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DEPARTMENT OF MINES
SOUTH AUSTRALIA
GEOLOGICAL SURVEY

NON FERROUS METALS SECTION

### GEOLOGICAL INVESTIGATION OF LEAKAGE

FROM AROONA DAM

# FINAL REPORT ON DRILLING

by

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NON FERROUS METALS SECTION
GEOLOGICAL SURVEY

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# DEPARTMENT OF MINES SOUTH AUSTRALIA

#### GEOLOGICAL INVESTIGATION OF LEAKAGE

#### FROM AROONA DAM

### FINAL REPORT ON DRILLING.

#### INTRODUCTION

Drilling of the four diamond drill holes recommended in the interim report was completed on 30/7/62 and pressure water testing of the holes was done in the same week.

This present report discusses the results of drilling and testing and the remedial measures indicated.

#### GEOLOGY

The main features of the geology which require reiterating are the dip of the thin bedded quartzites with their interbedded shaley sandstones upstream towards the dam (northerly) and their strike across the narrow ridge forming the reservoir rim, on the eastern side of the dam; the presence of numerous joints of two main systems; the narrowness of the ridge and the presence of a blanket of talus up to 15 feet vertical thickness on the western slope of the ridge.

#### ENGINEERING GEOLOGY:

The results of the drilling and testing broadly confirm the supposition that leakage is coming through the ridge in a network of interconnecting cracks rather than through a number of discrete cracked and fractured fault zones.

The cores of the diamond drill holes testify to the multitude of cracks along joints. Total number of joints in the cores were counted and the count ranged from 40 joints in

<sup>\*</sup> JOHNSON, W., 1962 - Interim Report on Leakage from the rim of Aroona Reservoir. UNPUBLISHED REPORT, DEPT. OF MINES, S. AUST. 54/155

a 14 feet long section of the core of AL3 to 200 joints in a 19 feet long section of the core of AL2. The majority of these cracks are tight. This is shown by the pump+in water tests. In AL2 between 52 feet and 81 feet the loss was .58 g.p.m. under a collar pressure of 20 p.s.i. and 280 joints were counted in this section. In AL3 the loss between 52 feet and 81 feet was 8.7 g.p.m. under a collar pressure of 20 p.s.i. and 82 joints were counted.

The general tightness of individual cracks is confirmed by a calculation of the mass permeability of the ridge over the 1000 feet long section downstream of the abutment of the dam. Assuming an average water depth in the reservoir of 55 feet, a leakage rate of 8,000,000 gallons a week, and an average water gradient of .1 in the ridge, the permeability works out as 10 millidarcies, which is well down in the range of permeabilities of naturally occurring materials.

The water test results demonstrate also the effect of position in the ridge on the opening of the cracks. In D.D.H. AL3 no pressure was obtained with the packer set at 41.5 feet below the surface (maximum pump rate 13 g.p.m.) and generally losses were greater in this hole than in the other 3 holes. Cores from the holes and the profiles across the ridge show that AL3 is in the narrowest section of the ridge and at a position where the talus is thicker. This may be a sufficient cause of the increased opening of the cracks.

Owing to the steepness of the slope of the ridge the thickness of rock between the hole and the slope surface increases comparatively slowly with depth. The effect of this is shown in the water test results. In each hole the increase in rate of water loss is proportional to the length of hole tested, up to a certain depth below the surface, varying in each hole. At this depth the rate suddenly increases, indicating a sharp increase in permeability of the surrounding rock. As discussed in the previous paragraph the variation in depth at which this

occurs is due probably to the situation of the hole in relation to the bedrock surface.

Water levels in the various holes show clearly the increase in groundwater gradient southwards from the left abutment of the dam. This can be due only to a decrease in permeability southwards, which is consistent with the expected tightening of the cracks where the ridge becomes wider and higher.

#### REMEDIAL MEASURES

The investigations have shown that it should be possible to prevent most of the leakage by sealing the network of cracks in the ridge through which the water is flowing.

It remains to discuss how best this can be accomplished.

In my opinion the grouting of the cracks by a single row of holes, commencing at the left abutment of the dam and finishing between AL3 and AL4, would stop 90% of the leakage. Grouting any other length would stop an amount of the leakage proportional to the length grouted.

It would be unnecessary to grout below R.L. 805 as the indications are that the cracks below this level are tight. It would be unnecessary also to grout above R.L. 860. Therefore it is suggested that if grouting is done that the holes be drilled from a bench excavated in talus to intersect the talus/bedrock interface at R.L. 860.

Because of the general narrowness of the cracks a maximum spacing of 5 feet centres for the grout holes is advisable. At this spacing 180 holes would be required to grout the entire required 900 feet length of the proposed curtain. Drilling would total 9,900 feet and vertical holes drilled with an AX size solid bit would be satisfactory.

It is believed that the cracks would be groutable with thin mixtures of cement grout. Tests should be made on the existing drill holes to confirm this opinion. The only alternative to grouting would be to form a clay blanket over the inlet area for leakage. This would need to be at least 1 foot thick and protected to prevent erosion by wave action. An area 1500 feet long from 200 feet north of the intersection of the projected centre line of the dam with the eastern slope of the ridge to beyond the major curve in the reservoir run to the south would need to be blanketed. This is not considered such a permanent and satisfactory solution of the leakage problem as grouting a curtain from the abutment. Estimation of comparative costs would show which treatment would be the more expensive.

Natural sealing of the ingress points for the leakage by silt will not help materially in reducing leakage during the life of the coal field.

#### CONCLUSION AND RECOMMENDATIONS

The test holes have confirmed the opinion expressed previously that leakage water is traversing the rim of the reservoir through a network of interconnecting cracks which individually have narrow openings. These cracks tighten southwards as the ridge forming the rim becomes wider and higher.

Prevention of leakage by grouting a curtain of holes, at 5 feet centres in the ridge, extending 900 feet south from the left abutment should be possible. A total of 4,400 feet of drilling would effect this curtain. The only alternative would be a protected clay blanket over the 1500 long inlet area of leakage in the reservoir and this would not be so permanent as the grout curtain.

It is recommended that the economy of these two methods of leakage prevention be investigated.

Senior Geologist aNON FERROUS METALS SECTION

- 1. 42°-60° at 190° to bedding dip
  - 2. 75°-78° " 100 " " "
  - 3. 35° " 150 " "
  - 4. 15° " 270 " "
  - 5. 50° " 2**3**0 " "

# GEOLOGICAL LOG OF DRILL HOLE

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Quartzite		8	NX- 0.2	87			i :	1	•	
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Drill No.						Logged		Vert.	Scale	
Driller						Sheet No. Drawn			of	
Commenced						Checked Submitted			ing No. 0-7.60 80	

12°-60° of 190° to bedding dip 15°-78° " 100° " " " 35° " 150° " " " " 16° " 270° " " "

7 15	290° 1	bedding	dip

Drill No..

Completed

Type ..... Sheet No. Sheet ..... of . Drawn Checked Drawing No. Commenced

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Vert. Scale....

# DEPARTMENT OF MINES - SOUTH AUSTRALIA

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