

DEPARTMENT OF MINES
SOUTH AUSTRALIA

REPORT ON THE GEOLOGY OF
KANGAROO CREEK DAM

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INTRODUCTION

The site for the Kangaroo Creek Dam is on the Torrens River, 14 miles northeast of Adelaide (Fig. 1). The dam is to provide 250,000 acre feet of storage for the Adelaide metropolitan water supply system. A diversion tunnel in the right bank, constructed during 1966, will provide permanent outlet works during operation of the reservoir.

Details of the proposed dam are as follows:-

Rock fill, concrete slab upstream face.

Upstream face 1.3 : 1, Downstream face 1.4 : 1

Total volume of rockfill 450,000 cu. yds.

Maximum height above stream bed 190ft.

Crest length 440ft.

Dam crest level, R.L. 910ft.

Full supply level R.L. 900ft.

A channel spillway, crest level R.L. 900ft. in the left bank is designed to pass a maximum flood of 40,000 cusecs. It is proposed to use rock from the spillway excavation as rockfill in the dam.

Geological investigations of the site have included the following:

..... Regional geological mapping. Use was made of aerial photos and 1-inch to 1-mile maps of the Geological Survey of South Australia (Ref. 2 and Fig. 1).

- Detailed geological mapping. Outcrop maps, sections and profiles were prepared on scales of 1in. = 40ft. and 1in. = 10ft. (Figs. 2,3,5,6, and 8,9,10).
- Detailed logging of cuttings along Old Gorge Road, Gorge Road Deviation and Access Road (Fig. 3).
- Diamond drilling. 27 holes were drilled using NX and NMLC equipment (Appendix A).
- Water pressure testing of drill holes (Appendix A).
- Exploratory adits. Two adits were constructed in the left bank, upstream from the site and logs were prepared on a scale of 1in. = 10ft. (Appendix B.)
- Diversion tunnel. Logs were prepared on a scale of 1in. = 20ft. (Appendix C).
- Laboratory tests on rocks. Samples were tested for strength and durability (Appendices D & E.)

GEOLOGY OF REGION

Adelaide is situated on an uplifted coastal plain at the eastern margin of the Gulf St. Vincent. The plain is bounded to the east by the Mount Lofty Ranges, a series of step-faulted ridges and plateaus trending roughly northeast. The River Torrens is the largest of several streams deeply entrenched into the western part of the ranges, and discharging on to the coastal plain. Between the headwaters and the plain the Torrens flows through a gorge about six miles long.

The geology of the Adelaide region is shown on Fig. 1 and is described by Stapledon (Ref. 1) and Campana (Refs. 2 and 3).

The succession is summarised as follows:-

AGE	DESCRIPTION	LOCATION
Recent to Pleistocene	Unconsolidated marine clays and sands; alluvial clays, sands and gravels.	Coastal Plain
Tertiary	Marine sediments; fossiliferous limestone, calcareous sandstones, marls, sands and clays. Lacustrine sediments; sands, clays and lignites.	
Proterozoic	Slates, phyllites, sandstones, quartzites, limestones, dolomites and tillites.	
Archaean	Schists and gneisses.	Mt. Lofty Ranges

The dam site is located near the southern tip of an elongated belt of Archaean rocks, known as the Houghton Complex. The Archaean rocks are bounded on both sides and to the south by Proterozoic rocks of the Torrens Group. The Kitchener Fault crosses the river about 600ft. upstream from the dam site and dips 40° to 50° to the southeast (downstream), forming the eastern boundary between the Torrens Group and Houghton Complex rocks. It is a zone, several hundred feet wide, containing numerous narrow crushed seams.

GEOLOGY OF SITE AREA

Topography

The dam site is located close to the upstream entrance to the steepest portion of the Torrens Gorge. In the site area the gorge is up to 700ft. deep. The river follows a straight course for 1,000ft., in a direction slightly north of west. The gradient is approximately 1 in 35.

The valley is generally asymmetric with the left and right banks in marked contrast. On the right bank the ridge rises 600 to 800ft. above river level and in the lower 250ft. consists mainly of rock outcrops. Slopes range from 30° to 45° near the downstream toe of the dam to 45° to vertical on the upstream side of the dam axis. The left bank ridge rises up to

550ft. above the river level and consists of rock outcrops in minor ridges trending upslope and separated by soil-filled gullies. Slopes are mainly 30° to 45° , flattening near the top of the ridge. The valley floor is from 30 to 60ft. wide and is mainly occupied by the river bed.

Rock Types

Type and Distribution

The terms "rock material" and "rock mass" are used, as defined by John (Ref. 4, p. 3).

Three main types of rock material have been recognised.

Schist. This is a rather weak, fissile rock consisting essentially of extremely fine-grained sericite and quartz which enclose quartz augen or lenses generally less than 2mm. thick. It shows pronounced planar foliation along which it breaks readily into platy or tabular fragments under a light hammer blow.

Gneiss. This consists essentially of quartz, feldspar, sericite and chlorite. It is coarser grained, and has a more banded appearance than the schist. The banded appearance is due to a pronounced gneissic foliation, but the rock is appreciably stronger and less fissile than the schist.

Granitic gneiss. This consists essentially of quartz and feldspar crystals 1 to 10mm. across. Foliation is either absent or poorly developed. The rock commonly contains thin bands or lenses of schist, and quartz in veins or mineralised vugs. The bands of granitic gneiss are up to 15ft. thick and generally occur at intervals of 20 to 50ft.

The rock mass at the dam site is composed of alternating layers and lenses of these three rock types. The boundaries between the layers and lenses are generally parallel to the foliation planes in the rocks, and are usually not clearly

defined; there is a gradation from one type to the other. The left bank is underlain almost entirely by schist, and the right bank mainly by gneiss, with localized bands of schist and granitic gneiss.

Physical Properties

The results of unconfined compression tests on dry cores of the three types of rock material are given in Appendix D. Table 1 summarises the results.

TABLE I
PHYSICAL PROPERTIES OF ROCK MATERIALS

ROCK TYPE	NO. OF SAMPLES	UNCONFINED COMPRESSION STRENGTH lb / sq. in.		MODULUS OF ELASTICITY lb / sq. in. x 10 ⁶	
		Average	Range	Average	Range
Schist	11	3,650	3,040	2.5	4.4
Gneiss	9	10,660	7,660	7.3	8.0
Granitic Gneiss	4	11,300	8,800	5.9	0.5

A further series of unconfined compression strength tests were conducted on paired samples of schist. One of each pair was tested dry: the other after soaking in water for one or two weeks. The test results are given in Appendix D. The samples showed between 20 and 70% loss of strength after soaking.

In both the wet and dry tests the unconfined compressive strength shows a marked increase as the angle between foliation planes and applied stress directions changes from 40° to 90°.

The results of laboratory tests on rock spoil from the exploratory adits and on drill cores and rock spalls are given in Appendices D and E.

Geological Structures

Although the rock materials are relatively strong and compact in small samples, the rock mass is weakened to varying degrees by geological defects of the type shown in Fig. 4. In this figure, and in the following text, the terms spacing and extent are used as defined by John (Ref. 4). The orientations of most types of defect are shown in the diagram on Fig. 3.

Foliation, strikes N. 320° to 360° E (i.e. 45° to 60° to the river direction) and dips 45° to 60° E (upstream). The foliation is the oldest structure and is a defect inherent in most of the rock material.

Joints occur in 4 main sets. The spacings of the joints within each set are variable over the site area.

Set (i) joints strike N 320° to 360° E. dip 45° to 65° E (i.e. parallel to the foliation). They generally extend 50ft. or more. They have slickensided surfaces and appear to have been formed by shearing. They are planar or slightly curved so as to intersect each other and divide the rock into platy slabs. Where exposed in sections of the diversion tunnel unaffected by weathering, most Set (i) joints are spaced between 3 and 15ft. and are tightly closed. In sections of the Adits which have been affected by weathering, Set (i) joints are commonly slightly open and partly clay-filled.

Set (ii) joints strike N 65° to 75° E, (i.e. approx. 35° to river direction) dip 45° to 80° N. They have rough and slightly irregular surfaces and commonly occur en echelon (Fig. 4). In the diversion tunnel Set (ii) joints are spaced between 5 and 30ft. and are commonly slightly open. They are the source of many water seepages into the tunnel. Surface exposures on the right bank show Set (ii) joints extending from 10 to 50ft.

Set (iii) joints strike N 120° to 145° E, (i.e. parallel to the river direction) dip 75° N through vertical to 75° S. Their surfaces are generally rough and irregular. Cliff exposures on the right bank show them spaced from 2 to 40ft. and extending from 50 to 80ft.

Set (iv) joints strike N 15° to 25° E (i.e. approximately perpendicular to the main river direction) and dip 65° to 75° W (downstream). They are similar in appearance and occurrence to Set (ii) joints.

Minor Faults are mainly parallel to Set (i) joints. Two types of faults occur, and are distinguished on the basis of the engineering properties of the fault materials (Fig. 4).

.... Crushed Seams consist mainly of material with soil properties, usually a silt soil with fragments of rock (ML to GP in the Unified Soils Classification System, Ref. 5, p. 14).

.... Sheared Zones are very fissile but may have essentially rock properties if the joints are cemented, or they may behave as soils (gravels) if the joints are clay-coated.

The majority of the minor faults in the site area consist of sheared zones up to 1ft. thick containing one or more crushed seams up to 0.05ft. thick. In the diversion tunnel these faults are exposed at intervals of 5 to 100ft. (Appendix C).

Bankung or exfoliation joints occur more or less parallel to the natural ground surface. They are believed to be formed as a result of weathering processes, and are discussed below.

Weathering

Weathering is defined here as disintegration of rock due to the action of surface agencies and phenomena. Two distinct types of weathering have been recognized, namely mechanical and chemical.

Mechanical Weathering. This is mechanical failure of the rock due to the opening up of joints near the ground surface, and is believed to be initiated by the redistribution and release of stresses within the rock mass when overburden is removed by erosion. Once fine cracks develop, the mechanical weathering process is continued by the roots of vegetation which grow down along them, and perhaps by deposition of clays with expansive properties. Other factors, e.g. climatic, probably also contribute.

In rocks which contain few joints of tectonic origin, irregular joints almost parallel to the ground surface tend to form as part of the mechanical weathering process. Keislinger (Ref. 6) describes these as Bankung or exfoliation joints. They are clearly formed by failure of the rock across its fabric.

On the right bank Bankung type joints are exposed in road cuttings and cliffs, spaced from 4 to 20ft. They are mostly open, commonly as much as 0.3ft., or filled with plastic soils. Much of the ground surface near the downstream toe of the dam is formed by one or more of these joints. In the downstream section of the diversion tunnel the rock mass is partly loosened within 15ft. of the ground surface and several Bankung joints are exposed in the portal excavation. In the tunnel, near the upstream portal, the rock mass is considerably loosened due to mechanical weathering at depths of up to 40ft. below the ground surface.

On the left bank there are very few typical Bankung joints, and it is clear that mechanical weathering has resulted in small movements along joints and faults of tectonic origin.

Trench 1 beside the Old Gorge Road (Fig. 3) exposes joints containing infilled clay up to 0.4ft. thick and penetrated by roots, up to 0.2ft. diameter. The base of this trench is 15ft. below the original ground surface. In parts of Adit No. 2 up to 70ft. vertically below the ground surface, several joints and minor faults contain seams of infilled clay up to 0.05ft thick.

Chemical Weathering. This is decomposition of the rock material due largely to the action of groundwaters. The rock materials are virtually impermeable and the groundwater has gained access to the rock mass mainly by percolating along joints and faults. The degrees of chemical weathering are defined according to the physical properties of the weathering products, as set out in Table II

TABLE II
WEATHERING PRODUCTS OF ROCKS

TERM	ABBREVIATION	DEFINITION
Fresh	Fr.	The rock shows no discolouration, loss of strength or any other effect due to weathering.
Slightly weathered	SW	The rock is slightly discoloured, but not noticeably weaker than the fresh rock.
Moderately weathered	MW	The rock is discoloured and noticeably weakened, but NX drill cores cannot be broken up by hand across the rock fabric.
Highly weathered	HW	The rock is discoloured and weakened to such an extent that NX drill cores can be broken up readily by hand, across the rock fabric. Wet strength usually much lower than dry strength.
Completely weathered	CW	The rock is discoloured and is entirely changed to soil, but the original rock fabric is mostly preserved. The properties of the soil depend upon the composition and structure of the parent rock.

The change from rock to soil properties is gradational, but is placed nominally between the highly and completely weathered states. Material is defined as soil when it can be excavated by hand methods or sampled by driven tube methods without assistance from structural defects such as joints.

The depth and degree of chemical weathering in the rock at the dam site are extremely variable, as they are related more

to the pattern of joints and faults than to the depth below the ground surface.

On the left bank, drill cores and adits show mainly slightly to highly weathered materials in the first 10 to 40ft. vertically below the ground surface. Below this, much of the schist is fresh, but highly weathered adjacent to some joints and faults. The right bank is formed mainly by fresh or slightly weathered gneiss outcrops. At the upstream end of the diversion tunnel the gneiss was mainly slightly weathered, with some moderately to highly weathered material near joints, up to 35ft. below the ground surface. The gneiss is fresh throughout the remainder of the tunnel, except for locally weathered zones adjacent to a few minor faults, and in the roof near the downstream portal. (Appendix C).

In many places on both banks the outcrops contain shallow, irregular cavities, generally up to 2ft. in the largest dimension. A few deeper cavities are developed at the intersection of joints and range from 10 to 20ft. in the largest dimension. They appear to have resulted from differential weathering of zones rich in accessory sulphide minerals.

Superficial Deposits

Spoil from construction of the Gorge Road Deviation fills the river channel and covers most of the ground surface on the lower slopes of the right bank, extending in several gullies up to R.L. 860. The spoil consists of rock fragments ranging from silt sizes to boulders 6ft. across, the larger fragments occurring mainly at lower levels. Drill Hole KC30 encountered 16ft. of spoil before entering bedrock at R.L. 718ft. (Fig. 3). At the upstream portal of the diversion tunnel, rock in-situ was 10 to 20ft. below the surface of the spoil. At the downstream portal, bedrock was under a veneer of spoil (Appendix C). Natural soil (up to 6ft. deep in drill hole benches) covers

most of the right bank above Bachelor's Bridge (Fig. 3), and occurs in some places under the road spoil at the site.

On the left bank, soil covers up to 50% of the ground surface. It occurs mainly as a veneer 1 to 3ft. deep over in-situ schist, but thicknesses in excess of 5ft. have been exposed in benches for Drill Holes KC25 and KC27. Landslide debris occurs in isolated deposits, as shown on Fig. 3.

Stability of Natural Slopes

Surface mapping at the dam site has shown scars of numerous landslides, mainly on the left bank (Fig. 3). These can be classified into two distinct types.

Soil slides are recognized by surface morphology. They form saucer shaped depressions having a steep back and sides, with a mound of soil and obviously disturbed boulders some distance down-slope. They occur mainly in the floors and on the sides of soil-filled gullies on the left bank. Their depth has not been determined.

Block slides are relatively intact blocks of rock, isolated from the main rock mass by seams and joints along which they have moved, usually only 2 or 3ft., downslope. A small slide mass of this type occurs immediately downstream from the upstream face on the left bank (Fig. 3).

Road excavations show several V-shaped re-entrant gullies extending 50 to 80ft. above road level. These have clearly been formed by the removal, by sliding, of small wedges of rock during or since construction of the roads.

Groundwater

Water levels in diamond drill holes on the left bank suggest a water table corresponding closely to river level.

Measured water levels on the right bank are higher but do not suggest a simple water table. Wide variations occur from place to place, probably due to disconnected or partly connected bodies of water within the rock mass. This is typical of ground-water in jointed rocks (Ref. 7).

During winter months numerous seepages occur from and immediately above the steep cliff slopes on the right bank. Numerous seepages and small flows up to 10 gal./hr. occurred in the Diversion Tunnel as it was excavated (Appendix C). Most of these diminished or disappeared during the following three months.

Permeability of Rock Mass

Diamond drill holes at the dam site were water pressure tested by the Lugeon Method (Appendix A). Most holes showed moderate leakages of 10 to 40 Lugeons in the first 20 to 50ft. vertically below ground surface. Tests below these levels gave generally very low leakages (0 to 3 Lugeons), with moderate leakages in some isolated sections.

GEOLOGY OF INDIVIDUAL FEATURES

Cut-off Trench

The cut-off trench will be located at the upstream edge of the dam embankment. It will be approximately 700ft. in length, and sufficiently deep and wide to expose groutable rock over a minimum horizontal width of 12ft. Details of the design are shown on Fig. 7.

Left Bank

The surface geology is shown in plan on Fig. 3 and in sections on Fig. 5. The position of the concrete grout cap is approximate, and will depend on the depths of excavation. The surface geology is summarised in the following table.

TABLE III

CUT-OFF TRENCH, LEFT BANK, NOTES ON GEOLOGY

<u>R.L.(ft.)</u> <u>From</u> <u>To</u>		<u>Approx.</u> <u>Horizontal</u> <u>Distance (ft.)</u>	<u>Notes on Surface Geology</u>
735	753	60	Old Gorge Road and embankment. Fill consists of unsorted schist fragments up to 4ft. across. Position of in-situ rock under fill is unknown.
753	775	20	Cutting exposes fresh to slightly weathered schist and granitic gneiss, joints open up to 0.05ft. Slide block immediately downstream (Fig. 3).
775	800	25	V-shaped re-entrant gully formed during or since excavation of road. Cleanup (Trench 2) reveals sheared zone, 2 to 3ft. wide, with highly to completely weathered rock, in the base of the gully.
800	815	30	Rocky ridge - mainly fresh to slightly weathered schist at surface. Set (i) joints open up to 0.1ft., partly soil-filled.
815	830	30	Numerous small outcrops and loose boulders separated by soil.
830	860	50	Grass covered, soil-filled gully. Where this gully meets the gorge road, it is underlain by relatively weak, fissile schist containing several crushed seams up to 0.2ft. thick, soil-filled in part, with plant roots up to 0.2ft. wide. These are exposed in Trench 1.
860	885	45	Schist and gneiss boulders up to 3ft. with some outcrops, separated by soil.

River Channel

The river channel has been filled with spoil from road excavations. The spoil has been washed by several floods since its deposition. During normal flows (discharge from Millbrook reservoir) the water moves at depth through the spoil, and the upper few feet remain dry.

The spoil exposed at the surface is mainly fresh or slightly weathered schist and gneiss fragments, ranging in size from less than 0.1ft. up to 6ft. in the largest dimension. Drill Hole KC30, 80ft. upstream from the cut-off trench, passed through 16ft. of rock spoil before entering fresh rock at RL 718ft.

The rock recovered was in core lengths less than 0.5ft.

The spoil also contains some timber debris. Some of this is probably the remains of timber and vegetation in the channel prior to filling with spoil, and the remainder has been brought down by floods during and since deposition of the spoil.

Mapping upstream and downstream from the site, and inspection of old photos, suggests that originally the river bed occupied most of the valley floor, and it is expected that the river bed beneath the spoil consists mainly of fresh rock outcrops.

Minor faults located during mapping and drilling of the valley sides mostly strike obliquely to the river channel. It is usually found that where such localized weak zones occur in a stream bed, they have been eroded deeper by the river to form trenches or slots. Such slots are usually backfilled with alluvial materials.

Right Bank

The surface geology is shown in plan on Fig. 3, and in cross section on Fig. 6. Table IV summarizes the geology along the line of the Cut-off Trench shown in plan on Fig. 6. Section KK' on Fig. 6 is up to 20ft. upstream of this line.

TABLE IV

GUT-OFF TRENCH, RIGHT BANK, NOTES ON GEOLOGY

<u>R.L.(ft.)</u> <u>From</u>	<u>To</u>	<u>Approx.</u> <u>Horizontal</u> <u>Distance (ft.)</u>	<u>Notes on Geology</u>
735	775	145	Spoil from road excavation. Boulders of gneiss and schist up to 4ft. across. Generally larger sizes at lower levels. The Inlet Portal excavation, upstream of the cut-off trench, and between RL's 720 and 770, exposed in-situ gneiss beneath up to 20ft. of road spoil. The gneiss is mainly fresh to slightly weathered, with joints slightly open or clay-filled.
775	880	170	Outcrop, mainly of gneiss, with some granitic gneiss. Fresh to slightly weathered. Set (ii) and (iii) joints form steep cliffs. Joints are mainly tightly closed, but open in a few places up to 0.5ft. At RL 805 there is a pocket of soil with swamp type grasses. Seepages occur from joints upslope. Between RL 840 and RL 870, the line of the upstream face is up to 4ft. inside the proposed boundary of the knob to be removed i.e. the cut-off trench will be excavated within the knob excavation (Fig. 6 Section 00', See also section of report "Right Abutment Block and Access Bridge").

Rock Fill Zones

Left Bank

Slopes in the left bank foundation area range from 40° to 60° in the lower part including the cutting of the Old Gorge Road, to 30° at higher levels.

About 20% of the ground surface consists of schist outcrops, mainly slightly weathered. The rock outcrops mainly form ridges trending upslope. Joints in the outcrops are generally open at the surface up to 0.2ft. and partly filled with soil and plant roots up to 0.2ft. diameter.

A further 50% of the ground surface is covered by soil, mainly in gullies between the ridges. Where exposed in the road cutting, drill benches and exploratory adits, this soil is seen to be mainly less than 5ft. deep, extending to greater depths in isolated pockets along joint planes. In the road exposures, the soil overlies partly weathered and loosely jointed rock similar to that forming the outcrops.

The remaining 30% of the ground surface is covered by landslide scars and slide debris. The depth to which the slides affect the ground has not been determined. The slide material at the surface consists of angular schist boulders ranging from 1 to 10ft. across, loosely packed, in a clayey soil matrix.

River Channel

The river channel is filled mainly by road spoil with some timber debris, as discussed above under "Cut-off Trench."

Right Bank

Slopes on the right bank foundation area range from 20° on the road spoil near the river to 50° on the upper slopes, with several near-vertical cliffs up to 35ft. high.

Rock outcrop forms about 50% of the ground surface. It is mainly gneiss, containing bands and lenses of schist and granitic gneiss. The rock exposed is mainly fresh. However, road cuttings above the dam show loosely jointed, slightly to moderately weathered rock in several places. The bands of schist and granitic gneiss are generally more weathered than the gneiss.

Most joints are tightly closed. The intersection of partly open joints in a few places gives rise to semi-detached blocks up to 5 cu. yd. in size.

Foliation in the rocks strikes obliquely to the valley side, and dips into the bank. The rock is intersected by several crushed seams and sheared zones parallel to the foliation. In outcrop they are often partly cemented with limonite, or indicated as narrow slots and soil-filled channels. Road

cuttings show that the sheared zones are mostly less than 1ft. wide, containing seams of crushed rock and clay up to 0.1ft. thick. The rock within and near the zones is usually partly weathered.

Bankung joints occur at the surface in several places and are exposed within 10ft. of the surface in road cuttings.

Road spoil covers the remaining 50% of the ground surface. It occurs mainly at lower levels near the river and extends up the gullies. A study of old photos suggests that the spoil is mainly underlain by rock outcrops, similar in appearance to those exposed on the slopes above, and that natural soil and talus are present locally beneath it.

Channel Spillway

The spillway is shown in plan on Fig. 3 and in sections on Fig. 7. The dimensions of the cutting are as follow:

Length (horizontal distance)	<u>Feet</u> 900
Width of channel floor	36 to 44
Maximum vertical height, upslope face	210
Maximum depth on centre line	80
Width of berms	15
Vertical distance between berms	50
Cutting angle upslope side (between berms)	<u>Degrees</u> 45°
Overall angle top to bottom (including berms)	38° to 40°
Cutting angle downslope side	60°

Section J J', Fig. 7 shows the geological conditions at the surface along a line close to the deepest part of the spillway cutting. Sections KK', LL', MM' and NN' show the surface geology along lines across the spillway channel. Sub-surface information from nearby drill holes and exploratory adits is shown in summarized form on the sections.

The foliation strikes at about 30° to the proposed cutting, and dips 45° to 60° N.E., towards the river. Narrow crushed seams (mostly 0.01 to 0.05ft. wide) and clay-filled joints with partly weathered rock adjacent, occur at intervals of 5 to 10ft. throughout holes drilled in the spillway area. Exposures in the Old Gorge Road cutting indicate that the intersection of crushed seams parallel to the foliation, and Set (ii) joints, tend to divide the rock into V-shaped wedges with the long axes dipping downslope at 45° to 60° .

Exposures in road cuttings and the results of drilling (Holes KC.20 and KC.27) show that there are several crushed seams roughly parallel to the foliation which dip at angles of less than 35° .

More detailed information is given in Table V.

TABLE V.
CHANNEL SPILLWAY EXCAVATION

<u>Station</u> From To	<u>Horiz.</u> <u>Distance</u> (feet)	<u>Notes on Geology</u>
0+00 5+35	535	Approx. 90% soil-covered, 10% outcrops and loose blocks, mainly of schist. Drill benches show soil generally less than 5ft. deep. Soil and boulders locally deeper in deposits of slide debris in gullies. Adit No. 2 gives an indication of the depth of near-surface chemical and mechanical weathering under the ridge (Appendix B). The bench for Drill Hole KC27 shows 4ft. of soil. Drill Hole KC27 (Appendix A) shows:- 0 to 10ft. Schist and gneiss, fresh to (45" core slightly weathered, fractures recovered) spaced 0.1 to 0.5ft. 10 to 105ft. Schist, mainly fresh, fractures (100" core spaced 0.2 to 3ft., some clay recovered) filled joints.
5+35 6+85	150	Approx. 80% soil-covered, 20% outcrops of very flaky schist. Drill Holes KC19 and KC20, show closely-jointed and seamy, very flaky schist (Appendix A).
6+85 8+85	200	Approx. 50% fresh gneiss outcrops, 50% shallow soil containing gneiss blocks. Road cutting below the spillway discharge point shows fresh to slightly weathered gneiss. The bench for Drill Hole KC20 shows 2ft. of soil. Drill Hole KC20 (Appendix A) shows: 0 to 10ft. Schist, slightly weathered. (85% core recovered)

<u>Station</u>		<u>Horiz.</u>	<u>Notes on Geology</u>
<u>From</u>	<u>To</u>	<u>Distance</u> (feet)	
cont.		10 to 50ft. (100% core recovered)	Schist and granitic gneiss, moderately weathered to fresh, fractures spaced mainly 0.1 to 0.8ft.
		50 to 120ft. (100% core recovered)	Schist, gneiss and granitic gneiss, mainly fresh, fractures spaced mainly 0.1 to 1.5ft.

Left Abutment Block

The left abutment block will be a concrete gravity structure at the southern end of the dam and will also form the northern spillway wall between Spillway STA 251 and STA 350. (Fig. 8, Section LL'). The block will be 25 to 30ft. wide at the base and will be 37 to 42ft. high with a horizontal crest at RL.910ft. It will be constructed on a rock foundation made by horizontal continuation of the spillway cutting. The foundation ranges from 10 to 38ft. below the natural ground surface.

The ground surface at the site of the block is hummocky with several deposits of slide material (Fig. 3). It is covered mainly by soil and rock fragments, with several areas of schist outcrop. The bench for drill hole KC27, 50ft. south, exposed 4ft. of soil. The drill core shows:-

- 0 to 10ft. Schist and gneiss, fresh to slightly weathered. Core recovery 45 %.
- 10 to 105ft. Schist, mainly fresh, some clay-filled joints and several sheared zones approximately parallel to the foliation. Core recovery 100%.

Right Abutment Block and Knob Excavation

The Right Abutment Block (Fig. 9) will be a concrete gravity structure 63ft. long, 23ft. wide and up to 32ft. high.

The block will be linked with the Gorge Road Deviation by the existing access road which will be deepened near the top of the dam to give a horizontal surface at RL. 913.5ft. (Sections BB', DD' and FF', Fig. 9). The access road will be extended further to the east by filling to the same level.

Part of the right abutment consists of a steep, in places overhanging, knob with open joints and cavities in the lower part. This knob is to be excavated using a smooth blasting technique to produce a surface dipping towards the river at 50° . The knob is shown in plan and section on Fig. 9.

The surface geology is shown on Fig. 3. Exposures are mainly of slightly weathered and fresh gneiss, with several bands of slightly weathered granitic gneiss. Several sheared zones up to 0.5ft. thick and dipping 45° to 60° upstream, pass through the area. There are also several Bankung joints, approximately parallel to the slope. One of these, exposed in the cutting of the existing access road at about 7ft. below the original ground surface (Fig. 9, Section FF'), contains up to 0.5ft. of clay.

Intake Structure

The intake works will be housed in a 240ft. long inclined tower above the inlet portal of the diversion tunnel. Before commencement of the main dam works, it is proposed that a trench up to 16ft. deep and 20ft. wide will be excavated for the structure and the base of the inlet portal excavation deepened to expose a horizontal rock foundation for a concrete base. A steep faced knob of rock upstream of the intake structure (Fig. 10) will also be removed.

The surface geology of the area at present, is shown in plan on Fig. 3 and in sections on Fig. 10. Further information is given in Table VI.

TABLE VI

GEOLOGICAL CONDITIONS FOR INTAKE STRUCTURE

RIGHT BANK

<u>R.L. (ft.)</u> <u>From</u>	<u>To</u>	<u>Approx.</u> <u>Slope</u> <u>Distance(ft.)</u>	<u>Notes on Geology</u>
720	780	68	Mainly slightly weathered to fresh gneiss outcrops at the surface. Numerous Set (i) joints, some open up to 0.2ft. and clay-filled, intersect with Set (ii) and Set (iv) joints to form semi-detached blocks. Several soil-filled channels trend upslope. A steep, partly overhanging knob of rock occurs immediately upstream of the site for the Intake Structure (Fig. 10 Section DD', Elevation EE'). Upstream of the knob a Bankung joint forms a face dipping 40 to 65° towards the river, and appears to continue underneath the knob. Cracks near the top of the knob suggest that there has been some downslope movement.
780	822	53	Fresh to slightly weathered gneiss outcrops at the surface. Joints mainly tight; few are open to 0.02ft.
822	845	27	Slightly weathered granitic gneiss outcrops at the surface. Few joints, tightly closed.
845	905	95	Surface partly covered by thin veneer of road spoil. Outcrops are mainly slightly to moderately weathered gneiss with lenticular bands of granitic gneiss, mainly moderately weathered.

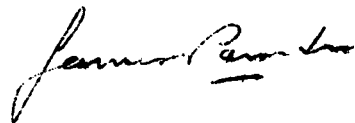
Access Shaft

The Access Shaft will be located at the northern end of the berm on the downstream face of the dam embankment, directly above the diversion tunnel at STA 2 + 67 (Appendix C). An Access House at the top of the shaft will be sited in a cutting which will provide a horizontal base 25ft. wide.

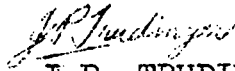
The shaft will be 8ft. in diameter and will extend approx. 37ft. below the base of the cutting, to the roof of the tunnel.

Mainly slightly weathered to fresh gneiss and granitic gneiss forms the ground surface over the shaft site (Fig. 3). Several bankung joints dipping towards the river at 35° to 45° form part of the surface in the vicinity of the proposed cutting.

The tunnel between Sta. 2 + 60 and Sta. 3 + 20 shows mainly fresh gneiss, with few tightly closed persistent Set (i) joints, and discontinuous, tightly closed Set (ii) joints.



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JACP:JPT:SMA

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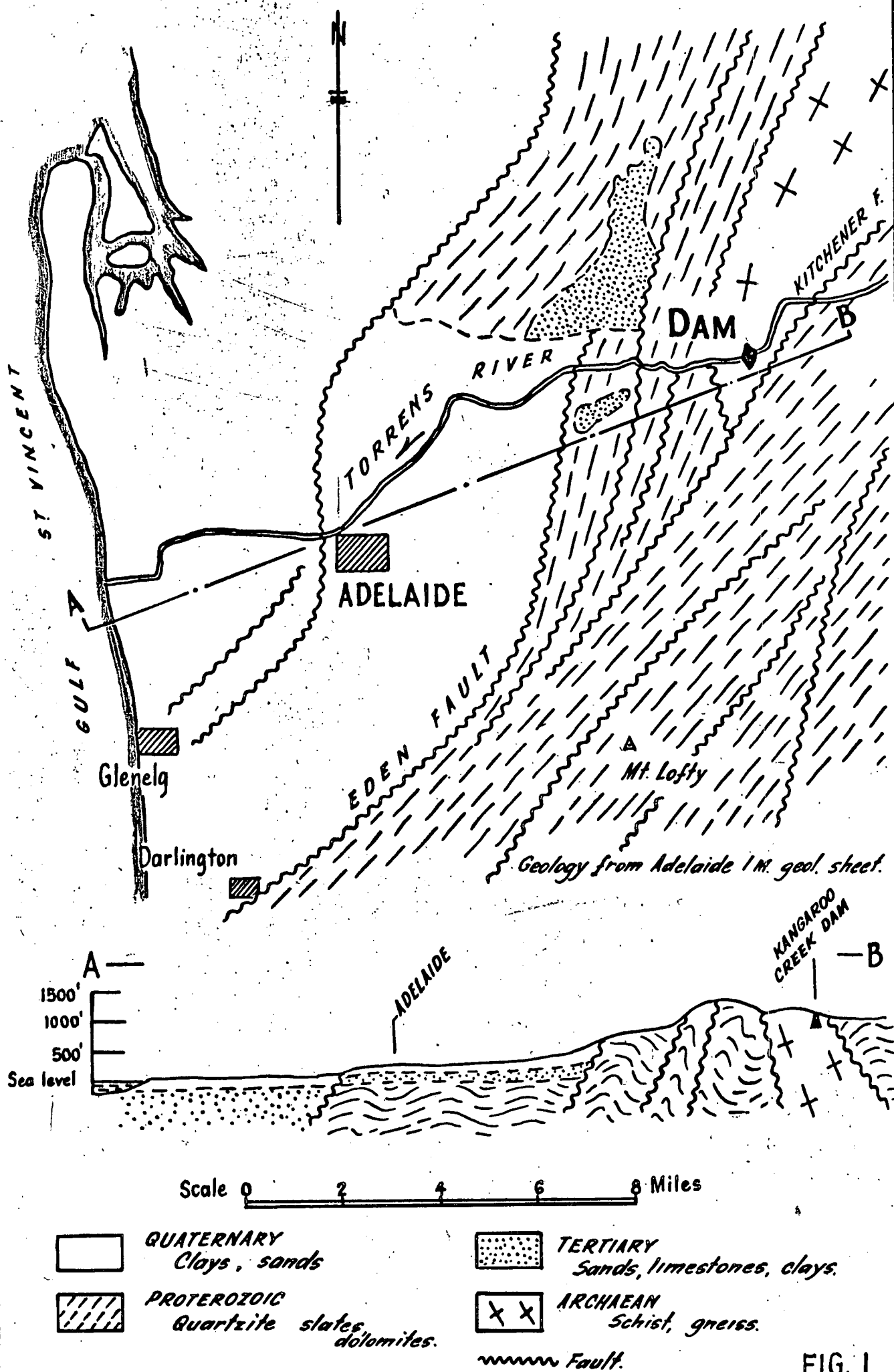


FIG. 1

DEPARTMENT OF MINES — SOUTH AUSTRALIA

ENGINEERING GEOLOGY SECTION	Drn. DRS	KANGAROO CREEK DAM LOCALITY PLAN & DIAGRAMMATIC SECTION	SCALE: <i>As shown.</i>
	Tcd. B.S.G.		S-5714 <i>Ha 5+7</i>
<i>LWP</i>	Ckd. DRS		
Director of Mines	Exd.		

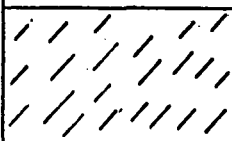
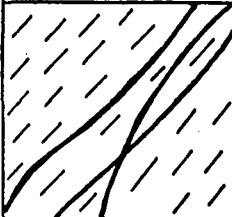
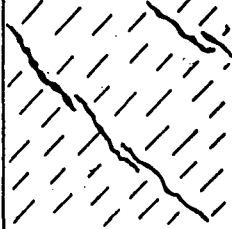
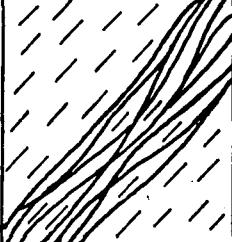
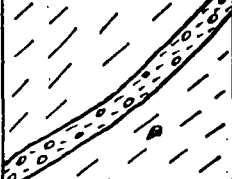
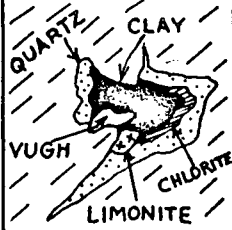
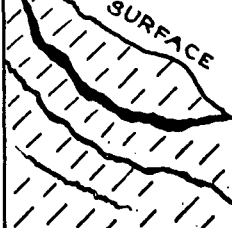
DEFECT	NAME	DESCRIPTION
	FOLIATION or SCHISTOSITY	Laminar structure formed by the parallel arrangement of tabular minerals—chlorite and sericite schist.
	JOINTS Set (i)	Almost planar, slightly curved, intersect with one another at 20 to 50 ft. intervals. Surfaces slickensided down dip; chlorite, limonite, and clay coatings.
	JOINTS Set (ii) & Set (iv)	Almost planar, mostly en echelon—single joints generally persist less than 50 ft. Surfaces rough, irregular. Slightly open or limonite- and clay-filled.
	JOINTS Set (iii)	Almost planar, slickensided
	SHEARED ZONE Set (i)	Zone of near-parallel slickensided joints which intersect one another and divide the rock into thin platy or wedge-shaped blocks. Narrow crushed seams usually present.
	CRUSHED SEAM Set (i)	Almost planar seam of mechanically disintegrated rock; commonly composed of small rock fragments in silty matrix.
	QUARTZ VEINS WITH VUGHS	Irregularly shaped veins and masses composed of quartz, chlorite limonite and clay and containing irregular cavities or vughs generally less than 2 cm. across. Not a continuous planar defect.
	EXFOLIATION JOINTS (BANKUNG)	Curved, irregular joints, almost parallel to ground surface. Many gaping or clay-filled within 10 ft. of ground surface. Generally tighter at greater depths.

FIG. 4

DEPARTMENT OF MINES — SOUTH AUSTRALIA

ENGINEERING GEOLOGY SECTION Director of Mines	Drn.DHS	KANGAROO CREEK DAM DEFINITIONS OF ROCK DEFECTS	SCALE: —
	Tcd.JPT		S 5746 Ha 5+7
	Ckd.		DATE: 21 MARCH '67
	Exd.Awf		

APPENDIX A

KANGAROO CREEK DAM

LOGS OF DIAMOND DRILL HOLES

WITH EXPLANATORY NOTES

APPENDIX A

LOGS OF DIAMOND DRILL HOLES

EXPLANATORY NOTES

INTRODUCTION

Twenty-seven holes totalling 2775ft. in depth have been drilled in the site area as part of the geological investigations for Kangaroo Creek Dam. Details of the holes are summarised below:

Hole No.	Co-ordinates*(Ft.)		Angle to Horizontal	Direction	Depth (Feet)
	E	N			
KC1	22,551	6,795	90°	-	176.7
KC2	22,605	6,815	90°	-	100.1
KC3	22,650	6,835	90°	-	75.2
KC4	22,674	6,865	45°	025°	100.0
KC5	22,703	6,933	90°	-	75.8
KC6	22,745	6,989	90°	-	75.1
KC7	22,726	7,034	90°	-	50.5
KC8	22,718	7,068	90°	-	176.0
KC10	22,477	6,751	50°	270°	70.1
KC11	22,479	6,752	55°	090°	143.3
KC12	22,721	7,159	60°	336°	135.7
KC13	22,628	6,772	65°	069°	125.2
KC14	22,630	6,773	50°	249°	131.9
KC15	22,773	7,007	70°	204°	134.8
KC17	22,691	6,810	90°	-	71.7
KC18	22,572	6,821	60°	260°	127.5
KC19	22,054	6,996	60°	225°	114.5
KC20	21,931	6,933	45°	236°	120.0
KC23	22,423	6,795	45°	265°	101.9
KC25	22,267	6,903	90°	-	99.3
KC26	22,263	6,905	40°	184°	53.3
KC27	22,249	6,786	90°	-	121.3
KC28	22,596	6,875	90°	-	100.3
KC29	22,651	7,173	60°	185°	140.0
KC30	22,624	6,974	90°	-	51.5
KC31	End of Adit No. 2		+1°	248°	50.8
KC32	End of Adit No. 1		+1°	240°	52.5

The geological logs of the holes are arranged in the same order as in this table. The notes below explain the procedures adopted in the drilling, and the various details entered on the log sheets.

*The co-ordinates used here are in feet, and are obtained from the state grid co-ordinates (given in yards) by multiplying the last four figures by 3.

NOTES ON DRILLING PROCEDURES

Equipment

The core sizes are as follows:-

<u>Symbol</u>	<u>Nominal Diameter of Cores</u>	
	<u>Inches</u>	<u>Centimetres</u>
(NXC (NX casing)	2.8	7.2
NMLC	2.0	5.1
NMS	1.8	4.6

The NMS and NMLC cores were obtained with "M" type stationary inner tube core barrels fitted with bottom discharge bits. The inner tubes were of the split type, ensuring minimum disturbance of the core during removal from the barrel.

Storing and Marking of Core

Cores are stored in wooden boxes, each compartment of which is designed to contain five feet of core. The internal length of each compartment is actually five feet one inch, to allow for 100 per cent core recovery, when roughness of the ends of the core, and small inaccuracies in measurement when breaking it to fit the box, make it difficult to fit five feet of core in a compartment of exactly that length. The boxes are marked with consecutive compartment numbers at one end, and the drilled depths from the surface in feet at the other.

The cores of most holes were boxed in this manner at the drill sites, the core being placed in its appropriate place in the box as soon as it was extracted from the core barrel. The bottom of each lift was marked with paint immediately it was placed in the box, and a corresponding paint mark was made on the side of the core box. The measured depth of the hole in feet from the surface was painted on the side of the core box and on the core. Core losses where their position was not known, were assumed to occur at the bottom of each lift. Timber blocks cut to the correct length were used to indicate core not recovered, or core removed for testing.

The cores of Drill Holes KC1 to KC8 inclusive were originally boxed by a different method, but have been re-arranged in the manner described above.

All of the cores are available for inspection at the Department of Mines, Drilling and Mechanical Branch, Dalglish Street, Thebarton, South Australia.

NOTES ON DETAILS SHOWN ON LOG SHEETS

At the head of the sheet, details of the hole are given, consisting of co-ordinates, reduced level at ground surface, angle from horizontal and direction of hole.

The angle from horizontal and direction given are as measured at the ground surface. The drill holes were not surveyed at depth, and there may be some slight deviation at depth from the figures given.

The logs are plotted on a scale of 1 inch = 10 feet (1:120). In the column headed "Log", places where core was obtained are shown by stippling, and the traces of bedding, joints, faults, and seams are shown diagrammatically by means of symbols.

Places where core was lost are shown by blank spaces. The descriptions given on the log sheet refer only to material recovered as core. Core is lost by the material being ground or washed away during the drilling process; it may usually be inferred that such material is relatively weak. Near the surface this weakness may arise from the unconsolidated nature of soils or weathered rocks. At greater depths the weakness may arise from weathering confined to narrow seams in otherwise fresh rock, or from sheared, crushed or jointed rock. It cannot always be assumed that the material not recovered is weak, since even solid rock core may be ground away and lost during drilling operations.

The core size symbol is shown on the log sheets under the heading "Size of Core."

The drilling lifts and the approximate percentage core recovery are shown in the column "Lift and Core Recovery."

In the column "Structures", angles shown on joints, bedding or other geological structures are the angles they make with the plane at 90° to the axis of the core, unless noted otherwise.

Results of water pressure tests carried out on the drill holes, to obtain some measure of the permeability of the rock mass, are shown in the column headed "Water Pressure Test."

NOTES ON WATER PRESSURE TESTING

Procedures

Drill Holes KC1 to KC8 inclusive were tested at various intervals during the drilling by sealing the hole with an expandable rubber packer placed at the base of the casing, and pumping in water at measured pressures. Considerable difficulties were experienced with these tests, and the results should be viewed with caution.

(All other holes, with the exceptions of KC31 and KC32, were water pressure tested using the single-packer method, as follows:

- a. Immediately after drilling of the test section, usually 20 feet long, the hole was cleaned out by flushing with water pumped down through the drill rods, until the returning water was clear;
- b. A mechanically expandable rubber packer in series with NX drill rods, was placed down the hole at the top of the test section and expanded to form a seal against the walls of the hole;
- c. Water was pumped into the test section between the packer and the bottom of the hole at a constant pressure measured by a pressure gauge. The pressure was maintained for a period of 15 minutes and the quantity of water pumped into the hole during this time was measured by a water meter. Without moving the packer the test was repeated at increased pressures, usually by increments of about 20lb. per sq. in., up to a maximum pressure not exceeding the weight of a column of rock of the same height as the depth of the packer below the surface;
- d. Drilling was resumed and the hole deepened a further 20 feet; this new section was then tested in the manner described above.

These tests are considered to have given reliable results. The results have been used to calculate permeability figures for the rock mass, as described below.

Calculation of Permeability Figures

The results of water pressure testing of most drill holes have been plotted as Lugeon units in the form of histograms on the logs.

One Lugeon unit is defined in Talobre (1957 p. 151-5) as a water loss of 1 litre per minute per metre of drill hole of diameter 46 to 76 mm at a pressure of 10 bars (10.2 kg/cm²) maintained for 10 minutes.

The testing procedure used on these holes has been described above. The conditions of test differed in some respects from those required by the above definition, but were sufficiently close to warrant the use of Lugeon units.

The drill holes tested were 72 mm in diameter. The length of test section was 20 feet. The water pressure applied to the test section was measured on a pressure gauge at ground surface, and maintained for a period of 15 minutes. Usually each section was tested at three different pressures.

In computing the Lugeon units in holes commenced above the water table, corrections were applied to the test data to allow for the weight of the column of water in the drill rods which thereby increased the effective pressure at the top of the test section. The leakage rate per minute was plotted in graphical form against the effective pressure acting on the test section. In no case did the effective pressure reach 10.2 kg/cm² (148 lb/sq. in.); it was assumed that the leakage was directly proportional to the effective pressure and accordingly the graph of effective pressure - leakage rate per minute per metre was extrapolated to the value of 10.2 kg/cm².

In some tests water was pumped into the test section at full pump capacity without registering any pressure in the gauge at the surface. In these places the Lugeon value has been calculated assuming that the drill rods were filled with water, although it is most likely that the rods were only partly filled because no pressure was registered. In cases such as these the actual Lugeon value would be more than that calculated and is therefore shown on the detailed log as a "minimum value."

The results of water pressure testing of drill holes has been described using the following terminology:

Low leakages	1 to 5 Lugeon units
Moderate leakages	5 to 20 " "
High leakages	20 to 50 " "

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. **1**

PROJECT **KANGAROO CREEK DAM.**

CO-ORDINATES **E 22,551
N 8,195**

R.L. **847.3 FT**

FEATURE **FOUNDATION**

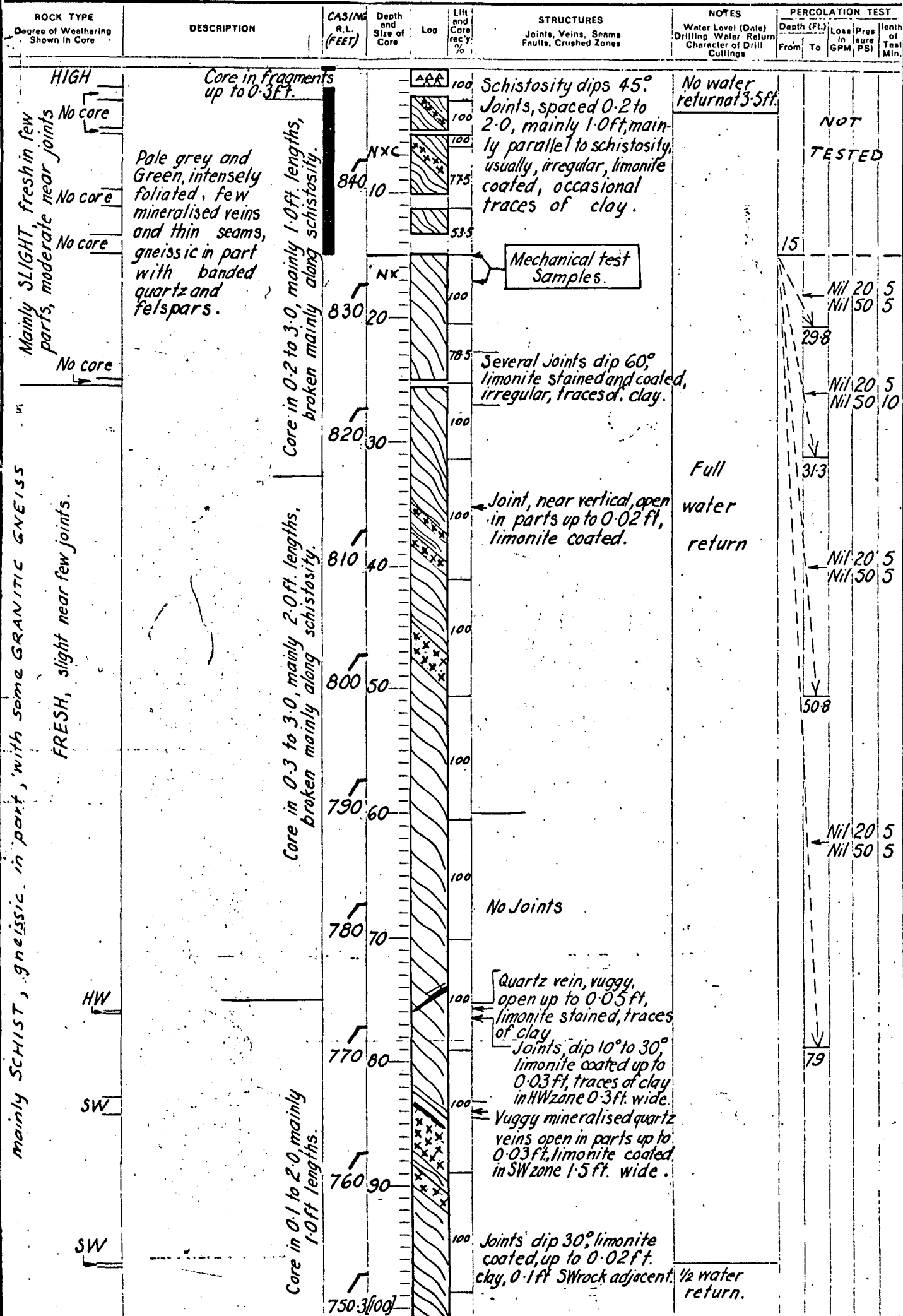
HUNDRED **ONKAPARINGA**

DIRECTION **°**

LOCATION **LEFT ABUTMENT**

SECTION **335**

ANGLE FROM HORIZONTAL **Vertical**



Drill No. **16 DD95/60**
 Type **Mindrill 1000**
 Driller **N. Thompson**
 Commenced **5 Feb 60**
 Completed **18 Feb 60**

HW highly weathered
 SW slightly



SCHIST



GRANITIC GNEISS

Logged **J.A.C.P.**
 Sheet No. **DE**
 Drawn **DE**
 Checked **DOS**
 Submitted

ins to 10 ft.
 Vert. Scale

Sheet **1** of **2**
53802
 Drawing No. **Has 7**

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE
 E 22, 551

Hole No. 1

PROJECT KANGAROO CREEK DAM

CO-ORDINATES N 6.795

R.L. 847.3 FT

FEATURE FOUNDATION

HUNDRED ONKAPARINGA

DIRECTION —

LOCATION LEFT ABUTMENT

SECTION 335

ANGLE FROM HORIZONTAL Vertical

ROCK TYPE Degree of Weathering Shown in Core	DESCRIPTION	CASING R.L. (FEET)	Depth and Size of Core	Log	Lift and Core rec'y %	STRUCTURES Joints, Veins, Seams Faults, Crushed Zones	NOTES Water Level (Date) Drilling Water Return Character of Drill Cuttings	PERCOLATION TEST Depth (Ft.) From To Loss in GPM PSI Length of Test Min.
SCHIST FRESH No core SW	Pale grey, grey - green, mainly intensely foliated.	740	110	100	100	Joint, dip 45° limonite and clay coated. Schistosity dips 40° to 60° contorted in parts. Joints dip 40° to 60° Spaced 0.2 to 2.0 ft, mainly 0.5 ft, mainly along schistosity, usually limonite stained. Joints, irregular dip 30° to 60°, limonite coated SW rock adjacent.	1/2 water return	FROM 15 ft. 6 20 5 26 50 5 109
GNEISS FRESH	Pale grey and whitish, banded, medium grained.	730	120	50	50			20 20 10 46 50 4
GNEISS No core		720	130	100	100	Vuggy quartz, irregular, mineralised, open in parts up to 0.03 ft, limonite stained.	No water return at 127.6 ft	127.5 20 20 8
GNEISS No core		710	140	95	95	Joints, irregular, limonite coated, mineralised, dip 70° to 80° Sample.	Hole cemented	131.3 15 20 12
SCHIST FRESH		700	150	98	98			136.5 15 20 8
GNEISS FRESH TO SLIGHT No core	Pale grey to whitish, medium to coarse grained.	690	160	100	100	Mineralised quartz vein, Vuggy, open in parts up to 0.05 ft, limonite coated. Sample.	1/2 water return.	144.4 14 20 10
SCHIST FRESH		680	170	100	100	Joints dip 30 to 70°, lim- onite coated, mineralised. Joints, near vertical, lim- onite stained, mineralised.		154.2 12 20 8
		673.7		100	100			176.7
						176 Feet. END OF HOLE.		

Drill No. 16 DD 95/60
 Type Mindrill 1000
 Driller N. Thompson
 Commenced 5th Feb. 1960
 Completed 18 Feb. 1960

EXPLANATION



SCHIST



GRANITIC GNEISS

SW. slightly weathered

Water
level,
data

Logged
Sheet No.
Drawn
Checked
Submitted

J.A.C.P.
D.E.
DMS

1 inch = 10 feet.
Vert. Scale.

Sheet 2 of 2
 338020 Has 7
 Drawing No.

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. **2**

PROJECT **KANGAROO CREEK DAM**

CO-ORDINATES **N 6815 E 22605**

R.L. **800.6 FT**

FEATURE **FOUNDATION**

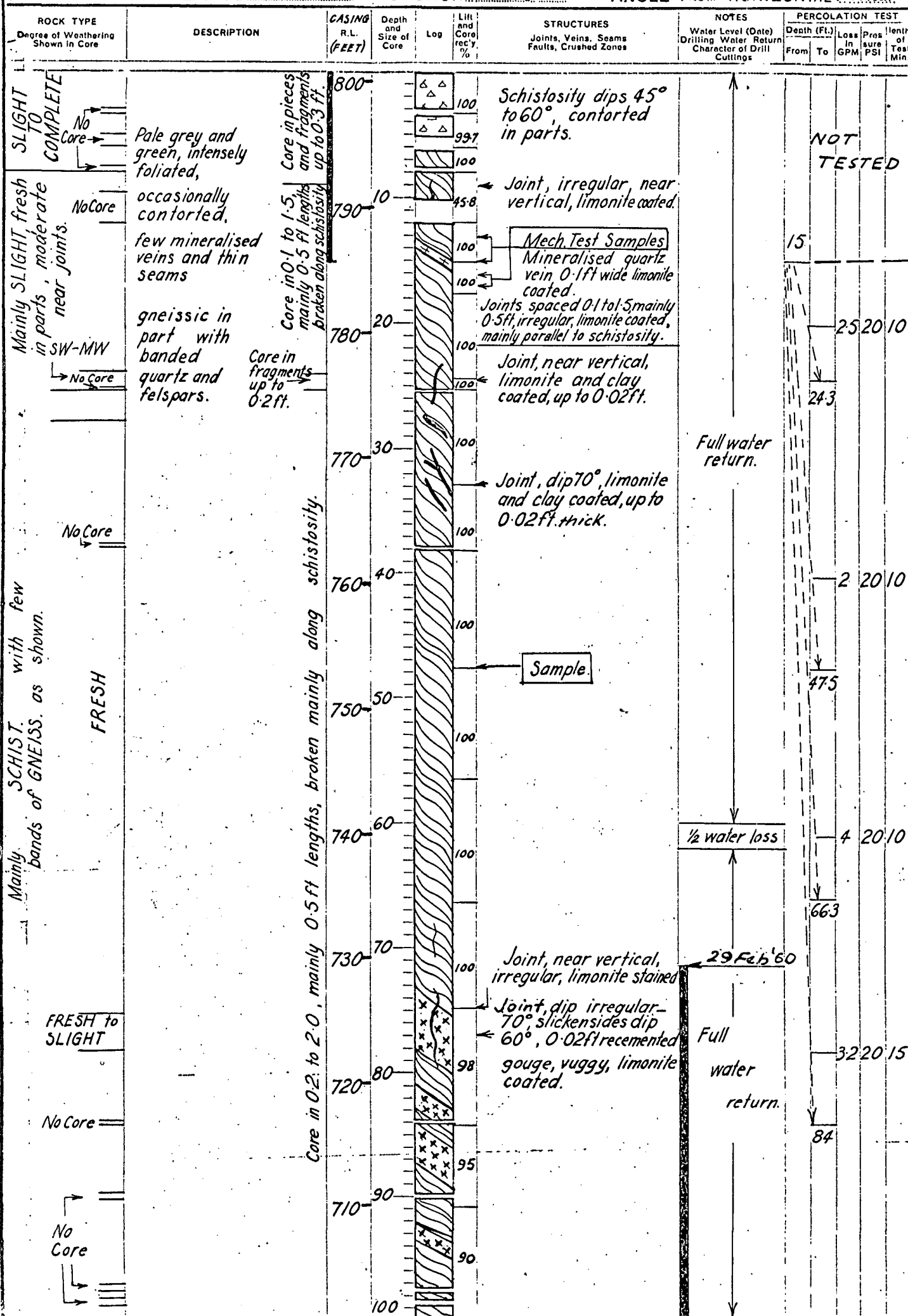
HUNDRED ONKAPARINGA

DIRECTION **Vertical**

LOCATION **LEFT ABUTMENT**

SECTION **335**

ANGLE FROM HORIZONTAL **Vertical**



Drill No. **16DD105/60**
 Type **Mindrill E1000**
 Driller **N. Thompson**
 Commenced **24 Feb '60**
 Completed **29 Feb '60**

SCHIST
GRANITIC GNEISS

29 Feb '60
 WATER LEVEL, DATE

Logged
 Sheet No.
 Drawn
 Checked
 Submitted

J.A.C.P.
D.E.
D.K.

10 feet = 1 inch.
 Vert. Scale
 Sheet **1** of **1**
33801
 Drawing No. **H05+7**

E 22,650

CO-ORDINATES N. 6,835

R.L. 756.7 FT

HUNDRED ONKAPARINGA

DIRECTION —

SECTION 335

ANGLE FROM HORIZONTAL 90°

[illegible]

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. 4

PROJECT KANGAROO CREEK DAM

CO-ORDINATES N. 6,865 E 22,674

R.L. 724 FT

FEATURE FOUNDATION

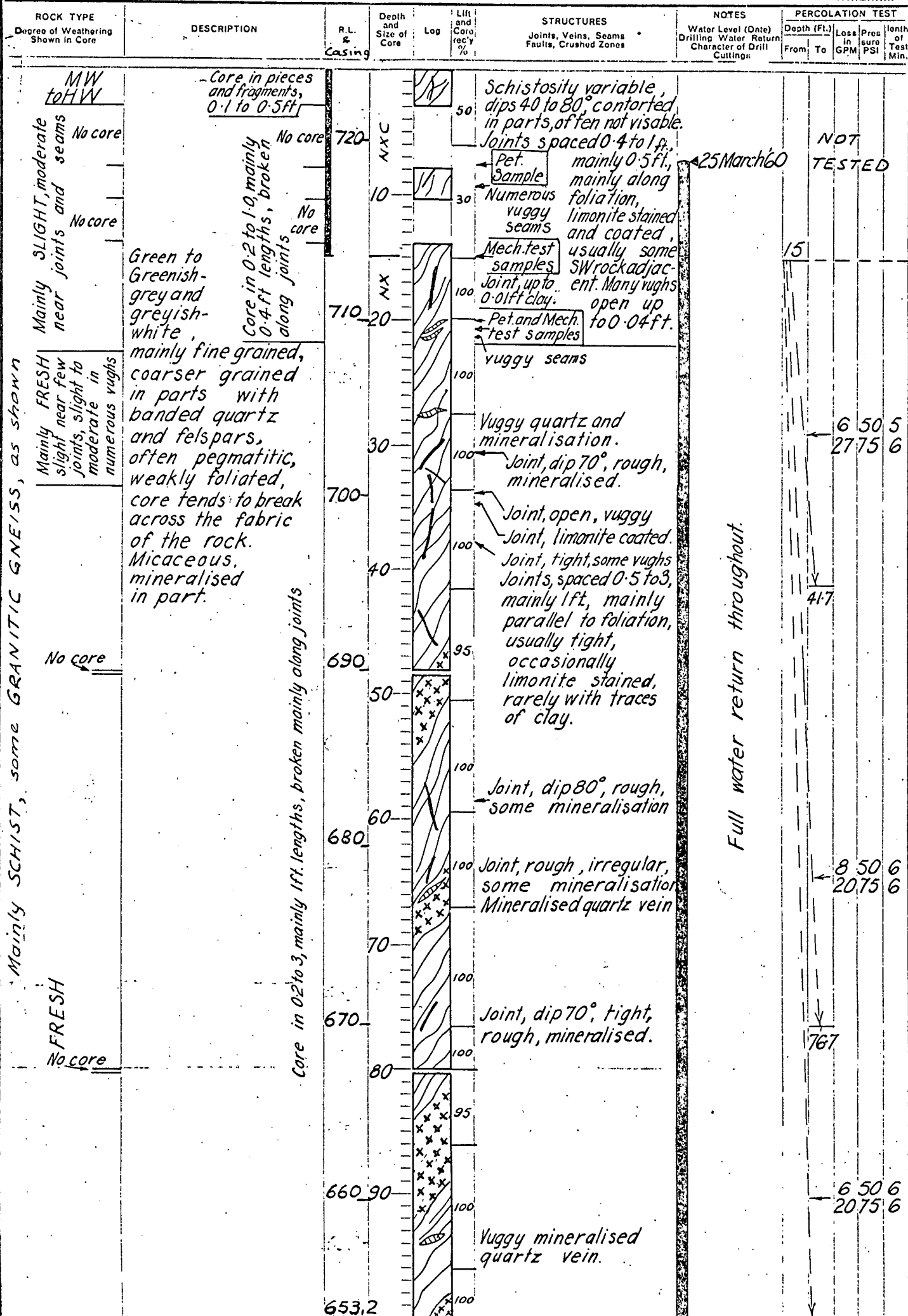
HUNDRED ONKAPARINGA

DIRECTION 025°

LOCATION RIVER CHANNEL

SECTION 335

ANGLE FROM HORIZONTAL 45°



Full water return throughout.

Drill No. 7.D.D. 115/60
Type Mindrill E1000
Driller M. Sharrad
Commenced 18 March 60
Completed 25 March 60

MW Moderately Weathered
HW Highly Weathered

Water level
Pet. Petrographic
Mech. Mechanical

Date, water level.

Logged
Date
Drawn
Checked
Submitted

J.A. Painter
July 64
D.E.
DPS

10 ft to 1 inch
Vert. Scale
Sheet of
33832 Ha517
Drawing No.

GEOLOGICAL LOG OF DRILL HOLE

E 22,703

PROJECT KANGAROO CREEK DAM

CO-ORDINATES N 6,933

R.L.721-9 FT

FEATURE FOUNDATION

HUNDRED YATALA

DIRECTION _____

LOCATION RIGHT ABUTMENT

SECTION 5497

ANGLE FROM HORIZONTAL 90.....°

ROCK TYPE Degree of Weathering Shown in Core	DESCRIPTION	R.L. & Casing	Depth and Size of Core	Log	Lift and Core rec'y %	STRUCTURES Joints, Veins, Seams Faults, Crushed Zones	NOTES Water Level (Dial) Drilling Water Return Character of Drill Cuttings	PERCOLATION TEST			
								Depth (Ft.) From To	Loss in GPM	Pres- sure PSI	Length of Test Min.
No core	No core		720	X X X		Joint rough, grooved, limonite coated. Foliation dips 30 to 50°					
SLIGHT	Dark grey to greenish grey foliated	No core	710	/ / /		Joints spaced 0.3 to 1.5, mainly lft, mainly parallel to schis- tosity, mainly tight, lim- onite stained and coated above 15 ft. Joints at angle to foliation, usually rough and irregular, often mineralised.		10			
No core	Micaceous	No core		x x x		Mainly very fine grained, coarser grained in parts with banded quartz and felpars becoming coarse grained and pegmatitic in parts.			15	50	3
			700	+ + +							
			690	- - -		Joints, dip 40 to 70° irregular, limonite coated, some quartz mineralisation.					
			680	* * *		Joint, dip 70°, irregular, mineralised.					
			670	. . .		Joints, dip 40°, tightly closed, limonite coated					
			660			Seam, 0.1 ft, chlorite, quartz and pyrite Joints, rough, mineralised					
			650	.		Joint, 0.01 ft, CW rock vuggy quartz adjacent					
			646.1	.		Mineralised seam, up to 0.03 ft, vuggy.					
								68.4			
</											

Drill No. 7 (D.D. 120/60)

Type *Mindrill E1000*Driller: M. SharradCommenced 30 March 60Completed 4 April 1960

GNEISS, schistose
in part.

GRANITIC GNEISS

Logged

LACP.

Sheet No.

.....
D.E

Drawn

... ..
DH

Submitted

10 feet to 1 inch
Vert. Scale.....

Sheet 1 of 1

S3829 Hd5+7

Drawing No.

250--7.60 8036

GEOLOGICAL LOG OF DRILL HOLE

E 22,745

PROJECT KANGAROO CREEK DAM

CO-ORDINATES N. 6989

R.L. 804.7 FT

FEATURE FOUNDATION

HUNDRED YATALA

DIRECTION

LOCATION RIGHT ABUTMENT

SECTION 5497

ANGLE FROM HORIZONTAL 90°

ROCK TYPE Degree of Weathering Shown in Core	DESCRIPTION	R.L. & Casing	Depth and Size of Core	Log	Lift and Core Rec'y %	STRUCTURES Joints, Veins, Seams Faults, Crushed Zones	NOTES Water Level (Date) Drilling Water Return Character of Drill Cuttings	PERCOLATION TEST Depth (Ft.) From To Loss in GPM Pres sure PSI Length of Test Min.
SCHIST, gneissic in part No core	Pale green to pinkish white, medium to coarse grained, foliated or weakly banded in parts, core tends to break across the foliation; micaceous, numerous, vuggy and mineralised quartz veins, frequent pyritic mineralisation	800	NXC	95		Foliation dips 30 to 60°	Water lost at 3 and 13 ft.	NOT TESTED
		790	NX	100		Joint, limonite-coated		
		780	NX	100		Irregular vuggy quartz vein, limonite and clay-coated		
		770	NX	100		Joint, limonite-coated. Joints spaced 0.2 to 2.5, mainly 1 ft., limonite stained and coated, often with traces of clay.		
		760	NX	100		Irregular, vuggy quartz veins, limonite and clay-coated		
		750	NX	100		Joints, mainly parallel to foliation.		
		740	NX	100		Joints, rough, limonite coated. Vuggy quartz veins, clay and limonite coated.		
		730	NX	100		Joints, limonite coated, up to 0.01 ft.		
			NX	100		Vuggy quartz veins, SW to CW, limonite stained.		
			NX	90		Joint, limonite coated, vuggy quartz mineralisation.		
			NX	100		Vuggy quartz veins, limonite coated.		

75.1 ft. END OF HOLE

Drill No. DD. 107/60
Type Mindrill E1000
Driller M. Sharrod
Commenced 1 March 60
Completed 7 March 60

Water level  Date

Logged J.A.C.P.
Sheet No. DE
Drawn DE
Checked DHJ
Submitted

10 ft to 1 inch.
Vert. Scale
Sheet 1 of 1
S3830 Ha5+7
Drawing No.

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. 7

PROJECT KANGAROO CREEK DAM

CO-ORDINATES N. 7,034

R.L. 835.8 FT

FEATURE FOUNDATION

HUNDRED YATALA

DIRECTION

LOCATION RIGHT ABUTMENT

SECTION 5497

ANGLE FROM HORIZONTAL 90°

ROCK TYPE Degree of Weathering Shown in Core	DESCRIPTION	R.L. casing	Depth and Size of Core	Log	STRUCTURES Joints, Veins, Seams Faults, Crushed Zones	NOTES Water Level (Date) Drilling Water Return Character of Drill Cuttings	PERCOLATION TEST Depth (Ft.) From To Loss in GPM PSI Length of Test Min.
No Core	SW to HW Core in fragments up to 0.2 ft	No Core			Schistosity dips 30° to 50°	Hole blocked at 12. Static water level not determined.	NOT TESTED
No Core	Dark grey to greenish grey, pinkish white. Were gneissic, closely foliated, very fine grained, coarser grained with banded quartz and feldspars where gneissic, micaceous, common vuggy mineralised quartz veins	No Core	830	70	Vuggy quartz	Joints spaced 0.2 to 1, mainly 0.5 ft, limonite coated, mainly parallel to foliation	Water lost at 6 ft. Full water return after casing seated.
No Core	SLIGHT, moderate to high near joints and seams.	No Core	820	100	Sample, MECH. TEST		18 15 10
No Core	Core in 0.1 to 1, mainly 0.4 ft broken along joints and foliation.	No Core	810	100	Joints, rough, limonite coated up to 0.03 ft.		17.7
No Core	Core in 0.2 to 2 mainly 1 ft lengths broken mainly along foliation	No Core	800	100	Joint, dip 50°, limonite coated		Nil 15 9
No Core		No Core	790	95	Joint, tight, irregular, limonite coated.		233
No Core		No Core	780	95	Vuggy quartz veins, limonite coated, mineralised.		25 15 10
No Core		No Core	770	95	Joints, rough, irregular, limonite coated.		
No Core		No Core	760	95	Joints, rough, limonite coated, some vuggy mineralisation.		
No Core		No Core	750	95	Joints spaced 0.4 to 4, mainly 1 ft. limonite coated, rough usually tightly closed		

50.5 feet END OF HOLE

505

Drill No. 7 (DD 102/60)

Type Mindrill E 1000

Driller M.E. Sharrad

Commenced 24 Feb 1960

Completed 26 Feb 1960

SW Slightly Weathered
HW Highly Weathered.

Logged

J.A.C.P.

Sheet No.

Drawn

Checked

Submitted

D.E.

D.R.S.

10 feet to 1 inch
Vert. Scale

Sheet 1 of 1

53831 H05-7

Drawing No.

250-7.60 8038

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. 8

PROJECT KANGAROO CREEK DAM CO-ORDINATES N. 7,068 E 22,716

R.L. 849.5 FT

FEATURE FOUNDATION

HUNDRED YATALLA

DIRECTION

LOCATION UPPER RIGHT ABUTMENT SECTION 5497

ANGLE FROM HORIZONTAL 90°

ROCK TYPE Degree of Weathering Shown in Core	DESCRIPTION	Casing R.L. feet.	Depth and Size of Core Log	Lift and Core rec'y %	STRUCTURES Joints, Veins, Seams Faults, Crushed Zones	NOTES Water Level (Date) Drilling Water Return Character of Drill Cuttings	PERCOLATION TEST Depth (Ft.) From To Loss in GPM Pres. in PSI Length of Test Min.
Soil and rock fragments		NX	Δ X	25			
NO CORE		NXC		45			
Moderately weathered		840	10			FULL WATER RETURN Water lost. at 10 regained at 11 ft.	NOT TESTED
No CORE							
GRANITIC GNEISS	Pale green to white-banded granitic gneiss				SAMPLES MECHANICAL TESTS Foliation dips 30° to 40° Joints spaced 0.2 to 1.5 feet, predominantly 0.5 feet; limonite stained, irregular surfaces. Most joints parallel to foliation, few dip 60 to 80°. Several vuggy quartz veins, with lenticular cavities up to 0.05 ft. across occur as shown.	Full water return	Nil 10 10
Mainly Slight, Moderate to high near some joints and vughs.		830	20				20 3 10 10
		820	30			1/2 water return	
Slightly weathered	White to pale grey, schistose, slightly banded, fine grained.	810	40				1 10 10
		800	50			Full water return	50
		790	60				Nil 10 10
		780	70				70
		770	80		Joints spaced 0.2 to 2 feet, mainly 1 foot. Most are parallel to foliation, few dip 70° to 80°. The joints are limonite stained or coated with irregular surfaces, polished in some cases. Several vuggy quartz veins with lenticular cavities up to 0.05 ft. across occur as shown.		Nil 10 10
		760	90				
GRANITIC GNEISS	Pale green, Coarse grained quartz felspar rock, with poorly developed foliation dipping approx 45°	750	100				97.5

Drill No. 7
Type Mindrill E1000
Driller M.E. Sharrad
Commenced 5 Feb '60
Completed 19 Feb '60

EXPLANATION
Casing
Static Water Level
10th March 1960

Logged
Sheet No.
Drawn
Checked
Submitted
E.R. Hillwood
D.H. Stapledon
D.E.
D.K.

10 ft. to lynch.
Vert. Scale
Sheet 1 of 2
53774a
Drawing No.
Ha 5+7
250-7.60 6033

GEOLOGICAL LOG OF DRILL HOLE

PROJECT KANGAROO CREEK DAM CO-ORDINATES E 22,716 R.L. 849.5 FTFEATURE FOUNDATION HUNDRED YATALA DIRECTION —LOCATION RIGHT ABUTMENT SECTION 5497 ANGLE FROM HORIZONTAL 90°

ROCK TYPE Degree of Weathering Shown in Core	DESCRIPTION	R.L. Casing	Depth and Size of Core	Log	Lift and Core rec'd of 70	STRUCTURES Joints, Veins, Seams Faults, Crushed Zones	NOTES Water Level (Date) Drilling Water Return Character of Drill Cuttings	PERCOLATION TEST Depth (Ft.) From To Loss in GPM PSI Month of Test
GRANITIC GNEISS Fresh	Pale green, coarse grained, poorly foliated					Vuggy quartz vein dip 35°, 0.05 feet thick.		FROM 13 FEET
Mainly SERICITE GNEISS with some GRANITIC GNEISS, as shown.	Grey to white, shows pronounced banding, contorted in part.		740-110			Joints spaced from 0.3 to 4 ft, predominantly 2 feet, mostly parallel to schistosity, few nearly vertical Joint surfaces mostly clean.	19 Feb '60	15 10 10
GRANITIC GNEISS			730-120					126
FRESH			720-130					
			710-140					2 10 15
FRESH			700-150			Calcite vein, tightly sealed contacts.		
			690-160					160
	Becoming finer grained and less banded.		680-170					15 10 15
GRANITIC GNEISS	Off-white, massive.		673.8					176

176 FEET, END OF HOLE

Drill No. 7
 Type Mindrill E1000
 Driller M.E. Sharrad
 Commenced 5 Feb. 60
 Completed 19 Feb. 60

Casing

EXPLANATION

Static Water Level
 10" March
 1960

Logged
 Sheet No.
 Drawn
 Checked
 Submitted

E.R. Hillwood
 D.H. Stapledon

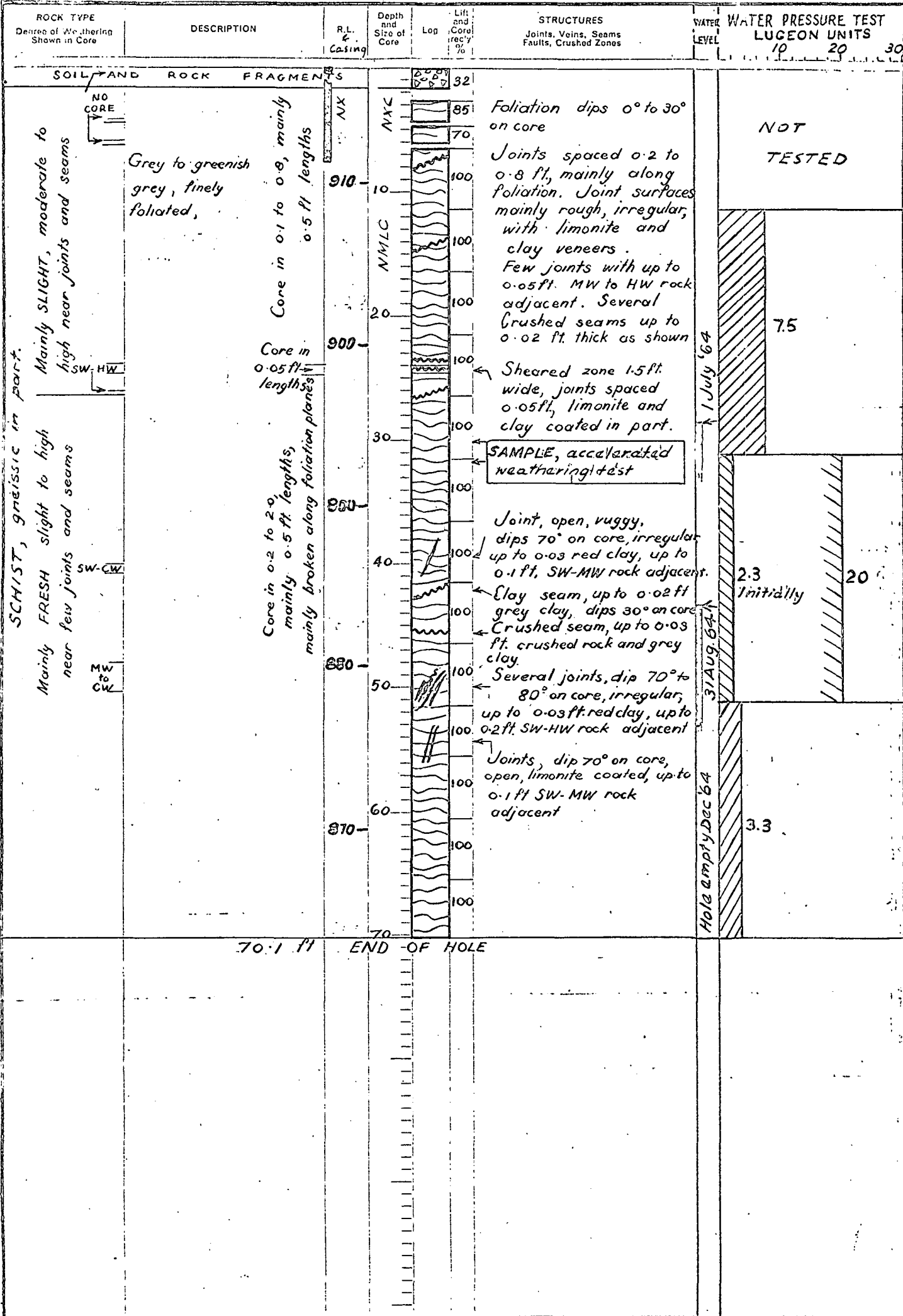
D.E.
 DAS

10 ft to 1 inch.
 Vert. Scale
 Sheet 2 of 2
 Drawing No. 53774
 Ha 5+7
 250-7.60 8036

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. 10

PROJECT KANGAROO CREEK DAM CO-ORDINATES E. 22,477 N. 6,751 R.L. 916.8 FT
FEATURE FOUNDATION HUNDRED Onkaparinga DIRECTION 270°
LOCATION UPPER LEFT BANK SECTION 335 ANGLE FROM HORIZONTAL 50°



Drill No. 24
Type MINDRILL E 1000
Driller J. Jensen
Commenced 25 June '64
Completed 1 July '64

EXPLANATION

SW slightly weathered
MW moderately "
HW highly "
CW completely "

WATER LEVEL DATE

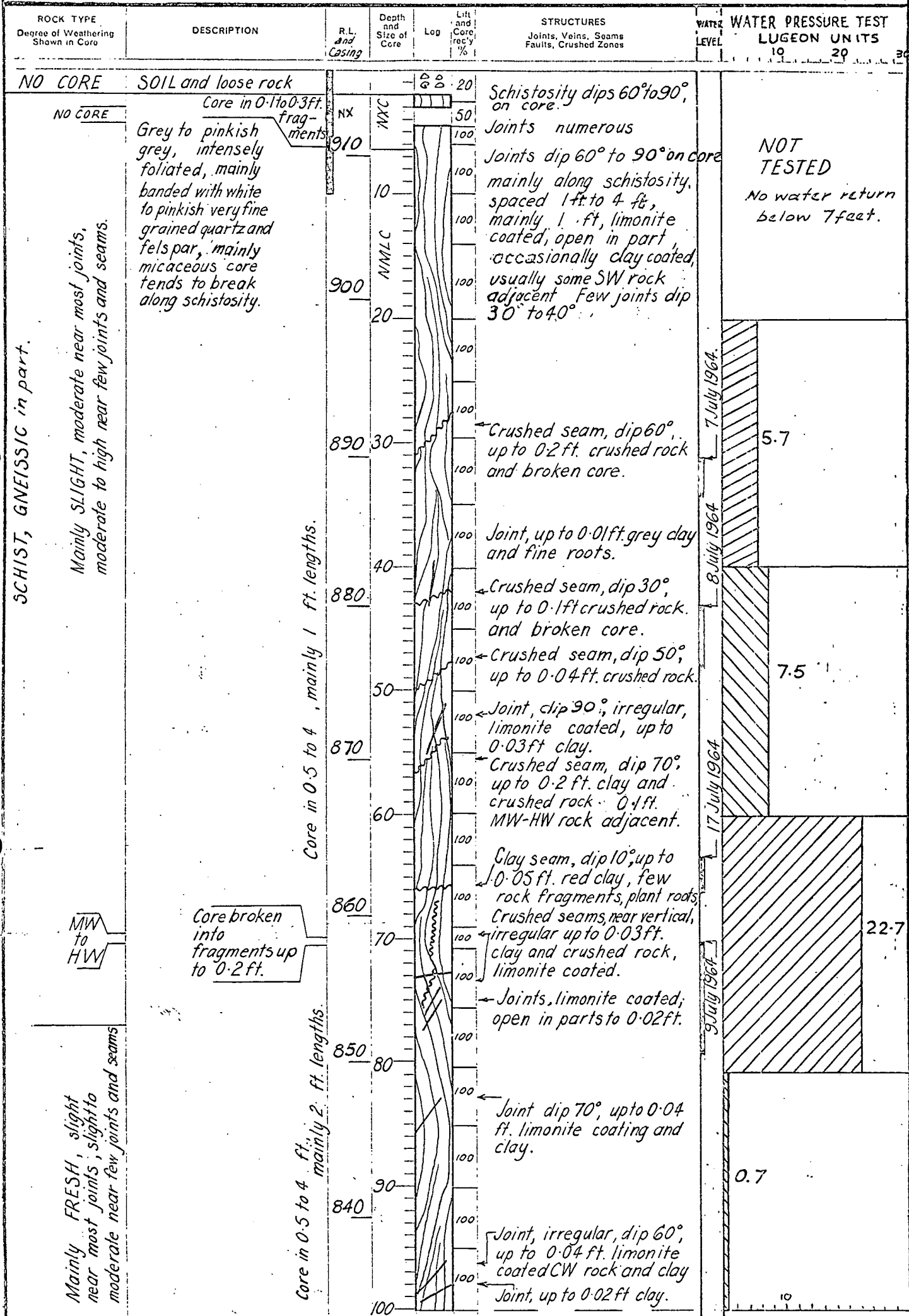
Logged J.A.C.P.
Date 2 July '64
Drawn J.A.C.P.
Checked DMS
Submitted

Vert. Scale 1" = 10 ft
Sheet 1 of 1
S 3767
Drawing No. Ho. 5+7
250-7.60 C336

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. 11

PROJECT KANGAROO CREEK DAM CO-ORDINATES E 22,479 N 6,752 R.L. 915 FT
FEATURE FOUNDATION HUNDRED ONKAPARINGA. DIRECTION 090°
LOCATION UPPER LEFT BANK SECTION 335 ANGLE FROM HORIZONTAL 55°



Drill No. 24
Type Mindrill E 1000
Driller J. Jensen
Commenced 3 July 1964
Completed 17 July 1964

EXPLANATION
All dip measurements made on core.
SW Slightly weathered
MW Moderately "
HW Highly "
CW Completely "

WATER LEVEL DATE
Casing.

Logged JACP
Date 17 July 64
Drawn JACP
Checked D.H.S.
Submitted

lin. = 10 ft.
Vert. Scale

Sheet 1 of 2
53790 Ha5+7
Drawing No.

250-7.60 2326

E 22,479

CO-ORDINATES N 6,752

R.L. 9/5 FT

HUNDRED ONKAPARINGA

DIRECTION 090°

SECTION 335

ANGLE FROM HORIZONTAL 55 °

WATER LEVEL	WATER PRESSURE TEST LUGEON UNITS			
	10	20	30	
	< 0.5			
	< 0.5			

Hole Empty, Dec '64

143.3 feet. END OF HOLE.

Drill No. <u>24</u>	EXPLANATION	WATER LEVEL	DATE	Logged	<u>JACP</u>	1 ins = 10 ft.
Type <u>Mindrill F1000</u>				Date	<u>17 July '64</u>	Vert. Scale
Driller <u>J. Jensen</u>				Drawn	<u>JACP</u>	Sheet <u>2</u> of <u>2</u>
Commenced <u>3 July '64</u>				Checked	<u>DHS</u>	<u>53790445+7</u>
Completed <u>17 July '64</u>				Submitted		Drawing No.
						250-7.60 9033

GEOLOGICAL LOG OF DRILL HOLE

CO-ORDINATES

E. 22,721
N. 7,159

R.L. 904 FT

4 HUNDRED

YATAI A

DIRECTION 338

SECTION 5497

ANGLE FROM HORIZONTAL 60

 ≤ 0.5

Completed 2 Sept. '64.

WATER LEVEL

DATE

Subvivi

.....

S3865 Hq54

Drawing No.

250-7,60 2035

HOLE No. 12

SERIAL No.....

GEOLOGICAL LOG OF DRILL HOLE

SHEET.....2.....OF.....2.....

PROJECT KANGAROO CREEK DAM

CO-ORDINATES *E.22,721 N.7159*

R.L. 904

FEATURE FOUNDATION

HUNDRED YATA LA

DIRECTION 338.

LOCATION: UPPER RIGHT ABUTMENT

SECTION 5497

.....DIRECTION 000
ANGLE FROM HORIZONTAL 60°

[illegible]

DRILL No. 24.....

TYPE E1000

DRILLER Jensen

COMMENCED 25.Aug.'64.

COMPLETED ... 2 Sept '64.

EXPLANATION

CASING IN HOLE DURING DRILLING

X / SERICITE GNEISS

x x x GRANITIC GNEISS

SSS CHLORITE SCHIST

WATER LEVEL IN DRILL HOLE n ← (DATE)

HW Highly weathered

SW Slightly weathered

ENGINEERING GEOLOGY AND
SOILS SECTION

LOGGED BY DHS

DRAWN BY DE

CHECKED BY.....DIV.....

DRAWING No. 538650.H05

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. 13

PROJECT KANGAROO CREEK DAM

CO-ORDINATES

E 22,828
N 6,772

R.L. 807.8 FT

FEATURE FOUNDATION

HUNDRED ONKAPARINGA

DIRECTION 069°

LOCATION LEFT BANK

SECTION 33.5

ANGLE FROM HORIZONTAL 65°

ROCK TYPE Degree of Weathering Shown in Core	DESCRIPTION	R.L.	Depth and Size of Core	Log	Lift and Core Rock %	STRUCTURES Joints, Veins, Seams Faults, Crushed Zones	WATER PRESSURE TEST LUGEON UNITS 10 20 30
SCHIST FRESH	Green to greenish-grey, intensely foliated, very fine-grained, micaceous, common pyritic mineralisation Core in 0.5 to 4 ft. mainly 2 ft lengths Core in 0.05 to 0.5 ft. fragments	710 110 700 120 690.7	NMLC	100 100 100 100 100		Few joints, spaced 0.5 to 4 ft, tight, usually rough, mainly parallel to cleavage Mineralised seam. SHEARED, partly crushed zone, 1 ft. wide Mineralised seam, friable, pyrite and chlorite. Drill water lost	33 Minimum NOT TESTED
						125.2 feet. END OF HOLE	

Drill No. 4
Type Mindrill E1000
Driller J. Jensen
Commenced 30 July '64
Completed 12 Aug. '64

EXPLANATION

WATER LEVEL DATE

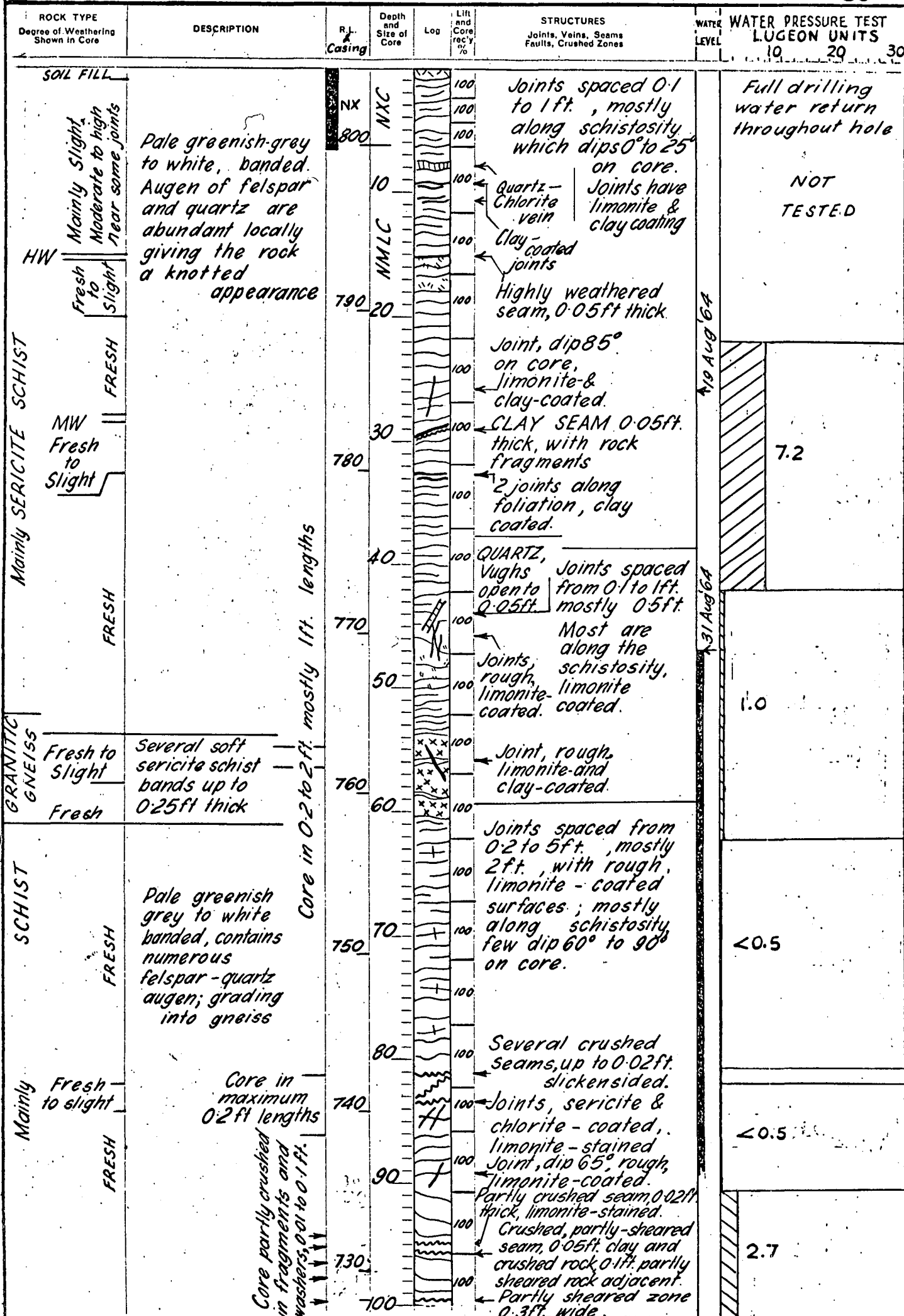
Logged JACP
Date 13 Aug. '64
Drawn D.E.
Checked DMS
Submitted

10ft to 1 inch
Vert. Scale
Sheet 2 of 2
53823a H05.7
Drawing No.

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. 14

PROJECT KANGAROO CREEK DAM CO-ORDINATES E 22,630 N 6773 R.L. 805 FT
FEATURE FOUNDATION HUNDRED ONKAPARINGA DIRECTION 24.9°
LOCATION LEFT ABUTMENT SECTION 335 ANGLE FROM HORIZONTAL 50°



Drill No. 24
Type Mindrill E1000
Driller Jensen
Commenced 14 Aug 64
Completed 29 Sept 64

EXPLANATION
SCHIST
GRANITIC GNEISS
HW Highly weathered
MW Moderately weathered.

WATER LEVEL DATE

Logged
Sheet No.
Drawn
Checked
Submitted

DH.5
20 Aug 64
T.P.S.
DHS

10 ft to lynch
Vert. Scale

Sheet 1 of 2
S3836
Ha5+7

PROJECT **KANGAROO CREEK DAM** CO-ORDINATES **E 22630 N 6773** R.L **805** FT
 FEATURE **FOUNDATION** HUNDRED **ONKAPARINGA** DIRECTION **249** °
 LOCATION **LEFT ABUTMENT** SECTION **335** ANGLE FROM HORIZONTAL **50** °

Drill No. <u>24</u>	EXPLANATION		Logged	<u>J.A.C.P.</u>	Vert. Scale <u>10ft = 1 in</u>
Type <u>Mindrill E 1000</u>	☒ SCHIST	WATER LEVEL	Date	<u>5 Nov '64</u>	Sheet <u>2</u> of <u>2</u>
Driller <u>J. Jensen</u>	☒ GRANITIC GNEISS		Traced	<u>T.P.S.</u>	<u>S3836</u>
Commenced <u>14 Aug '64</u>			Checked	<u>DHS</u>	<u>Ha 5+7</u>
Completed <u>19 Aug '64</u>			Submitted		
					250-7.60 8036

GEOLOGICAL LOG OF DRILL HOLE

PROJECT KANGAROO CREEK DAM

CO-ORDINATES E22773 N7007

R.L. 825.6 FT

FEATURE FOUNDATION

HUNDRED

YATALA

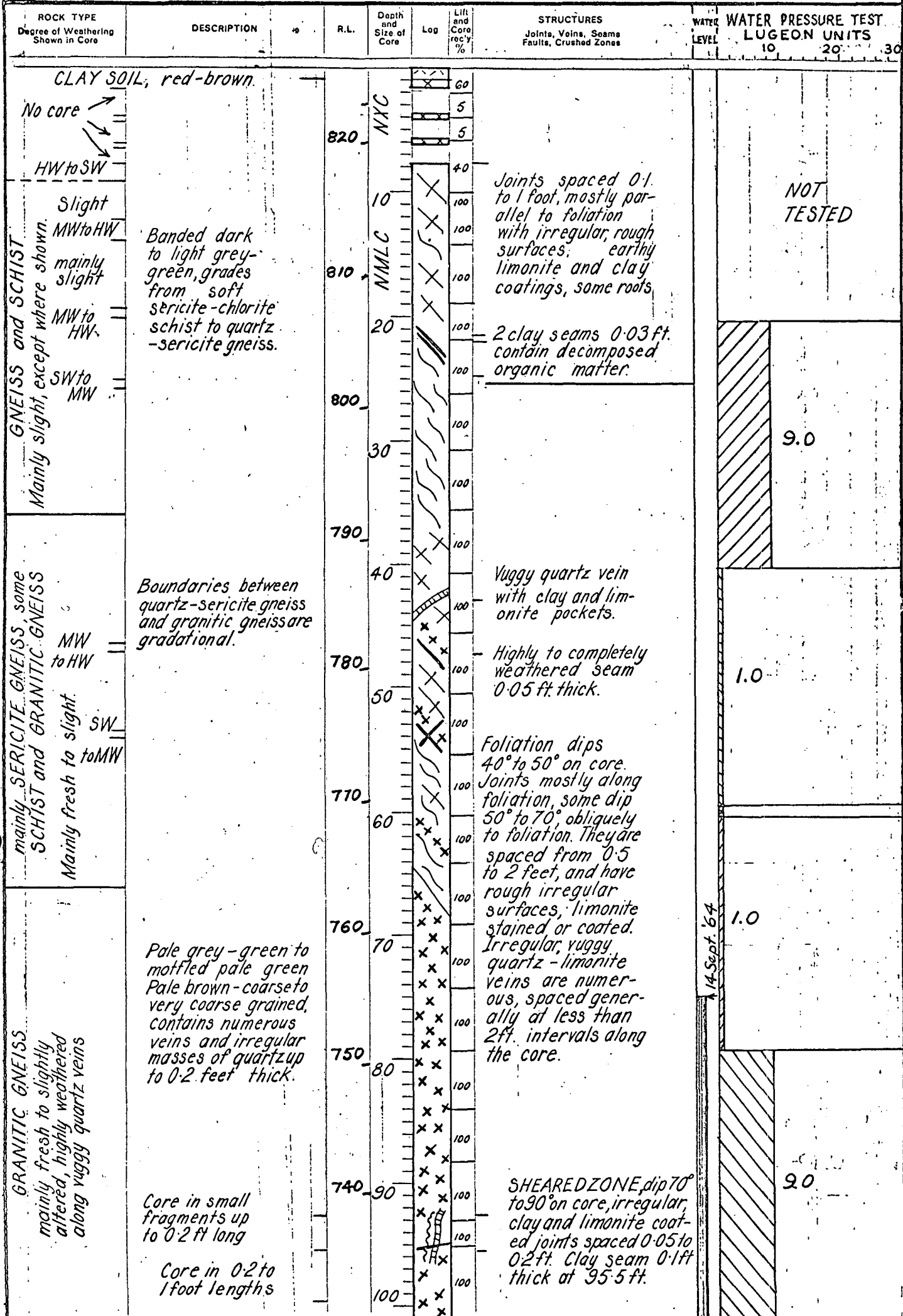
DIRECTION 204°

LOCATION RIGHT ABUTMENT

SECTION

5497

ANGLE FROM HORIZONTAL 70°



Drill No. 24

Type Mindrill E1000

Driller Jensen

Commenced 4 Sept. 64

Completed 14 Sept. 64

EXPLANATION



SCHIST

WATER LEVEL

DATE



GNEISS



GRANITIC GNEISS

Logged

Date

Drawn

Checked

Submitted

D.H.S.

11 Sept. 64

D.R.P.E.

D.R.

10 feet to ins.

Vert. Scale

Sheet 1 of 2

S3888 Ha5+7

Drawing No.

ES-7.60 6038

GEOLOGICAL LOG OF DRILL HOLE

PROJECT KANGAROO CREEK DAM

CO-ORDINATES E 22773 N7007

R.L. 825.6 FT

FEATURE FOUNDATION

HUNDRED YATALA

DIRECTION 204 °

LOCATION RIGHT ABUTMENT

SECTION 5497

ANGLE FROM HORIZONTAL 70 °

ROCK TYPE Degree of Weathering Shown in Core	DESCRIPTION	R.L.	Depth and Size of Core	Log	Lift and Core rec'y %	STRUCTURES Joints, Veins, Seams Faults, Crushed Zones	WATER LEVEL	WATER PRESSURE TEST LUGEON UNITS 10 20 30
Mainly SERICITE CHLORITE SCHIST Some GNEISS as shown. FRESH	Core in 0.1 to 0.8, mainly 0.3 ft lengths.	730				Joints spaced 0.1 to 0.5 ft. Irregular wuggy quartz veins		
	Core in 0.2 to 2, main- ly 0.4 ft lengths	720				Joints spaced 0.2 to 2, mainly 0.4 ft, dip 40° to 70° mainly parallel to schistosity. Usually slightly rough and irregular with traces of clay and coat- ings of sericite, often some mineralisation (pyrite) occasionally smooth and slickensided(?) when actually parallel to schistosity	Water lost at bit. (Drillers note) 9.0	
	Core in fragments up to 0.1 ft.	710				Irregular, near-vertical joints, discontinuous		
	Core in 0.2 to 2 mainly 0.4 ft. lengths							1.8
	Core in fragments up to 0.1 ft.	700				Crushed seam, up to 0.03 ft thick.		
						END OF HOLE 134.75 ft.		

Drill No. 24
Type Mindrill E1000
Driller Jensen
Commenced 4 Sept '64
Completed 14 Sept '64

EXPLANATION

WATER LEVEL DATE

Logged D.H.S.
Date 11 Sept 64
Drawn D.R.P.E.
Checked D.K.
Submitted

10 ft to 1 inch
Vert. Scale

Sheet 2 of 2
53888a Ha5
Drawing No.

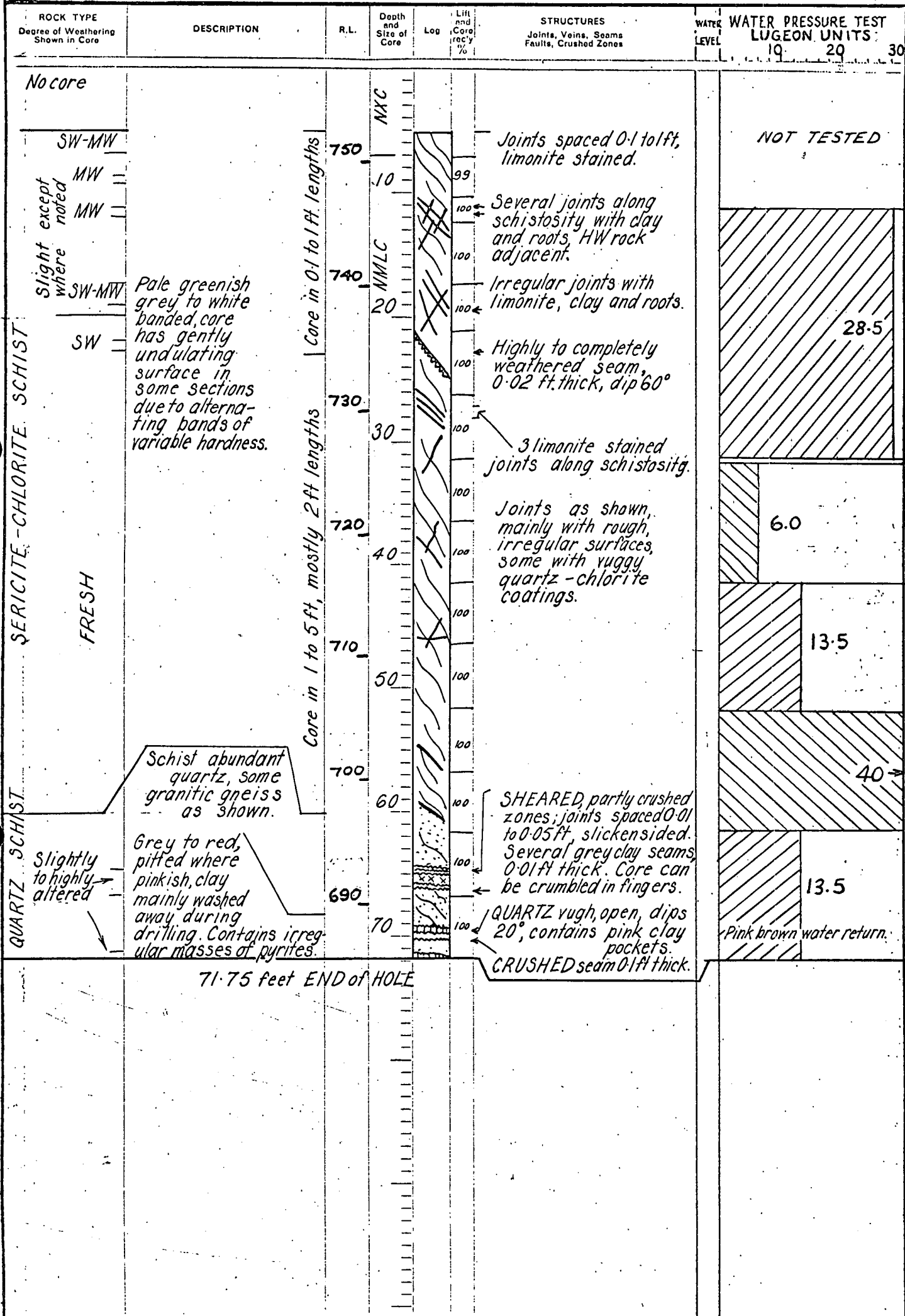
DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. **17**

PROJECT **KANGAROO CREEK DAM**
 FEATURE **FOUNDATION**
 LOCATION **LOWER LEFT ABUTMENT**

CO-ORDINATES **N6810 E22691**
HUNDRED ONKAPARINGA
 SECTION **335**

R.L. **757.5 FT**
 DIRECTION **—**
 ANGLE FROM HORIZONTAL **90**



Drill No. **24**
 Type **Mindrill E1000**
 Driller **Jensen**
 Commenced **18 Sept 64**
 Completed **22 Sept 64**

EXPLANATION

WATER LEVEL **DATE**

Logged **DHS**
 Date **22 Sept 64**
 Drawn **D.R.P.E.**
 Checked **DHS**
 Submitted

10 ft to 1 inch
 Vert. Scale
 Sheet **1** of **1**
33889
 Drawing No.
Has 5-7
 250-7.60 8036

PROJECT	KANGAROO CREEK DAM	CO-ORDINATES	Not Obtained	R.L.	825	FT
FEATURE	FOUNDATION	HUNDRED	ONKAPARINGA	DIRECTION	260	°
LOCATION	LEFT ABUTMENT	SECTION	335	ANGLE FROM HORIZONTAL	60	°

Drill No. <u>24</u>	EXPLANATION WATER LEVEL ↑ DATE	Logged	<u>J.P.T. & J.A.C.P.</u>	Vert. Scale <u>1 ft. = 1 in.</u>
Type <u>Mindrill E1000</u>		Date	<u>2 Nov '64</u>	Sheet <u>1</u> of <u>2</u>
Driller <u>J. Jensen</u>		Traced	<u>T.P.S.</u>	S 3961
Commenced <u>22 Oct '64</u>		Checked	<u>DWS</u>	Hd5+7
Completed <u>28 Oct '64</u>		Submitted		250-7.60 6336

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. 18

PROJECT KANGAROO CREEK DAM CO-ORDINATES Not Obtained R.L. 825 FT
FEATURE FOUNDATION HUNDRED ONKAPARINGA DIRECTION 260 °
LOCATION LEFT ABUTMENT SECTION 335 ANGLE FROM HORIZONTAL 60 °

ROCK TYPE Degree of Weathering Shown in Core	DESCRIPTION	R.L.	Depth and Size of Core	Log	Lift and Core rec'y %	STRUCTURES Joints, Veins, Seams Faults, Crushed Zones	WATER LEVEL	WATER PRESSURE TEST LUGEON UNITS:
								10 20 30
SCHIST gneissic in part.	Green to grey-green, foliated, very fine- grained, banded and gneissic in part, patches of chlorite and pyrite.					Partly sheared seam, 0.02 ft. thick, chloritic. Foliation dips 5° to 20° on core.		< 0.5
GRANITIC GNEISS	Pale grey to grey- green, coarse- grained, schistose in part, rich in quartz, common concentrations of mica and chlorite sericite.	730- 110				Irregular vuggy quartz, with mica and chlorite. Joints not numerous, spaced 0.4 to 2 ft, mainly along foliation.	Drilling water lost	14 Minimum value
SCHIST	Green to grey-green, intensely foliated.	720-120				Crushed seam 0.04 ft. thick, alteration of minerals to kaolin. Partly sheared zone, up to 0.2 ft. thick, chloritic.		

127.5 FT. END OF HOLE

Drill No. 24
Type Mindrill E1000
Driller J. Jensen
Commenced 22 Oct '64
Completed 28 Oct '64

EXPLANATION
[Symbol] SCHIST
[Symbol] GRANITIC GNEISS
MW Moderately weathered
HW Highly weathered

WATER LEVEL DATE

Logged J.P.T. & J.A.C.P.
Date 5 Nov '64
Traced T.P.S.
Checked D.V.S.
Submitted

Vert. Scale 10 ft. = 1 in.
Sheet 2 of 2
S 3961a
Ha5+7
250-7.60 8336

GEOLOGICAL LOG OF DRILL HOLE

PROJECT KANGAROO CREEK DAM

CO-ORDINATES E 22 054 N 6996

R.L. 677 FT

FEATURE FOUNDATION

HUNDRED ONKAPARINGA

DIRECTION 225 °

LOCATION LOWER LEFT ABUTMENT

SECTION 335

ANGLE FROM HORIZONTAL 60 °

ROCK TYPE Degree of Weathering Shown in Core	DESCRIPTION	R.L. & Casing	Depth and Size of Core	Log	STRUCTURES Joints, Veins, Seams Faults, Crushed Zones	WATER LEVEL	WATER PRESSURE TEST LUGEON UNITS
No Core							10 20 30
No Core	Pale grey to pale greenish grey, intensely foliated, micaceous, chloritic, sericitic, pyritic in parts, some haematite in parts.		Core in 0.1 to 1.5 ft. lengths	NX	Schistosity dips 0° to 20° on core		Intermittant partial drilling water returns throughout hole.
FRESH TO SLIGHT				NXC	Joints spaced 0.2 to 1 ft. mainly 0.5 ft, mainly parallel to foliation. Sheared partly crushed seams, 0.06 to 0.2 ft. thick, clay & HW to CW crushed & fragmented rock.		Not Tested
				NMLC	Crushed seams up to 0.01 ft. thick parallel to cleavage, spaced 0.5 to 2 ft. between 8 & 23 ft.		
					Crushed seam, up to 0.02 ft. thick, dips 50° & 20° on core.		
					Joints dip 50° on core, clay & limonite coated up to 0.01 ft.		
FRESH	White to very pale gray, micaceous, chloritic						24
	haematitic				Sheared, partly crushed seam 0.04 ft. thick		
Some SW					Crushed seams 0.01 ft. thick, limonite		
					Sheared zone, core largely in thin platy laminae, few crushed seams up to 0.01 ft, parallel to foliation and dip 40° to 80° on core.		< 0.5
	Haematite in bands and disseminated grains						1.5
					Joint dips 10°, limonite stained		
					Joints, dip 10° & 40°, limonite coated		12.5
					Joints, irregular, cemented, limonite up to 0.01 ft. thick		
							NOT TESTED

Drill No. 8

Type F 15

Driller A. Martin

Commenced 5 Feb. '65

Completed 12 Feb. '65

EXPLANATION

SW Slightly Weathered

MW Moderately "

HW Highly "

CW Completely "

WATER LEVEL DATE

Logged

Date

Drawn

Checked

Submitted

J.A.C.P.

10 Feb. '65

J.A.C.P.

D.A.S.

1 in. = 10 ft.
Vert. Scale

Sheet 1 of 2

S4147

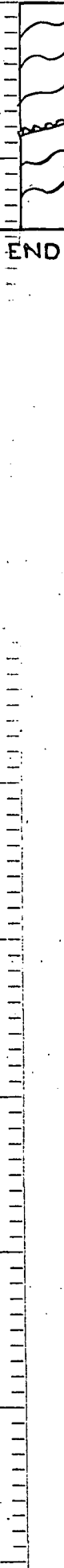
Drawing No. 545+7

250-7.60 E036

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. 19

PROJECT KANGAROO CREEK DAM CO-ORDINATES E 22,054 N 6996 R.L. 803 FT
FEATURE FOUNDATION HUNDRED ONKAPARINGA DIRECTION 225 °
LOCATION LOWER LEFT ABUTMENT SECTION 335 ANGLE FROM HORIZONTAL 60 °

ROCK TYPE Degree of Weathering Shown in Core	DESCRIPTION	R.L.	Depth and Size of Core	Log	Lift and Core rec'y %	STRUCTURES Joints, Veins, Seams Faults, Crushed Zones	WATER LEVEL	WATER PRESSURE TEST LUCEON UNITS
SCHIST, Gneissic in part FRESH	White to very pale grey	710	110		100	CRUSHED SEAM, dips 10° on core, 0.01 ft. thick		NOT TESTED
114.5 ft. END OF HOLE								

Drill No. 8	EXPLANATION	Logged JACP/DHS	1 in = 10 ft.
Type F 15		Date 15 Feb '65	Vert. Scale
Driller A. Martin		Drawn J.A.C.P.	Sheet 2 of 2
Commenced 5 Feb '65		Checked DHS	54147a
Completed 12 Feb '65		Submitted	Has + 7

WATER LEVEL DATE

Drawing No. 250-7.60 6036

R.L. 893 FT

DIRECTION 236

ANGLE FROM HORIZONTAL 45

Drill No. <u>8</u>	EXPLANATION		WATER	DATE	Logged	J.A.C.P.	1 in = 10 ft.
Type <u>F/5</u>	SW <u>Slightly weathered</u>		LEVEL		Date	26 Jan 65	Vert. Scale
Driller <u>A. Martin</u>	MW <u>Moderately weathered</u>				Drawn	T.P.S.	Sheet <u>1</u> of <u>2</u>
Commenced <u>19 Jan 65</u>	HW <u>Highly weathered</u>				Checked	DWS	<u>54515</u>
Completed <u>26 Jan 65</u>					Submitted		Drawing No. <u>Ha 547</u>
							250-7.60 C336

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE

Hole No. 20

PROJECT KANGAROO CREEK DAM CO-ORDINATES E 21,931 N 6933 R.L. 893 FT
FEATURE FOUNDATION HUNDRED ONKAPARINGA DIRECTION 236°
LOCATION UPPER LEFT ABUTMENT SECTION 335 ANGLE FROM HORIZONTAL 45°

ROCK TYPE Degree of Weathering Shown in Core	DESCRIPTION	R.L.	Depth and Size of Core	Log	Lith and Core rec'y % / 10	STRUCTURES Joints, Veins, Seams Faults, Crushed Zones	WATER LEVEL	WATER PRESSURE TEST LUGEON UNITS 10 20 30
Schist	Fine to coarse-grained, foliated to banded in parts, common irregular vuggy quartz. Fresh to slight limonite stained & SW along and near most joints	820	NMLC	Core in 0.2 to 2 mainly 0.5 ft lengths	100	Partly crushed seam, 0.02 ft limonite and crushed rock.	0.7	
Gneissic pegmatitic					100	Joints spaced 0.2 to 1.5 ft, mainly 0.5 ft, mainly dip 0° to 20° on core, parallel to foliation, limonite-stained and coated, in parts up to 0.1 ft. SW rock adjacent, a few dip 40° to 60° on core.		
Schist		810			100			
Pegmatite								
Schist		Massive white quartz and feldspar						
120 FT. END OF HOLE								

Drill No. 8
Type FIS
Driller A. Martin
Commenced 19 Jan. 65
Completed 26 Jan. 65

EXPLANATION

WATER LEVEL DATE

SW. Slightly weathered

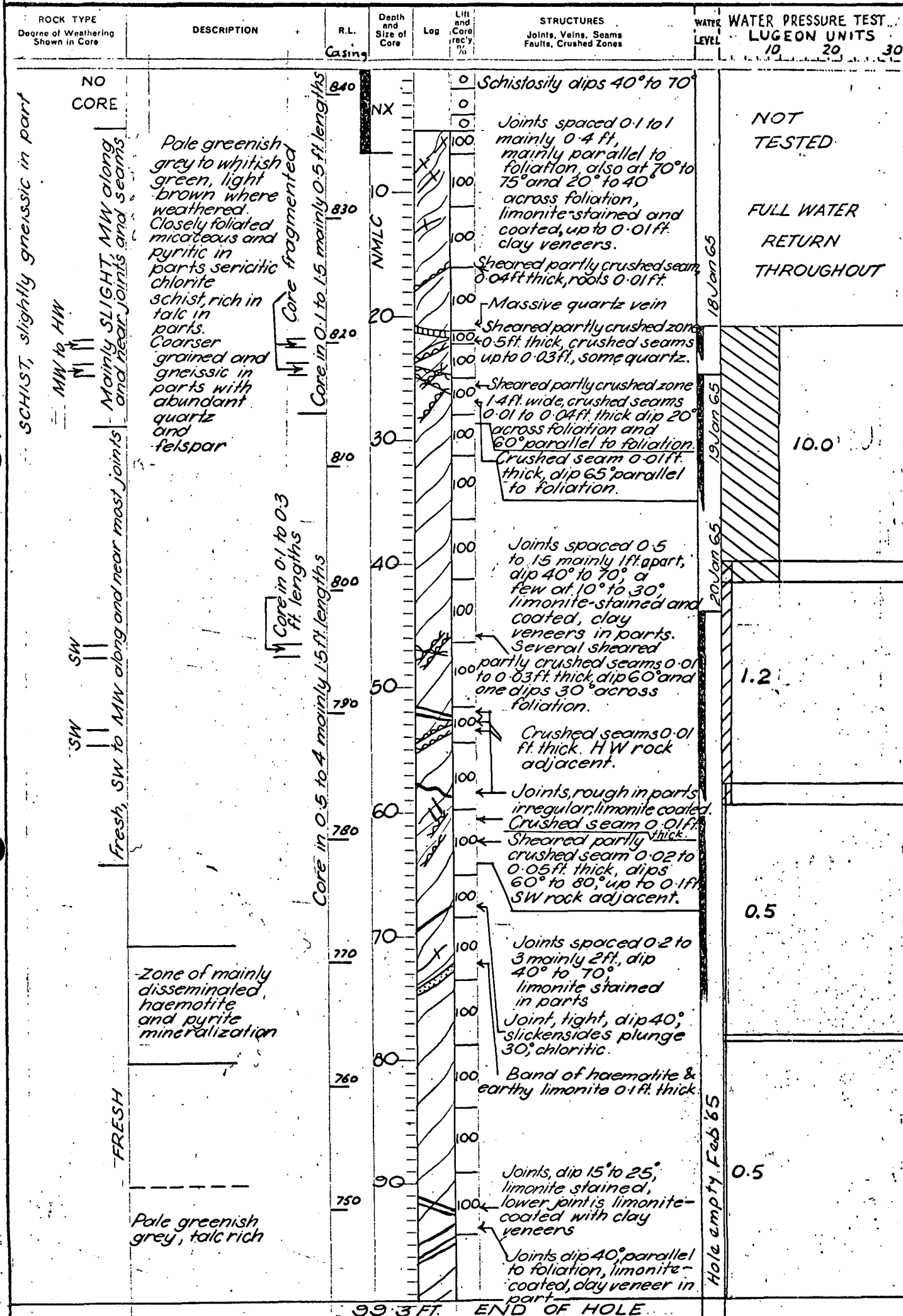
Logged J.A.C.P.
Sheet No. 28 Jan. 65
Drawn T.P.S.
Checked DMS
Submitted

1 in = 10 ft
Vert. Scale
Sheet 2 of 2
545150
Drawing No. 11a. 5.17
250-7.60 6036

DOCKET.....		DEPARTMENT OF MINES — SOUTH AUSTRALIA		HOLE No. 23			
SERIAL No.....		GEOLOGICAL LOG OF DRILL HOLE		SHEET 1 OF 1			
PROJECT KANGAROO CREEK DAM		CO-ORDINATES E 22.423 N 67.95		R.L. 890 FT.			
FEATURE FOUNDATION		HUNDRED ONKAPARINGA		DIRECTION 265			
LOCATION UPPER LEFT ABUTMENT		SECTION 335		ANGLE FROM HORIZONTAL 45°			
ROCK TYPE A DEGREE OF WEATHERING SHOWN IN CORE	DESCRIPTION OF CORE OR CUTTINGS WHERE CORE LOST	R. L. FEET CABING	DEPTH FEET SIZE OF CORE	LOG LIFT & CORE RECOVERY %	STRUCTURES JOINTS, VEINS, SEAMS, FAULTS, CRUSHED ZONES	WATER LEVEL ETC.	WATER PRESSURE TEST LUGEON UNITS 10 20 30
Mainly SCHIST with some GNEISS as shown.		Core in 0.1 to 1 ft. lengths		Schistosity dips 0° to 10° on core		NOT TESTED.	
Fresh to slight, moderate to complete along & near some joints		Core in 0.1 to 0.5 ft. lengths		SEAMS of brown clay and completely to moderately weathered rock, up to 0.06 ft. thick, with roots		FULL WATER RETURN THROUGHOUT	
Slight		Core in 0.05 to 0.5 ft. lengths		SHEARED zone; dip approximately 10° on core; joints spaced 0.05 to 0.5 ft. with slickensided limonite, chlorite & few clay veneers		4.0	
Fresh to slight		The more gneissic bands contain abundant quartz & feldspar grains		CRUSHED seam, 0.03 ft. thick, micaceous silt with fine roots at 24 ft.		2.0	
MW to HW Zones up to 0.1 ft. wide near joints & seams		Core in 0.1 to 2 ft., mostly 0.5 ft. lengths		To end of hole: Joints spaced 0.2 to 2 ft. generally 0.5 ft., mostly along schistosity dip 0° to 10°. Most have veneers of earthy limonite; several, where shown on log, have up to 0.01 ft. clay and limonite, and weathered rock adjacent		3.0	
GRANITIC GNEISS		Core in 0.1 to 2 ft., mostly 0.5 ft. lengths		Foliation dips 10° on core		+2	
mainly slight, moderate near some joints & seams		Core in 0.1 to 2 ft., mostly 0.5 ft. lengths		gradational boundary			
SCHIST		Core in 0.1 to 2 ft., mostly 0.5 ft. lengths		Highly weathered zones 0.25 ft. thick possibly sheared, & partly crushed			
mainly fresh to slight, moderate to high along and near some joints		Core in 0.1 to 2 ft., mostly 0.5 ft. lengths		Several irregular joints with up to 0.01 ft. red-brown clay coatings			
Pale greenish-grey to white, banded in part, quartz-chlorite-saricite schist. Contains haematite as disseminated grains		Core in 0.1 to 2 ft., mostly 0.5 ft. lengths		Moderately to highly weathered zone 0.2 ft. wide near joints			
		Core in 0.1 to 2 ft., mostly 0.5 ft. lengths		101.9 ft. END OF HOLE			
DRILL No. 24		EXPLANATION		ENGINEERING GEOLOGY AND SOILS SECTION		LOGGED BY DHS 23 Dec '64	
TYPE Mind. ill. E1000		CABING IN HOLE DURING DRILLING		WATER LEVEL IN DRILL HOLE (DATE)		DRAWN BY DHS	
DRILLER Jansen		MW Moderately weathered				CHECKED BY S4073 Ha	
COMMENCED 15 Dec '64		HW Highly				DRAWING No. 547	
COMPLETED 7 Jan '64							

GEOLOGICAL LOG OF DRILL HOLE

PROJECT **KANGAROO CREEK DAM** CO-ORDINATES **E 22.267 N 6.903** R.L. **842** FT
 FEATURE **FOUNDATION** HUNDRED **ONKAPARINGA** DIRECTION **—** °
 LOCATION **LEFT ABUTMENT** SECTION **335** ANGLE FROM HORIZONTAL **90** °



Drill No. 24

Type Mindrill E100

Driller J. Jensen

Commenced 15 Jan. 65

Completed 21 Jan. 65

EXPLANATION

WATER LEVEL

DATE

SW Slightly weathered
 MW Moderately weathered
 HW Highly weathered

Logged

Date

Drawn

Checked

Submitted

J.A.C.P.

22 Jan. 65

T.P.S.

DMS

1 in = 10 ft.

Vert. Scale

Sheet 1 of 1

54514

Drawing No.

250-7.60 2036

PROJECT	KANGAROO CREEK DAM	CO-ORDINATES	E 22,263	N 6905	R.L.	842	FT
FEATURE	FOUNDATION	HUNDRED	ON KAPARINGA	DIRECTION	184°		
LOCATION	LEFT ABUTMENT	SECTION	335	ANGLE FROM HORIZONTAL	40°		

53.3 FT. END OF HOLE

53.3 FT. END OF HOLE

Drill No. <u>24</u>	EXPLANATION	Logged ☒	J.A.C.P.	1 in = 10 ft.
Type <u>Mindrill E1000</u>		Date <u>28 Jan 65</u>		Vert. Scale.....
Driller <u>J. Jensen</u>	WATER LEVEL	Drawn <u>T.P.S.</u>		Sheet <u>1</u> of <u>1</u>
Commenced <u>22 Jan 65</u>	<u>SW - Slightly weathered</u>	Checked <u>DNS</u>		<u>54513</u>
Completed <u>26 Jan 65</u>	<u>MW - Moderately weathered</u>	Submitted		Drawing No. <u>Has 7</u>
	<u>CW - Completely weathered</u>			250-7.60 E036

DOCKET.....
SERIAL No.....
PROJECT KANGAROO CREEK DAM
FEATURE FOUNDATION
LOCATION UPPER LEFT ABUTMENT

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE
CO-ORDINATES E 22 249 N 6786
HUNDRED ONKAPARINGA
SECTION 335

HOLE No. 27
SHEET 1 OF 2
R.L. 929 FT.
DIRECTION.....°
ANGLE FROM HORIZONTAL 90°

ROCK TYPE & DEGREE OF WEATHERING SHOWN IN CORE	DESCRIPTION OF CORE OR CUTTINGS WHERE CORE LOST	R. L. FEET CASING → SIZE OF CORE	DEPTH FEET	LOG	STRUCTURES JOINTS, VEINS, SEAMS, FAULTS, CRUSHED ZONES	WATER LEVEL ETC.	WATER PRESSURE TEST LUGEON UNITS 10 20 30
SLIGHT TO FRESH limonite stained and SW near and along joints	light grey to pale greenish-grey micaceous, sericitic, chloritic, slightly pyritic in parts, closely foliated, coarser grained in parts with tendency towards banding of quartz and felspars. Few purplish patches of haematitic mineralisation	Core in fragments and lengths 0.1 to 0.4 ft.	0	0	0		
			10	10	10		
			20	20	20		
			30	30	30		
			40	40	40		
			50	50	50		
			60	60	60		
			70	70	70		
			80	80	80		
			90	90	90		
Mainly FRESH, limonite-stained along & near most joints	disseminated haematitic mineralisation	Core in 0.2 to 3 mainly 1 ft. lengths	100	100	100		
			110	110	110		
			120	120	120		
			130	130	130		
			140	140	140		
			150	150	150		
			160	160	160		
			170	170	170		
			180	180	180		
			190	190	190		
Common areas of haematitic	haematitic		200	200	200		
			210	210	210		
			220	220	220		
			230	230	230		
			240	240	240		
			250	250	250		
			260	260	260		
			270	270	270		
			280	280	280		
			290	290	290		

Schist - gneissic in part

NOT TESTED

Water lost at 20.7 ft.
50% water return to 50 ft.
No water return below 50 ft.

0.5

10.5

<0.5

3.5

DRILL No. 24 TYPE E1000 DRILLER J. Jensen COMMENCED 4 Feb. 65 COMPLETED 10 Feb. 65	EXPLANATION CASING IN HOLE DURING DRILLING WATER LEVEL IN DRILL HOLE (DATE)	ENGINEERING GEOLOGY AND SOILS SECTION LOGGED BY J.A.C.P. DRAWN BY R.A. CHECKED BY D.H.S. DRAWING No. S4205 Ha
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DOCKET.....		DEPARTMENT OF MINES — SOUTH AUSTRALIA				HOLE No. 27	
SERIAL No.....		GEOLOGICAL LOG OF DRILL HOLE				SHEET 2 OF 2	
PROJECT KANGAROO CREEK DAM		CO-ORDINATES E 22 249 N 6786				R.L. 929 FT.	
FEATURE FOUNDATION		HUNDRED ONKAPARINGA				DIRECTION - °	
LOCATION UPPER LEFT BANK		SECTION 335				ANGLE FROM HORIZONTAL 90°	
ROCK TYPE A DEGREE OF WEATHERING SHOWN IN CORE	DESCRIPTION OF CORE OR CUTTINGS WHERE CORE LOST	R. L. DEPTH FEET CASING → SIZE OF CORE	LOG	STRUCTURES JOINTS, VEINS, SEAMS, FAULTS, CRUSHED ZONES	WATER LEVEL ETC.	WATER PRESSURE TEST LUGEON UNITS 10 20 30	
SCHIST Gneissic in part	FRESH Pale grey to greenish grey, intensely foliated	Core in 0.1 to 2, mainly 1 ft. lengths fragmented	NMLC 100 110 120	Joints mainly along schistosity CLAY SEAM, 0.1 to 0.2 ft. thick, dip 70° red-brown, with 0.4 ft. SW to MW rock adjacent. Joints as shown, partly open SHEARED, partly crushed seams 0.01 & 0.04 ft. thick SW to MW.		3.5	
	FRESH to SLIGHT purple colour and concentrations of haematite.					6.5	
121.25 ft. END OF HOLE							
TEST PRESSURES SHOWN IN POUNDS PER SQ. INCH MEASURED AT GROUND SURFACE							
DRILL No. 24		EXPLANATION				ENGINEERING GEOLOGY AND SOILS SECTION	
TYPE E1000		CASING IN HOLE DURING DRILLING				WATER LEVEL IN DRILL HOLE (DATE)	
DRILLER J. Jansen						LOGGED BY J.A.C.P.	
COMMENCED 4 Feb '65						DRAWN BY RA.D.H.S.	
COMPLETED 10 Feb '65						CHECKED BY D.H.S.	
						DRAWING No. S4205a H4 5x7	

DOCKET.....
SERIAL No.....
PROJECT KANGAROO CREEK DAM
FEATURE FOUNDATION
LOCATION LOWER LEFT ABUTMENT

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE
CO-ORDINATES E 22.596 N 6875
HUNDRED ONKAPARINGA
SECTION 335

HOLE No. 28
SHEET 1 OF 1
R.L. 755 FT.
DIRECTION — °
ANGLE FROM HORIZONTAL 90 °

ROCK TYPE A DEGREE OF WEATHERING SHOWN IN CORE	DESCRIPTION OF CORE OR CUTTINGS WHERE CORE LOST	R. L. DEPTH FEET CASING → SIZE OF CORE	LOG LIFT & CORE RECOVERY %	STRUCTURES JOINTS, VEINS, SEAMS, FAULTS, CRUSHED ZONES	WATER LEVEL E.T.C.	WATER PRESSURE TEST BURGEON UNITS 10 20 30
SCHIST FRESH FRESH FRESH FRESH FRESH FRESH FRESH	Slightly weathered, limonite-stained FRESH, limonite stained, along and SW in parts, near most joints.	Core in pieces up to 0.5 ft. 750 740 730 720 710 700 690 680 670 660	20 50 60 10 20 30 40 50 60 70 80 90	Schistosity dips 50° to 70° To 37 ft., joints spaced 0.3 to 3 mainly 1 ft., mainly parallel to foliation, mainly tight, limonite stained and coated, a few dip 20° to 40° across foliation. Crushed seam 0.02 ft. clay, some CW crushed rock, limonite coated. Joint, open in parts up to 0.06 ft., partly filled with limonite and limonite-coated vuggy quartz. Crushed seam dip 70° 0.05 ft. CW crushed rock, some clay and quartz, up to 1 ft SW rock adjacent. Crushed seam 0.01 ft. Joint dip 30° Below 37 ft., few joints, widely spaced, tight, core breaks along foliations. Partly sheared seams parallel to schistosity, 0.1 to 0.3 ft. thick, joints spaced 0.01 to 0.4 ft., chlorite and talc veneers Sheared zone 0.9 ft. wide, joints spaced 0.01 to 0.1 ft., mainly parallel to foliation, chlorite and talc coated, contains crushed seam 0.05 ft. thick at 71.5 ft. Sheared partly crushed zone 0.5 ft. wide, dip 40° Crushed seam 0.02 ft. thick, recemented in part. Crushed seam 0.03 ft. thick. Pyritic mineralisation, 0.3 ft. thick zone.		NOT TESTED 7.5 3.4 1.6 < 0.5

DRILL No. 24
TYPE E1000
DRILLER J. Jensen
COMMENCED
COMPLETED 19 Feb 65

EXPLANATION
CASING IN HOLE DURING DRILLING
WATER LEVEL IN DRILL HOLE (DATE)

ENGINEERING GEOLOGY AND SOILS SECTION
LOGGED BY J.A.C.P.
DRAWN BY T.P.S.
CHECKED BY D.H.S.
DRAWING No. S4204
Ha5+7

200-8.64 8118

DOCKET.....
SERIAL No.....
PROJECT **KANGAROO CREEK DAM**
FEATURE **FOUNDATION**
LOCATION **UPPER RIGHT BANK**

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE
CO-ORDINATES **E 22651 N 7173**
HUNDRED **YATALA**
SECTION **5497**

HOLE No. **29**
SHEET **1** OF **2**
R.L. **905 FT.**
DIRECTION **185 1/2**
ANGLE FROM HORIZONTAL **60°**

ROCK TYPE & DEGREE OF WEATHERING SHOWN IN CORE	DESCRIPTION OF CORE OR CUTTINGS WHERE CORE LOST	R. L. FEET CASING → SIZE OF CORE	DEPTH LOG	LIFT & CORE RECOVERY %	STRUCTURES JOINTS, VEINS, SEAMS, FAULTS, CRUSHED ZONES	WATER LEVEL ETC.	WATER PRESSURE TEST
							LOGGED UNITS 10 20
NO CORE							
GNEISS, Schistose in part, some GRANITIC GNEISS as shown	FRESH, limonite stained along most joints	SLIGHT (NW)					NOT TESTED
SCHIST, gneissic in part	Mainly grey, intensely foliated, coarser grained gneissic bands.						>30LU
mainly GRANITIC GNEISS, some SCHIST and GNEISS	Mainly SLIGHT, moderate to high along many joints and limonite stained joints	FRESH to SLIGHT, limonite stained joints					0.8LU
mainly GRANITIC GNEISS, some SCHIST and GNEISS	Mainly SLIGHT, moderate to high along many joints and limonite stained joints	FRESH to SLIGHT, limonite stained joints					23LU
SCHIST and GNEISS as shown	FRESH, limonite stained and coated along most joints	SLIGHT					<0.5LU

DRILL No. **5**
TYPE **E. 1000**
DRILLER **F. Gaden**
COMMENCED **23 Mar. 65**
COMPLETED **5 Apr. 65**

EXPLANATION
CASING IN HOLE DURING DRILLING **1**
WATER LEVEL IN DRILL HOLE **1** (DATE)
MW - moderately weathered
SW - slightly
CW - completely weathd. - weathered.

ENGINEERING GEOLOGY AND
SOILS SECTION
LOGGED BY **JACP & DHS**
DRAWN BY **RH**
CHECKED BY **DS**
DRAWING No. **54332/H5-7**

200-8.64 8118

DOCKET.....
SERIAL No.....
PROJECT: KANGAROO CREEK DAM
FEATURE: FOUNDATION
LOCATION: RIVER BED

DEPARTMENT OF MINES — SOUTH AUSTRALIA
GEOLOGICAL LOG OF DRILL HOLE
CO-ORDINATES E 22624 N 6914
HUNDRED ONKAPARINGA
SECTION 335
ANGLE FROM HORIZONTAL 90°

HOLE No. 30
SHEET 1 OF 1
R.L. 734 FT.

ROCK TYPE A DEGREE OF WEATHERING SHOWN IN CORE	DESCRIPTION OF CORE OR CUTTINGS WHERE CORE LOST	R. L. DEPTH FEET Casing → SIZE OF CORE	LOG	STRUCTURES JOINTS, VEINS, SEAMS, FAULTS, CRUSHED ZONES	WATER PRESSURE TEST LUGEON UNITS 10 20 30
MW NO CORE FR-SW NO CORE SW NO CORE FR-SW NO CORE SW	Erratic pebbles and boulders of schist and gneiss— talus debris from road cutting, fresh to slightly weathered ?	730 720 710 700 690	730 720 710 700 690	Scree and talus debris Foliation dips 20° to 40° Few joints, widely spaced, tight, regular. Joint dip 60°, limonite stained. Joints dip 50°-80°, chlorite veneers, pyritic, tight. Joints dip 60°, rough, chlorite veneers, tight. Partly crushed seam, talc veneer, less than 0.01 ft. crushed rock Several joints, irregular dip 30° to near vertical, chlorite veneers, tight. Joint dip 50°, open, partly filled with up to 0.01 ft. quartz and calcite. Core broken mainly along foliations.	NOT TESTED 18 6.8
?					
Schist	Dark grey to greenish grey, very fine-grained, intensely foliated, chloritic, micaceous, sericitic, pyritic in parts				
Granitic gneiss	coarser grained, lighter grey				
Schist	intensely foliated.				
Granitic gneiss	grey to greenish grey, medium to coarse grained, schistose and intensely foliated in parts. Several vuggy, mineralized quartz veins				
51.5 ft. END OF HOLE					

DRILL No. 8
TYPE F.15
DRILLER A. Martin
COMMENCED 22 Feb 65
COMPLETED 24 Feb 65

EXPLANATION
CASING IN HOLE DURING DRILLING
WATER LEVEL IN DRILL HOLE (DATE)

ENGINEERING GEOLOGY AND
SOILS SECTION
LOGGED BY J.A.C.P.
DRAWN BY T.P.S.
CHECKED BY DIS
DRAWING No. S4202
Ha5+7

DOCKET.....		DEPARTMENT OF MINES — SOUTH AUSTRALIA				HOLE No. <u>31</u>									
SERIAL No.....		GEOLOGICAL LOG OF DRILL HOLE				SHEET <u>1</u> OF <u>1</u>									
PROJECT <u>KANGAROO CREEK DAM</u>		CO-ORDINATES <u>NOT OBTAINED</u>				R.L. <u> </u> FT.									
FEATURE <u>FOUNDATION</u>		HUNDRED <u>ONKAPARINGA</u>				DIRECTION <u>248°</u>									
LOCATION <u>END OF ADIT 2, LEFT BANK</u>		SECTION <u>335</u>				ANGLE FROM HORIZONTAL <u>+1°</u>									
ROCK TYPE + DEGREE OF WEATHERING SHOWN IN CORE	DESCRIPTION OF CORE OR CUTTINGS WHERE CORE LOST	CORE LOSS LIFT % 20 60	CORE SIZE DEPTH RL. FT.	LOG	FRACTURE LOG 1 4 16 64 2 8 32 128	STRUCTURES JOINTS, VEINS, SEAMS FAULTS, CRUSHED ZONES	% DRILL WATER LOSS 50	WATER PRESSURE TESTS PERMEABILITY IN LUQUEON UNITS							
								10 20 30 40 50 60 70 80 90 100							
GNEISS	FRESH limonite stained along and near all joints.	No core →	NXC	NMS	10	Foliation dips 40° to 60° on core.			NOT WATER TESTED						
										SCHIST	SW-MW MW-EW	Very fine grained, light grey, pinkish & brown where weathered. Intensely foliated.	SHEARED SEAM dips 20° on core, 0.03 ft. wide HW but limonite cem- ented 0.1 to 0.4 HW rock adjacent.		
														Light grey to grey and greenish. Fine to medium grained, coarser grained in parts. Quartz and felspars frequently banded. Intensely foliated.	Joint irregular, limonite- stained and coated. Several joints dip parallel to foliation, limonite coated, clay veneer.
Joints parallel to foliation, limonite coated, most have clay veneer.															
	Few joints, limonite stained, occasionally with clay veneer, mainly parallel to foliation.														
		Irregular quartz and chlorite, few joints with clay.													
			Joints, limonite-coated, clay veneer, up to 0.04 ft. SW rock adjacent.												
Quartz, vuggy, limonite- coated, mineralised.															
	50.8 feet END OF HOLE														

DRILL No. <u>E.1000</u>	EXPLANATION		ENGINEERING AND SOILS GEOLOGY SECTION
TYPE <u>2A</u>	CASING IN HOLE DURING DRILLING	WATER LEVEL IN DRILL HOLE ← (DATE)	LOGGED BY <u>J.A.C.P.</u>
DRILLER <u>J. Jensen</u>	FRACTURE LOG 1 4 16 64 12 3 3/4 3/16 1 25 05 015	Breaks in core per foot or Inches Equivalent Feet Diameter	DRAWN BY <u>R.H.</u>
COMMENCED <u>15 Sept. 65</u>			CHECKED BY
COMPLETED <u>16 Sept. 65</u>			DRAWING No. <u>S4726 Ha5+7</u>

DOCKET.....		DEPARTMENT OF MINES — SOUTH AUSTRALIA				HOLE No. 32			
SERIAL No.....		GEOLOGICAL LOG OF DRILL HOLE				SHEET 1 OF 1			
PROJECT KANGAROO CREEK DAM.		CO-ORDINATES NOT OBTAINED				R.L. FT.			
FEATURE FOUNDATION.		HUNDRED ONKAPARINGA.				DIRECTION 240°			
LOCATION END OF ADIT No. 1.		SECTION.....				ANGLE FROM HORIZONTAL 1/°			
ROCK TYPE A DEGREE OF WEATHERING SHOWN IN CORE	DESCRIPTION OF CORE OR CUTTINGS WHERE CORE LOST	CORE LOSS LIFT % 20 40 60	CORE SIZE DEPTH RL. FT.	LOG	FRACTURE LOG 1 4 16 64 1 2 4 8 16 32	STRUCTURES JOINTS, VEINS, SEAMS FAULTS, CRUSHED ZONES	% DRILL WASTE LOST 50	WATER PRESSURE TESTS PERMEABILITY IN LUQUEON UNITS	
GNEISS generally schistose.	Grey to greenish-grey, mainly fine-to medium-grained, banded quartz and feldspar, intensely foliated.	FRESH limonite coatings on most joints.	FRESH	NMLC NX 10 20 30 40 50		Foliation dips 40° to 60° on core.	NOT TESTED		
						SHEARED seams 0.02 to 0.1 ft. thick, limonite stained and SW in parts. Most joints limonite coated, often with veneer of red-brown clay, mainly parallel to foliation. vuggy quartz, limonite coated.			
						Partly SHEARED zone 0.5 ft. wide.			
						SHEARED ZONE 1-8 ft. wide, talc rich, sericitic, several CRUSHED seams up to 0.1 ft. thick, limonite stained and SW in parts, red-brown clay on joints.			
						CRUSHED seam 0.1 ft. thick, with quartz sericitic, talc rich.			
						Partly SHEARED ZONE 2.5 ft. wide, joints spaced 0.01 to 0.2 ft., chlorite and some calcite on joints, possibly SW.			
						Partly SHEARED partly CRUSHED ZONE 0.5 ft. wide, mineralised with Chalcopryrite, pyrite, etc.			
						Numerous joints, spaced 0.01 to 0.3 ft.			
						SHEARED partly CRUSHED zone 0.04 to 0.12 ft. wide.			
						END OF HOLE 52.5 ft.			

DRILL No. 24	EXPLANATION		ENGINEERING AND SOILS GEOLOGY SECTION.
TYPE E100	CASING IN HOLE DURING DRILLING	WATER LEVEL IN DRILL HOLE (DATE)	LOGGED BY J.A.C.P.
DRILLER J. Jensen.	FRACTURE LOG		DRAWN BY S.W.
COMMENCED 21 Sept. 1965	1 4 16 64 Breaks in core per foot or Diameter of fragments in feet.		CHECKED BY
COMPLETED 23 Sept. 1965	12 3 3/4 3/16 Inches Equivalent		DRAWING No. S4818aHa5-7
	1 .25 .06 .015 Feet Diameter		

APPENDIX B

LOGS OF EXPLORATORY ADITS,
WITH EXPLANATORY NOTES

<u>FIGURES</u>	<u>DWG. NO.</u>
Kangaroo Creek Dam, Exploratory Adit No. 1, Geological Log	65-816
Kangaroo Creek Dam, Exploratory Adit No. 2, Geological Log	65-827
Kangaroo Creek Dam, Exploratory Cross Adits 1 & 2, Geological Log	65-817
Kangaroo Creek Dam, Exploratory Adits Geological Section	64-330 65-320

APPENDIX B

LOGS OF EXPLORATORY ADITS WITH EXPLANATORY NOTES

INTRODUCTION

Two horizontal adits 6.5ft. wide and 9ft. high were constructed as part of the geological investigations for Kangaroo Creek Dam. Details are summarised below:

ADIT NO.	INVERT R.L. (FT.)	BEARING	LENGTH (FT.)
1	757	240°	120
2	847.7	248°	139

NOTES ON DETAILS SHOWN ON LOG SHEETS

The title block in the lower right hand corner shows the scale and the position of the sheet in the sequence when more than one log sheet is used. Headings on the left hand side indicate the type of information contained in the horizontal columns.

Tunnel Stations

Positions in the tunnel are given by stations, one station being equal to 100ft. measured horizontally along the centre line of the tunnel, e.g. Sta. 1 + 15 is 115ft. from the Datum, Sta. 0 + 00.

Progress

The position of the heading at the end of each working day is recorded.

Rock Type

The rock types shown graphically elsewhere on the log sheet are here described in words. Degrees of weathering are also described.

Log of Roof and Walls

Geological information is projected on to three strips representing the roof and walls of the tunnel.

The strips are obtained geometrically by rotating the walls about their join lines with the roof outwards through 90°, and then projecting them, together with the roof, on to a horizontal plane tangential to the roof. (The method is shown in a diagram on the log sheet). This projection enables the user of the log to obtain a 3-dimensional picture of the tunnel, by folding the wall strips downwards. The roof and walls are drawn as if viewed from outside the tunnel, and this must be borne in mind when using the log sheets during an inspection of the tunnel.

The information plotted graphically includes the rock types and the traces of structural features in the rock. The true strike and dip of these geological features in relation to the tunnel direction, are plotted by conventional symbols in the lines labelled "Plan", above the below the graphic strips.

Excavation Condition

The figure in this column describes the condition of the rock surrounding the completed excavation, taking into account the rock material, the geological defects (joints, seams etc.) and their orientation, and the effects of blasting and stress re-distribution. The figures used are from the following table, based on tables by Talobre and Terzaghi (Refs. 1 and 2).

<u>CLASSIFICATION</u>	<u>CHARACTERISTICS</u>
5	The rock mass is perfectly sound and very compact.
4	The rock mass is sound, but somewhat loosened along joints.
3	The rock mass is considerably loosened along joints.
2	The rock mass is very loosely jointed and seamy, requiring continuous support.
1	The rock mass exerts considerable pressure on supports.

Percent Breakage along Joints

The percentage of the area of the roof and walls of the tunnel which consist of natural joint faces (as distinct from fresh fractures across the rock fabric) is estimated to the nearest 10 per cent.

Support During Construction

Steel supports are shown as thick vertical lines.

Excavation

The distance the tunnel has advanced in each cycle is shown by a vertical line. The number of holes drilled and their length, and the weight (in pounds) of explosives used per round is recorded. When records have been incomplete a summary in words is used to cover the appropriate length of tunnel.

REFERENCES

1. TALOBRE, J. (1957) La Mechanique des Roches (Dunod: Paris) p.16.
2. TERZAGHI, Karl (1946) Rock Tunneling with Steel Supports (The Commercial Shearing and Stamping Co: Youngstown, Ohio) p. 91.

TUNNEL STATIONS	0+00	CROSS ADIT NO. 2				0+50	0+00	CROSS ADIT No 1	
DIRECTION, INVERT LEVEL, SLOPE									
PROGRESS HEADING AT, DATE		27 July	28 July	30 July	31 July		13 July	14 July	
ROCK TYPE and DEGREE of WEATHERING		SECTION STA. 0+28				FACE STA. 0+49	SCHIST and GNEISS Mainly FRESH, moderate to high in mineralised zones		
LOG OF FACE Looking in direction of tunnel stations AND SECTIONS SHOWING OVERBREAK									
PLAN, 4 feet above floor									
STRUCTURES JOINTING PATTERN-ATTITUDE, SPACING, PERSISTENCE, CHARACTER SURFACE, SEPARATION COATING FAULTS SHEARED AND CRUSHED ZONES, ATTITUDE, RELATIVE DISPLACEMENT, WIDTH, CHARACTER OF MATERIAL									
EXCAVATION CONDITION		4 - 3					4		
PERCENT BREAKAGE ALONG JOINTS		45					40		
SUPPORT DURING CONSTRUCTION									
EXCAVATION STRIPPING		Rounds of mainly 21 holes, 5 ft. long. 23 to 30 lbs An 75, 4 to 5 ft. advances.					Rounds of mainly 20 holes 5 ft. long, 21 to 30 lbs An 60, 5 ft. advances.		
GROUND WATER		Mainly dry, Some seepages Dry (May '67)					Dry Dry (May '67)		
FEELER HOLES & GROUTING									
PHOTOGRAPHS CATALOGUE No									
FINAL SUPPORT OR LINING AS CONSTRUCTED									

STRIKE & DIP OF JOINT
 STRIKE OF VERTICAL JOINT
 HORIZONTAL JOINT
 STRIKE & DIP OF SCHISTOSITY
 STRIKE & DIP OF BEDDING

HIGHLY WEATHERED
 COMPLETELY WEATHERED
 CRUSHED SEAM
 Showing dip
 SHEARED or CRUSHED ZONE
 Showing dip and width.
 FAULT Showing relative movement.

LEGEND

 200 WATER INFLOW
200 gallons per hour.
 SEEPAGE
 PHOTO BLACK & WHITE
 PHOTO COLOUR

SCHIST
 GNEISS
 SPECIMEN COLLECTED

TUNNEL SUPPORTS

 STEEL SETS
 WALL PLATES
 ROCK BOLTS
 MESH
 GUNITE

ENGINEERING GEOLOGY SECTION

LOGGED
DHS
JPT

DRAWN
DHS

J.P. Trudinger
GEOLOGIST
DHS
SENIOR GEOLOGIST

S. A. DEPARTMENT OF MINES

KANGAROO CREEK DAM

EXPLORATORY CROSS ADITS 1&2

GEOLOGICAL LOGS

DATE: 31 July '65

SCALE: 1 in = 10 ft

SHEET 1 OF 1

65-817 Ho5+7

TUNNEL STATIONS		0+00				0+50				1+00				1+20	
DIRECTION, INVERT LEVEL, SLOPE															
PROGRESS HEADING AT, DATE		2 July		3 July		5 July		6 July		7 July		8 July		9 July	
ROCK TYPE and DEGREE of WEATHERING		SCHIST Mainly SLIGHT, moderate to high near joints and seams				SCHIST and GNEISS FRESH with some limonite stained joints and vuggy quartz veins				Mainly FRESH, slight to high near joints and seams					
LOG OF FACE Looking in direction of tunnel stations AND SECTIONS SHOWING OVERBREAK															
PLAN, 4 feet above floor															
SOUTH SIDE															
ROOF															
NORTH SIDE															
PLAN, 4 feet above floor															
STRUCTURES JOINTING PATTERN-ATTITUDE, SPACING, PERSISTENCE, CHARACTER SURFACE, SEPARATION COATING FAULTS SHEARED AND CRUSHED ZONES, ATTITUDE, RELATIVE DISPLACEMENT, WIDTH, CHARACTER OF MATERIAL															
EXCAVATION CONDITION PERCENT BREAKAGE ALONG JOINTS		2		4		5		5		4		4			
SUPPORT DURING CONSTRUCTION															
EXCAVATION STRIPPING ADVANCE NO of HOLES EXPLOSIVES, lbs.															
GROUND WATER INITIAL QUANTITY, DATE QUANTITY, DATE TEMPERATURE															
FEELER HOLES & GROUTING															
PHOTOGRAPHS CATALOGUE NO															
FINAL SUPPORT OR LINING ESTIMATED AS CONSTRUCTED															

LEGEND

STRIKE & DIP OF JOINT
 STRIKE OF VERTICAL JOINT
 HORIZONTAL JOINT
 STRIKE & DIP OF CLEAVAGE
 STRIKE & DIP OF SCHISTOSITY
 HW HIGHLY WEATHERED
 CW COMPLETELY WEATHERED
 CRUSHED SEAM Showing dip
 SHEARED or CRUSHED ZONE Showing dip and width.
 FAULT Showing relative movement.

200 @ WATER INFLOW 200 gallons per hour.
 S SEEPAGE
 O PHOTO BLACK & WHITE
 • PHOTO COLOUR
 Vein of QUARTZ/PEGMATITE
 SCHIST
 GNEISS
 III STEEL SETS
 WALL PLATES
 ROCK BOLTS
 MESH
 GUNITING
 C2 CLEANUP POSITION.
 • SPECIMEN COLLECTED

ENGINEERING SERVICES SECTION

LOGGED J.P.T. J.P. Trudinger GEOLOGIST

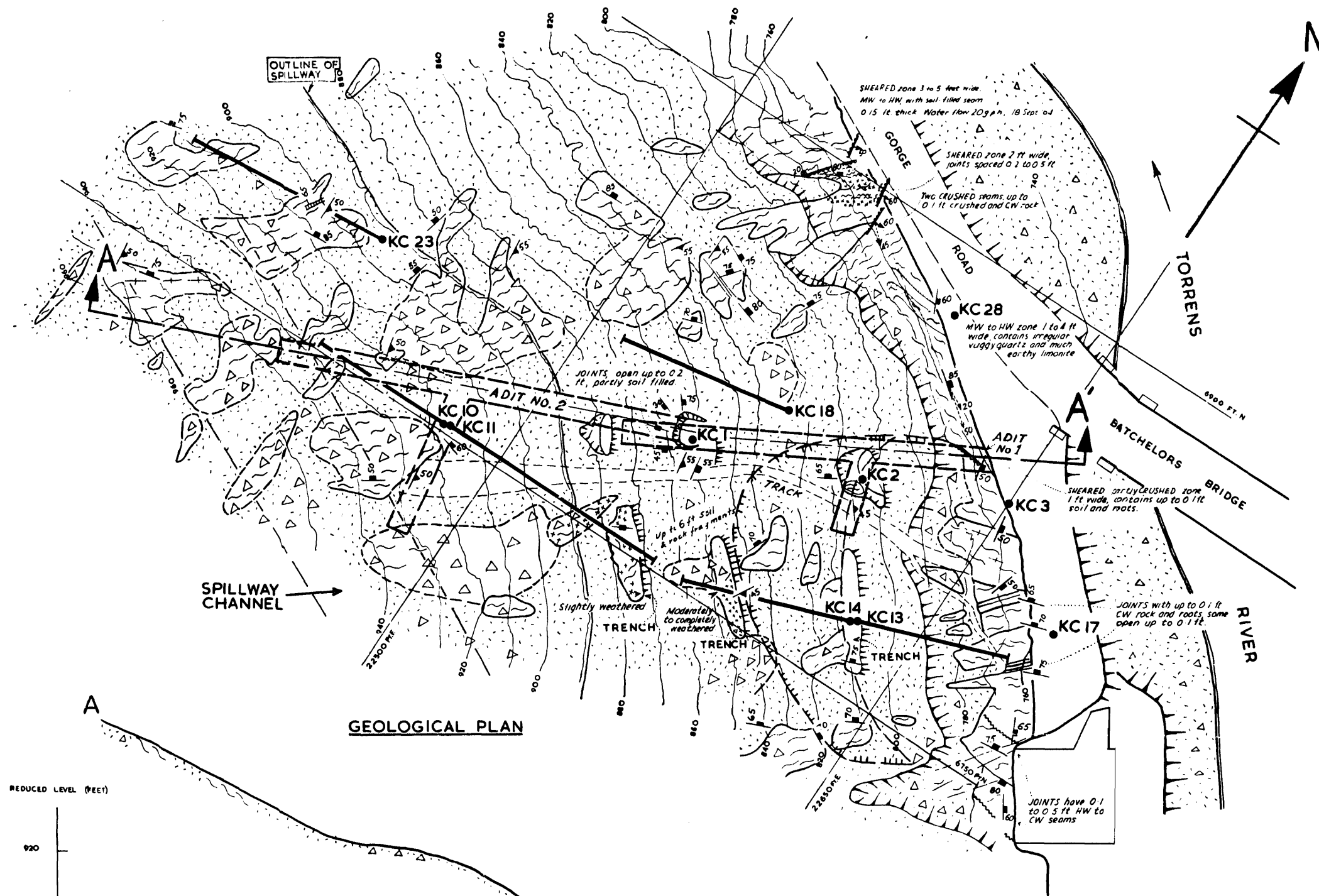
DRAWN D.H.S. SENIOR GEOLOGIST

S. A. DEPARTMENT OF MINES

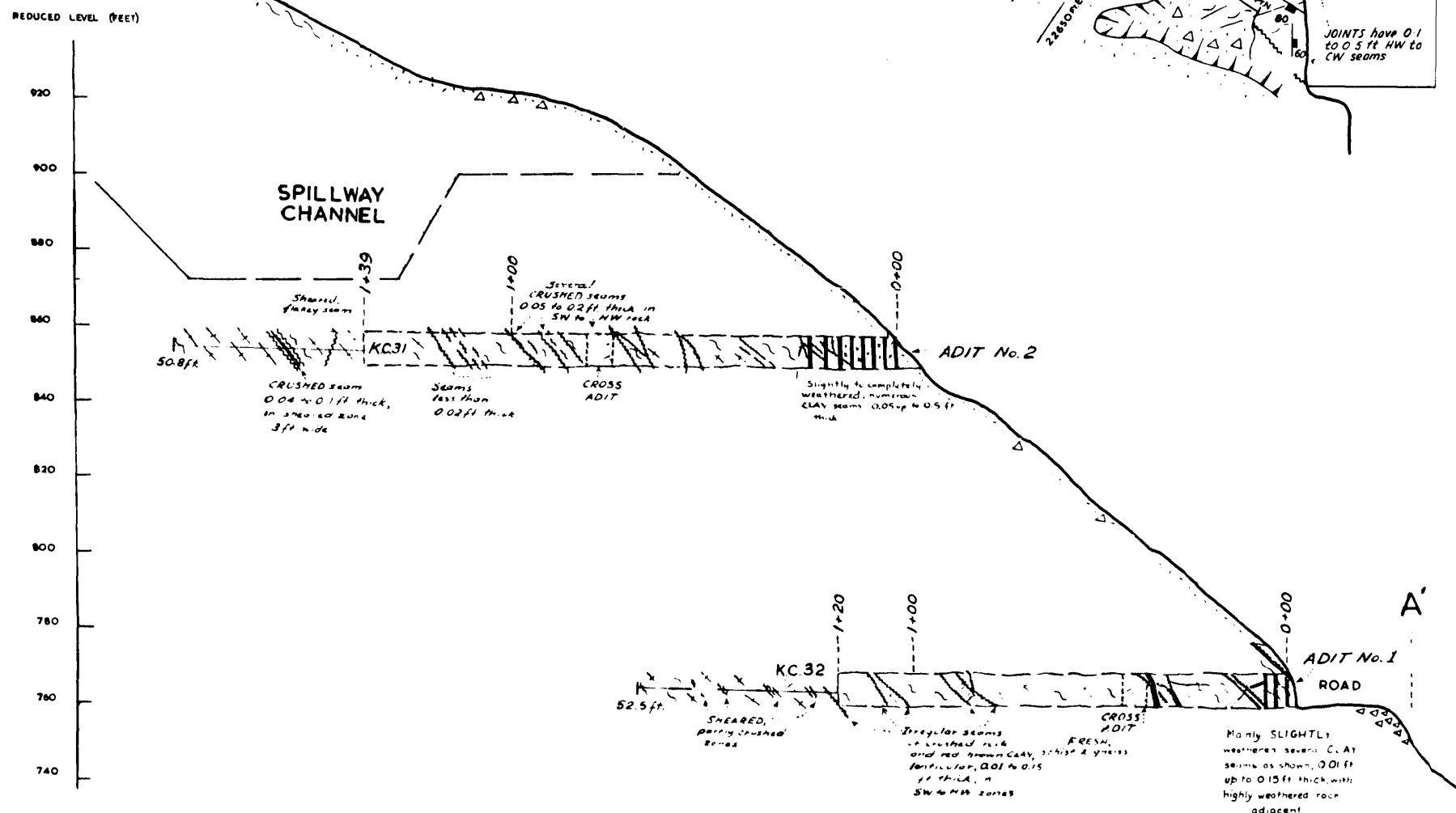
KANGAROO CREEK DAM EXPLORATORY ADIT No. 1

GEOLOGICAL LOG

SCALE: 1 in. = 10 ft. DATE: 28 July 65 SHEET 1 OF 1

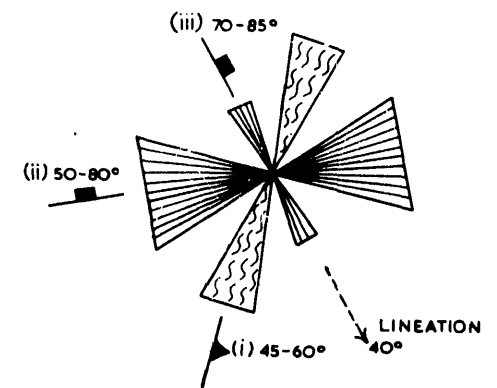


GEOLOGICAL PLAN



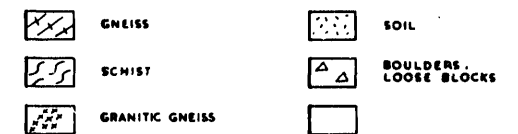
SECTION A-A'

DIAGRAM SHOWING DIRECTION OF GEOLOGICAL STRUCTURES

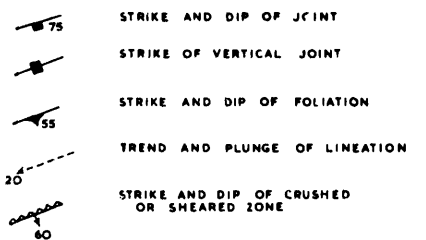


LEGEND

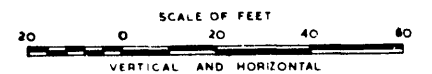
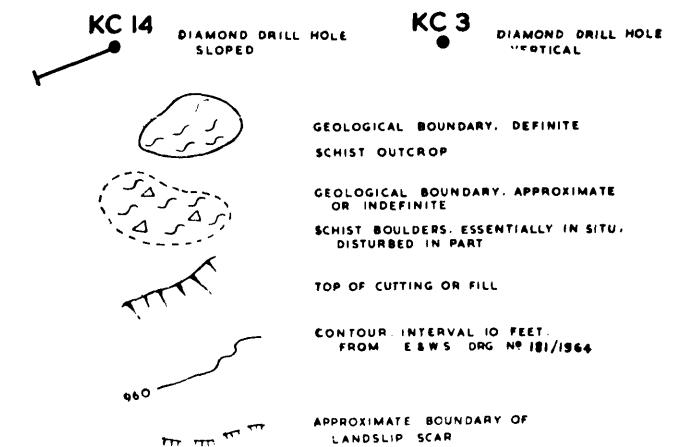
ROCK TYPE



STRUCTURES



WEATHERING



DEPARTMENT OF MINES - SOUTH AUSTRALIA

KANGAROO CREEK DAM
EXPLORATORY ADITS
GEOLOGICAL PLAN AND SECTION

ENGINEERING	J. P. Trudinger	Drm. DW	SCALE: AS SHOWN
GEOLOGY SECTION	GEOLOGIST	Tel. Jace	65-320
		Chd. DW	Ha 5+7
		Ext. 103	DATE: 6 Apr '65

Geology of Adits
made DMS 21 July 65
DMS 21 Sept 65

TUNNEL STATIONS		0+00		0+50		1+00		1+40																	
DIRECTION, INVERT LEVEL, SLOPE																									
PROGRESS HEADING AT, DATE		15 July '65		16 July		19 July		20 July '65		21 July		22 July		23 July		24 July		26 July		27 July		28 July		29 July '65	
ROCK TYPE and DEGREE of WEATHERING		GRANITIC GNEISS and SCHIST Mainly moderate to high								SCHIST and GNEISS Mainly FRESH to SLIGHT. Moderate to high near joints and seams.															
LOG OF FACE Looking in direction of tunnel stations AND SECTIONS SHOWING OVERBREAK																									
PLAN, 4 feet above floor																									
SOUTH SIDE																									
ROOF																									
NORTH SIDE																									
STRUCTURES JOINTING PATTERN-ATTITUDE, SPACING, PERSISTENCE, CHARACTER SURFACE, SEPARATION COATING FAULTS SHEARED AND CRUSHED ZONES, ATTITUDE, RELATIVE DISPLACEMENT, WIDTH, CHARACTER OF MATERIAL																									
EXCAVATION CONDITION		PERCENT BREAKAGE ALONG JOINTS: 25, 45, 20, 60, 5 SUPPORT DURING CONSTRUCTION: SOUTH SIDE (Springing line), ROOF (Unsuported), NORTH SIDE																							
EXCAVATION STRIPPING		ADVANCE NO of HOLES: Jack pick, 6 to 12 holes 1 to 2 ft. long, 1 to 4 lbs. AN 60 INITIAL QUANTITY, DATE: Rounds mainly 19 to 21 holes, 4 to 5 ft. long, with 25 to 30 lbs AN 60 gelignite, 4 to 5 ft. advance.																							
GROUND WATER		QUANTITY, DATE: Mainly dry, several areas of seepage TEMPERATURE: Dry. (May '67)																							
FEELER HOLES & GROUTING		None																							
PHOTOGRAPHS CATALOGUE NO		KC 49/8/65, KC 48/8/65, KC 60/8/65, KC 51/8/65, KC 47/8/65, KC 50/8/65, KC 62/8/65, KC 52/8/65, KC 45/8/65, KC 53/8/65																							
FINAL SUPPORT ESTIMATED OR LINING AS CONSTRUCTED																									
STRIKE & DIP OF JOINT STRIKE OF VERTICAL JOINT HORIZONTAL JOINT STRIKE & DIP OF FOLIATION STRIKE & DIP OF BEDDING		HW HIGHLY WEATHERED CW COMPLETELY WEATHERED CRUSHED SEAM Showing dip SHEARED or CRUSHED ZONE Showing dip and width. FAULT Showing relative movement. LEGEND 200 @ WATER INFLOW 200 gallons per hour. S SEEPAGE ○ PHOTO BLACK & WHITE ● PHOTO COLOUR Vein of QUARTZ SCHIST GNEISS GRANITIC GNEISS SPECIMEN COLLECTED TUNNEL SUPPORTS III STEEL SETS WALL PLATES ROCK BOLTS MESH GUNIT																							
ENGINEERING GEOLOGY SECTION		LOGGED J.P.T. DRAWN J.P.T. GEOLOGIST SENIOR GEOLOGIST																							
S. A. DEPARTMENT OF MINES		KANGAROO CREEK DAM EXPLORATORY ADIT No 2 GEOLOGICAL LOG SCALE 1" = 10' DATE LOGGED 2 Aug. '65 SHEET 1 OF 1 65-827 Ho. 5+7																							

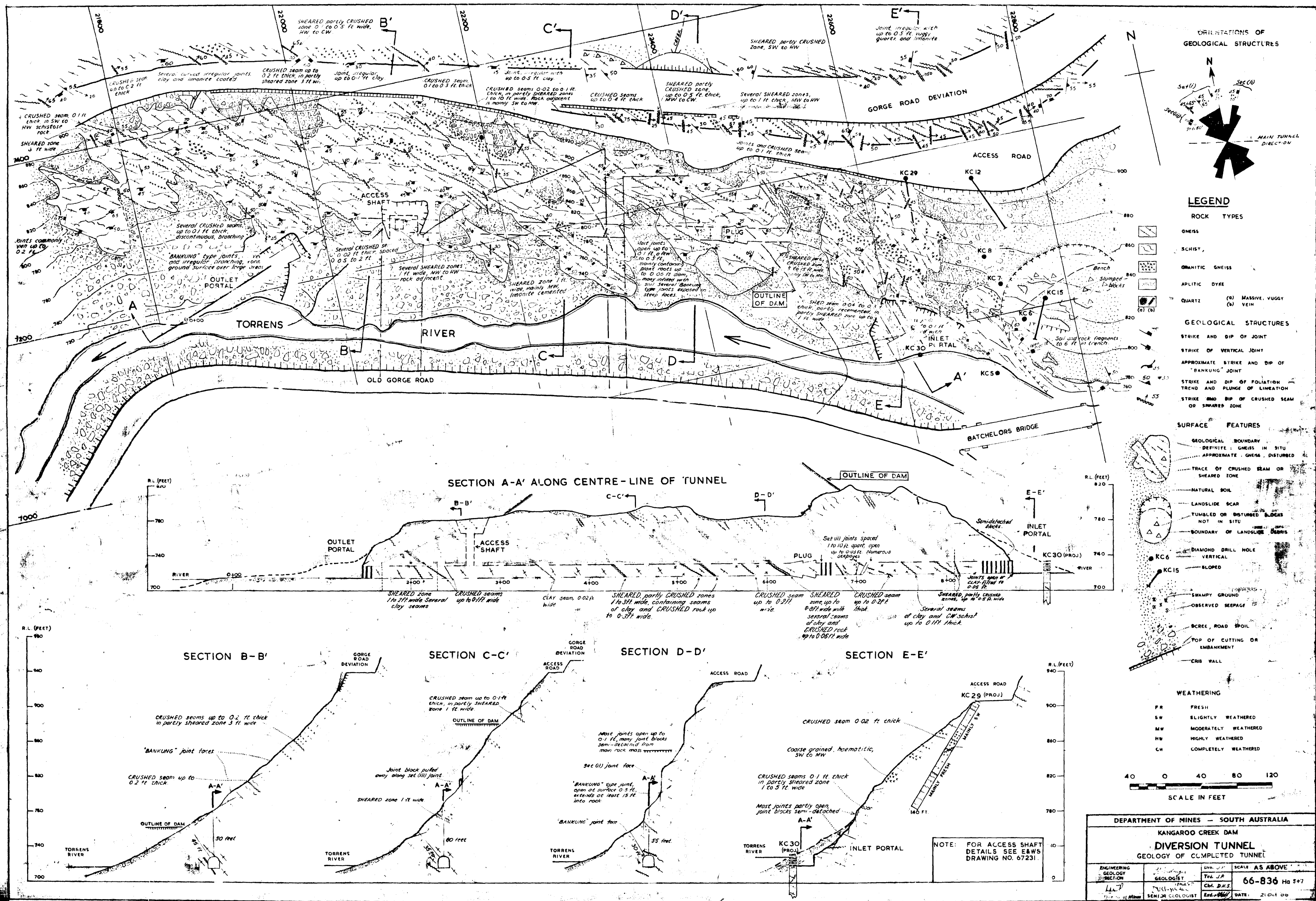
APPENDIX C

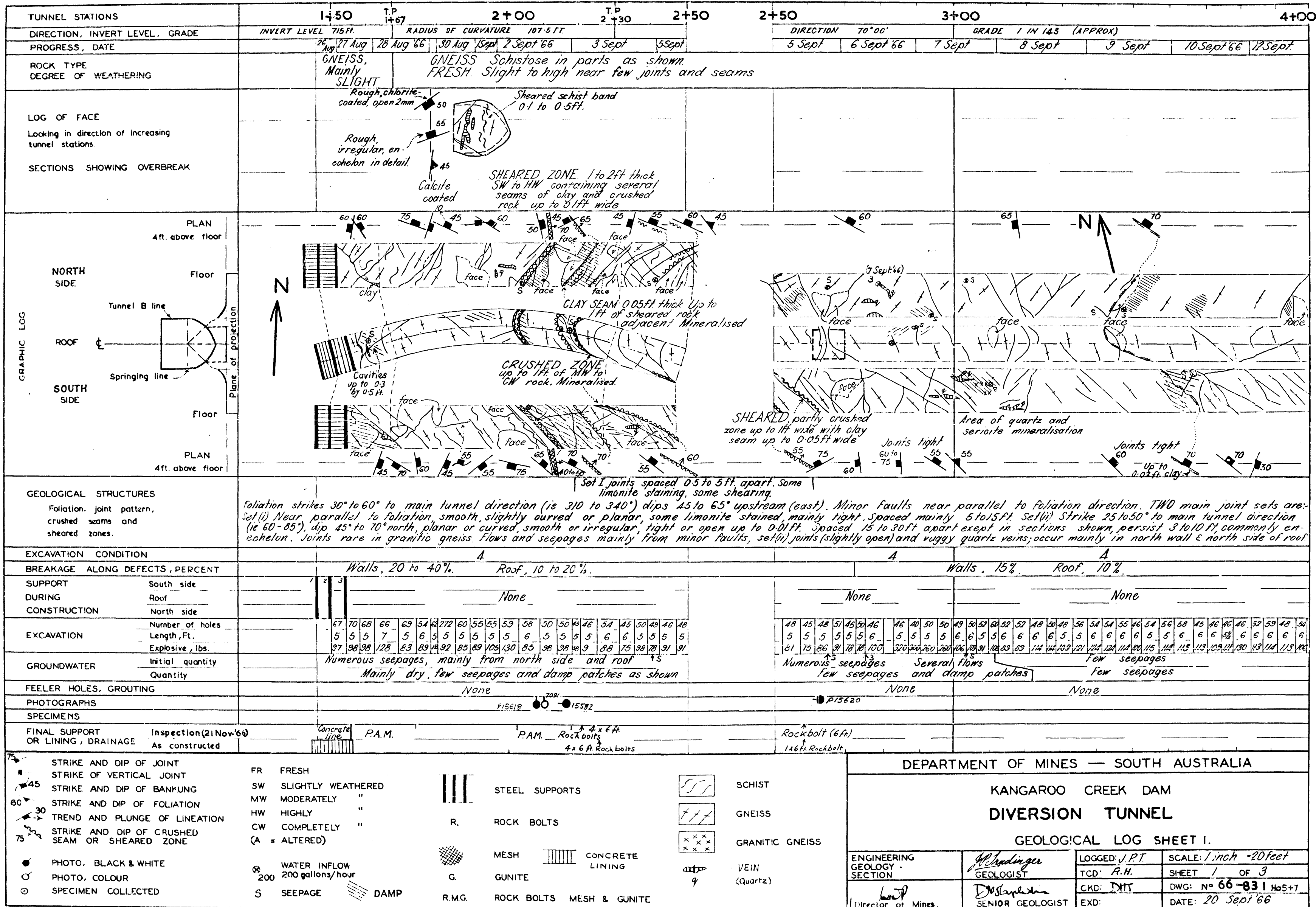
LOGS OF DIVERSION TUNNEL

The explanatory notes in Appendix B also
apply to Appendix C.

<u>FIGURES</u>	<u>DWG. NO.</u>
Kangaroo Creek Dam, Diversion Tunnel, Geological Log Sheet 1	66-831
Kangaroo Creek Dam, Diversion Tunnel, Geological Log Sheet 2	66-980
Kangaroo Creek Dam, Diversion Tunnel, Geological Log Sheet 3	66-991
Kangaroo Creek Dam, Diversion Tunnel, Geology of Completed Tunnel	66-836

DEPARTMENT OF MINES — SOUTH AUSTRALIA			
KANGAROO CREEK DAM DIVERSION TUNNEL GEOLOGICAL LOG SHEET 2			
ENGINEERING GEOLOGY SECTION	<i>J. Lindinger</i> GEOLOGIST	LOGGED: <i>J.P.T.</i> TCD: <i>R.H.</i>	SCALE: <i>1 inch = 20 feet</i> SHEET <i>2</i> OF <i>3</i>
<i>Lee</i> Director of Mines.	<i>D. S. L. Phillips</i> SENIOR GEOLOGIST	CKD: <i>DWS</i> EXD:	DWG: <i>Nº 66-980 Ha5-7</i> DATE: <i>3 Nov '66</i>





TUNNEL STATIONS

DIRECTION, INVERT LEVEL, GRADE

PROGRESS, DATE

ROCK TYPE

DEGREE OF WEATHERING

LOG OF FACE

Looking in direction of increasing tunnel stations.

SECTIONS SHOWING OVERBREAK

7+00

7+50

8+00

8+20

8+20

283°33'

RADIUS OF CURVATURE 107.5 FT.

GRADE 1 IN 143 (APPROX.)

3 Oct '66

4 Oct '66

5 Oct '66

6 Oct '66

7 Oct '66

11 Oct '66

12 Oct '66

Mainly GNEISS and GRANITIC GNEISS. Some SCHIST.

Mainly FRESH SLIGHT to MODERATE patches in GRANITIC GNEISS.

SLIGHT near joints and seams.

PLAN

4ft. above floor

Floor

PLAN

4ft. above floor

NORTH SIDE

ROOF

SOUTH SIDE

Tunnel B line

Springing line

Plane of projection

70

75

50

80

60

35

80

55

45

66

Several joints spaced 0.5 to 3ft. apart. Open up to 0.02 ft. Seepages.

3 seams of CLAY 0.01 to 0.03ft wide.

Pyrite mineralisation.

SHEARED, partly CRUSHED zone 0.02 to 0.04ft wide. Up to 0.02ft of CLAY and CW rock.

70

75

50

80

60

35

80

55

45

66

60

55

55

DIRECTION 161°30'

INVERT LEVEL RL 720 FT.

13 Oct '66

14 Oct '66

17 Oct '66

18 Oct '66

20 Oct '66

21 Oct '66

24 Oct '66

Mainly GNEISS.

FRESH to SLIGHT.

60

55

55

SHEARED, partly CRUSHED zone 0.1 to 0.5 ft wide.

Faces coated with up to 0.02ft limonite and clay.

60

55

55

60

55

55

Tunnel parallel to foliation.

large joint faces.

60

55

55

60

55

55

Joints contain up to 0.05ft of CLAY. Some open up to 0.02ft.

60

55

55

60

55

55

SEAM contains up to 0.05ft of grey CLAY and CW rock.

Irregular weathered seam, up to 0.3ft wide.

Foliation smooth, slightly curved or planar, some limonite stained, mainly tight. Spaced 5 to 15ft. Set (ii). Strike 25 to 50° to main tunnel direction (ie 60 to 85°), dip 45 to 70° north, planar or curved, smooth or irregular, tight or open up to 0.01ft. Spaced mainly 15 to 30ft apart, except in sections shown, persist 3 to 10ft, commonly en echelon. Joints rare in granitic gneiss. Flows and seepages mainly from minor faults, set (i) joints (slightly open), and ruggy quartz veins; occur mainly in north wall and north side of roof.

60

55

55

60

55

55

Foliation strikes 30-60° to main tunnel direction (ie 310 to 340) dips 45 to 65° upstream (east). Minor faults near parallel to foliation direction. TWO main joint sets are: Set (i) Near parallel to foliation direction. Spaced 5 to 15ft. Set (ii) Strike 25 to 50° to main tunnel direction (ie 60 to 85°), dip 45 to 70° north, planar or curved, smooth or irregular, tight or open up to 0.01ft. Spaced mainly 15 to 30ft apart, except in sections shown, persist 3 to 10ft, commonly en echelon. Joints rare in granitic gneiss. Flows and seepages mainly from minor faults, set (i) joints (slightly open), and ruggy quartz veins; occur mainly in north wall and north side of roof.

60

55

55

60

55

55

SEAM contains up to 0.05ft of grey CLAY and CW rock.

Irregular weathered seam, up to 0.3ft wide.

Foliation smooth, slightly curved or planar, some limonite stained, mainly tight. Spaced 5 to 15ft. Set (ii). Strike 25 to 50° to main tunnel direction (ie 60 to 85°), dip 45 to 70° north, planar or curved, smooth or irregular, tight or open up to 0.01ft. Spaced mainly 15 to 30ft apart, except in sections shown, persist 3 to 10ft, commonly en echelon. Joints rare in granitic gneiss. Flows and seepages mainly from minor faults, set (i) joints (slightly open), and ruggy quartz veins; occur mainly in north wall and north side of roof.

60

55

55

60

55

55

SEAM contains up to 0.05ft of grey CLAY and CW rock.

Irregular weathered seam, up to 0.3ft wide.

Foliation smooth, slightly curved or planar, some limonite stained, mainly tight. Spaced 5 to 15ft. Set (ii). Strike 25 to 50° to main tunnel direction (ie 60 to 85°), dip 45 to 70° north, planar or curved, smooth or irregular, tight or open up to 0.01ft. Spaced mainly 15 to 30ft apart, except in sections shown, persist 3 to 10ft, commonly en echelon. Joints rare in granitic gneiss. Flows and seepages mainly from minor faults, set (i) joints (slightly open), and ruggy quartz veins; occur mainly in north wall and north side of roof.

60

55

55

60

55

55

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60

55

55

60

55

55

SEAM contains up to 0.05ft of grey CLAY and CW rock.

Irregular weathered seam, up to 0.3ft wide.

Foliation smooth, slightly curved or planar, some limonite stained, mainly tight. Spaced 5 to 15ft. Set (ii). Strike 25 to 50° to main tunnel direction (ie 60 to 85°), dip 45 to 70° north, planar or curved, smooth or irregular, tight or open up to 0.01ft. Spaced mainly 15 to 30ft apart, except in sections shown, persist 3 to 10ft, commonly en echelon. Joints rare in granitic gneiss. Flows and seepages mainly from minor faults, set (i) joints (slightly open), and ruggy quartz veins; occur mainly in north wall and north side of roof.

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SEAM contains up to 0.05ft of grey CLAY and CW rock.

Irregular weathered seam, up to 0.3ft wide.

Foliation smooth, slightly curved or planar, some limonite stained, mainly tight. Spaced 5 to 15ft. Set (ii). Strike 25 to 50° to main tunnel direction (ie 60 to 85°), dip 45 to 70° north, planar or curved, smooth or irregular, tight or open up to 0.01ft. Spaced mainly 15 to 30ft apart, except in sections shown, persist 3 to 10ft, commonly en echelon. Joints rare in granitic gneiss. Flows and seepages mainly from minor faults, set (i) joints (slightly open), and ruggy quartz veins; occur mainly in north wall and north side of roof.

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SEAM contains up to 0.05ft of grey CLAY and CW rock.

Irregular weathered seam, up to 0.3ft wide.

Foliation smooth, slightly curved or planar, some limonite stained, mainly tight. Spaced 5 to 15ft. Set (ii). Strike 25 to 50° to main tunnel direction (ie 60 to 85°), dip 45 to 70° north, planar or curved, smooth or irregular, tight or open up to 0.01ft. Spaced mainly 15 to 30ft apart, except in sections shown, persist 3 to 10ft, commonly en echelon. Joints rare in granitic gneiss. Flows and seepages mainly from minor faults, set (i) joints (slightly open), and ruggy quartz veins; occur mainly in north wall and north side of roof.

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SEAM contains up to 0.05ft of grey CLAY and CW rock.

Irregular weathered seam, up to 0.3ft wide.

Foliation smooth, slightly curved or planar, some limonite stained, mainly tight. Spaced 5 to 15ft. Set (ii). Strike 25 to 50° to main tunnel direction (ie 60 to 85°), dip 45 to 70° north, planar or curved, smooth or irregular, tight or open up to 0.01ft. Spaced mainly 15 to 30ft apart, except in sections shown, persist 3 to 10ft, commonly en echelon. Joints rare in granitic gneiss. Flows and seepages mainly from minor faults, set (i) joints (slightly open), and ruggy quartz veins; occur mainly in north wall and north side of roof.

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SEAM contains up to 0.05ft of grey CLAY and CW rock.

Irregular weathered seam, up to 0.3ft wide.

Foliation smooth, slightly curved or planar, some limonite stained, mainly tight. Spaced 5 to 15ft. Set (ii). Strike 25 to 50° to main tunnel direction (ie 60 to 85°), dip 45 to 70° north, planar or

APPENDIX D

KANGAROO CREEK DAM
LABORATORY TESTS ON ROCK MATERIALS

CONTENTS

TABLE 1.	Spoil from Exploratory Adits, Particle Size Distribution.	
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NOTE Tables 1 and 2 by E. & W.S. Concrete Laboratory, Sassafrass
 Tables 3 and 4 and Figure 1, from Unconfined Compressive Tests by Dams Section, E. & W.S. Department.

APPENDIX D

KANGAROO CREEK DAM LABORATORY TESTS ON ROCK MATERIALS - SPOIL FROM EXPLORATORY ADITS

TABLE 1 - PARTICLE-SIZE DISTRIBUTION

		Sieve Sizes % Weight Passing																
		18"	12"	9"	7"	6"	5"	4"	1½"	¾"	⅜"	3/16"	7"	14"	25	52	100	200
		100.0	97.3	94.8	91.8	88.8	83.4	76.2	60.2	44.2	31.1	20.4	17.1	12.6	9.2	6.7	5.3	4.5
% Weight Retained			2.7	2.5	3.0	3.0	5.4	17.2	16.0	16.0	13.1	10.7	3.3	4.5	3.4	2.5	1.4	0.8
% Weight of each type retained	Schist		1.4	1.3	1.5	1.3	2.0	2.8										
	Gneiss		1.3	0.8	1.3	1.3	2.2	3.4										
	Granite Gneiss		-	0.4	0.2	0.4	1.2	1.0										

APPENDIX D (CONT'D)

TABLE 2 - RESULTS OF LABORATORY TESTS

		Size	Los Angeles %	S.G. S.S.D.	Absorption %	Soundness 5 cycles Av. % Loss	Elongation Index %	Flakiness Index %	Liquid Limit	Plastic Limit	Plasticity Index	Linear Shrinkage	Shrinkage Ratio
Only 1 rock was taken for each test due to large size	Schist	+6"		2.80	0.242	0.22							
	Gneiss	+6"		2.74	0.400	0.75							
	Granite Gneiss	+6"		2.68	0.475	0.80							
	Schist	-1½" + 1"	42.6	2.68	0.780	2.71	64.1	50.7					
	Gneiss	-1½" + 1"	36.2	2.71	0.580	5.45	Combined Gneiss and Granite	55.20 16.20					
	Granite Gneiss	-1½" + 1"	38.2	2.62	0.695	5.04			Minus	36+	fraction		
	Combined Sample	-3"	38.6	2.70	0.570	2.45			22.8	12.3	10.5	1.3	1.79

SIZE OF CORE SAMPLE IN MM. 1	DRILL HOLE	DEPTH (ft) 2	ROCK TYPE	FOLIATION	ANGLE 3	WEATHERING	OTHER GEOLOGICAL FEATURES	UCS. 4	YOUNGS MODULUS 5	FRACTURE
54 x 101	HC3	13	Schist	Intensely foliated.	35°	Fresh. Limonite stained along foliation in part.	Sericitic. Some disseminated haematite and pyrite.	2210	800,000	Two fractures, 60° to 80°, irregular, very rough. Few Sericite coatings.
54 x 139	HC6	10	Schist	Intensely foliated to banded, abundant quartz and feldspar.	40°	Slightly weathered, common limonite staining.	Abundant sericite. Abundant pyrite and 'leached haematite'?	3020	2,100,000	Single fracture, 60°. Planar, regular, slightly rough, sericite coated.
54 x *	HC6	11	Schist	Mainly intensely foliated, few distinct coarser bands.	40°	Slight to moderate, limonite stained throughout.	Abundant sericite and 'leached haematite'?	6100	5,500,000	Complex fracture. Several at 60° to 90°.
46 x 144	HC1	16	Schist	Intensely foliated, commonly coarser grained and banded.	45°	Fresh to slight, limonite stained in parts, limonite coated on joints.	Sericite rich, some pyrite and haematite. Several joints.	2880	1,800,000	Two fractures 65°. Planar, slightly irregular, slightly rough, part influenced by joints.
46 x *	HC1	15	Schist	Intensely foliated, few coarser grains, banded in part.	50°	Slight, limonite stained throughout.	Sericite rich.	3120	1,400,000	? Single fracture, 60°. Planar, slightly rough.
54 x 121	HC3	12	Schist	Intensely foliated, very irregular in part.	50°	Fresh. Some slight limonite staining.	Some haematite and crystalline pyrite. Sericitic.	2970	920,000	Single fracture, 65°. Planar, slightly irregular, very rough. Common Sericite coatings.
54 x 127	HC2	15.5	Schist	Intensely foliated to coarse grained and banded, irregular.	50°	Slight to moderate, limonite stained and coated throughout.	Sericite in schistose bands.	5250	5,200,000	Complex. Main fracture 70°, planar but irregular, rough. Several other breaks.
46 x 152	HC1	17	Schist	Intensely foliated.	50°	Fresh. Slight to moderate along joint near top of core.	Sericitic. Joint parallel to foliation at top of core.	3980	2,350,000	Two fractures. One part parallel to, part steeper than foliation. Other along joint.
62 x 149	HC2	12	Schist	Intensely foliated, banded in part.	50°	Slight to moderate. Abundant limonite staining throughout.	Sericitic, some disseminated haematite.	4320	2,200,000	Single fracture, 65°. Planar, slightly irregular, slightly rough.
54 x 152	HC6	14	Schist	Intensely foliated to banded, coarse to very coarse grained in part.	50°	Slight, limonite stained throughout, limonite coated on joints.	Sericite rich. Some pyrite and haematite. Several joints.	4500	5,000,000	Two near vertical fractures, one across fabric, one along joint.
62 x 151	HC2	13	Schist	Intensely foliated to banded, commonly irregular.	60°	Slight to moderate, limonite stained throughout.	Sericitic. Abundant disseminated haematite.	2880	2,700,000	Single fracture, 65°. Planar to very irregular, slightly rough. Sericite coatings.
54 x 152	HC3	15	Schist	Intensely foliated, slightly banded in few parts.	70°	Slight. Abundant limonite staining through fabric of rock.	Sericitic. Some disseminated pyrite and haematite.	5030	2,600,000	Single fracture, 70°. Planar, slightly irregular, slightly rough. Near parallel to foliation.
54 x 152	HC4	18	Gneiss	Banded to intensely foliated.	20°	Slight. Mainly limonite stained through fabric of rock.	Abundant sericite, some pyrite. Several joints.	12,900	7,400,000	Single fracture, 70°, very irregular, rough. Several other cracks along joints.
64 x 128	HC5	11	Gneiss	Intensely foliated to banded. Mainly fine to very fine grained.	30°	Fresh.	Some sericite in foliated bands. Some disseminated pyrite.	12,400	12,000,000	Complex. Main fracture irregular, very slightly rough, few sericite coatings. Several other breaks.
54 x *	HC7	10.5	Gneiss	Mainly fine grained, banded to closely foliated, poorly developed.	30°	Slight, limonite stained throughout.	Some sericite and disseminated haematite.	10,600	4,300,000	Complex fractures.
54 x 152	HC4	15	Gneiss	Mainly intensely foliated, few coarser bands, often irregular.	40°	Fresh to slight. Some limonite staining.	Abundant disseminated pyrite and haematite.	11,670	7,000,000	Single fracture, 70°, along limonite coated joint. Few other breaks across core.
54 x 151	HC5	13	Gneiss	Mainly intensely foliated, slightly banded in part.	40°	Fresh.	Some disseminated pyrite.	10,000	8,400,000	Single fracture, very irregular. Part along foliation, smooth part across fabric, rough.
54 x 152	HC7	13	Gneiss	Banded, intensely foliated in parts. Coarse grained.	40°	Slight. Mainly limonite stained throughout.	Abundant sericite. Pyrite disseminated and in crystals.	5,440	4,000,000	Single fracture, 70°. Planar, slightly irregular, rough, few sericite coatings.
54 x 134	HC5	12	Gneiss	Intensely foliated, few coarser bands, mainly poorly developed.	45°	Fresh.	Some disseminated pyrite.	8700	12,000,000	Single fracture, 65°. Planar, slightly irregular, slightly rough. Few other cracks.
54 x 152	HC7	12	Gneiss	Mainly banded, intensely foliated in part.	50°	Fresh to slight, some limonite staining.	Sericitic. Disseminated pyrite and haematite.	11,100	5,000,000	Complex. Main fracture 65°, planar, irregular, rough. Several other irregular fractures.
54 x 151	HC4	21	Granitic Gneiss	Very coarse grained, foliation very poorly developed.	20°	Fresh. Slight limonite staining in few parts.	Mainly quartz & feldspar crystals.	13,100	5,600,000	Two fractures, very rough, irregular, 70° to 90°.
46 x 150	HC8	16	Granitic Gneiss	Mainly coarse grained, banded, closely foliated in part.	30°	Fresh to slight. Some limonite staining in coarser bands.	Some disseminated haematite.	10,800	6,000,000	Single fracture, 70°. Planar, slightly irregular, rough. Few other breaks.
46 x 131	HC8	13.5	Granitic Gneiss	Mainly banded, intensely foliated in few parts.	40°	Fresh.	Coarse to very coarse grained. Some sericite.	13,400	6,000,000	Single fracture, very irregular, very rough. Few other irregular fractures.
46 x *	HC8	14	Granitic Gneiss	Banded to intensely foliated, poorly developed.	40°	Fresh. Some limonite staining in parts.	Coarse to very coarse grained.	14,900	6,000,000	Complex. Two fractures at 70° to 90°.

NOTES

- 1 Size of core samples in millimetres, diameter x length
- 2 Approximate depth to top of sample
- 3 Approximate angle between plane of foliation and the plane normal to the longitudinal axis of the core, i.e. dip of foliation on core (β)
- 4 Unconfined compressive strengths, pounds per square inch
- 5 Youngs Modulus, E, pounds per square inch. Calculated at a stress of 1000 or 2000 lb/sq inch

* Not known.

TESTS CARRIED OUT BY E&WS DEPT - DESIGN BRANCH

TABLE 3

DEPARTMENT OF MINES — SOUTH AUSTRALIA			
KANGAROO CREEK DAM			
STRENGTHS OF ROCKS			
RESULTS OF UNCONFINED TESTS			
ENGINEERING GEOLOGY SECTION	James Rankin GEOLOGIST	Dr. J.P.	SCALE: —
		Tot. ALT	66-251
		Chd. L.V.W.	No 5+7
		Ext. ALT	DATE: 5.4.1966
Director of Mines	SENIOR GEOLOGIST		

SAMPLE No	DRILL HOLE	DEPTH (feet)	ROCK TYPE	FOLIATION	ANGLE (2)	WEATHERING (3)	OTHER GEOLOGICAL FEATURES	U.C.S. DRY	WET (4)	YOUNG'S MODULUS DRY	WET (5)	FRACTURE
P1362/65	KC10	13.8	SAMPLE DESTROYED BEFORE TESTING.									
P1363/65	KC10	14.2	Schist	Mainly banded, closely foliated in parts.	30°	Slight Limonite staining common through fabric of rock	Abundant sericite and disseminated haematite	-	3250 (2wks)	-	530,000	Single fracture, irregular Surface rough, irregular, part coated with sericite
P1366/65	KC23	12.1	Schist	Banded, mainly coarser grained	10°	Slight Limonite stained	Some sericite	7100	-	1,090,000	-	-
P1367/65	KC23	12.5	SAMPLE DESTROYED BEFORE TESTING									
P1371/65	KC27	31.9	Schist	Presumed as below	45°	Presumed as below		3600	-	1,310,000	-	-
P1370/65	KC27	31.5	Schist	Part banded, part intensely foliated	45°	Slight to moderate abundant limonite staining throughout	Abundant sericite, some disseminated haematite	-	2,000 (2wks)	-	570,000	Two fractures at 60°. Several discontinuous cracks Surfaces rough, irregular
P29/66	KC27	93.1	Schist	Mainly banded, foliated in part	40°	Fresh	Sericite rich. Common disseminated haematite	2320	-			Single fracture, planar, slightly rough. Common sericite coatings (6)
P28/66	KC27	92.7	Schist	Close foliation more common.	40°	Fresh. Some slight limonite staining	As above	-	3470 (2wks)	-	-	As above. More irregular
P1369/65	KC23	45.7	Schist	Presumed as below	10°	Presumed as below		6,400	-	415,000		
P1368/65	KC23	45.3	Schist	Foliated to banded, irregular, poorly developed	10°	Fresh to slight. Some limonite staining within fabric of rock	Abundant sericite and disseminated haematite	-	4450 (1wk)	-	417,000	Single fracture. Planar, very rough
P22/66	KC20	31.8	Schist	Foliated to banded	10°	Fresh	Abundant sericite, some pyrite in coarser bands	5800	-			Single fracture, very irregular, rough. Common sericite coatings.
P23/66	KC20	32.3	Schist	As above, but coarser grained, more banded	10°	Fresh	As above.	-	4140 (2 wks)			Complex fracture, numerous cracks. "Cone" failure evident
P25/66	KC23	32.6	Schist	Fine grained, foliation very poorly developed	0°	Fresh	Some disseminated haematite	12,830	-			Complex fracture, numerous cracks "Cone" failure evident.
P24/66	KC23	32.2	Schist	As above.	0°	Fresh	As above	-	8280 (2 wks)			Single fracture, planar, rough. Several parallel discontinuous cracks.
P1373/65	KC20	28.2	Schist	Presumed as below	0°	Presumed as below		7100	-	336,000	-	-
P1372/65	KC20	27.7	Schist	Intensely foliated, few coarser bands, irregular	0°	Fresh	Sericite rich	-	5450 (1wk)	-	310,000	Single fracture. Very irregular, rough. Few sericite coatings
P1364/65	KC10	56.1	Schist	Mainly intensely foliated, few coarser bands	20°	Fresh. Some limonite staining in coarser bands		5300	-	614,000	-	-
P1365/65	KC10	56.5	Schist	As above.	20°	As above		-	3800 (1wk)	-	547,000	Single fracture, planar, smooth to slightly rough. Sericite coated (pre-existing fracture?)
P26/66	KC25	92.6	Schist	Intensely foliated. Coarser grains not banded.	50°	Fresh	Sericite rich, some pyrite	3,660	-			Single fracture. Mainly planar, irregular in part, rough. Rare Sericite coatings
P27/66	KC25	93.0	Schist	As above	50°	Fresh	As above, with some disseminated haematite	-	1300 (2wks)			Single fracture Planar slightly rough

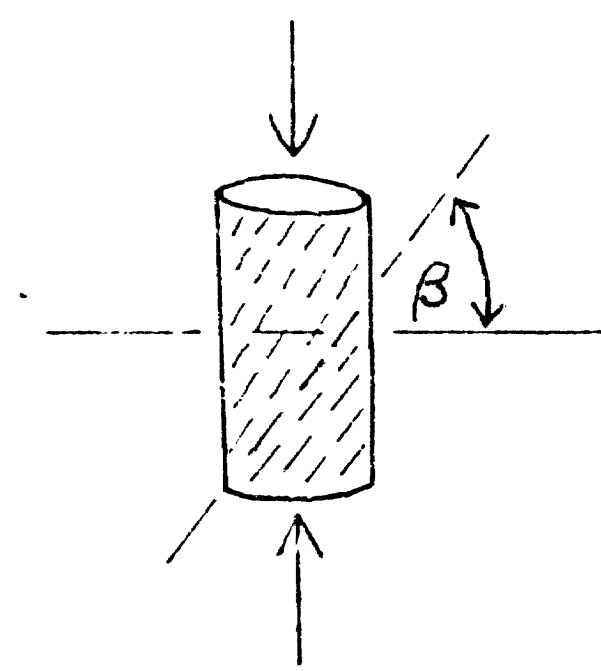
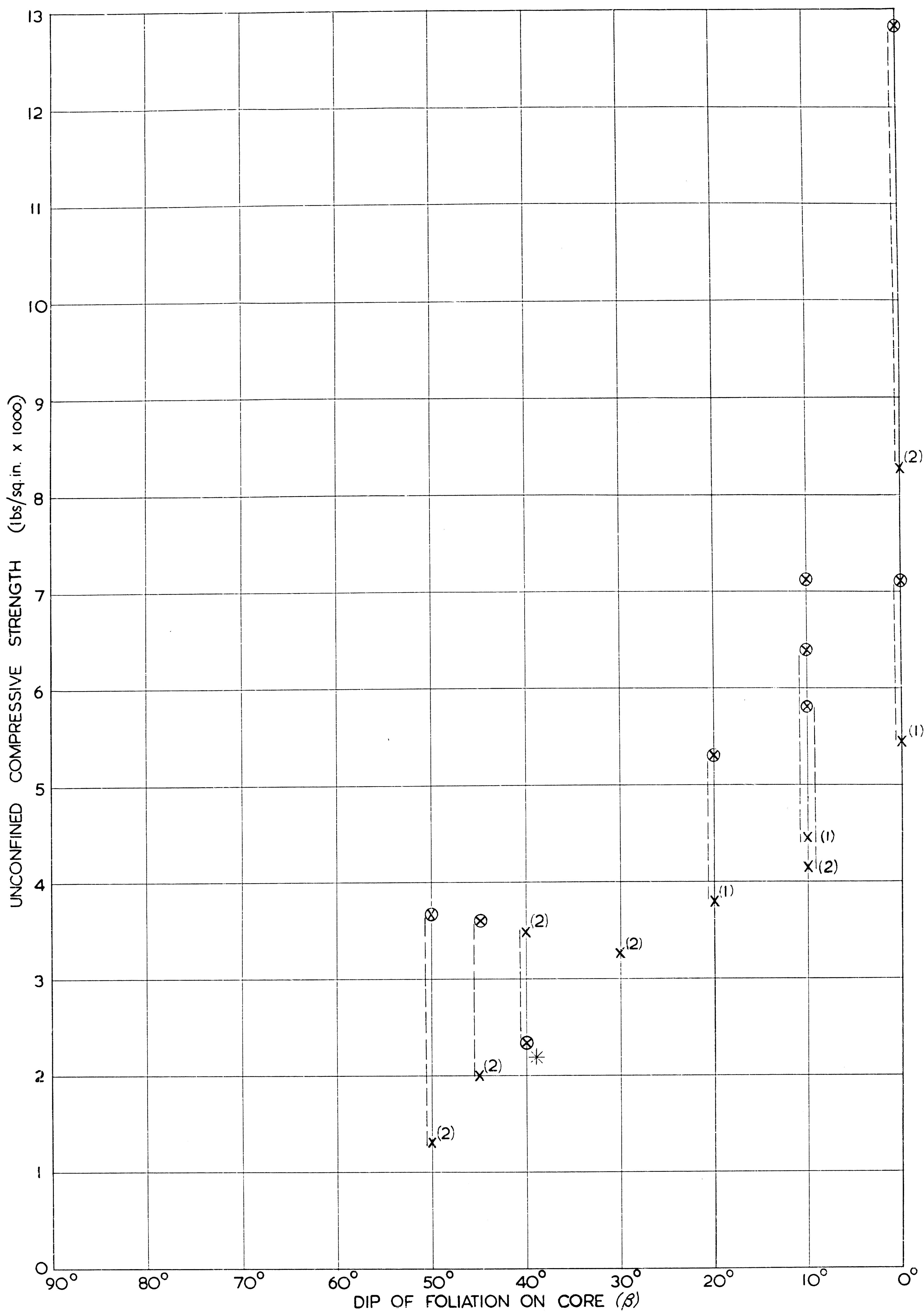
NOTES

1. Approximate depth to top of sample.
2. Approximate angle between plane of foliation or fracture and the plane normal to the longitudinal axis of the core i.e. dip of foliation on core (β)
3. Degrees of weathering are defined as follows:
 Fresh: The rock shows no discoloration or loss of strength
 Slight: The rock is slightly discolored but not noticeably lower in strength than the fresh rock
 Moderate: The rock is usually discolored and noticeably weakened, but NMLC or NMS cores cannot be broken in unaided hands.
4. Unconfined compressive strength, pounds per square inch. Samples were tested in pairs. One of each pair was tested dry. The other of the pair was soaked in water for 1 or 2 weeks before testing [Indicated under test value (2wks)]
5. Young's Modulus was evaluated for each specimen under a stress of 1000 lbf/inch
6. Low dry strength may be due to error in testing procedure

TESTS CARRIED OUT BY E&W'S DEPT - DESIGN BRANCH

TABLE 4

DEPARTMENT OF MINES - SOUTH AUSTRALIA			
KANGAROO CREEK DAM			
WET/DRY STRENGTHS OF ROCKS			
RESULTS OF UNCONFINED TESTS			
ENGINEERING GEOLOGY SECTION	Dr. J.P. Tol. RLT	SCALE: -	66-256
Director of Mines	Chd. L.V.W.	Ha 5.7	
SENIOR GEOLOGIST	Ext. L.V.W.	DATE: 6.4.66	



NOTES

- FOR DETAILS OF SAMPLES AND TYPES OF FAILURE SEE DRAWING NO. 66-256.
- ⊗ AIR DRY SAMPLE.
x WET SAMPLE.
(1) SOAKED FOR 1 WEEK.
(2) SOAKED FOR 2 WEEKS.
- ⊗
x PAIRED SAMPLE.
* AN ERROR OCCURED IN EXPERIMENTAL PROCEDURE DURING TESTING OF AIR DRY SAMPLE.

FIGURE 1

TESTING CARRIED OUT BY E.&W.S. DEPT. - DESIGN BRANCH.

DEPARTMENT OF MINES — SOUTH AUSTRALIA			
KANGAROO CREEK DAM			
WET/DRY STRENGTHS OF SCHIST			
EFFECT OF ANISOTROPY ON STRENGTH			
ENGINEERING GEOLOGY SECTION	Drn. J.P.	SCALE:	
Lu J.P.	Tcd. M.F.D.	66 - 346	
Senior Geologist	Ckd. L.V.W.	Ho 5+7.	
Exd. Lu J.P.	DATE: 18-5-66		

APPENDIX E

ACCELERATED WEATHERING TESTS ON SCHIST

REPORT BY HIGHWAYS AND LOCAL GOVERNMENT
DEPARTMENT

C.R. SANDMAN
Testing Officer

RECEIVED BY HIGHWAYS AND LOCAL GOVERNMENT DEPARTMENT
H. & L.G.D. 3008/64
Laboratory Project No.
120

1.12.1964.

1. INTRODUCTION

In connection with dam site investigations at Kangaroo Creek being conducted by the Department of Mines on behalf of the Engineering and Water Supply Department, the following laboratory test work was carried out.

- (1) Specific Gravity and water absorption tests on bulk samples on crushed aggregate.
- (2) Standard wet/dry weathering test as conducted by D.M.R. (N.S.W.).
- (3) Combined effect of temperature cycles and weak salt solutions: A.S.T.M. C218 - 48T.
- (4) Chemical analysis of extract waters recovered from weathering tests.
- (5) Sodium sulphate soundness test.

2. SUMMARY

Specific Gravity and water absorption results (see Table 1) show that there was no significant difference between the diamond drill core samples and the spall material. Water absorption of all samples tested was comparatively low, ranging from 1.05 to 1.21%. Weathering tests conducted on spall samples and on crushed aggregate showed that they could withstand repeated conditions of wetting and drying, without suffering any significant mechanical disintegration. No physical breakdown of spall samples occurred during 20 wet/dry cycles, and only slight breakdown of crushed aggregate was apparent after 10 wet/dry cycles (see Table 4).

Chemical analyses of extract water recovered from the 1st, 5th and 10th wet cycle of weathering (spalls and $\frac{3}{4}$ inch material) showed no significant increase in soluble salt content. However, there was a sharp increase in soluble salt concentration after 20 wet/dry cycles (see Tables 2 and 3). The combined effect of temperature and weak salt solutions (A.S.T.M. C218 - 48T) indicated no significant trends in the behaviour of the test specimens. The results (see Table 5) show that absorptions varied in the range -4.3 to +7.0% and volumes in the range -0.39 to +2.43%. One test specimen C3-5, from Hole 11 failed completely after 30 cycles. This particular specimen showed partial failure prior to testing. All other specimens tested were not visibly affected after 30 cycles.

The resistance of crushed aggregate ($-1\frac{1}{2}'' + 3/16''$) to disintegration by saturated sodium sulphate solution was 7.5%. This figure indicates that the material would not be subject to serious disintegration when exposed to normal conditions of weathering and frost action.

3. MATERIAL EXAMINED

Three samples of fresh rock material were submitted for testing, namely,

- (1) Spalls from an excavation on the left bank
- (2) Core from Drill Hole K.C. 10, 30 to 31-1ft., schistosity at 90° to core.
- (3) Core from Drill Hole K.C. 11, 78 to 80ft., schistosity at 10° to core.

4. SAMPLE PREPARATION

Because of the small amount of drill core available only a limited number of specimens could be prepared for testing as in A.S.T.M. 218 - 48T. Wherever possible core specimens measuring 3 inches in length were cut using a diamond saw operated with a copious flow of water. In similar fashion irregular cubes were cut from individual spalls considered representative of the rock type. It was not possible to obtain perfect cubes as specified. Samples of crushed material used for Specific Gravity determinations and for the D.M.R. (N.S.W.) Weathering Test were prepared by stage crushing designed to minimise the production of fines.

5. EXPERIMENTAL PROCEDURE

5.1 Specific Gravity and Water Absorption

This test work was conducted according to the test method described in British Standard 812:1960. Test results are given in Table 1.

5.2 Weathering Tests

Accelerated weathering tests were done on lump material and on aggregate stage-crushed to pass a $\frac{3}{4}$ inch sieve. Distilled water was used for each of the soaking cycles and controlled drying was effected by use of sand baths. At the end of the 1st, 5th, 10th and 20th wet cycles, sufficient water was syphoned from each test on which to conduct analyses for total soluble salts. The results of these analyses are shown in Tables 2 and 3.

Table 1 Specific Gravity and Water Absorption

Sample	Specific Gravity and Water Absorption
Spall samples	S.G. (Appt.) = 2.80 S.G. (S.S.D.) = 2.75 S.G. (Bulk) = 2.72 Water Absorption % = 1.11
Crushed Spall Samples $\frac{3}{4}$ " $\frac{3}{8}$ "	S.G. (Appt.) = 2.80 S.G. (S.S.D.) = 2.75 S.G. (Bulk) = 2.72 Water Absorption % = 1.09
Core specimens Hole K.C. 10	S.G. (Appt.) = 2.79 S.G. (S.S.D.) = 2.74 S.G. (Bulk) = 2.70 Water Absorption % = 1.21
Core Specimens Hole K.C. 11	S.G. (Appt.) = 2.80 S.G. (S.S.D.) = 2.75 S.G. (Bulk) = 2.72 Water Absorption % = 1.05

NOTE: S.G. (S.S.D) Denotes Specific Gravity on surface saturated dry basis.

S.G. (Bulk) Denotes Specific Gravity on surface dry basis.

Table 2 Chemical Analysis of Decant Water from
Weathering of Spall Samples

Assumed Composition	Soluble Salt Concentration gr./gal.			
	After 1st Cycle	After 5th Cycle	After 10th Cycle	After 20th Cycle
CaCO ₃	0.87	0.66	1.32	1.71
CaSO ₄	-	-	-	2.65
CaCl ₂	-	-	-	-
MgCO ₃	0.83	0.31	0.83	-
MgCl ₂	-	-	-	0.04
MgSO ₄	-	-	-	0.75
Na ₂ CO ₃	1.22	1.70	-	-
Na ₂ SO ₄	0.85	0.68	1.25	-
NaCl	1.48	1.12	1.42	2.76
NaNO ₃	0.10	0.15	0.10	0.10
KCl	-	-	-	-
Total	5.35	4.62	4.92	8.01

Table 3 Chemical Analysis of Decant Water from Weathering of
-3/4" Aggregate

Assumed Composition	Soluble Salt Concentration gr./gal.			
	After 1st Cycle	After 5th Cycle	After 10th Cycle	After 20th Cycle
CaCO ₃	0.50	1.51	2.04	6.64
CaSO ₄	-	1.20	1.20	15.30
CaCl ₂	-	-	-	2.82
MgCO ₃	0.62	-	-	-
MgCl ₂	-	-	-	1.54
MgSO ₄	-	0.13	2.32	-
Na ₂ CO ₃	1.34	-	-	-
Na ₂ SO ₄	0.85	2.19	0.57	8.75
NaCl	0.49	0.75	0.87	-
NaNO ₃	0.10	0.10	0.10	0.10
KCl	-	-	-	-
Total	3.90	5.88	7.1	35.15

Table 4 Weathering Test on Stage-Crushed minus $\frac{3}{4}$ " Material

Sieve Size B.S.S.	Grading % Passing	
	Before Weathering	After Weathering
$\frac{3}{4}$ inch	100	100
$\frac{5}{8}$ "	83	90
$\frac{1}{2}$ "	55	59
$\frac{3}{8}$ "	34	39
$\frac{1}{4}$ "	22	29
3/16 inch	18	24
7 mesh	11	18
14 "	7	13
25 "	5	10
36 "	4	9
52 "	3	8
100 "	3	7
200 "	2	6

5.3 Effect of Temperature and Weak Salt Solutions

A.S.T.M. Designation: C218 - 48T.

This test is designed to determine the effect of temperature cycles and weak salt solutions on crystalline natural building stones, exposed to the weather above ground level.

Test specimens were prepared from drill cores and spall samples submitted, and subjected to 30 wet/dry cycles as specified in the test.

Generally most of the specimens showed no visible changes in physical characteristics except in one specimen (C3-5 from Hole 11), which showed distinct failure prior to test. Results of the tests are shown in Table 5.

Table 5 Absorption and Volume Changes - A.S.T.M. C218 - 48T

Sample	W ₁	W ₂	W ₃	W ₄	W ₅	Increase in Absorption %	Increase in Volume %
<u>Core From Hole 10</u>							
C2-1	427.35	433.44	274.13	433.18	274.40	-4.3	-0.35
C2-2	360.84	365.96	231.85	366.15	232.80	3.5	0
C2-3	400.22	405.35	255.12	405.42	254.99	1.56	0.41
C2-4	143.28	145.00	92.35	145.04	92.32	2.5	0.12
<u>Core From Hole 11</u>							
C3-1	422.35	427.85	273.03	427.15	269.75	7.0	2.43
C3-2	423.88	428.85	271.83	429.11	271.95	5.1	0
C3-3	426.81	431.41	274.92	431.44	273.95	0.65	0.60
C3-4	428.89	433.55	277.27	433.79	277.10	5.1	0.4
C3-5	426.80	431.64	273.75	430.80	273.10	-0.14	-0.39
<u>Spalls-</u>							
Cube 1	701.88	712.45	441.45	713.04	442.50	4.98	-0.16
" 2	630.33	642.65	402.39	643.10	401.98	4.10	0.52
" 3	615.08	622.86	395.24	622.92	393.95	0.79	0.55
" 4	716.79	720.27	457.55	720.74	458.40	0.24	-0.17

NOTE:

W₁ = Original weight of oven dried specimen.

W₂ = Original weight of surface-dried specimen after 24 hours immersion in water.

W₃ = Original weight of specimen suspended in water, after 24 hours immersion in water.

W₄ = Final weight of surface-dried specimen after 30 cycles of the test and 24 hours immersion in water.

W₅ = Final weight of specimen suspended in water, after 30 cycles of the test and 24 hours immersion in water.

APPENDIX F

INCHES TO DECIMAL FEET - CONVERSION

Inches	Feet	Usually adopted	Inches	Feet
12	1.00	1.0	1	0.08
11	0.91	0.9	$\frac{1}{2}$	0.04
10	0.83	0.8	$\frac{1}{4}$	0.02
9	0.75	0.75		
8	0.66	0.7	$\frac{1}{8}$	0.01
7	0.58	0.6		
6	0.50	0.5	$\frac{1}{16}$	0.005
5	0.42	0.4		
4	0.33	0.3		
3	0.25	0.25		
2	0.17	0.2		
1	0.08	0.1		