fresh
Decomposed
Weathered
Altered
Not
Applicable

3 FRACTURE LOG

1 4 16 64
12 3 3 3
4 16

(3.5) Maximum effective pressure (bars) reached during test.
Min. = Minimum value.

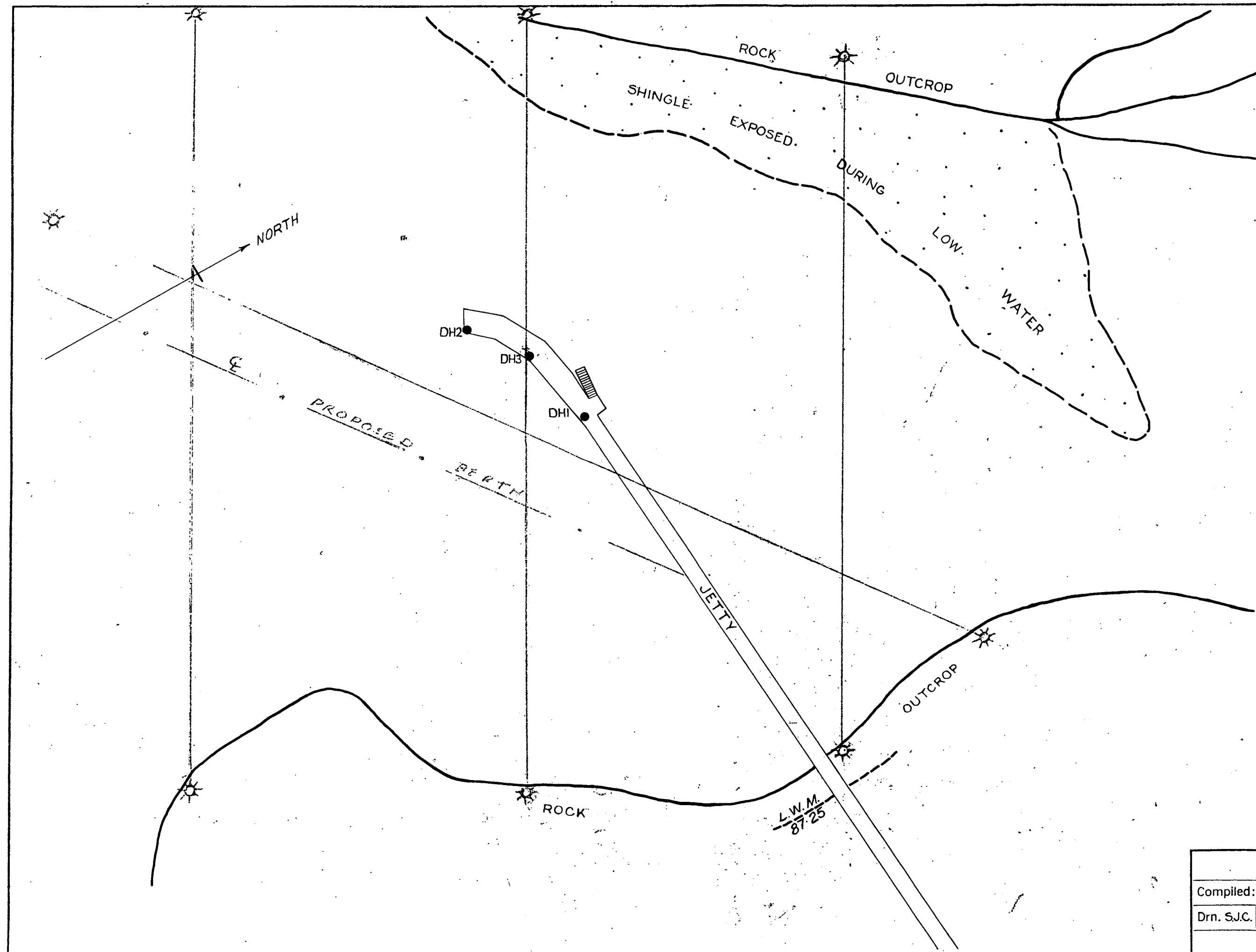
ENGINEERING GEOLOGY SECTION

DRILL No. **24**
TYPE **E 1000**
DRILLER **Aschmoneit**
START. **21 Dec 70**
FINISH **23 Dec 70**

LOGGED **W.P.R. Baucout**
DATE **14 Jan 70**
TRACED **E.B.T.**
CHECKED **W.P.B.**

SHEET **1** OF **1**

DRG. No. **S9148 HC11**



- LEGEND**
- DH3 Diamond drill hole No. 3
(Approximate location)
 - Rock in outcrop is greywacke.
(Kanmantoo Group)
 - *—*— Proposed seismic
refraction traverse

FIG. 1

DEPARTMENT OF MINES - SOUTH AUSTRALIA		Scale: 1" = 40 feet
Compiled: W.R.P.B.	FERRY BERTH - CAPE JERVIS	Date: 21st. JAN. '71
Drn. S.J.C. Ckd. E.B.T.	MARINE RES. HD. WAITPINGA	Drg. No.
	LOCATION OF DRILL HOLES	71-57 Hc II